

[Water Resources Research]

Supporting Information for

[Global runoff partitioning based on Budyko-constrained machine learning][Shujie Cheng^{1,2}, Petra Hulsman², Akash Koppa², Hylke E. Beck³, Lei Cheng¹, and Diego G. Miralles²]

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1 Method

Baseflow curve based on limit concept

In general, the water balance can be written as:

$$\frac{dS}{dt} = P - E_a - Q \quad (S1)$$

where S is water stored in underground, P is precipitation, E_a is actual evaporation, Q is discharge which can be partitioned into Q_b is baseflow and Q_q is quick flow ($Q = Q_b + Q_q$).

The basic limit concept of the Budyko framework for estimating E_a is: $E_a/P \rightarrow 1$ as $E_p/P \rightarrow \infty$ for very dry conditions, and $E_a \rightarrow E_p$ as $E_p/P \rightarrow 0$ for very wet conditions, where E_p is potential evaporation. The demand limit of E_a is E_p and the supply limit is P . Fu (1981) proposed E_a can be calculated with:

$$\frac{E_a}{P} = 1 + \frac{E_p}{P} - \left[1 + \left(\frac{E_p}{P}\right)^{a_1}\right]^{1/a_1} \quad (S2)$$

Assuming $\frac{dS}{dt} \approx 0$ on long term time scales and with the catchment retention defined as

$$CR = E_a + Q_b \quad (S3)$$

Equation S1 can be expressed as:

$$P = CR + Q_q \quad (S4)$$

The demand limit for CR is $CR_0 = E_p + Q_{b,p}$. The E_p and $Q_{b,p}$ are the potential values for E and Q_b , respectively. According to Zhang et al. (2008), the limits concept of Budyko can also be applied to CR such that: $CR/P \rightarrow 1$ as $CR_0/P \rightarrow \infty$ for very dry conditions, and $CR \rightarrow CR_0$ as $CR_0/P \rightarrow 0$ for very wet conditions. Then CR can be estimated as:

$$\frac{CR}{P} = 1 + \frac{CR_0}{P} - \left[1 + \left(\frac{CR_0}{P}\right)^{a_2}\right]^{1/a_2} \quad (S5)$$

Combining Eq. S2, Eq. S3 and Eq. S5:

$$\frac{Q_b}{P} = \frac{Q_{b,p}}{P} + \left[1 + \left(\frac{E_p}{P}\right)^{a_1}\right]^{1/a_1} - \left[1 + \left(\frac{E_p + Q_{b,p}}{P}\right)^{a_2}\right]^{1/a_2} \quad (S6)$$

Under very limited storage capacity conditions (for instance an impervious catchment), no/limited water is stored in the subsurface such that the baseflow also approaches zero (i.e., $Q_b/P \rightarrow 0$ if $Q_{b,p}/P \rightarrow 0$). Under that condition, Eq. S11 changes to $0 \approx \left[1 + \left(\frac{E_p}{P}\right)^{a_1}\right]^{1/a_1} - \left[1 + \left(\frac{E_p}{P}\right)^{a_2}\right]^{1/a_2}$.

This equation can only be satisfied if $a_1 = a_2$. Thus Eq. S11 can be written as:

$$\frac{Q_b}{P} = \frac{Q_{b,p}}{P} + [1 + (\frac{E_p}{P})^\alpha]^{1/\alpha} - [1 + (\frac{E_p + Q_{b,p}}{P})^\alpha]^{1/\alpha} \quad (S7)$$

2 Figures

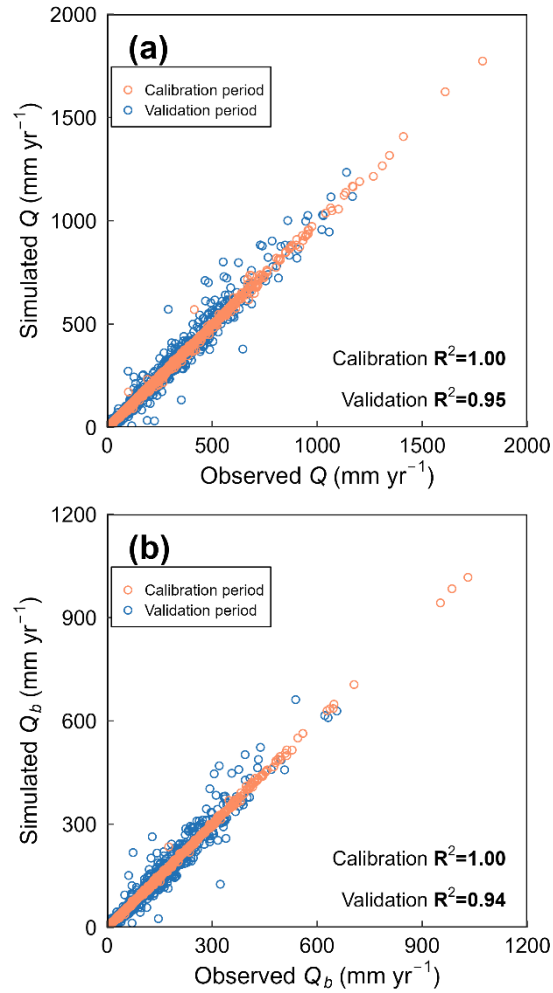


Figure S1. Performance of (a) Q and (b) Q_b at catchment scale during the calibration (orange) and validation (blue) periods.

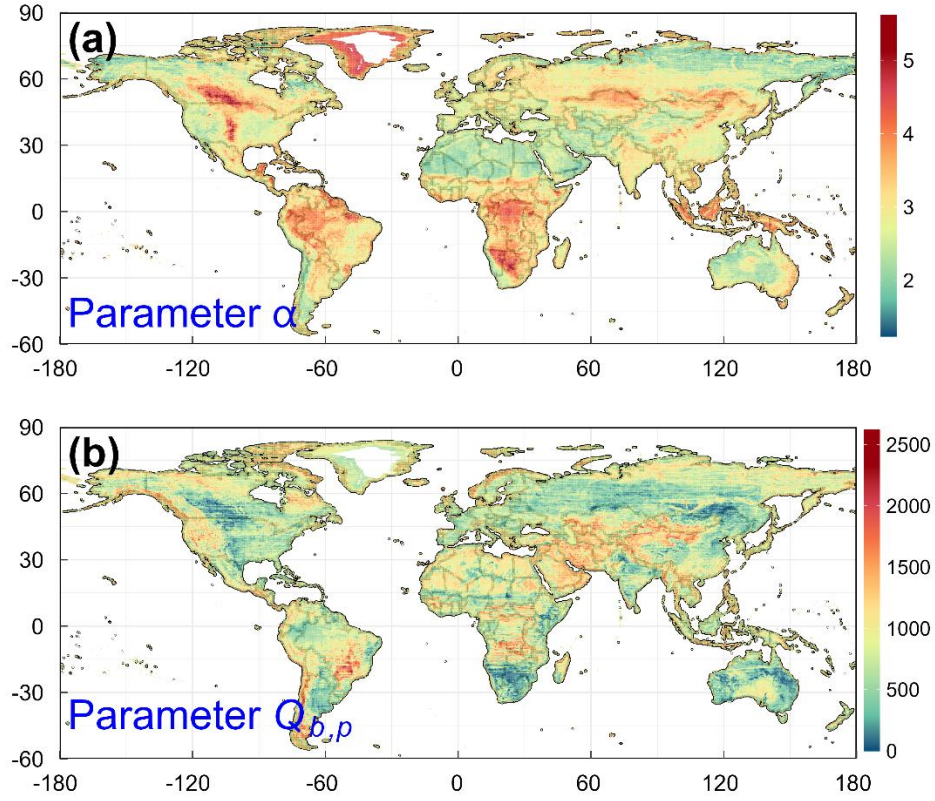


Figure S2. Global maps of (a) parameter α in the Budyko curve (Eq. 3) and BFC curve (Eq. 4), and (b) parameter $Q_{b,p}$ in BFC curve estimated as the mean of 10 BRT models.

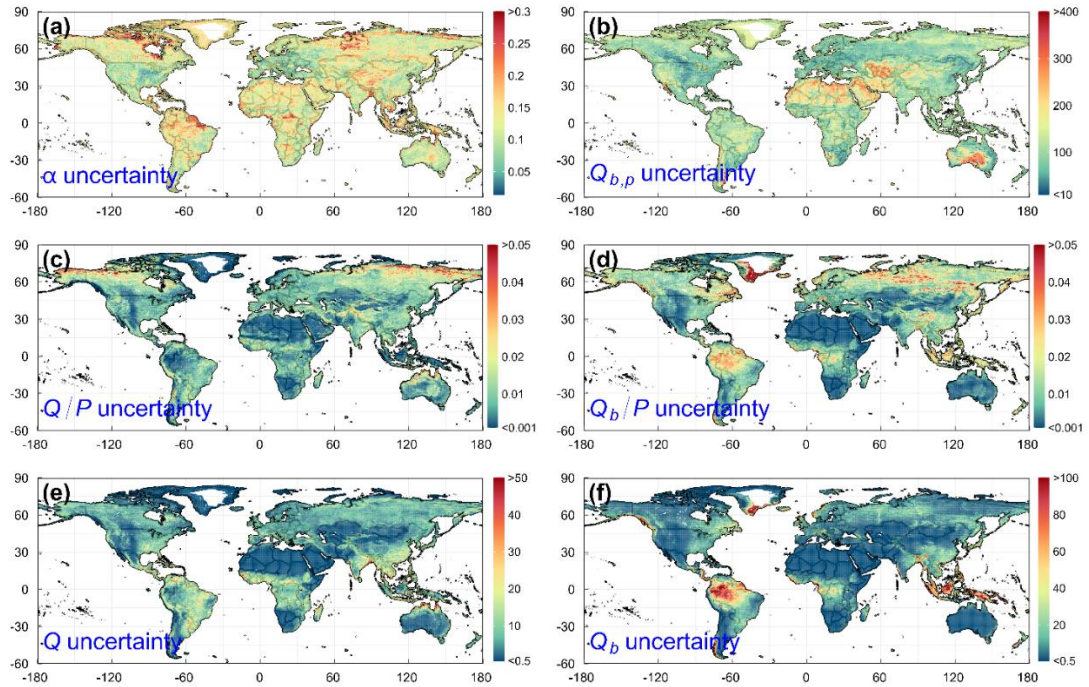


Figure S3. Global map of the uncertainty of (a) parameter α , (b) parameter $Q_{b,p}$, (c) runoff coefficient ($RC=Q/P$), (d) baseflow coefficient ($BFC=Q_b/P$), (e) runoff (Q), and (f) baseflow (Q_b). These uncertainty values are equal to the standard deviation of the 10 trained BRT models using the 10-fold cross-validation strategy.

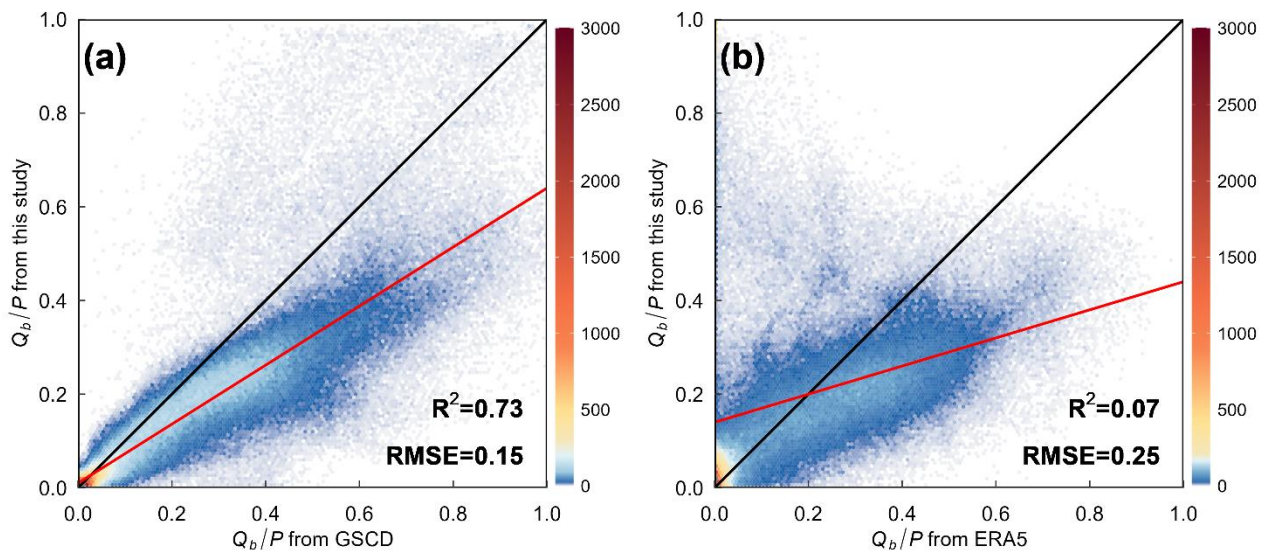


Figure S4. Comparison of the baseflow coefficient (Q_b/P) from this study with estimates according to (a) GSCD and (b) ERA5-Land.

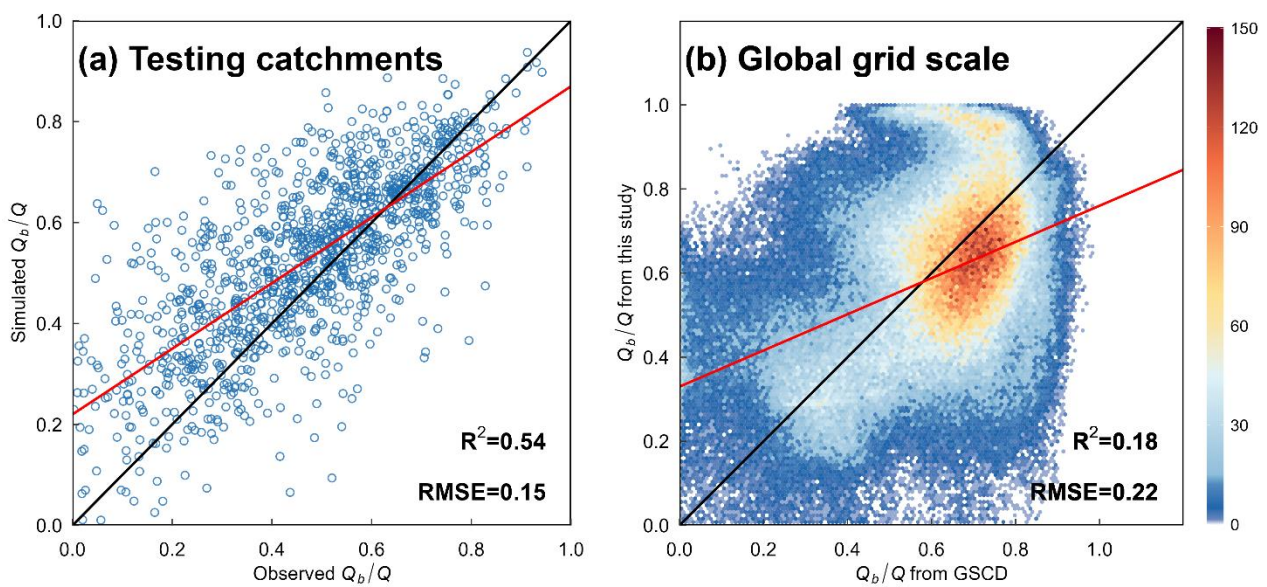


Figure S5. Comparison of the baseflow index (Q_b/Q) as estimated in this study with (a) field observations and (b) GSCD estimates.