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2 **Crustal conditions favoring convective downward migration of fractures in deep**
3 **hydrothermal systems**

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9 **Key Points:**

- 10 • Numerical modeling supports convective downward migration of fractures as a source
11 mechanism for hydrothermal systems
- 12 • Fluid flow, fracture opening and propagation in a thermo-poroelastic rock mass are
13 simulated in different geological settings in the crust
- 14 • Crustal stresses are key to understanding whether a hydrothermal system can evolve in
15 regions away from active zones of volcanism
16

17 **Abstract**

18 Cooling magma plutons and intrusions are the heat sources for hydrothermal systems in volcanic
19 settings. To explain system longevity and observed heat transfer at rates higher than those
20 explained by pure conduction, the concept of fluid convection in fractures that deepen because of
21 thermal rock contraction has been proposed as a heat-source mechanism. While recent numerical
22 studies have supported this half a century old hypothesis, understanding of the various regimes
23 where convective downward migration of fractures can be an effective mechanism for heat
24 transfer is lacking. Using a numerical model for fluid flow and fracture propagation in thermo-
25 poroelastic media, we investigate scenarios for which convective downward migration of
26 fractures may occur. Our results support convective downward migration of fractures as a
27 possible mechanism for development of hydrothermal systems, both for settings within active
28 zones of volcanism and spreading and, under favorable conditions, in older crust away from such
29 zones.

30 **Plain Language Summary**

31 Geothermal energy is transferred through and stored in the rock and fluids of the earth's crust. If
32 temperature increases sufficiently with depth and the crust provides sufficient pathways for water
33 to flow through, colder water sinks and percolates downward, gets heated at depth and then rises
34 due to its lower density at higher temperature. This creates a hydrothermal circulation system
35 that transports heat from the deep crust to shallower depths from where it can be produced. Wells
36 drilled into these systems produce hot water and/or steam for direct heat utilization or electricity
37 production. To understand the renewability of hydrothermal systems, we need to understand how
38 heat is transferred deep in the crust. A hypothesis has been proposed, suggesting that fractures,
39 propagating downwards because of contraction of the water-cooled surrounding rock, are central
40 to maintaining the heat transfer from the deep crust. Based on settings in Iceland, we show how
41 the fluid flow and propagation of fractures can be important for development of hydrothermal
42 systems, using computer simulations, both in active regions of volcanism and, under favorable
43 conditions, also in older crust away from such regions. The latter results are important for the
44 identification of hidden geothermal systems.

45 **1 Introduction**

46 Hydrothermal fluid circulation within the earth's crust is driven by the combination of
47 sufficient heating from below and permeability for fluids to flow (Lapwood, 1948). It is an
48 important mechanism of mass and heat transfer in the crust and is seen as the explanation of
49 anomalous temperature profiles with depth that are not consistent with heat transfer by
50 conduction alone (Elder, 1965; Pálmason, 1967). While the concept was originally developed
51 considering porous rocks, it was later expanded to include rocks with secondary permeability in
52 the form of fractures, dikes and other structural features providing the main fluid conduits
53 (Bodvarsson & Lowell, 1972). For hydrothermal systems, Bodvarsson and Lowell (1972)
54 suggested how contraction induced by buoyancy-driven convective cooling would lead to tensile
55 fracture opening and consequently strongly affect permeability at depth. A conceptual model of
56 fractures migrating downwards due to convective cooling was described further by Lister (1974)
57 and Bodvarsson (1982), including also analytical estimates of propagation speeds based on
58 simplifying assumptions. Bodvarsson (1982) was the first to name the process "convective
59 downward migration of fractures" (CDM) and specifically considered its role in transferring heat
60 from cooling magma bodies to hydrothermal system over the lifespan of the hydrothermal

61 activity. As the magma cools, a layer of gradually thickening solidified rock develops, providing
62 an insulation between the heat source and the hydrothermal system. If this layer is impermeable,
63 and the intrusive intensity of the magma is low, heat transfer from the magma to the
64 hydrothermal system will decrease with time, which is inconsistent with the high heat output of
65 such systems over long time scales (Bodvarsson, 1982; Björnsson et al., 1982). For hydrothermal
66 systems in Iceland, Bodvarsson (1982) argued that the intrusive intensity would be low, and,
67 hence, hypothesized CDM to be an important mechanism for heat transfer.

68 Bodvarsson, (1982; 1983) and Axelsson (1985) also suggested that CDM could be
69 effective as a source mechanism in systems with elevated heat flux but away from central
70 magmatic heat sources, and may account for some of the long-lasting low-enthalpy hydrothermal
71 activity in the Icelandic crust. For such settings, they both proposed that the onset of the process
72 would depend on local stress conditions. Such settings are not only limited to Iceland but can
73 also be found in other areas (Jolie et al., 2021; Limberger et al., 2018). A better understanding of
74 the settings controlling the highly coupled processes governing CDM may therefore also shed
75 light on the existence of hydrothermal systems in other parts of the world.

76 While a comprehensive understanding of the geological settings where CDM can occur is still
77 lacking, two recent numerical modeling studies support the hypothesis. Patterson & Driesner,
78 (2021) present a model of large-scale natural convection in a downward propagating fracture
79 zone (of dimensions: $H=3\text{km}$, $L=8\text{km}$, $W=1\text{m}$) in a thermo-elastic medium, considering what we
80 in the present context will denote a low geothermal gradient of $55^\circ\text{C}/\text{km}$. They investigate the
81 effect of thermoelastic rock stresses and fracture fluid pressure on fracture-zone transmissivity
82 by use of a Barton-Bandis relationship between fracture transmissivity and effective normal
83 stress (Bandis et al., 1983; Barton et al., 1985). Expanding on the conceptual model by Lister
84 (1974) and Axelsson (1985), Stefansson et al., (2021b) present a fully coupled numerical
85 approach for fracture propagation and deformation that allow for multiple fractures in a thermo-
86 poroelastic medium. The effect of thermo-poroelastic stresses on fracture transmissivity is
87 incorporated through a fracture contact mechanics model. In the work of Stefansson et al.
88 (2021b), the downward migration of fractures due to convective cooling is considered for a test
89 case with a set of smaller fractures ($H=200\text{m}$, $L=200\text{m}$, $W=2\text{mm}$) at the bottom of a geothermal
90 system. The study applied parameters which are representative for a geothermal system in a
91 geological setting with a high geothermal gradient of $150^\circ\text{C}/\text{km}$.

92 In this paper we use numerical modeling to investigate CDM as a source mechanism for
93 hydrothermal activity. We consider both young crust in active zones of volcanism and spreading
94 as well as older crust away from such zones. The numerical approach builds on the methodology
95 by Stefansson et al. (2021b), accounting for flow and fracture propagation in thermo-poroelastic
96 media. This enables us to study effects of the stress regime and thermal gradients, as well as
97 effects of important rock parameters such as the permeability in the medium surrounding the
98 fractures. The results by Stefansson et al. (2021b) indicate that CDM can be a plausible source
99 mechanism in systems away from central heat sources if the thermal gradient is sufficiently high.
100 Furthermore, it is clear that local stress setting (e.g. in spreading systems) can be favorable for
101 CDM. This leads to the following hypotheses:

- 102 1. No central magmatic heat sources are needed for CDM, a high geothermal gradient is
103 sufficient to maintain the process.

104 2. With lower geothermal gradients, crustal stress conditions in a range of geological
105 settings are still favorable for CDM as a mechanism for heat transfer.

106 Using simulation models, we test these hypotheses with different thermal gradients, and show
107 how, for lower thermal gradients found away from volcanic belts, local stress settings are a
108 dominating factor for the onset of CDM.

109 As basis for the simulations, geological conditions found in Iceland are chosen. Iceland is
110 famous for its hydrothermal systems providing its nation with both electricity and space heating
111 through the utilization of geothermal fluids. Zones of spreading and volcanism cut through the
112 center of the country along the Mid-Atlantic Ridge, explaining the elevated heat content in its
113 crust. The volcanic belts rockmainly consist of very long fracture-zones dominated by spreading
114 and injection of extremely long dikes at depth. Several central volcano complexes are
115 interspersed in the zone, but these take up a very small part of the total area of the zone. For the
116 study of CDM two regional settings are chosen, (1) within the spreading zone but away from any
117 central volcanoes and (2) away from the spreading zone. Those two settings provide scenarios
118 with elevated heat flux, that we in the present context will denote by a high geothermal gradient
119 on one hand and low geothermal gradient on the other hand. As discussed in section 2, similar
120 settings can be found in other regions of the world.

121 **2 Geological settings for CDM**

122 Compared to normal conditions on the earth's surface, the heat flux through
123 hydrothermally active areas is elevated. In systems located within volcanically active areas one
124 might assume that intense magma intrusion frequency and resulting conduction, could at least
125 partly sustain these systems (Björnsson et al., 1982; Gunnarsson et al., 2010); however, this is an
126 unlikely case for most systems (Bodvarsson, 1954; Hochstein, 1995; Weir, 2001). We will look
127 at the effect of thermal stress changes, induced by cooling at depth by buoyancy driven
128 convection, and how this process can lead to enhanced permeability and heat transfer by
129 convection in propagating fractures. The process of fracture propagation at depth allows for
130 thermal fluid being in direct contact with hot formation deep within the systems (White, 1968;
131 Björnsson et al., 1982; Björnsson & Stefansson, 1987). The process evolves over time to give
132 fluid access to new parts of the rock, which can be related to the lifetime and the intensity of
133 hydrothermal activity. Hence, CDM should be considered as a possible source mechanism of
134 hydrothermal activity.

135 We study a model of vertical fractures in the roots of geothermal systems, first proposed by
136 Lister (1974) and Bodvarsson (1982). Convection of geothermal fluid in the fractures cools down
137 the surrounding rock, causing horizontal tensile stresses in the rock, which lead to (1) the rock to
138 contract and (2) the fractures to propagate downward. By this self-sustained process, the
139 convection of thermal fluid extends downward constantly reaching fresh hot rock, enhancing the
140 heat flux to the geothermal system above. The process, combined with heat conduction, could
141 sustain the hydrothermal systems in accordance with observed heat output.

142 2.1 Extension deformation that favors vertical permeability

143 Areas of elevated heat flow and heat content that favor the development of hydrothermal
144 systems are located at divergent plate boundaries, where the spreading of the lithosphere leads to
145 ascending magma and intrusion into the crust. Regional extension tectonics create both regional
146 and local structures that furthermore affect permeability. Some examples of divergent plate

147 boundaries include the Mid-Atlantic Ridge, Red Sea Rift, Baikal Rift Zone, East African Rift
148 (Great Rift Valley), East Pacific Rise, Gakkel Ridge, Galapagos Rise, Explorer Ridge, Juan de
149 Fuca Ridge, Pacific-Antarctic Ridge, and West Antarctic Rift System. Many hydrothermal
150 systems are located in those settings, for example in Iceland (mid-Atlantic Ridge), Eritrea,
151 Djibouti, Ethiopia, Uganda, Kenya, Tanzania and Malawi (western and eastern branches of the
152 East Africa Rift) (Hochstein, 2005). Hydrothermal vents along the seabed are known to form
153 along divergent mid-ocean ridges, such as the East Pacific Rise and the Mid-Atlantic Ridge
154 (Petersen et al., 2018).

155 Divergent plate boundaries are examples of extension-controlled tectonics. Extension
156 deformation that can enhance vertical permeability can also be found in locations away from
157 convergent or transform plate boundaries, such as in back-arc basins (Lau Basin in the East
158 Pacific), in continental extension zones (Rio Grande Rift Zone, East-African Rift Zone, Western
159 Turkey (Bozkurt & Mittwede, 2005), and in releasing bends along strike-slip faults and in zones
160 of thickened crust (gravitational spreading). Known areas of hydrothermal activity associated
161 with continental rifting are, for example, located in the Great Basin in Western USA, the
162 countries in the western and eastern branches of the East African Rift, in west Turkey and in
163 Cyprus (Bettison-Varga et al., 1992; Murat Özler, 2000). Areas of hydrothermal activity
164 associated with back-arc activity are e.g. located in the Taupo Volcanic Zone New Zealand
165 (Kissling & Weir, 2005), and the Okinawa Trough Japan (Halbach et al., 1989; Yang et al.,
166 2020).

167 Extension deformation due to regional tectonics alone can act to enhance vertical permeability and
168 therefore give rise to the circulation of fluids at intermediate depths in the crust. This, however,
169 does not explain increased hydrothermal activity in tectonically less active areas. Pálmason,
170 (1981) speculated on the effect of cooling of the lithosphere as it moves away from the rift axis
171 and suggests that thermal stresses consequently induce enhanced vertical permeability for
172 geothermal fluids at depths on the flanks of the active rifting. Hence, we consider the effects of
173 fluid circulation in existing fractures and how increased thermal stress may cause fracture
174 propagation, thus increasing vertical permeability. It is expected that both temperature settings in
175 the crust and regional stresses influence the initiation and maintenance of CDM.

176 **3 Mathematical and numerical modeling of CDM**

177 We use a mathematical model based on a discrete fracture matrix representation. The
178 medium is 3D, consisting of the rock matrix and embedded fractures modelled as 2D planes. The
179 model describes energy transport and fluid flow in rock matrix and fractures, thermo-poroelastic
180 deformation of the rock, and fracture deformation and propagation. We assume single phase
181 fluid conditions with the reservoir rock fully saturated, and with local thermal equilibrium
182 between the fluid and the solid. We impose a balance of momentum, mass and energy in the rock
183 matrix and a balance of mass and energy in the fractures, along with kinematic constraints and
184 constitutive laws for fracture deformation (Stefansson et al., 2021a; see also Barton, 1976). In the
185 following, key components of the model are reviewed. A full description of the mathematical
186 model, including coupling between variables in the rock matrix and the fracture (Jaffré et al.,
187 2011; Martin et al., 2005; Stefansson et al., 2021b), is provided in the supplementary material of
188 this paper.

189 Dimension reduction of the balance equations which is necessary to derive the flow of mass and
190 energy in the fracture is detailed in Stefansson et al. (2021a) and Keilegavlen et al. (2021a).

191 The aperture of a dimensionally reduced fracture is given by

$$a = a_0 + \llbracket \mathbf{u} \rrbracket_n. \quad (1)$$

192 Here, a_0 is the residual hydraulic aperture in the undeformed state, and $\llbracket \mathbf{u} \rrbracket_n$ the normal
 193 component of a displacement-jump over the fracture, defined as the difference in the
 194 displacement, \mathbf{u} , computed on the opposing fracture walls. The fracture aperture, a , will be
 195 affected by fluid pressure as well as thermo-poromechanical forces in the matrix. The flow in the
 196 fracture is described by Darcy's law with a cubic law for the permeability, giving a strongly non-
 197 linear relation between the aperture and the fluid flow.

198 We consider propagation due to tensile forces, modeled by the stress intensity factor (Stefansson
 199 et al., 2021b; see also Nejadi et al., 2015),

$$SI_I = \sqrt{\frac{2\pi}{R_d}} \left(\frac{\mu}{\kappa + 1} \llbracket \mathbf{u} \rrbracket_n \right), \quad (2)$$

200 where R_d is the distance between the point where the displacement jump is evaluated and the
 201 fracture tip, μ is the shear modulus of the rock, and κ is the Kolosov constant for plain strain
 202 described as a function of the shear and the bulk moduli of the rock (see supplementary
 203 material). The fracture tip propagates when SI_I exceeds a critical value,

$$SI_I \geq SI_{Icrit}, \quad (3)$$

204 which can be viewed as the rock toughness.

205 The mathematical model is implemented in the open-source simulation tool PorePy,
 206 which is tailored for representing complex multiphysics processes in fractured porous media
 207 (Keilegavlen et al., 2021a). The fractures are explicitly represented in the computational grid
 208 which allows for direct modelling of processes in the fracture and on the fracture walls. In the
 209 computational grid, pressure and temperature are represented in both rock matrix and fractures,
 210 the displacement is confined to the rock matrix and on the fracture walls, and contact tractions
 211 are represented on the fractures. Fracture propagation is represented by extending the fracture
 212 grid, with minimal adjustments needed to the rest of the computational model.

213 **4 Simulations of CDM in different geological settings**

214 Two regional settings are considered to investigate the process of CDM as a source
 215 mechanism for hydrothermal activity. They are both considered representative of temperature
 216 conditions in the crust of Iceland: (1) within the Icelandic active zone of volcanism and
 217 spreading and (2) in older crust away from the active zone of spreading. The first represents
 218 regions rich with geothermal resources while the second represents regions which are considered
 219 to include fewer geothermal systems (Axelsson, et al., 2005). The heat source is thermal energy
 220 within the earth's crust, accumulated over time by heat flow from the lithosphere and intrusive
 221 activity. The background thermal gradient is 100-150°C/km (Flóvenz & Saemundsson, 1993) in
 222 young crust within the rifting zone, and varies between 50° and 100°C/km in older crust further
 223 away from the divergent ridge axis. These settings are distinct from known volcano complexes
 224 with associated high-enthalpy hydrothermal activity and heat sources of magmatic origin.

225 The depth at which fissures are assumed to be open varies between those regions: Close to the
 226 divergent axis, within the active zone, we assume fissures to be open down to 2 km depth,
 227 whereas away from the axis, in colder crust, we assume fissures to be open down to 1 km depth.
 228 Isothermal temperature with depth profiles from geothermal fields in Iceland strengthen this

229 assumption (Arnórsson et al., 2008; Axelsson, et al., 2000; Björnsson et al., 2000; Xianghui,
 230 2012). We assume that the depth of open fissures reflect the depth of the geothermal systems in
 231 the initial state of the simulations. Since we are investigating the longevity of the systems and the
 232 CDM as a key mechanism to maintain the systems, we consider the opening and propagation of
 233 fractures beyond those depths.

234 4.1 Simulation domain and setup

235 For the numerical investigation of different geological settings, we choose a three-
 236 dimensional domain, a cube with side-lengths of 400 m. At the top of the domain, five evenly
 237 spaced vertical planar fractures are located along the x-axis, each spanning 200 m in length and
 238 depth. The formation depth and thermal gradients are set in accordance with the two regional
 239 settings: For the two regional settings considered, the geothermal gradient is set accordingly to
 240 (1) 130 °C/km and (2) 80 °C/km, representing temperature conditions within and away from the
 241 active zone, respectively. The top of the simulation domain is located at (1) a depth of 2000 m
 242 and (2) a depth of 1000 m, respectively, thus the temperature at the top of the domain is 260 °C
 243 and 80 °C, respectively, for the two different cases. We denote settings corresponding to (1) as
 244 high-temperature (HT) regimes and settings corresponding to (2) as low-temperature (LT)
 245 regimes, respectively.

246 The background stress field is aligned with respect to the fractures, with vertical stress (S_V) equal
 247 to the weight of the overburden, the maximum horizontal stress (S_H) in direction of the fractures
 248 (along the y-axis), and the minimum horizontal stress (S_h) perpendicular to the fractures (x-axis).
 249 This background stress implies that fractures are favorably oriented for opening and propagation.
 250 Figure 1 (leftmost) shows the initial geometrical setup of the domain and the fractures.

251 The background stress is defined such that

$$252 S_h = \sigma_{xx} = b_1 \sigma_{zz}, S_H = \sigma_{yy} = b_2 \sigma_{zz}, S_V = \sigma_{zz} = \rho_S g z, \quad (4)$$

253 where ρ_S is the bulk density of the overburden, g is the acceleration of gravity, z is the depth and
 254 b_1 and b_2 are positive constants. Four background stress regimes (A-D) are defined (Table 1) for
 255 $b_1 = \{0.4, 0.6\}$ and for $b_2 = \{0.8, 1.2\}$. The choice of the background stress, which corresponds
 256 to either a strike-slip or a normal fault regime, is based on stress settings observed in Iceland
 257 (Ziegler et al., 2016), away from the central volcanism and therefore also away from the complex
 258 stress conditions associated with volcanic activity.

259 Motivated by the assumption of a low rock porosity of 5%, the bulk density of the overburden is
 260 set equal to that of the rock. The matrix permeability is assumed to be 10 μ D and the residual
 261 aperture to be 2 mm. Those values are in the lower range of what is suggested by measurements
 262 in active systems (Keilegavlen et al., 2021b; Massiot et al., 2017; Sigurdsson et al., 2000). The
 263 linear thermal expansion of the rock is chosen according to the temperature conditions at the two
 264 different settings, with the thermal expansion coefficient for the high temperature case set five
 265 times larger than for the second case, see Table 1 (Yin et al., 2021). The thermal expansion
 266 coefficient of water and water viscosity is chosen according to the overall temperature, while
 267 other parameters are constant, across the two different regional settings (1 and 2) shown in
 268 Table 1.

269 **Table 1:** Background-stress for regimes A-B and parameters for regional settings 1&2, defining
 270 conditions for the eight different cases modelled. Parameters that are identical for both settings
 271 are highlighted in gray.

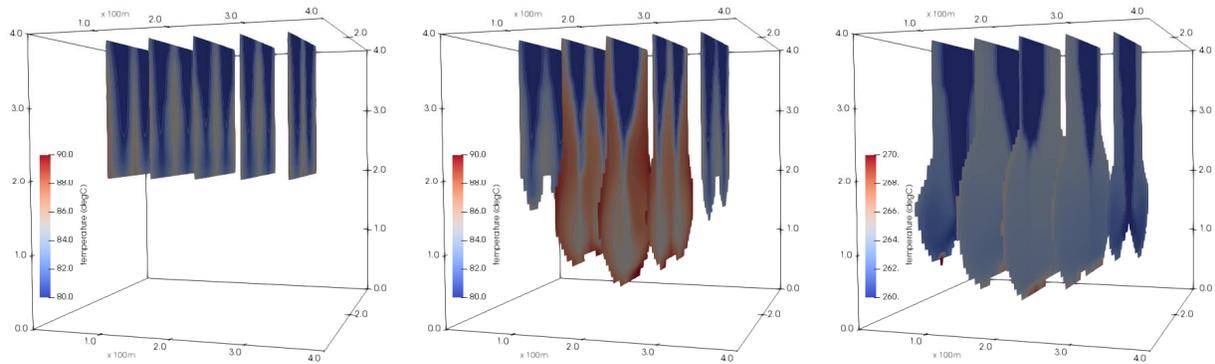
Stress regime	A	B	C	D
σ_{xx}	$0.6 \sigma_{zz}$	$0.4 \sigma_{zz}$	$0.4 \sigma_{zz}$	$0.6 \sigma_{zz}$
σ_{yy}	1.2	$1.2 \sigma_{zz}$	$0.8 \sigma_{zz}$	$0.8 \sigma_{zz}$
σ_{zz}	$\rho_s g z$	$\rho_s g z$	$\rho_s g z$	$\rho_s g z$
Regional setting		1	2	
Parameter	Symbol	Values	Values	Units
Depth @top of domain	z_0	2000	1000	M
Temp. gradient with depth	dT/dz	0.13	0.08	$^{\circ}\text{C}/\text{m}$
Temperature @top of domain	T_0	260	80	$^{\circ}\text{C}$
Dynamic viscosity	η	1.1×10^{-4}	3.5×10^{-4}	Pa s
Fluid volumetric thermal expansion	β_f	4×10^{-4}	2×10^{-4}	$^{\circ}\text{C}^{-1}$
Solid linear thermal expansion	β_s	5×10^{-5}	1×10^{-5}	$^{\circ}\text{C}^{-1}$
Bulk modulus of the fluid	B_f	2.5×10^9	2.5×10^9	Pa
Bulk modulus of the rock	B_s	2.2×10^{10}	2.2×10^{10}	Pa
Biot coefficient	α	0.8	0.8	–
Reference fluid density	$\rho_{0,f}$	1×10^3	1×10^3	kg m^{-3}
Reference solid density	$\rho_{0,s}$	2.7×10^3	2.7×10^3	kg m^{-3}
Fluid specific heat	c_f	4.2×10^3	4.2×10^3	$\text{J kg}^{-1} \text{ } ^{\circ}\text{C}^{-1}$
Solid specific heat	c_s	7.9×10^2	7.9×10^2	$\text{J kg}^{-1} \text{ } ^{\circ}\text{C}^{-1}$
Fluid thermal conductivity	κ_f	0.6	0.6	$\text{W m}^{-1} \text{ } ^{\circ}\text{C}^{-1}$
Solid thermal conductivity	κ_s	2.0	2.0	$\text{W m}^{-1} \text{ } ^{\circ}\text{C}^{-1}$
Fluid compressibility	c	4×10^{-10}	4×10^{-10}	Pa^{-1}
Shear modulus of the rock	μ	2×10^{10}	2×10^{10}	Pa
Matrix porosity	ϕ	0.05	0.05	–
Matrix permeability	k	1×10^{-17}	1×10^{-17}	m^2
Residual aperture	a_0	2.0×10^{-3}	2.0×10^{-3}	m
Friction coefficient	F	0.8	0.8	–
Dilation angle	ψ	3.0	3.0	$^{\circ}$
Critical stress intensity factor	SI_{crit}	5×10^5	5×10^5	Pa

272 Dirichlet boundary conditions are chosen for the temperature and pressure. This means that
 273 temperature gradient and hydrostatic pressure are fixed on the sides of the numerical domain. At
 274 the top of the domain the boundary conditions are imposed on both the rock matrix and the
 275 fractures. Neumann boundary conditions are chosen for the displacement by imposing the
 276 anisotropic tractions defined in Table 1, assuming zero displacement in the centre of the bottom
 277 boundary. Considering the onset of natural convection, these boundary conditions represent a
 278 conservative choice given the prescribed linear temperature profile on the vertical boundaries.

279 4.2 Results

280 In total, eight simulations were run, representing eight different geological settings, based on the
 281 two regional settings (1-2) and the four background stress regimes (A-D). For the HT regimes,
 282 onset of propagation occurs for all the four background stress conditions shown in Table 1. For
 283 the LT regimes, onset of propagation only occurs for cases B and C.

284 The modelled fracture evolution can be seen in Figure 1, that shows the modeled temperature in
 285 all five fractures: Before fracture propagation (left) and at the end of the simulation (center) for
 286 setting 2C (LT, normal stress), and at the end of the simulation for setting 1A (HT, strike-slip)
 287 (right). At the end of the simulation period the middle fracture has propagated 160m and 180m
 288 downward, respectively, in the LT and HT cases. The average speed of the migrating front is
 289 therefore 3.3 and 3.5 m/year for the two different cases.

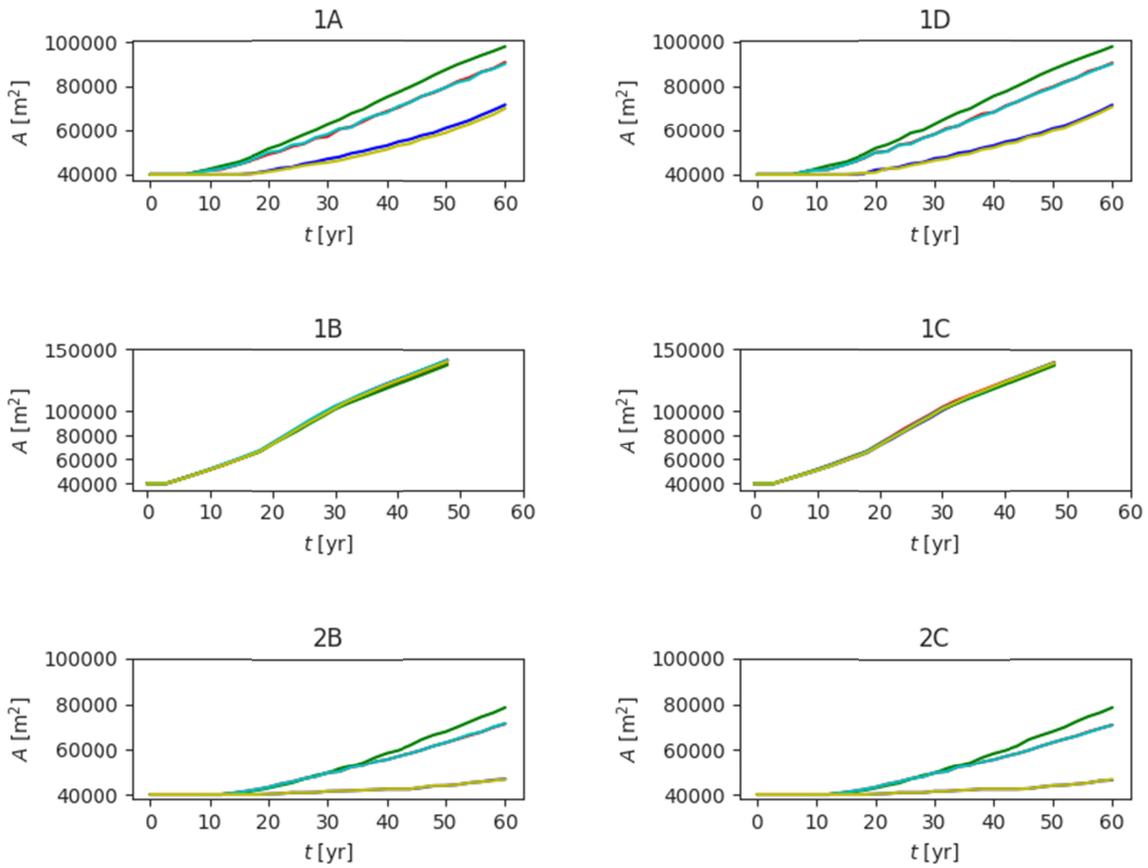


290

291 **Figure 1:** Temperature distribution in the five fractures: Left: Setting 2C (low temperature,
 292 normal stress) after 10 years simulation time (before onset of propagation), therefore, also
 293 showing the original geometry of the domain. Center: Setting 2C at the end of the simulation
 294 (60 yr.). Right: Setting 1A (high temperature, strike-slip stress) at the end of the simulation
 295 (60 yr.).

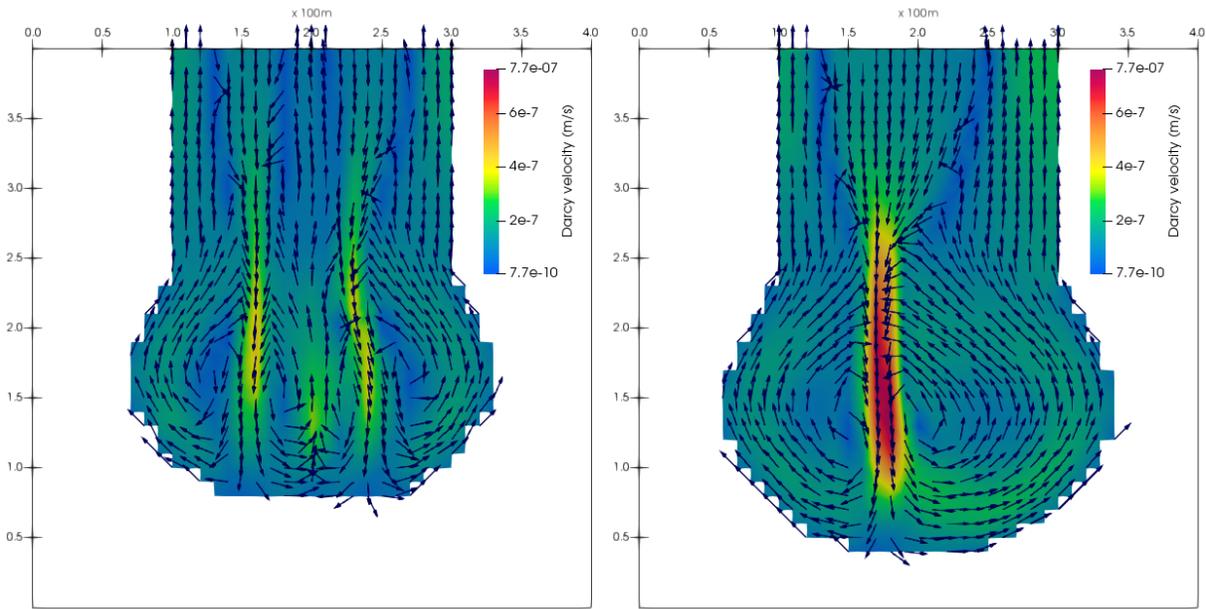
296 The onset of propagation and the propagation speed of the five fractures is shown in Figure 2 for
 297 the six simulations where propagation occurs. The onset of propagation in HT regimes (1A to
 298 1D) is after 7-8 years, for the thermal expansion coefficient set according to the predicted
 299 thermal conditions at 2 km depth within the crust. However, with thermal expansion coefficient
 300 set according to the predicted thermal conditions at 1 km depth within the crust in the LT
 301 setting (2), there is no onset of propagation for stress regimes A and D, when the background minimum
 302 horizontal stress is 60% of the vertical stress. When the background minimum horizontal stress is
 303 40% of the vertical stress (2B and 2C), the thermal stress imposed in the vicinity of the fracture
 304 is sufficient to overcome the background stress. The onset of propagation in those settings is
 305 after 12-13 years. Based on additional simulation studies, the transition to a regime of
 306 propagation is estimated to occur when the minimum horizontal stress is between 45% and 40%
 307 of the vertical stress.

308 In Figure 3 the Darcy velocity in the center fracture is shown for the low temperature case after
 309 50 and 60 years. As the figure shows, fluid circulation in the fracture forms convection cells,
 310 however the flow pattern and number of cells change as the fracture propagates. This pattern is
 311 observed in both HT and LT cases and is due to changes in the fracture geometry as well as
 312 coupling to the surrounding rock matrix.



313

314 **Figure 2:** Propagation of the five fractures depicted as growth in surface area of each fracture.
 315 The high temperature regimes are presented in the upper two rows and the low temperature
 316 regimes in the bottom row. The left side involves a strike-slip background stress regime, and the
 317 right side a normal background stress regime.



318

319 **Figure 3:** Darcy velocity in the center fracture in setting 2C (low temperature, normal stress),
 320 with the permeability related to the aperture by the relation $K_l = a^2/12$, after 50 and 60 years
 321 simulation time (left and right, respectively).

322 5 Conclusions

323 Our results contribute to ongoing discussion on (a) the convective downward migration
 324 of fractures (CDM) in the roots of geothermal systems, and (b) CDM's importance in explaining
 325 the origin and sustainability of hydrothermal activity. Many have contributed to the development
 326 of the mathematical model and description of the phenomenon; however, the complexity of the
 327 coupled processes of fluid flow, heat transfer and fracture and rock deformation, have put
 328 limitations on its understanding. Based on numerical simulations, we show that this process is
 329 plausible in different geological settings known to host hydrothermal systems.

330 The results of the numerical study show that the proposed CDM is highly relevant in
 331 understanding the nature of hydrothermal systems and the origin of hydrothermal activity.
 332 Notably, the study shows that CDM is possible in settings away from central heat sources, such
 333 as magma or cooling intrusion. As proposed by Bodvarsson (1982; 1983) and Axelsson (1985), a
 334 relatively low geothermal gradient is sufficient to initiate the process. This suggestion is
 335 supported by a recent numerical study (Patterson and Driesner, 2021). We have further shown
 336 that, in the absence of a high thermal gradient (e.g., in old crust away from active zones of
 337 volcanism and spreading), the local stress settings are important. The present numerical
 338 simulations show that CDM is possible in both strike-slip and normal stress regimes. In the case
 339 of lower thermal gradient, the stress perpendicular to the fracture must be low compared to the
 340 vertical stress—as already pointed out by previous studies, but now strengthened by results of
 341 the present numerical simulation. Therefore, our results indicate that crustal stresses are a clue as
 342 to whether a hydrothermal system can evolve in regions away from volcano-tectonic activity. In
 343 the search for hidden hydrothermal activity, this could be a key factor.

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347 **Open Research**

348 The data and source code for the results presented herein is available at
349 <https://doi.org/10.5281/zenodo.8123952>, and the results can be reproduced using version 1.4.2 of
350 PorePy (Keilegavlen et al., 2021a).

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