

Consecutive Ruptures on a Complex Conjugate Fault System During the 2018 Gulf of Alaska Earthquake

Shinji Yamashita^{1,*}, Yuji Yagi^{2,*}, Ryo Okuwaki^{2,3,4}, Kousuke Shimizu¹, Ryoichiro Agata⁵, and Yukitoshi Fukahata⁶

¹Graduate School of Life and Environmental Sciences, University of Tsukuba, Tsukuba, Ibaraki 305-8572, Japan

²Faculty of Life and Environmental Sciences, University of Tsukuba, Tsukuba, Ibaraki 305-8572, Japan

³Mountain Science Center, University of Tsukuba, Ibaraki 305-8572, Japan

⁴COMET, School of Earth and Environment, University of Leeds, Leeds LS2 9JT, UK

⁵Japan Agency for Marine-Earth Science and Technology, 3173-25 Showa-machi, Kanazawa-ku, Yokohama 236-0001, Japan

⁶Disaster Prevention Research Institute, Kyoto University, Uji, Kyoto 611-0011, Japan

*Corresponding author: Shinji Yamashita (syamashita@geol.tsukuba.ac.jp)

**Second corresponding author: Yuji Yagi (yagi-y@geol.tsukuba.ac.jp)

ABSTRACT

We developed a flexible finite-fault inversion method for teleseismic P waveforms to obtain a detailed rupture process of a complex multiple-fault earthquake. We estimate the distribution of potency-rate density tensors on an assumed model fault plane to clarify rupture evolution processes, including variations of fault geometry. We applied our method to the 23 January 2018 Gulf of Alaska earthquake, setting the model fault area to fit the distribution of aftershocks occurring within one week of the mainshock. The obtained source model, which successfully explained the complex teleseismic P waveforms, shows that the 2018 earthquake ruptured a conjugate system of N-S and E-W faults. The spatiotemporal rupture evolution indicates irregular rupture behavior involving a multiple-shock sequence, which is likely associated with discontinuities in the fault geometry that originated from E-W sea-floor fracture zones and N-S plate-bending faults.

Introduction

The 23 January 2018 Gulf of Alaska earthquake (moment-magnitude M_w 7.9¹) struck offshore Kodiak Island (55.9097°N, 149.0521°W, 10.4 km depth; Alaska Earthquake Information Center, AEIC¹), in the seaward-region of the Alaska-Aleutian subduction zone. The Global Centroid Moment Tensor (GCMT) project^{2,3} reported that the 2018 Alaska earthquake had strike-slip faulting with a large non-double-couple component (47%). Aftershock seismicity determined by the AEIC¹ shows a lineation extending about 120 km N-S near the epicenter and two aftershock clusters centered about 60 km northeast and about 50 km west from the epicenter (Fig. 1). The GCMT solutions of aftershocks are dominated by strike-slip faulting, but include normal and reverse faulting (Fig. 1).

39 Several pioneering studies that built finite-fault models based on the aftershock distribution
40 demonstrated that the 2018 Alaska earthquake ruptured a quasi-orthogonal multiple-fault system
41 oriented approximately N-S and E-W⁴⁻⁸. However, it is difficult to adopt a reasonable fault model
42 because the fault model parametrization, number of fault segments, and fault geometries differ by
43 study, partly due to the spatial spread of the aftershock distribution (Fig. 1). Based on the static
44 slip distribution estimated from Global Navigation Satellite System and tsunami data, major slips
45 occurred on E-W-striking segments^{5,7,8}. Finite-fault inversions estimated that the maximum slip
46 occurred around the boundary between the crust and uppermost mantle in the N-S-oriented
47 segment^{4,6}, which would have played a significant role in tsunami generation. However, it remains
48 challenging to adequately explain the complex characteristics of the observed teleseismic body
49 waveforms by conventional finite-fault inversion methods due to the uncertainty on the fault
50 geometry, which lead to significant model errors.

51 In the framework of finite-fault waveform inversion, uncertainties on the Green's function
52 and fault geometry have been the major sources of model errors⁹⁻¹³. Those due to uncertainty on
53 the Green's function arose from a discrepancy between the true and calculated Green's functions.
54 To mitigate the effect of this uncertainty, Yagi and Fukahata¹³ explicitly introduced the error term
55 of the Green's function into the data covariance matrix. As a result, their inversion framework
56 allowed the stable estimation of the spatiotemporal distribution of slip-rate, usually without the
57 non-negative slip-rate constraint, which had been commonly applied in conventional waveform
58 inversion methods to obtain a plausible solution^{14,15}.

59 Model errors due to uncertainty on the fault geometry arose from inappropriate
60 assumptions about the fault geometry^{11,12}. For strike-slip earthquakes, many seismic stations are
61 distributed in the vicinity of nodal planes where the radiation pattern is sensitive to the assumed
62 fault geometry. An obtained solution can easily be distorted by inappropriate assumptions of strike
63 and dip¹². These effects can be mitigated by increasing the degrees of freedom in the assumed
64 seismic source model. Shimizu et al.¹² proposed an inversion method to express slip vectors on
65 the assumed model plane as the seismic potency tensor. Because their method adopts a linear
66 combination of five basis double-couple components¹⁶, the slip direction is not restricted to the
67 two slip components compatible with the fault direction. Of course, the true fault geometry should
68 be compatible with the actual slip direction. Nonetheless, because the teleseismic *P*-wave Green's
69 function is insensitive to slight changes in the absolute source location, their inversion method
70 enabled the spatiotemporal resolution of not only the detailed rupture evolution, but also variation
71 of the focal mechanism, including information on the fault geometry, which may differ from the
72 assumed model plane.

73 In this study, we developed a flexible finite-fault inversion framework that can estimate
74 both the rupture evolution and focal mechanism of earthquakes that ruptured along multiple
75 complex fault segments. This method incorporates appropriate smoothness constraints and a high-
76 degree-of-freedom planar model into the inversion framework of Shimizu et al.¹². Application of
77 our framework to the 2018 Alaska earthquake shows that our source model sufficiently reproduced
78 the observed complex waveforms without assumptions on fault geometry. The model also clarified
79 multiple, distinct rupture events in the conjugate fault system that have not been revealed by
80 conventional finite-fault inversion methods.

81 **Method**

82 In the inversion framework of Shimizu et al.¹², the seismic waveform u_j observed at a station j is
 83 given by

84
$$u_j(t) = \sum_{q=1}^5 \int_S (G_{qj}(t, \xi) + \delta G_{qj}(t, \xi)) * \dot{D}_q(t, \xi) d\xi + e_{bj}(t), \quad (1)$$

85 where G_{qj} is the calculated Green's function of the q th basis double-couple component, δG_{qj} is
 86 the model error on G_{qj} ¹³, \dot{D}_q is the q th potency-rate density function on the assumed fault model
 87 plane S , e_{bj} is background and instrumental noise, ξ represents a position on S , and $*$ denotes the
 88 convolution operator in the time domain.

89 Shimizu et al.¹² represented the assumed fault model plane S as a rectangle horizontally
 90 covering the seismic source region. However, for earthquakes with complex fault geometries, such
 91 as the 2018 Alaska earthquake, such a horizontal rectangular model plane includes areas beyond
 92 the seismic source region. Therefore, we further extended their inversion framework such that a
 93 horizontal non-rectangular model plane can be set according to the shape of the ruptured region as
 94 estimated from other information (e.g., aftershock seismicity). In other words, we introduced *a*
 95 *priori* information about the possible ruptured area into the inversion framework. In numerical
 96 tests, the use of a non-rectangular model plane improved spatial resolution and computation costs
 97 compared to a rectangular one (see Supplementary Material S1 and Figs. S1–S4).

98 In general, inversions are stabilized by adding smoothness constraints either implicitly or
 99 explicitly^{17,18}. In the formulation of Shimizu et al.¹², the smoothness constraints on each potency-
 100 rate density function \dot{D}_q in space and time are represented as

101
$$\nabla^2 \dot{D}_q(t, \xi) + \alpha_q = 0, \quad (2)$$

102
$$\frac{\partial^2}{\partial t^2} \dot{D}_q(t, \xi) + \beta_q = 0, \quad (3)$$

103 where α_q and β_q are assumed to be Gaussian noise with zero mean and covariances of $\sigma^2 \mathbf{I}$ and
 104 $\tau^2 \mathbf{I}$, respectively, where \mathbf{I} is an $M \times M$ (M is the number of model parameters) unit matrix.
 105 Because they introduced identical Gaussian distributions for all basis components and determined
 106 the optimal values of the hyperparameters σ^2 and τ^2 by Akaike's Bayesian information criterion
 107^{18,19}, the potency-rate density functions of basis components with relatively high amplitudes
 108 become smoother than those of basis components with relatively low amplitudes, which may bias
 109 the solution. Thus, when the amplitudes of the potency-rate density functions differ for each basis
 110 component, the standard deviations of the smoothness constraints should depend on the amplitude
 111 of each basis component.

112 In this study, we set the standard deviation of the smoothness constraints for each basis
 113 double-couple component to be proportional to its amplitude. That is, instead of α_q and β_q , we
 114 directly introduced Gaussian noise with zero mean and covariances $\sigma_q^2 \mathbf{I}$ and $\tau_q^2 \mathbf{I}$, respectively, as

115
$$\sigma_q^2 \mathbf{I} = k^2 m_q^2 \sigma^2 \mathbf{I}, \quad (4)$$

116
$$\tau_q^2 \mathbf{I} = k^2 m_q^2 \tau^2 \mathbf{I}, \quad (5)$$

117 where k is a scaling factor and m_q is the total potency of the q th basis double-couple component,
118 which is independently derived from the moment tensor solution. To avoid extremely small
119 standard deviations destabilizing the solution, we adjusted $k|m_q|$ so that it does not fall below
120 10% of its maximum absolute value. Following Yagi and Fukahata¹³, we determined the
121 hyperparameters σ^2 and τ^2 by Akaike's Bayesian information criterion^{18,19}. In numerical tests,
122 these improved smoothness constraints mitigated the excessive smoothing of the dominant basis
123 component imposed by conventional smoothness constraints and, when combined with a non-
124 rectangular model plane, outperformed the conventional framework (see Supplementary Material
125 S1, Figs. S1–S4 and Table S1).

126 Data and Fault Parameterization

127 We used teleseismic P waveforms (vertical components) recorded at stations with epicentral
128 distances of 30–90° (downloaded from the Incorporated Research Institutions for Seismology Data
129 Management Center). Of these, we selected 78 stations with good data quality and azimuthal
130 coverage (Fig. 2c) and converted the P waveforms to velocity waveforms at a sampling rate of 0.8
131 s. The theoretical Green's functions for teleseismic body waves were calculated by the method of
132 Kikuchi and Kanamori¹⁶ at a sampling rate of 0.1 s, and the attenuation time constraint t^* for the
133 P wave was taken to be 1.0 s. We adopted a 1-D velocity structure derived from the CRUST1.0
134 model (see Supplementary Table S2)²⁰ to calculate the theoretical Green's functions. Following
135 Shimizu et al.¹², we did not low-pass filter the observed waveforms or calculated Green's
136 functions. For the smoothness constraints, we calculated m_q based on the GCMT solution of the
137 2018 Alaska earthquake. The GCMT solution shows that the M1 (strike-slip) component is more
138 prominent than the others (see Supplementary Table S3), including the M4 (dip-slip) component
139 (see Supplementary Fig. S4)¹⁶. The scaling factor k in eqs. (4) and (5) was set such that
140 $\min(k|m_q|) = 1$ (Table S3).

141 Based on the aftershock distribution, the 2018 Alaska earthquake is considered to have
142 occurred on a quasi-orthogonal multiple-fault system^{4–8}. To cover the high point density area of
143 aftershocks within one week of the event (Fig. 2a)¹, we set up a non-rectangular horizontal model
144 fault plane with a maximum width and length of 130 km, which was expanded using a bilinear B-
145 spline with a knot spacing of 10 km. We adopted the epicenter as that determined by the AEIC¹:
146 55.9097°N, 149.0521°W. The depth of the model fault plane was set at 33.6 km according to the
147 GCMT centroid depth. For the inversion analysis, we adopted a potency-rate density function on
148 each knot, each representing a linear combination of B-splines at an interval of 0.8 s. The
149 maximum rupture-front velocity, which defines the rupture starting time at each knot, was set to
150 7.0 km/s to account for the possibility of supershear rupture propagation. The rupture ending time
151 at each knot was set to 65 s from the origin time based on previous inversion results^{4,6}. We
152 evaluated the sensitivity of our model by perturbing the model parameters (see Supplementary
153 Material S2, and Figs. S5 and S6).

154 Results

155 We estimated the spatiotemporal distribution of the potency density tensor for the 2018 Alaska
156 earthquake by applying our flexible finite-fault inversion method to teleseismic P waveforms. The
157 estimated total moment tensor, calculated by taking the spatial and temporal integrals of the

158 potency-rate density functions, expresses strike-slip faulting, including 36% non-double-couple
159 components (Fig. 2a). The spatial distribution of the potency density tensor, obtained by
160 temporally integrating the potency-rate density functions at each knot, is also dominated by strike-
161 slip focal mechanisms, with a maximum slip of 6 m about 50 km north of the epicenter (Fig. 2a).
162 The moment rate function is elevated over two time periods, separated at 27 s from the origin time:
163 the first period is characterized by three large spikes and the second by numerous smaller spikes
164 (Fig. 2b). The total seismic moment is 14.9×10^{20} N m (M_w 8.05). The synthetic waveforms from
165 the obtained source model well reproduce the observed waveforms (see Supplementary Fig. S11),
166 including those at stations near the nodal planes (Fig. 2d).

167 Based on the moment rate function and snapshots of the potency-rate density tensors (Figs.
168 2b and S12, respectively), we report the detailed rupture history by dividing it into main (A, 0–27
169 s) and secondary rupture stages (B, 27–65 s). Based on the location, timing, and continuity of the
170 rupture, we further identified three phases (A1–A3) during the main stage and five (B1–B5) during
171 the secondary stage.

172 Main Rupture Stage (A)

173 The initial phase, A1 (0–9 s), started at the hypocenter and propagated bilaterally northward and
174 southward with strike-slip focal mechanisms (snapshot at 2 s in Fig. 3a). Although it is generally
175 difficult to identify the preferred fault plane from the two possible nodal planes in this earthquake,
176 the direction of rupture propagation during phase A1 coincided with the N-S directed nodal plane.
177 The spatial distribution of focal mechanisms shows that the strike of the fault plane gradually
178 rotated counterclockwise from north to south of the epicenter; we obtained a strike/dip of $174^\circ/82^\circ$
179 around 20 km north of the epicenter, but $163^\circ/76^\circ$ around 20 km south of the epicenter (6 s in Fig.
180 3a). The northward rupture seems to have stagnated near the 56° N fracture zone (FZ) after about
181 9 s²¹.

182 Phase A2 (7–27 s) started about 50 km northeast of the epicenter at around 7 s after the
183 origin time and propagated west along the Aka FZ (8 s in Fig. 3a)²¹. This rupture direction is
184 consistent with the obtained E-W strike directions (e.g., 10 s in Fig. 3a). The westward rupture
185 propagated to 149.2° W, where the Aka FZ intersects the N-S aftershock lineation, until 11 s, then
186 turned southward, indicating that the N-S strike direction is the preferred fault plane (12 s in Fig.
187 3a). The southward rupture halted at around 12 s at the same location where the northward rupture
188 of phase A1 had stagnated at about 9 s. After 12 s, a discontinuous rupture occurred along the Aka
189 FZ: ruptures propagating southward and northward from the Aka FZ near 148.6° W are detected at
190 around 16 and 20 s, respectively (Fig. 3a). The rupture on the Aka FZ near 149.2° W is again
191 apparent at around 24 s, and gradually ceased by 27 s.

192 Phase A3 (16–27 s), started about 40 km northwest of the epicenter, near the 56° N FZ,
193 around 16 s after the origin time (Fig. 3a). This rupture propagated bilaterally to the northeast and
194 southwest until around 18 s, then gradually abated until around 20 s. At that time, another western
195 rupture occurred at the northwest end of the model region and propagated to the south (20 s in Fig.
196 3a), stagnating at the 56° N FZ about 50 km west of the epicenter at around 22 s (24 s in Fig. 3a).

197 Secondary Rupture Stage (B)

198 We identified seven peaks in the moment rate function during the secondary rupture stage (Fig.
199 2b), which we attribute to five phases in the snapshots (Fig. 3b). Phase B1 (28–44 s) occurred
200 along the Aka FZ. In particular, phase B1 ruptures at around 32.8 and 40.0 s were relatively large,

201 and appear as individual peaks in the moment rate function (Figs. 2b and 3b). Phase B2 (44–52 s)
202 mainly ruptured the region west of the epicenter. The rupture at around 44.8 s occurred along the
203 56°N FZ and that at around 49.6 s struck about 30 km south of the 56°N FZ (Fig. 3b). Phase B3
204 (53–60 s) occurred mainly northeast of the epicenter, but also struck the intersection of the Aka
205 FZ and the N-S aftershock lineation at around 52.8 s (Fig. 3b). A northward rupture from the Aka
206 FZ was also detected at around 57.6 s. The last peak of the moment rate function corresponds to
207 two independent phases that occurred at around 63.2 s: B4 (62–65 s) ruptured about 20 km south
208 of the Aka FZ and B5 (62–64 s) ruptured about 30 km south of the epicenter (Fig. 3b).

209 **Discussion**

210 Our inversion results indicate that the main rupture stage (0–27 s after origin) affected segments
211 oriented both N-S and E-W, suggesting that the 2018 Alaska earthquake ruptured a conjugate fault
212 system, as proposed in previous studies^{4–8}. Our source model suggests that the rupture occurred
213 along weak zones in the sea floor: fracture zones extending E-W and plate-bending faults parallel
214 to N-S magnetic lineaments^{22,23}. The N-S plate bending faults have been interpreted as pre-
215 existing oceanic spreading features that were reactivated by subduction of the Pacific Plate²³.
216 Krabbenhoft et al.²¹ associated these pre-existing features with the radiation of high-frequency
217 waves based on back-projection and the aftershock distribution.

218 A notable irregular rupture propagation highlighted by our inversion results is the
219 northward rupture at around 9 s in phase A1 and the southward rupture at around 12 s in phase A2,
220 both of which stopped near the 56°N FZ (8 and 12 s, respectively, in Fig. 3a). The N-S aftershock
221 lineation is divided into northern and southern clusters across the 56°N FZ (Fig. 3a). Given the
222 phase A1 and A2 ruptures and the geometrical offset of the N-S aftershock lineation, the northern
223 and southern fault system crossing the 56°N FZ can be regarded as a strike-slip step over. Based
224 on our obtained focal mechanisms, these two N-S faults are both right-lateral strike-slip faults that
225 dip steeply to the west (8 and 12 s in Fig. 3a), and the counterclockwise rotation of the strike angle
226 during phase A1 is consistent with the southern N-S aftershock lineation (6 s in Fig. 3a). Because
227 irregular rupture behaviors are generally a result of geometric complexities, including barriers
228 caused by discontinuous fault steps^{24–26}, we interpret that this fault step over caused the rupture to
229 stagnate at around 9 and 12 s.

230 Multiple sub-events occurring in a conjugate strike-slip fault system have been reported in
231 previous studies^{27–31}. In this study, we have shown a causal link between the multiple rupture
232 episodes during the 2018 Alaska earthquake (stages A and B) and pre-existing bathymetric features
233 by resolving both the rupture evolution and variation of fault geometry using only teleseismic body
234 waves. Similar observations were made during the M_w 8.6 2012 Sumatra earthquake in the
235 Wharton basin. That earthquake involved multiple $M_w > 8$ sub-events along a conjugate fault
236 system^{30,32}, which developed by deep ductile shear localization beneath the brittle upper
237 lithosphere of the oceanic plate³³.

238 We evaluated how the newly developed method improved the source model of the 2018
239 Gulf of Alaska earthquake by performing the inversion analysis with the conventional smoothness
240 constraints (Fig. S7)¹². The inversion result with the conventional smoothness constraints show
241 general agreement with that obtained by the improved smoothness constraints (Fig. S7). However,
242 the spatiotemporal rupture propagation of the conventional smoothness constraints is smoother
243 than that of the improved ones by the excessive smoothing for the most dominant $M1$ component
244 for the earthquake (Fig. S8), which provides the blurrier image, making it difficult to clearly

245 resolve the multiple sub-events (Figs. 3 and S7). A resolvability of the complex episode of multiple
246 sub-events was further confirmed by the numerical test using the solution of the 2018 Alaska
247 earthquake (Fig. 3) as an input model, which was robustly reproduced by the new method (see
248 Supplementary Fig. S9).

249 It is possible that the complex waveforms observed during the 2018 Alaska earthquake
250 were contaminated by reverberations due to the bathymetric setting that cannot be reproduced by
251 the theoretical Green's function, resulting in dummy multiple events^{34–37}. We evaluated this
252 possibility by using empirical Green's functions^{38,39} and confirm that it is unlikely that the multiple
253 rupture stages originated from such reverberations (see Supplementary Material S3 and Fig. S10).

254 The sub-events that occurred after the main A1 phase can be regarded as early aftershocks
255 missing from global catalogs⁴⁰. Although it is difficult to distinguish whether such early near- to
256 intermediate-field aftershocks were dynamically or statically triggered⁴⁰, it is noteworthy that the
257 rupture propagated from A1 to A2 at more than 5 km/s (see Supplementary Material S2 and Fig.
258 S6); this is faster than the surface wave velocity (3–4 km/s), suggesting that the A2 rupture was
259 triggered by the A1 rupture.

260 Conclusions

261 We developed a finite-fault inversion method for teleseismic *P* waveforms with improved
262 smoothness constraints to obtain source processes for earthquakes with complex multiple-fault
263 ruptures. We applied our inversion method to the 2018 Alaska earthquake and estimated its
264 spatiotemporal rupture process. Although the observed waveforms are very complicated, reflecting
265 the complex rupture process and fault geometry, the waveforms calculated from our source model
266 fit well. The obtained source model suggests a complex multiple-shock sequence on a conjugate
267 fault system, consistent with pre-existing bathymetric features. Irregular rupture stagnation about
268 20 km north of the epicenter may have been promoted by a fault step across a sea-floor fracture
269 zone.

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- 379

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389 **Author contributions**

390 S.Y. and Y.Y. conceptualized this study, compiled the data and conducted the analyses. S.Y., Y.Y.,
391 R.O., K.S, R.A. and Y.F. contributed to the methodology. S.Y., Y.Y., R.O. and K.S. processed and
392 interpreted the data. S.Y. and Y.Y. wrote the manuscript which was revised and edited by R.O.,
393 K.S., R.A. and Y.F. All authors approved the submitted manuscript. All authors agreed both to be
394 personally accountable for the author's own contributions and to ensure that questions related to
395 the accuracy or integrity of any part of the work, even ones in which the author was not personally
396 involved, are appropriately investigated, resolved, and the resolution documented in the literature.

397 **Additional information**

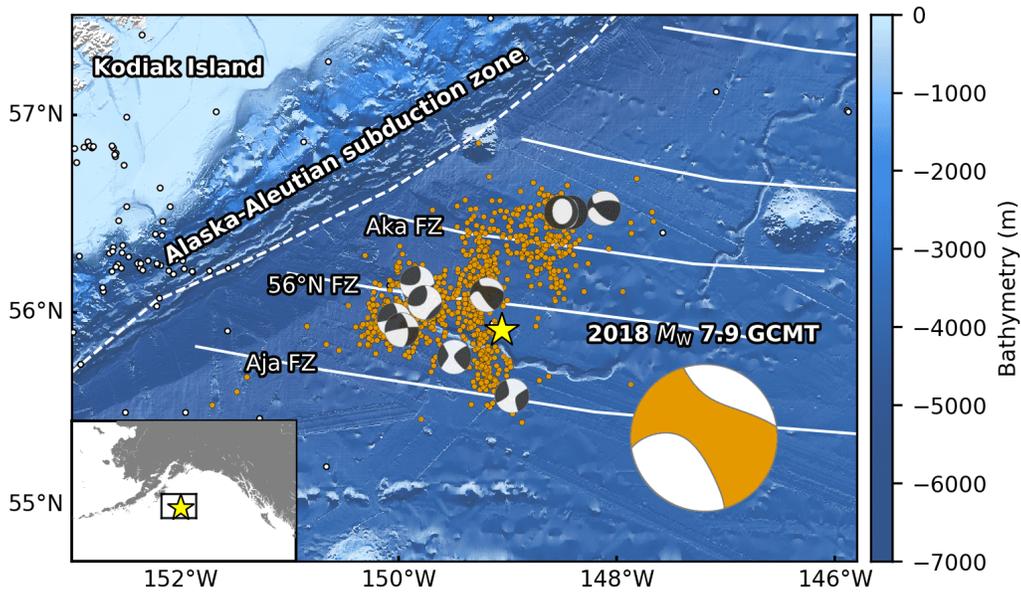
398 Correspondence and requests for materials should be addressed to S.Y. or Y.Y.

399 **Data Availability**

400 Waveform data was downloaded through the IRIS Wilber 3 system
401 (https://ds.iris.edu/wilber3/find_stations/10607586). Teleseismic waveforms were obtained from
402 the following networks: the Canadian National Seismograph Network (CN;
403 <https://doi.org/10.7914/SN/CN>); the Caribbean USGS Network (CU;
404 <https://doi.org/10.7914/SN/CU>); the GEOSCOPE (G; <https://doi.org/10.18715/GEOSCOPE.G>);
405 the Hong Kong Seismograph Network (HK; <https://www.fdsn.org/networks/detail/HK/>); the New
406 China Digital Seismograph Network (IC; <https://doi.org/10.7914/SN/IC>); the IRIS/IDA Seismic
407 Network (II; <https://doi.org/10.7914/SN/II>); the International Miscellaneous Stations (IM;
408 <https://www.fdsn.org/networks/detail/IM/>); the Global Seismograph Network (IU;
409 <https://doi.org/10.7914/SN/IU>), and the Pacific21 (PS; <https://www.fdsn.org/networks/detail/PS/>).
410 The moment tensor solutions are obtained from the GCMT catalog
411 (<https://www.globalcmt.org/CMTsearch.html>). The CRUST 1.0 model is available at
412 <https://igppweb.ucsd.edu/~gabi/crust1.html>. The fracture zone data is obtained from the Global
413 Seafloor Fabric and Magnetic Lineation Data Base Project website
414 (<http://www.soest.hawaii.edu/PT/GSFML/>).

415

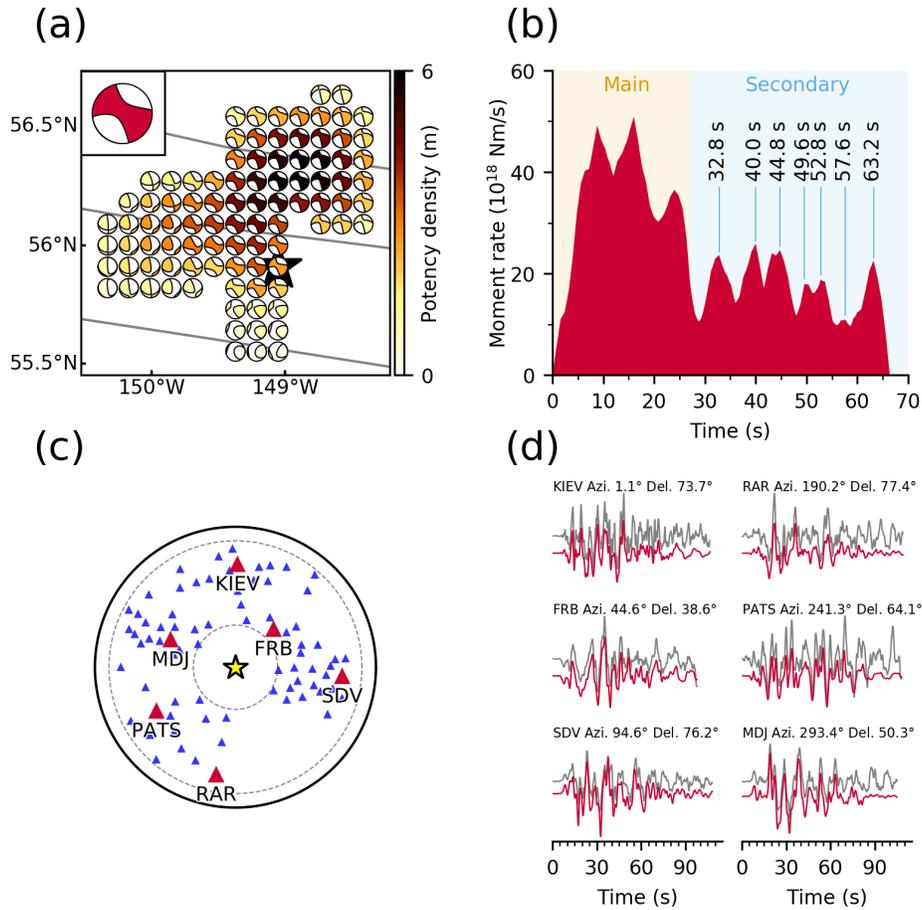
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417

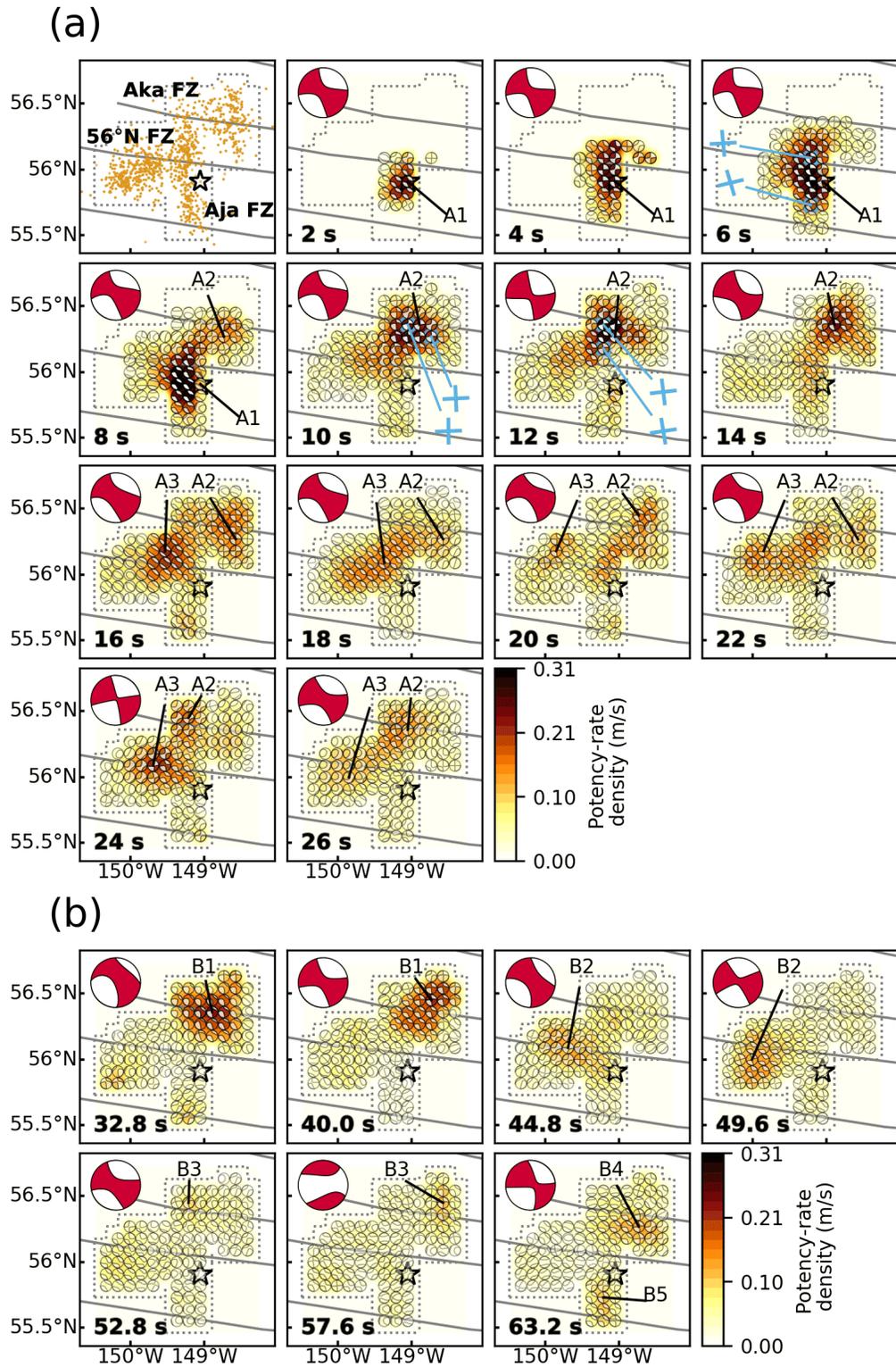
418 **Figure 1.** Overview of the source region of the 2018 Gulf of Alaska earthquake. The star is the
 419 mainshock epicenter, orange dots are aftershocks ($M \geq 3$) that occurred within one week of the
 420 mainshock, and white dots show background seismicity before the mainshock ($M \geq 3.5$, 1 January
 421 2008 to 22 January 2018); all epicentral locations are from AEIC¹. The ‘beachball’ diagrams show
 422 the GCMT solutions for the mainshock (large, bottom right) and aftershocks with $M \geq 3.5$. White
 423 dashed lines represent plate boundaries⁴⁴, and white solid lines represent fracture zones^{45,46}. The
 424 background bathymetry is derived from the GEBCO 2020 Grid⁴⁷. The inset map shows the
 425 regional setting.

426



427

428 **Figure 2.** Model setting and summary of results. (a) Map projection of the potency density tensor
 429 distribution on the assumed model fault plane. The star and solid lines indicate the epicenter¹ and
 430 fracture zones^{45,46}, respectively. Inset is the total moment tensor. (b) The moment rate function is
 431 divided into the main and secondary rupture stages at 27 s. The individual peaks during the
 432 secondary stage correspond to snapshots in Fig. 3b. (c) Azimuthal equidistant projection of the
 433 station distribution used in the inversion. The star denotes the epicenter, and triangles denote
 434 station locations (waveforms for red stations are shown in (d)). The inner and outer dotted lines
 435 show epicentral distances of 30° and 90°, respectively. (d) Comparison of observed waveforms
 436 (gray) with synthetic waveforms (red) at the selected stations in (c). Each panel is labeled with the
 437 station name, azimuth (Azi.), and epicentral distance (Del.) from the mainshock. Waveform
 438 comparisons for all stations are shown in Supplementary Fig. S11.
 439



440

441 **Figure 3.** Snapshots of the potency-rate density tensors for (a) the main rupture stage A and (b)
 442 the secondary rupture stage B. The corresponding time after onset for each snapshot is noted at the
 443 bottom-left of each panel. The dotted line shows the border of the assumed model fault plane. The

444 star and solid lines indicate the epicenter ¹ and fracture zones ^{45,46}, respectively. Blue crosses show
445 the strike directions of small beachball diagrams derived from the potency-rate density tensor. The
446 top-left panel in (a) is the epicentral distribution of aftershocks ($M \geq 3$) that occurred within one
447 week of the mainshock ¹. The large beachball in each panel indicates the corresponding total
448 moment tensor at each time.
449