

1 **Consecutive Ruptures on a Complex Conjugate Fault System During the 2018 Gulf**
2 **of Alaska Earthquake**
3

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20 **Key Points:**

- 21
- 22 • We developed a finite-fault inversion method to estimate rupture evolution and fault geometry for earthquakes rupturing multiple faults
 - 23 • Our source model of the 2018 Gulf of Alaska earthquake revealed that multiple-rupture stages evolved in a complex conjugate fault system
 - 24 • Fracture zones on the oceanic floor may have acted as barriers to irregular rupture evolution during the 2018 Gulf of Alaska earthquake
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28 **Abstract**

29 We developed a flexible finite-fault inversion method for teleseismic P waveforms to obtain a
30 detailed rupture process of a complex multiple-fault earthquake. We estimate the distribution of
31 potency-rate density tensors on an assumed model fault plane to clarify rupture evolution
32 processes, including variations of fault geometry. We applied our method to the 23 January 2018
33 Gulf of Alaska earthquake, setting the model fault area to fit the distribution of aftershocks
34 occurring within one week of the mainshock. The obtained source model, which successfully
35 explained the complex teleseismic P waveforms, shows that the 2018 earthquake ruptured a
36 conjugate system of N-S and E-W faults. The spatiotemporal rupture evolution indicates
37 irregular rupture behavior involving a multiple-shock sequence, which is likely associated with
38 discontinuities in the fault geometry that originated from E-W sea-floor fracture zones and N-S
39 plate-bending faults.

40 **Plain Language Summary**

41 On 23 January 2018, a large earthquake occurred in the Gulf of Alaska offshore from Kodiak
42 Island, rupturing the Pacific tectonic plate seaward of the Alaska-Aleutian trench. This
43 earthquake is known to have had a complex rupture process, with multiple rupture stages in
44 which rupture directions and speeds changed. It has been challenging to adequately explain the
45 observed seismic data, which record complex processes. We developed a method of using
46 seismic data recorded at great distances from the earthquake to estimate rupture evolution and
47 slip direction without making assumptions about fault geometry. We applied our method to the
48 2018 Gulf of Alaska earthquake. The earthquake process we estimated comprised multiple
49 ruptures that propagated along roughly north-south and east-west trends and was consistent with
50 the aftershock distribution and pre-existing fault zones beneath the sea floor. Our results suggest
51 that the irregular rupture was associated with discontinuities in the fault geometry related to pre-
52 existing subsea fracture zones and bending faults of the Pacific tectonic plate.

53 **1 Introduction**

54 The 23 January 2018 Gulf of Alaska earthquake (moment-magnitude M_w 7.9; U.S.
55 Geological Survey National Earthquake Information Center) struck offshore Kodiak Island
56 (55.9097°N, 149.0521°W, 10.4 km depth; Alaska Earthquake Center, AEC), in the seaward-
57 region of the Alaska-Aleutian subduction zone. The Global Centroid Moment Tensor (GCMT)
58 project (Dziewonski et al., 1981; Ekström et al., 2012) reported that the 2018 Alaska earthquake
59 had strike-slip faulting with a large non-double-couple component (47%). Aftershock seismicity
60 determined by the AEC (USGS, 2017) shows a lineation extending about 120 km N-S near the
61 epicenter and two aftershock clusters centered about 60 km northeast and about 50 km west from
62 the epicenter (Figure 1). The GCMT solutions of aftershocks are dominated by strike-slip
63 faulting, but include normal and reverse faulting (Figure 1).

64 Several pioneering studies that built finite-fault models based on the aftershock
65 distribution demonstrated that the 2018 Alaska earthquake ruptured a quasi-orthogonal multiple-
66 fault system oriented approximately N-S and E-W (Guo et al., 2020; Hossen et al., 2020; Lay et
67 al., 2018; Ruppert et al., 2018; Zhao et al., 2019). However, it is difficult to adopt a reasonable
68 fault model because the fault model parametrization, number of fault segments, and fault
69 geometries differ by study, partly due to the spatial spread of the aftershock distribution (Figure
70 1). Based on the static slip distribution estimated from Global Navigation Satellite System and

71 tsunami data, major slips occurred on E-W-striking segments (Hossen et al., 2020; Ruppert et al.,
72 2018; Zhao et al., 2019). Finite-fault inversions estimated that the maximum slip occurred
73 around the boundary between the crust and uppermost mantle in the N-S-oriented segment (Guo
74 et al., 2020; Lay et al., 2018), which would have played a significant role in tsunami generation.
75 However, it remains challenging to adequately explain the complex characteristics of the
76 observed teleseismic body waveforms by conventional finite-fault inversion methods due to the
77 uncertainty on the fault geometry, which lead to significant model errors.

78 In the framework of finite-fault waveform inversion, uncertainties on the Green's
79 function and fault geometry have been the major sources of model errors (e.g., Duputel et al.,
80 2014; Minson et al., 2013; Ragon et al., 2018; Shimizu et al., 2020; Yagi & Fukahata, 2011).
81 Those due to uncertainty on the Green's function arose from a discrepancy between the true and
82 calculated Green's functions. To mitigate the effect of this uncertainty, Yagi and Fukahata
83 (2011) explicitly introduced the error term of the Green's function into the data covariance
84 matrix. As a result, their inversion framework allowed the stable estimation of the spatiotemporal
85 distribution of slip-rate, usually without the non-negative slip-rate constraint, which had been
86 commonly applied in conventional waveform inversion methods to obtain a plausible solution
87 (e.g., Das & Kostrov, 1990; Hartzell & Heaton, 1983).

88 Model errors due to uncertainty on the fault geometry arose from inappropriate
89 assumptions about the fault geometry (e.g., Ragon et al., 2018; Shimizu et al., 2020). For strike-
90 slip earthquakes, many seismic stations are distributed in the vicinity of nodal planes where the
91 radiation pattern is sensitive to the assumed fault geometry. An obtained solution can easily be
92 distorted by inappropriate assumptions of strike and dip (Shimizu et al., 2020). These effects can
93 be mitigated by increasing the degrees of freedom in the assumed seismic source model. Shimizu
94 et al. (2020) proposed an inversion method to express slip vectors on the assumed model plane as
95 the seismic potency tensor. Because their method adopts a linear combination of five basis
96 double-couple components (Kikuchi & Kanamori, 1991), the slip direction is not restricted to the
97 two slip components compatible with the fault direction. Of course, the true fault geometry
98 should be compatible with the actual slip direction. Nonetheless, because the teleseismic *P*-wave
99 Green's function is insensitive to slight changes in the absolute source location, their inversion
100 method enabled the spatiotemporal resolution of not only the detailed rupture evolution, but also
101 variation of the focal mechanism, including information on the fault geometry, which may differ
102 from the assumed model plane.

103 In this study, we developed a flexible finite-fault inversion framework that can estimate
104 both the rupture evolution and focal mechanism of earthquakes that ruptured along multiple
105 complex fault segments. This method incorporates appropriate smoothness constraints and a
106 high-degree-of-freedom planar model into the inversion framework of Shimizu et al. (2020).
107 Application of our framework to the 2018 Alaska earthquake shows that our source model
108 sufficiently reproduced the observed complex waveforms without assumptions on fault geometry.
109 The model also clarified multiple, distinct rupture events in the conjugate fault system that have
110 not been revealed by conventional finite-fault inversion methods.

111 **2 Method**

112 In the inversion framework of Shimizu et al. (2020), the seismic waveform u_j observed at
113 a station j is given by

$$114 \quad u_j(t) = \sum_{q=1}^5 \int_S (G_{qj}(t, \xi) + \delta G_{qj}(t, \xi)) * \dot{D}_q(t, \xi) d\xi + e_{bj}(t), \quad (1)$$

115 where G_{qj} is the calculated Green's function of the q th basis double-couple component, δG_{qj} is
 116 the model error on G_{qj} (Yagi & Fukahata, 2011), \dot{D}_q is the q th potency-rate density function on
 117 the assumed fault model plane S , e_{bj} is background and instrumental noise, ξ represents a
 118 position on S , and $*$ denotes the convolution operator in the time domain.

119 Shimizu et al. (2020) represented the assumed fault model plane S as a rectangle
 120 horizontally covering the seismic source region. However, for earthquakes with complex fault
 121 geometries, such as the 2018 Alaska earthquake, such a horizontal rectangular model plane
 122 includes areas beyond the seismic source region. Therefore, we further extended their inversion
 123 framework such that a horizontal non-rectangular model plane can be set according to the shape
 124 of the ruptured region as estimated from other information (e.g., aftershock seismicity). In other
 125 words, we introduced *a priori* information about the possible ruptured area into the inversion
 126 framework. In numerical tests, the use of a non-rectangular model plane improved spatial
 127 resolution and computation costs compared to a rectangular one (Text S1 and Figures S1–S4).

128 In general, inversions are stabilized by adding smoothness constraints either implicitly or
 129 explicitly (e.g., Nocquet, 2018; Yabuki & Matsu'ura, 1992). In the formulation of Shimizu et al.
 130 (2020), the smoothness constraints on each potency-rate density function \dot{D}_q in space and time
 131 are represented as

$$132 \quad \nabla^2 \dot{D}_q(t, \xi) + \alpha_q = 0, \quad (2)$$

$$133 \quad \frac{\partial^2}{\partial t^2} \dot{D}_q(t, \xi) + \beta_q = 0, \quad (3)$$

134 where α_q and β_q are assumed to be Gaussian noise with zero mean and covariances of $\sigma^2 \mathbf{I}$ and
 135 $\tau^2 \mathbf{I}$, respectively, where \mathbf{I} is an $M \times M$ (M is the number of model parameters) unit matrix.
 136 Because they introduced identical Gaussian distributions for all basis components and
 137 determined the optimal values of the hyperparameters σ^2 and τ^2 by Akaike's Bayesian
 138 information criterion (Akaike, 1980; Yabuki & Matsu'ura, 1992), the potency-rate density
 139 functions of basis components with relatively high amplitudes become smoother than those of
 140 basis components with relatively low amplitudes, which may bias the solution. Thus, when the
 141 amplitudes of the potency-rate density functions differ for each basis component, the standard
 142 deviations of the smoothness constraints should depend on the amplitude of each basis
 143 component.

144 In this study, we set the standard deviation of the smoothness constraints for each basis
 145 double-couple component to be proportional to its amplitude. That is, instead of α_q and β_q , we
 146 directly introduced Gaussian noise with zero mean and covariances $\sigma_q^2 \mathbf{I}$ and $\tau_q^2 \mathbf{I}$, respectively, as

$$147 \quad \sigma_q^2 \mathbf{I} = k^2 m_q^2 \sigma^2 \mathbf{I}, \quad (4)$$

$$148 \quad \tau_q^2 \mathbf{I} = k^2 m_q^2 \tau^2 \mathbf{I}, \quad (5)$$

149 where k is a scaling factor and m_q is the total potency of the q th basis double-couple component,
 150 which is independently derived from the moment tensor solution. To avoid extremely small

151 standard deviations destabilizing the solution, we adjusted $k|m_q|$ so that it does not fall below
 152 10% of its maximum absolute value. Following Yagi and Fukahata (2011), we determined the
 153 hyperparameters σ^2 and τ^2 by Akaike's Bayesian information criterion (Akaike, 1980; Yabuki
 154 & Matsu'ura, 1992). In numerical tests, these improved smoothness constraints mitigated the
 155 excessive smoothing of the dominant basis component imposed by conventional smoothness
 156 constraints and, when combined with a non-rectangular model plane, outperformed the
 157 conventional framework (Text S1, Figures S1–S4, Table S1).

158 **3 Data and Fault Parameterization**

159 We used teleseismic P waveforms (vertical components) recorded at stations with
 160 epicentral distances of 30–90° (downloaded from the Incorporated Research Institutions for
 161 Seismology Data Management Center). Of these, we selected 78 stations with good data quality
 162 and azimuthal coverage (Figure 2c) and converted the P waveforms to velocity waveforms at a
 163 sampling rate of 0.8 s. The theoretical Green's functions for teleseismic body waves were
 164 calculated by the method of Kikuchi and Kanamori (1991) at a sampling rate of 0.1 s, and the
 165 attenuation time constraint t^* for the P wave was taken to be 1.0 s. We adopted a 1-D velocity
 166 structure derived from the CRUST1.0 model (Laske et al., 2013; Table S2) to calculate the
 167 theoretical Green's functions. Following Shimizu et al. (2020), we did not low-pass filter the
 168 observed waveforms or calculated Green's functions. For the smoothness constraints, we
 169 calculated m_q based on the GCMT solution of the 2018 Alaska earthquake. The GCMT solution
 170 shows that the M1 (strike-slip) component is more prominent than the others (Table S3),
 171 including the M4 (dip-slip) component (see Figure S4; Kikuchi & Kanamori, 1991). The scaling
 172 factor k in eqs. (4) and (5) was set such that $\min(k|m_q|) = 1$ (Table S3).

173 Based on the aftershock distribution, the 2018 Alaska earthquake is considered to have
 174 occurred on a quasi-orthogonal multiple-fault system (Guo et al., 2020; Hossen et al., 2020; Lay
 175 et al., 2018; Ruppert et al., 2018; Zhao et al., 2019). To cover the high point density area of
 176 aftershocks within one week of the event (determined by the AEC; Figure 2a), we set up a non-
 177 rectangular horizontal model fault plane with a maximum width and length of 130 km, which
 178 was expanded using a bilinear B-spline with a knot spacing of 10 km. We adopted the epicenter
 179 as that determined by the AEC: 55.9097°N, 149.0521°W. The depth of the model fault plane was
 180 set at 33.6 km according to the GCMT centroid depth. For the inversion analysis, we adopted a
 181 potency-rate density function on each knot, each representing a linear combination of B-splines
 182 at an interval of 0.8 s. The maximum rupture-front velocity, which defines the rupture starting
 183 time at each knot, was set to 7.0 km/s to account for the possibility of supershear rupture
 184 propagation. The rupture ending time at each knot was set to 65 s from the origin time based on
 185 previous inversion results (Guo et al., 2020; Lay et al., 2018). We evaluated the sensitivity of our
 186 model by perturbing the model parameters and comparing our results with those obtained using
 187 the conventional smoothness constraints (see Text S2 and Figures S5–S8).

188 **4 Results**

189 We estimated the spatiotemporal distribution of the potency density tensor for the 2018
 190 Alaska earthquake by applying our flexible finite-fault inversion method to teleseismic P
 191 waveforms. The estimated total moment tensor, calculated by taking the spatial and temporal
 192 integrals of the potency-rate density functions, expresses strike-slip faulting, including 36% non-

193 double-couple components (Figure 2a). The spatial distribution of the potency density tensor,
194 obtained by temporally integrating the potency-rate density functions at each knot, is also
195 dominated by strike-slip focal mechanisms, with a maximum slip of 6 m about 50 km north of
196 the epicenter (Figure 2a). The moment rate function is elevated over two time periods, separated
197 at 27 s from the origin time: the first period is characterized by three large spikes and the second
198 by numerous smaller spikes (Figure 2b). The total seismic moment is 14.9×10^{20} N m (M_w 8.05).
199 The synthetic waveforms from the obtained source model well reproduce the observed
200 waveforms (Figure S10), including those at stations near the nodal planes (Figure 2d).

201 Based on the moment rate function and snapshots of the potency-rate density tensors
202 (Figures 2b and S11, respectively), we report the detailed rupture history by dividing it into main
203 (A, 0–27 s) and secondary rupture stages (B, 27–65 s). Based on the location, timing, and
204 continuity of the rupture, we further identified three phases (A1–A3) during the main stage and
205 five (B1–B5) during the secondary stage.

206 4.1 Main Rupture Stage (A)

207 The initial phase, A1 (0–9 s), started at the hypocenter and propagated bilaterally
208 northward and southward with strike-slip focal mechanisms (snapshot at 2 s in Figure 3a).
209 Although it is generally difficult to identify the preferred fault plane from the two possible nodal
210 planes in this earthquake, the direction of rupture propagation during phase A1 coincided with
211 the N-S directed nodal plane. The spatial distribution of focal mechanisms shows that the strike
212 of the fault plane gradually rotated counterclockwise from north to south of the epicenter; we
213 obtained a strike/dip of $174^\circ/82^\circ$ around 20 km north of the epicenter, but $163^\circ/76^\circ$ around 20
214 km south of the epicenter (6 s in Figure 3a). The northward rupture seems to have stagnated near
215 the 56° N fracture zone (FZ) after about 9 s (Krabbenhoef et al., 2018).

216 Phase A2 (7–27 s) started about 50 km northeast of the epicenter at around 7 s after the
217 origin time and propagated west along the Aka FZ (8 s in Figure 3a; Krabbenhoef et al., 2018).
218 This rupture direction is consistent with the obtained E-W strike directions (e.g., 10 s in Figure
219 3a). The westward rupture propagated to 149.2° W, where the Aka FZ intersects the N-S
220 aftershock lineation, until 11 s, then turned southward, indicating that the N-S strike direction is
221 the preferred fault plane (12 s in Figure 3a). The southward rupture halted at around 12 s at the
222 same location where the northward rupture of phase A1 had stagnated at about 9 s. After 12 s, a
223 discontinuous rupture occurred along the Aka FZ: ruptures propagating southward and
224 northward from the Aka FZ near 148.6° W are detected at around 16 and 20 s, respectively
225 (Figure 3a). The rupture on the Aka FZ near 149.2° W is again apparent at around 24 s, and
226 gradually ceased by 27 s.

227 Phase A3 (16–27 s), started about 40 km northwest of the epicenter, near the 56° N FZ,
228 around 16 s after the origin time (Figure 3a). This rupture propagated bilaterally to the northeast
229 and southwest until around 18 s, then gradually abated until around 20 s. At that time, another
230 western rupture occurred at the northwest end of the model region and propagated to the south
231 (20 s in Figure 3a), stagnating at the 56° N FZ about 50 km west of the epicenter at around 22 s
232 (24 s in Figure 3a).

233 4.2 Secondary Rupture Stage (B)

234 We identified seven peaks in the moment rate function during the secondary rupture stage
235 (Figure 2b), which we attribute to five phases in the snapshots (Figure 3b). Phase B1 (28–44 s)

236 occurred along the Aka FZ. In particular, phase B1 ruptures at around 32.8 and 40.0 s were
237 relatively large, and appear as individual peaks in the moment rate function (Figures 2b and 3b).
238 Phase B2 (44–52 s) mainly ruptured the region west of the epicenter. The rupture at around 44.8
239 s occurred along the 56°N FZ and that at around 49.6 s struck about 30 km south of the 56°N FZ
240 (Figure 3b). Phase B3 (53–60 s) occurred mainly northeast of the epicenter, but also struck the
241 intersection of the Aka FZ and the N-S aftershock lineation at around 52.8 s (Figure 3b). A
242 northward rupture from the Aka FZ was also detected at around 57.6 s. The last peak of the
243 moment rate function corresponds to two independent phases that occurred at around 63.2 s: B4
244 (62–65 s) ruptured about 20 km south of the Aka FZ and B5 (62–64 s) ruptured about 30 km
245 south of the epicenter (Figure 3b).

246 **5 Discussion**

247 Our inversion results indicate that the main rupture stage (0–27 s after origin) affected
248 segments oriented both N-S and E-W, suggesting that the 2018 Alaska earthquake ruptured a
249 conjugate fault system, as proposed in previous studies (Guo et al., 2020; Hossen et al., 2020;
250 Lay et al., 2018; Ruppert et al., 2018; Zhao et al., 2019). Our source model suggests that the
251 rupture occurred along weak zones in the sea floor: fracture zones extending E-W and plate-
252 bending faults parallel to N-S magnetic lineaments (Naugler & Wageman, 1973; Reece et al.,
253 2013). The N-S plate bending faults have been interpreted as pre-existing oceanic spreading
254 features that were reactivated by subduction of the Pacific Plate (Reece et al., 2013).
255 Krabbenhoft et al. (2018) associated these pre-existing features with the radiation of high-
256 frequency waves based on back-projection and the aftershock distribution.

257 A notable irregular rupture propagation highlighted by our inversion results is the
258 northward rupture at around 9 s in phase A1 and the southward rupture at around 12 s in phase
259 A2, both of which stopped near the 56°N FZ (8 and 12 s, respectively, in Figure 3a). The N-S
260 aftershock lineation is divided into northern and southern clusters across the 56°N FZ (Figure 3a).
261 Given the phase A1 and A2 ruptures and the geometrical offset of the N-S aftershock lineation,
262 the northern and southern fault system crossing the 56°N FZ can be regarded as a strike-slip step
263 over. Based on our obtained focal mechanisms, these two N-S faults are both right-lateral strike-
264 slip faults that dip steeply to the west (8 and 12 s in Figure 3a), and the counterclockwise rotation
265 of the strike angle during phase A1 is consistent with the southern N-S aftershock lineation (6 s
266 in Figure 3a). Because irregular rupture behaviors are generally a result of geometric
267 complexities, including barriers caused by discontinuous fault steps (e.g., Aki, 1979; Das & Aki,
268 1977; Harris & Day, 1993), we interpret that this fault step over caused the rupture to stagnate at
269 around 9 and 12 s.

270 Multiple sub-events occurring in a conjugate strike-slip fault system have been reported
271 in previous studies (Fukuyama et al., 2015; Goldberg et al., 2020; Hudnut et al., 1989; Meng et
272 al., 2012; Ross et al., 2019). In this study, we have shown a causal link between the multiple
273 rupture episodes during the 2018 Alaska earthquake (stages A and B) and pre-existing
274 bathymetric features by resolving both the rupture evolution and variation of fault geometry
275 using only teleseismic body waves. Similar observations were made during the M_w 8.6 2012
276 Sumatra earthquake in the Wharton basin. That earthquake involved multiple $M_w > 8$ sub-events
277 along a conjugate fault system (Meng et al., 2012; Duputel et al., 2012), which developed by
278 deep ductile shear localization beneath the brittle upper lithosphere of the oceanic plate (Liang et
279 al., 2020).

280 It is possible that the complex waveforms observed during the 2018 Alaska earthquake
281 were contaminated by reverberations due to the bathymetric setting that cannot be reproduced by
282 the theoretical Green's function, resulting in dummy multiple events (e.g., Fan & Shearer, 2018;
283 Wiens, 1987, 1989; Yue et al., 2017). We evaluated this possibility by using empirical Green's
284 functions (Dreger, 1994; Hartzell, 1978) and confirm that it is unlikely that the multiple rupture
285 stages originated from such reverberations (Text S3 and Figure S9).

286 The sub-events that occurred after the main A1 phase can be regarded as early
287 aftershocks missing from global catalogs (Fan & Shearer, 2016). Although it is difficult to
288 distinguish whether such early near- to intermediate-field aftershocks were dynamically or
289 statically triggered (Fan & Shearer, 2016), it is noteworthy that the rupture propagated from A1
290 to A2 at more than 5 km/s (Text S2 and Figure S6); this is faster than the surface wave velocity
291 (3–4 km/s), suggesting that the A2 rupture was triggered by the A1 rupture.

292 **6 Conclusions**

293 Based on the framework of Shimizu et al. (2020), we developed a finite-fault inversion
294 method for teleseismic *P* waveforms with improved smoothness constraints to obtain source
295 processes for earthquakes with complex multiple-fault ruptures. We applied our inversion
296 method to the 2018 Alaska earthquake and estimated its spatiotemporal rupture process.
297 Although the observed waveforms are very complicated, reflecting the complex rupture process
298 and fault geometry, the waveforms calculated from our source model fit well. The obtained
299 source model suggests a complex multiple-shock sequence on a conjugate fault system,
300 consistent with pre-existing bathymetric features. Irregular rupture stagnation about 20 km north
301 of the epicenter may have been promoted by a fault step across a sea-floor fracture zone.

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310 2007), ObsPy (1.1.0: <https://doi.org/10.5281/zenodo.165135>) (Beyreuther et al., 2010) and
311 Generic Mapping Tools (Wessel et al., 2013).

312 **Data Availability Statement**

313 Waveform data was downloaded through the IRIS Wilber 3 system
314 (https://ds.iris.edu/wilber3/find_stations/10607586). Teleseismic waveforms were obtained from
315 the following networks: the Canadian National Seismograph Network (CN;
316 <https://doi.org/10.7914/SN/CN>); the Caribbean USGS Network (CU;
317 <https://doi.org/10.7914/SN/CU>); the GEOSCOPE (G; <https://doi.org/10.18715/GEOSCOPE.G>);
318 the Hong Kong Seismograph Network (HK; <https://www.fdsn.org/networks/detail/HK/>); the
319 New China Digital Seismograph Network (IC; <https://doi.org/10.7914/SN/IC>); the IRIS/IDA
320 Seismic Network (II; <https://doi.org/10.7914/SN/II>); the International Miscellaneous Stations
321 (IM; <https://www.fdsn.org/networks/detail/IM/>); the Global Seismograph Network (IU;

322 <https://doi.org/10.7914/SN/IU>), and the Pacific21 (PS; <https://www.fdsn.org/networks/detail/PS/>).
 323 The moment tensor solutions are obtained from the GCMT catalog
 324 (<https://www.globalcmt.org/CMTsearch.html>). The CRUST 1.0 model is available at
 325 <https://igppweb.ucsd.edu/~gabi/crust1.html>. The fracture zone data is obtained from the Global
 326 Seafloor Fabric and Magnetic Lineation Data Base Project website
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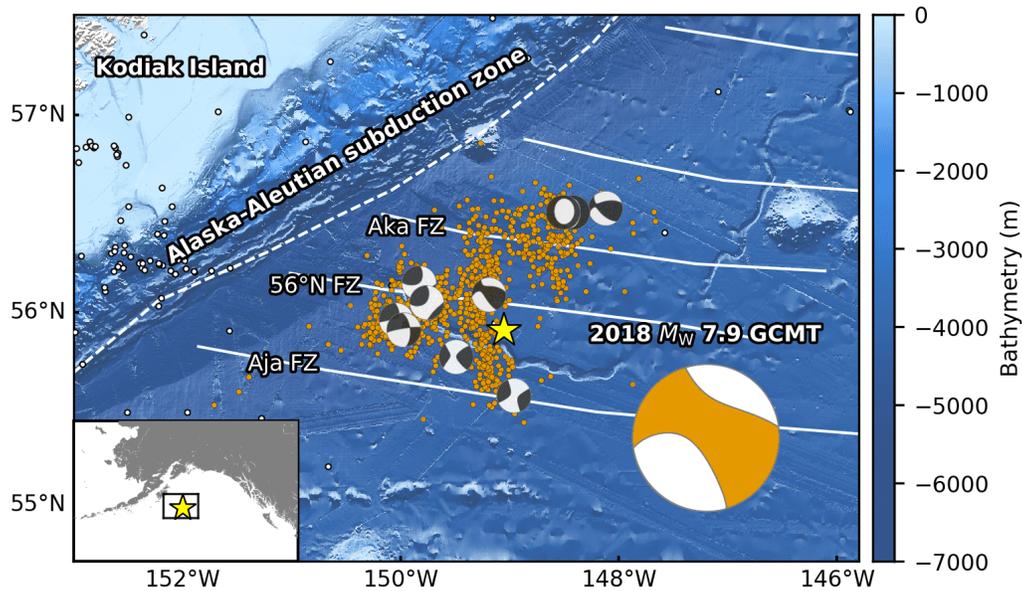
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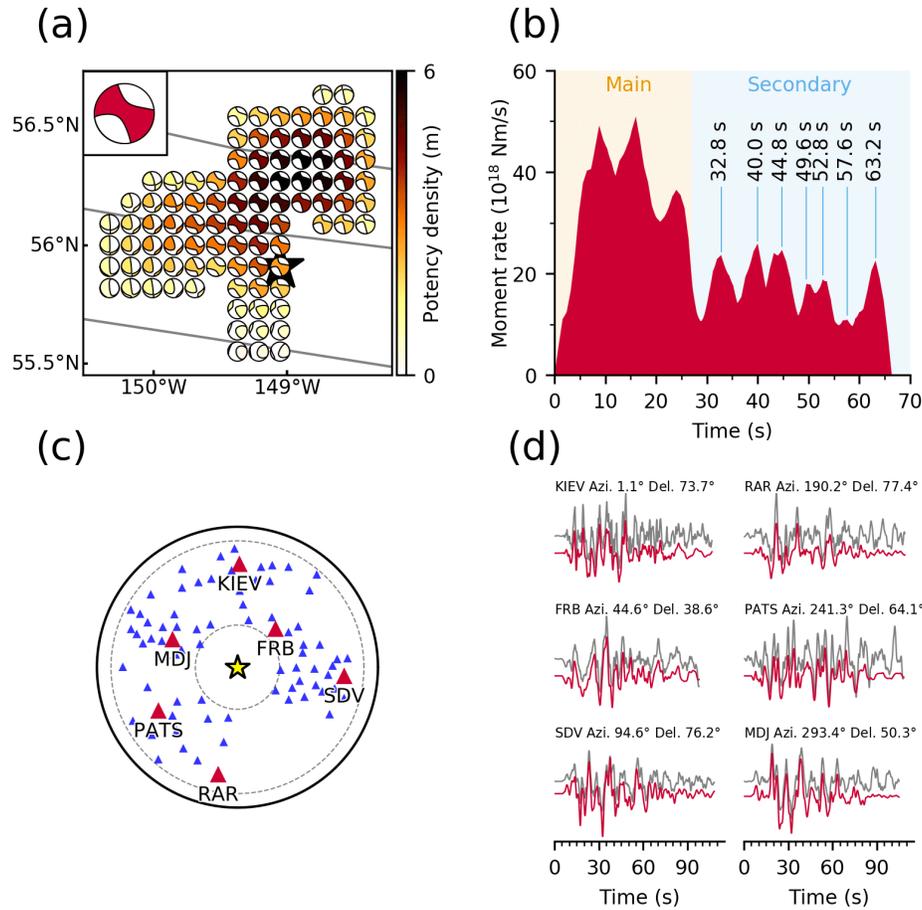
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476 **Figure 1.** Overview of the source region of the 2018 Gulf of Alaska earthquake. The star is the
 477 mainshock epicenter, orange dots are aftershocks ($M \geq 3$) that occurred within one week of the
 478 mainshock, and white dots show background seismicity before the mainshock ($M \geq 3.5$, 1
 479 January 2008 to 22 January 2018); all epicentral locations are from AEC. The ‘beachball’
 480 diagrams show the GCMT solutions for the mainshock (large, bottom right) and aftershocks with
 481 $M \geq 3.5$. White dashed lines represent plate boundaries (Bird, 2003), and white solid lines
 482 represent fracture zones (Matthews et al., 2011; Wessel et al., 2015). The background
 483 bathymetry is derived from the GEBCO 2020 Grid (GEBCO Compilation Group, 2020). The
 484 inset map shows the regional setting.

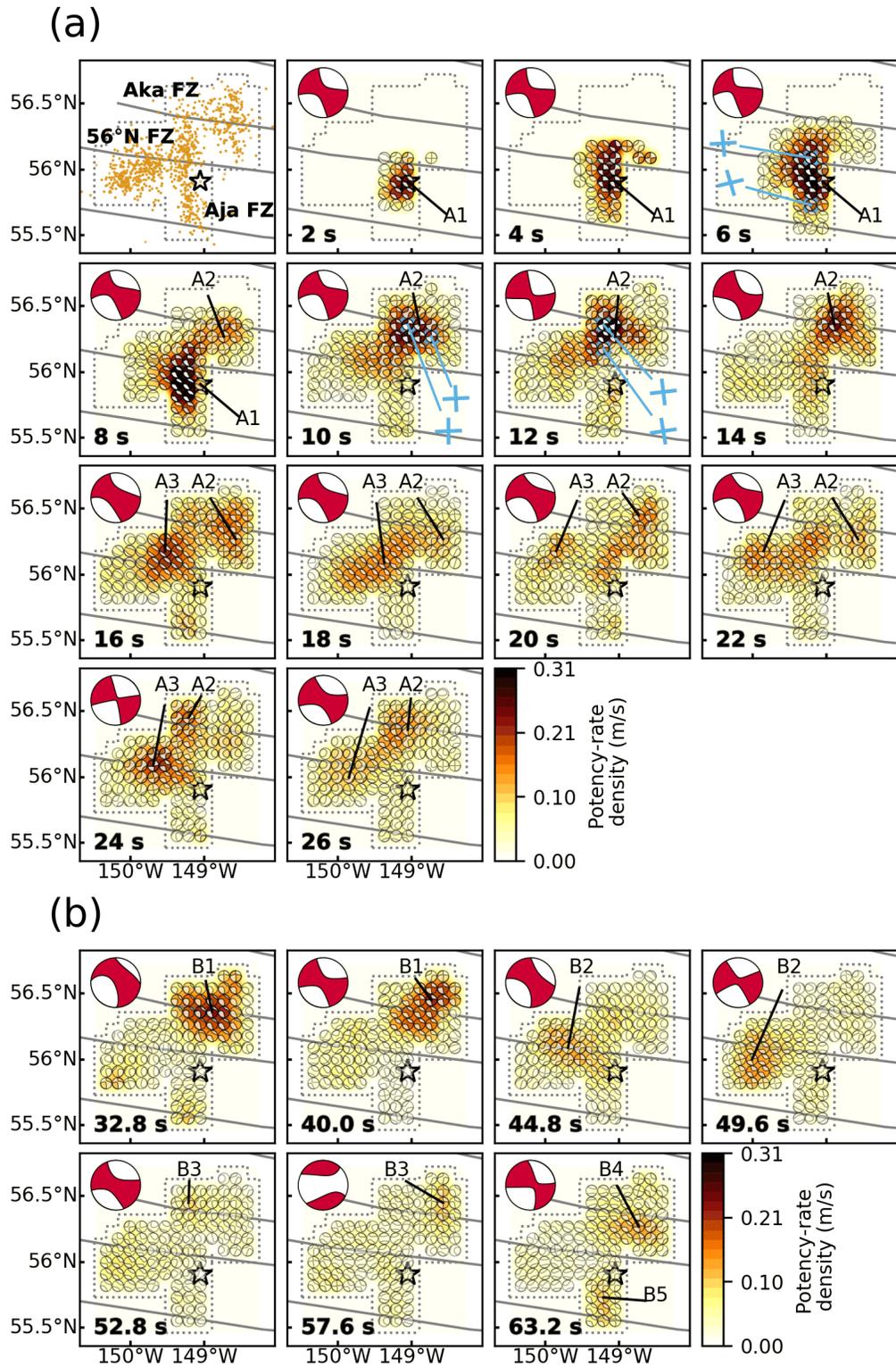
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487 **Figure 2.** Model setting and summary of results. (a) Map projection of the potency density
 488 tensor distribution on the assumed model fault plane. The star and solid lines indicate the
 489 epicenter (AEC) and fracture zones (Matthews et al., 2011; Wessel et al., 2015), respectively.
 490 Inset is the total moment tensor. (b) The moment rate function is divided into the main and
 491 secondary rupture stages at 27 s. The individual peaks during the secondary stage correspond to
 492 snapshots in Figure 3b. (c) Azimuthal equidistant projection of the station distribution used in the
 493 inversion. The star denotes the epicenter, and triangles denote station locations (waveforms for
 494 red stations are shown in (d)). The inner and outer dotted lines show epicentral distances of 30°
 495 and 90°, respectively. (d) Comparison of observed waveforms (gray) with synthetic waveforms
 496 (red) at the selected stations in (c). Each panel is labeled with the station name, azimuth (Azi.),
 497 and epicentral distance (Del.) from the mainshock. Waveform comparisons for all stations are
 498 shown in Figure S10.

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501 **Figure 3.** Snapshots of the potency-rate density tensors for (a) the main rupture stage A and (b)
 502 the secondary rupture stage B. The corresponding time after onset for each snapshot is noted at
 503 the bottom-left of each panel. The dotted line shows the border of the assumed model fault plane.

504 The star and solid lines indicate the epicenter (AEC) and fracture zones (Matthews et al., 2011;
505 Wessel et al., 2015), respectively. Blue crosses show the strike directions of small beachball
506 diagrams derived from the potency-rate density tensor. The top-left panel in (a) is the epicentral
507 distribution of aftershocks ($M \geq 3$) that occurred within one week of the mainshock (AEC). The
508 large beachball in each panel indicates the corresponding total moment tensor at each time.