

# Finite Fault Inversion of Mw4.1 and its Implications for Induced Earthquake Ruptures.

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## Key Points:

- A finite-fault slip model is obtained for a 2015  $M_w$  4.1 earthquake that occurred near Guthrie, Oklahoma.
- Both past seismicity and injection affect the observed heterogeneous slip pattern of the  $M_w$  4.1 earthquake.
- Faults in Oklahoma exhibit more heterogeneous slip compared to similar sized earthquake in plate boundary regions.

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**Abstract**

To better quantify how injection, prior seismicity and fault properties control rupture growth and propagation of induced earthquakes, we perform finite-fault slip inversion on a  $M_w$  4.1 earthquake that occurred in April 2015, which is the largest earthquake of an induced sequence near Guthrie, Oklahoma. The slip inversion reveals a complex rupture with multiple slip patches that are anti-correlated to the cumulative slip distributions of prior seismicity. This indicates that the  $M_w$  4.1 earthquake likely ruptured relatively strong asperities, while earlier seismicity driven by pore pressure occurred in weaker area. Compared to similar magnitude events in swarms from other regions, intraplate earthquakes in Oklahoma have higher number of well separated slip patches, indicating a difference in fault characteristics between regions. These observations suggest that both pore pressure perturbations, earthquake interactions, and fault characteristics control rupture propagation in moderate size earthquakes in Oklahoma, with the latter likely the dominant factor.

**Plain Language Summary**

Earthquake rupture initiates at a single point and can grow into a very large event, and the events final size is strongly affected by the heterogeneity within the fault system. Understanding how the rupture growth of induced intraplate earthquakes differs from interplate ones is important to the proper estimation of hazard. To better understand the factors that control the rupture and eventual size of earthquakes in Oklahoma we examine the rupture process of a  $M_w$  4.1 earthquake from an earthquake sequence near Guthrie, Oklahoma. Using seismic data, we calculate the slip pattern for the event and find that a majority of slip occurs on four distinct slip patches, that are outlined by past seismicity triggered by pore pressure changes from nearby injection wells. The slip patches that failed in this rupture likely represent the strongest locked portion of the fault that were pushed to a critical state through both pore pressure and past seismicity. When comparing the rupture processes of Oklahoma earthquakes to earthquakes of a similar size in other regions those in Oklahoma have a larger number of small slip patches. This suggests that fault zone properties in Oklahoma produce more heterogeneous distributions of asperities than in other regions.

## 1 Introduction

The central United States has experienced a significant increase in seismicity rates since 2009, which has been largely attributed to wastewater injection (Ellsworth, 2013; Keranen et al., 2014). It is well understood that the stress perturbations produced from wastewater injection reactivate pre-existing faults, which leads to an increase in earthquake occurrence. Fault structure, stress changes due to injection, and stress interactions between earthquakes play major roles in the spatiotemporal evolution of individual sequences (M. Brown & Ge, 2018; Pennington & Chen, 2017; Qin et al., 2018; Sumy et al., 2014). What is not well understood is how these factors affect the nucleation and rupture growth of future earthquakes within individual induced earthquake sequences. Investigation of their roles in controlling the propagation of future ruptures in a sequence is needed to not just better understand the underlying physics that govern rupture growth, but also the proper assessment of seismic hazard.

Previous investigations of coseismic slip for induced earthquakes have observed both spatial and temporal phases in slip growth. The 2011 Prague earthquake contained multiple slip patches (Sun & Hartzell, 2014), and rupture models of the 2016 Pawnee earthquake showed multiple peaks of slip and moment release (Grandin et al., 2017; Moschetti et al., 2019). Previous studies have shown that the nucleation of these events was affected by prior seismicity and injection, so these two factors could play a role in these events rupture processes (Sumy et al., 2014; Pennington & Chen, 2017; Chen et al., 2017; Norbeck & Horne, 2016). Due to lack of significant prior seismicity on the fault plane for both of these events, it makes it difficult to assess the relationship between prior seismicity and coseismic slip. Moreover, an examination by Moschetti et al. (2019) of the Pawnee earthquake did not find agreement between modeled pore pressure change along the fault and the location of its slip patches. On the other hand, the non-induced intraplate 2011  $M_w$  5.8 Mineral Virginia earthquake also has multiple slip patches (Hartzell et al., 2013). This indicates that the fault properties of these long dormant faults might also play an important role controlling coseismic slip patterns.

To better quantify how pore pressure and earthquake interactions effect earthquake rupture propagation, we examine the largest earthquake ( $M_w$  4.1) of the Guthrie sequence that occurred about ten months following fault activation. The sequence shows overall temporal correlation with the injection rate of nearby wells, showing that it is largely

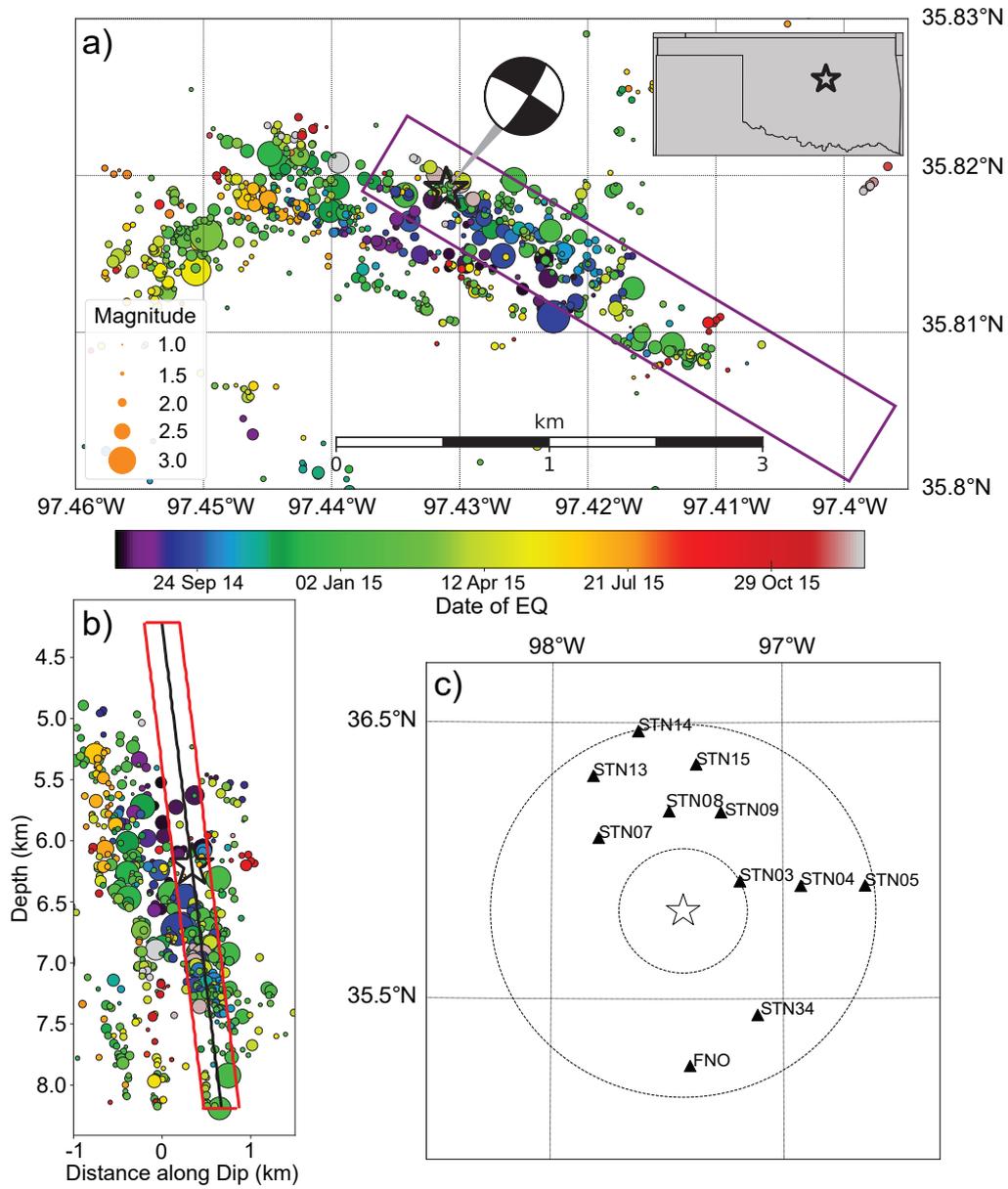
76 driven by injection (Chen et al., 2018; Haffener et al., 2018). The subevent modeling by  
77 Wu et al. (2019) of the  $M_w$  4.1 indicates a complex failure that contains 5 subevents,  
78 which indicates a complex triggering and rupture process. In this study, we model the  
79 spatial and temporal evolution of the  $M_w$  4.1 earthquake rupture and its relationship  
80 with prior seismicity to better understand the nucleation and triggering of large events  
81 during induced earthquake sequences. We quantify the distribution of asperities based  
82 on spatial gridding analysis and compare with other M4-5 earthquakes in both induced  
83 intraplate and interplate earthquake sequences, to better constrain the control factors  
84 of earthquake rupture complexity from different tectonic environments.

## 85 **2 Data:**

86 The sequence is comprised of 936 events which were analyzed in detail and relo-  
87 cated by (Chen et al., 2018; Chen & Abercrombie, 2020). The sequence started in early  
88 2014 and intensifies in July 2014 following an injection rate increase from nearby disposal  
89 wells, and gradually decreases in activity following the shut-in of nearby wells in May  
90 2015. A majority of the sequence occurred on two parallel 4 km long SE trending faults,  
91 which is bisected by an orthogonal fault trending to the NE (Benz et al., 2015; Chen et  
92 al., 2018) (Figure 1a). The  $M_w$  4.1 occurred on April 8, 2015 at 16:51:13 (UTC) along  
93 the main fault trending to SE, 10 months after seismicity began on that fault.

94 Due to the small magnitude of the target event, empirical Green’s function (EGF)  
95 method is used to retrieve source properties (Hartzell, 1978). The EGF event chosen is  
96 a nearly co-located M3.1 earthquake that occurred on September 15, 2014 at 00:10:38  
97 (UTC), which has similar focal mechanism with the target event and was previously used  
98 in the time-domain deconvolution of Wu et al. (2019). We download waveform data from  
99 Incorporated Research Institutes of Seismology (IRIS) data management center for 23  
100 stations within 75 km of the target event and manually pick both P and S phases. Data  
101 utilized in the inversion are required to have:  $>2s$  S-P travel time, an impulsive first mo-  
102 tion,  $\geq 100$  Hz sampling rate, and a signal to noise ratio  $\geq 10$ . 11 out of the original 23  
103 stations pass these criteria and are utilized in the inversion (Figure 1c).

104 Only the P-wave is used for the finite slip inversion analysis of the target earth-  
105 quake. This is based on the results from Wu et al. (2019) that the small initial sub-event  
106 is masked in the S-wave arrival by the P-wave’s coda. The waveforms for the target and



**Figure 1.** a) Map view of the Guthrie earthquake sequence with earthquakes colored by date and scaled by magnitude. The  $M_w$  4.1 (black star) and model fault (purple box) are also shown. (b) Perpendicular cross section across modeled model fault. Model fault is shown as black line, red box denote distance of 200m from model fault. Earthquakes that fall within these red bars are plotted on modeled slip in Figure 3. (c) Map view of stations (black triangles) used in the inversion, circles mark 25 km and 75km distance interval from event epicenter location (black star)

107 the EGF earthquakes are integrated to displacement, band-pass-filtered between 1 and  
 108 10 Hz, resampled to 100 Hz, and normalized by the maximum absolute value of the tar-  
 109 get earthquake for each component. The data was cut 0.5 seconds before the P arrival  
 110 and 2.5 seconds after, with the exception of STN03 which was closer in distance to the  
 111 target event and was cut to 2.2 seconds. The channels utilized in the inversion process  
 112 are the vertical component and the horizontal channel with highest amplitude. Due to  
 113 the horizontal channels having lower signal to noise, they are given half of the weight of  
 114 the vertical components in the inversion.

### 115 **3 Method:**

116 To constrain the slip of the  $M_w$  4.1 earthquake, we apply a linear slip inversion method  
 117 (Hartzell & Heaton, 1986; Uchide & Ide, 2007) based on empirical Green's Function (EGF)  
 118 (Hartzell, 1978). The workflow from Uchide and Song (2018) is followed to perform the  
 119 inversion:

- 120 1. The creation of the fault model over which the spatio-temporal slip distribution  
 121 will be calculated. We estimate the fault orientation using the target earthquakes  
 122 focal mechanism and the distribution of aftershocks and find a strike, dip and rake  
 123 of  $301^\circ$ ,  $81^\circ$ , and  $-10^\circ$  respectively, which agrees the directivity estimate of  $126.3^\circ$   
 124 (Wu et al., 2019). We base the extent of the fault model on the locations of the  
 125 sub-events found in the modeling by Wu et al. (2019), and refine it through trial  
 126 and error. The final fault model is 4 km long (along strike) and 4 km wide (along  
 127 dip), and the earthquake hypocenter is located 0.5 km along strike and 2 km along  
 128 dip (Figure 2a).
- 129 2. A linear cubic B-spline function is chosen as the basis function to describe the spa-  
 130 tiotemporal slip-distribution. The basis function has spatial nodes along the fault  
 131 at intervals of 0.25 km and at 0.1 s intervals in time. The expansion coefficients  
 132 controlling the amplitude of the basis function are the unknown parameters and  
 133 will estimated during the inversion. To reduce the number of parameters that are  
 134 being solved for, the start time of the first temporal basis function at each grid  
 135 point is set to a time when the rupture reaches that point and is restricted to 0.5  
 136 s in length. This assumes a causality between the rupture front and onset of slip  
 137 and introduces the unknown parameter of hypothetical rupture velocity  $V_{hr}$ .

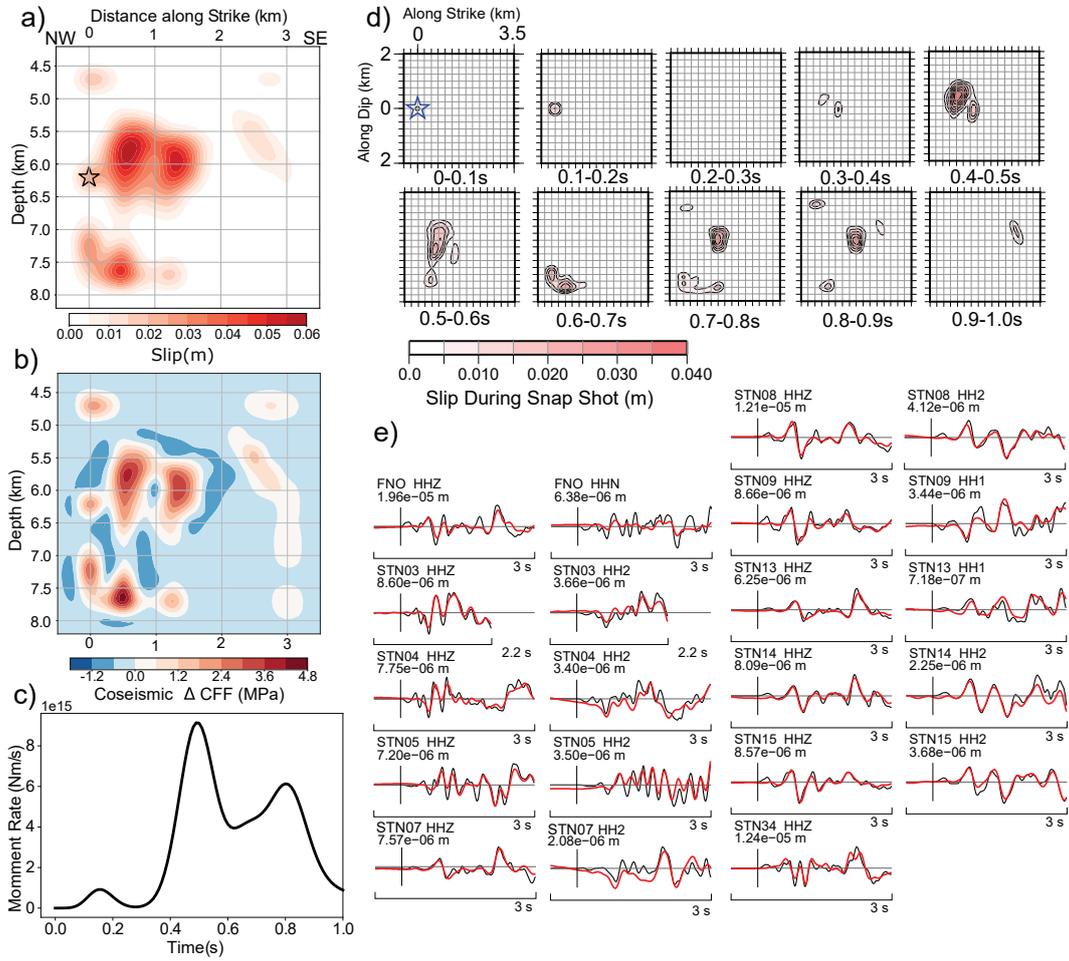
- 138 3. The determination of a hypothetical rupture velocity  $V_{hr}$ . The  $V_{hr}$  controls when  
 139 the rupture arrives at a grid point and therefore should be faster than the true  
 140 rupture velocity. In order to determine the optimal  $V_{hr}$  we perform the inversion  
 141 with multiple velocities from 1.6 km/s to 4.4 km/s at an interval of 0.2 km/s. The  
 142 model performance is measured by the variance reduction observed between the  
 143 synthetic and observed waveforms defined as  $1 - \frac{Var(d_{obs} - d_{syn})}{Var(d_{obs})}$ , where  $Var$  is vari-  
 144 ance and  $d_{syn}$  and  $d_{obs}$  are the synthetic observed waveforms.
- 145 4. In the final step we solve for the unknown expansion coefficients controlling the  
 146 amplitude of the basis function using a non-negative least squares algorithm (Lawson  
 147 & Hanson, 1987). In order to reduce the difference between the coefficients of spatio-  
 148 temporally neighboring basis functions and aid in the convergence toward a so-  
 149 lution, we introduce a temporal smoothing constraint. This assumes that the rup-  
 150 ture process progresses in a relatively smooth manner. We consider the intensity  
 151 of this constraint as a hyperparameter in Bayesian modeling and find through the  
 152 minimization of Akaike's Bayesian information criterion (Akaike, 1980; Ide, 2001;  
 153 Uchide & Ide, 2007; Uchide & Song, 2018; Yabuki & Matsu'ura, 1992).

## 154 4 Results:

155 Figure 2 depicts the results for the  $M_w$  4.1 earthquake. The estimated model pro-  
 156 duces good agreement between observed and synthetic waveforms with a variance reduc-  
 157 tion of 73.9%. This result was obtained using a  $V_{hr}$  of 3.2 km/s, which is the velocity  
 158 where improvement in variance reduction is  $< 0.01$ . This value agrees falls within the  
 159 range of 3.0 km/s and 3.5 km/s found in other studies using the same method (Uchide  
 160 & Song, 2018), but is higher than the 1.6 - 1.8 km/s found for this event by Wu et al.  
 161 (2019).

162 The resolved moment is  $3.25 \times 10^{15}$  Nm, which is equivalent to a  $M_w$  4.3. The seis-  
 163 mic moment and amount of fault slip are estimated as relative values to the EGF event's  
 164 moment and would decrease if it had a lower magnitude. To test the robustness of the  
 165 moment, alternative M2.1 EGF was tested, which produced a similar seismic moment  
 166 and slip distribution but had lower variance reduction.

167 The source time function shown in Figure 2c has a total duration of 1.1 seconds  
 168 and 3 distinct moment rate pulses. Figure 2d shows detailed spatiotemporal evolution



**Figure 2.** Slip inversion analysis results for the mainshock. (a) distribution of the final slip. (b) Distribution of the stress change. (c). Moment rate function. (d) Snapshots of the distribution of the slip rate as specified time intervals. (e) Comparison of between the observed (black) and synthetic waveforms (red).

169 of the rupture process: (1) rupture initiated around the hypocenter with the first small  
 170 pulse; (2) after a gap of 0.1 s, the 2nd larger slip patch starts with 250 m SE of the first,  
 171 which gradually propagate along strike; (3) at about 0.5 s, rupture propagates to a 3rd  
 172 slip patch at deeper depth; (4) at about 0.7 s, a 4th slip patch adjacent to the 2nd patch  
 173 is activated. The along-strike locations of these slip patches closely align with the pre-  
 174 vious sub-event modeling done by Wu et al. (2019), with the exception of one of the slip  
 175 patches in our model occurring at a deeper depth.

176 Based on the estimated slip model, the stress drop distribution is calculated using  
 177 the code from Okada et al. (2000) (Figure 2b). Maximum stress drop of 4.6 MPa oc-  
 178 curred during the 3rd slip patch at deeper depth. The 1st, 2nd, and 4th slip patches ex-  
 179 perience peak stress drops of 1.8, 4.2, 3.2 MPa, respectively. The average stress drop  
 180 from grids with stress drop above 0.5 MPa is 1.6 MPa, which is lower than the values  
 181 of 3.4 to 3.9 MPa obtained by other studies (Wu et al., 2019; Chen & Abercrombie, 2020).  
 182 The slip model's stress drop values are highly dependent on the spatial resolution of the  
 183 grid, so the values of peak stress drop should be considered the lower bound of actual  
 184 values.

## 185 **5 Discussion:**

### 186 **5.1 The Role of Prior Seismicity and Injection on Rupture Propagation.**

187 It has been observed in other swarms that the slip of prior seismicity often outlines  
 188 the slip of future events (Ide, 2002). To investigate the relationship between cumulative  
 189 slip from prior seismicity and the largest event, we first estimate the rupture radius of  
 190 earlier earthquakes based on the equation:  $r = (0.32\beta)/f_c$  (Eshelby, 1957; Madariaga,  
 191 1976), where  $f_c$  is the corner frequency, and  $\beta$  is 3.35 km/s, which is the average S-wave  
 192 velocity between 1.5 and 8 km depth. This assumes a simple circular rupture, which may  
 193 differ from actual rupture area. Then, we calculate cumulative stress drop within the fault  
 194 zone for each location by adding stress drops from events with overlapping rupture ar-  
 195 eas. The corner frequency ( $f_c$ ) and stress drop ( $\Delta\sigma$ ) values for each event are obtained  
 196 from S-wave spectral analysis in Chen and Abercrombie (2020). The results of this anal-  
 197 ysis are plotted in Figure 3. The key observations include:

- 198 1. Slip from previous earthquakes primarily concentrates within the gap between the  
 199 deeper and shallower slip patches (Figure 3). The abundance of seismicity and stress

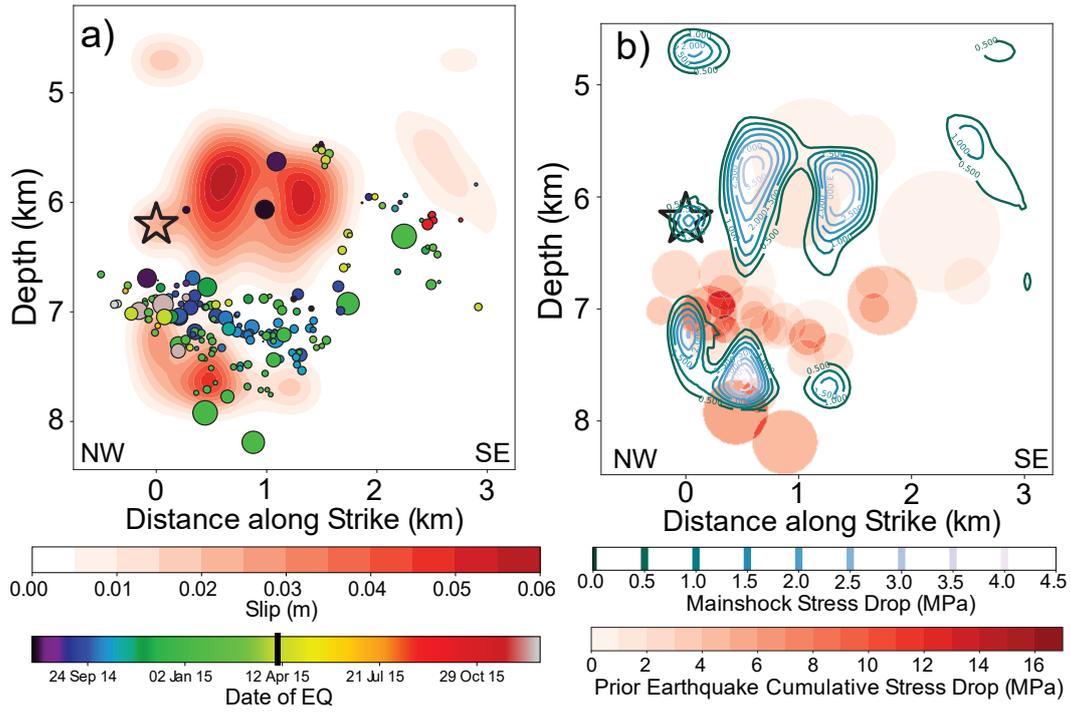
200 release in that region likely inhibited significant amount of slip during the largest  
201 event. The accumulated stress changes from these smaller events at deeper depth  
202 may have promoted activation of the 3rd slip patch during the largest event (M. Brown  
203 & Ge, 2018).

204 2. Those events that do overlap with the slip model are among the earliest earthquakes  
205 to occur and have relatively lower stress drop, coinciding with the low stress drop  
206 area between the 2nd and 4th slip patches during the largest earthquake (Figure  
207 3a). This is similar to findings for other swarms where stress drops are often lower  
208 for overlapping events that occur after previous earthquakes (Ide, 2002).

209 3. These observations suggest that slip from early events can influence the slip dis-  
210 tribution of a later larger event, suggesting importance of earthquakes themselves  
211 in sequence evolution and rupture propagation. The median relative location er-  
212 rors from Chen et al. (2018) is estimated to be 10m horizontally and 20m verti-  
213 cally with over 90% of events having location errors within 100m. Although the  
214 absolute locations can be systematically shifted, the relatively spatial patterns shown  
215 in Figure 3 should be robust.

216 Without detailed pore pressure change modeling along the fault's surface, which  
217 is beyond the scope of this paper, it is not possible to isolate the effects of pore pressure  
218 on slip distribution of an earthquake. Certain attributes of finite slip model can be linked  
219 to pore pressure changes based on past studies that performed modeling (Galis et al.,  
220 2017; Norbeck & Horne, 2016) and rupture directivity analysis (Lui & Huang, 2019; Folesky  
221 et al., 2016). These studies show that in general, rupture tends to propagate away from  
222 the area of injection when the absolute pore pressure perturbation is relatively low. When  
223 pore pressure perturbations are high, the rupture tends to propagate towards the injec-  
224 tion area, for example, the 2016  $M_w$  5.1 Fairview earthquake propagated towards high-  
225 rate injection zones (Lui & Huang, 2019).

226 Due to the relatively low injection volume from nearby disposal wells (within 5 km),  
227 the cumulative pore pressure within the Guthrie fault is only about 0.003 MPa, much  
228 lower than pressure modeling from other regions (Chen et al., 2018). Despite the rela-  
229 tively low-pressure amplitude, the diffusive migration of seismicity away from earliest  
230 seismicity suggest pressure diffusion within the fault zone (Figure 3a). Therefore, the first  
231 sub-event is likely initiated due to accumulated pore pressure. The rupture propagation



**Figure 3.** (a) Distribution of the final slip with mainshocks hypocenter (black star) and earthquakes within 200m of modeled fault shown. Earthquakes are scaled by magnitude and colored by date.(b) Stress drop distribution of modeled earthquake (blue contours). Cumulative stress drop along the model fault caused by previous seismicity (red shaded region).

232 away from possibly dominating disposal well is consistent with the mechanical model pro-  
233 posed in Galis et al. (2017).

## 234 5.2 Rupture Complexity

235 The well separated slip patches of the Guthrie  $M_w$ 4.1 earthquake resembles the fi-  
236 nite rupture model of the 2011 Prague and one of the models of 2016 Pawnee earthquake  
237 (Sun & Hartzell, 2014; Grandin et al., 2017). These events all exhibit complex cascad-  
238 ing ruptures where multiple separated slip patches combine to produce a large magni-  
239 tude earthquake (Ellsworth & Beroza, 1995). Rupture complexity for global large mag-  
240 nitude earthquakes shows spatial coherency and correlation with local geological struc-  
241 tures (Ye et al., 2018). While we observe the influence of prior seismicity on the slip dis-  
242 tributions of the Guthrie earthquake, this is not well observed for the Prague and Pawnee  
243 earthquakes. We hypothesize that the complex slip patterns of Oklahoma induced earth-  
244 quakes may likely be due to higher fault zone heterogeneity of intraplate faults with low  
245 tectonic loading rates .

246 To test this hypothesis, we compare the slip complexity observed in events in Ok-  
247 lahoma with other similar sized earthquakes from other tectonic environments, ideally  
248 strike-slip earthquakes that occur in swarm-like sequences. The events from tectonically  
249 active regions that we compare to are 7 earthquakes from 1998 Hida-Mountains Swarm  
250 sequence in Japan (Ide, 2001) and the two largest events that occurred in the 2012 Braw-  
251 ley swarm in Imperial Valley, California (Wei et al., 2013). These events are chosen be-  
252 cause they occur in swarm-like sequences that were driven by static stress changes and  
253 induced or natural pore pressure change (Aoyama, 2002; Wei et al., 2015). We obtain  
254 slip models for the 9 earthquakes, which have a magnitude range of 4.1 - 5.4 from the  
255 finite fault database SRCMOD (Mai & Thingbaijam, 2014). We compared these events  
256 to the Guthrie  $M_w$  4.1 and the Prague  $M_w$  5.6 (Sun & Hartzell, 2014) slip models, but  
257 not the Pawnee  $M_w$ 5.6 because it has multiple conflicting slip models (Grandin et al.,  
258 2017; Moschetti et al., 2019).

259 In order to quantify the number and the characteristics of the slip patches that oc-  
260 cur in each model, we follow a similar approach to Somerville et al. (1999). First, we trim  
261 the model to contain only the region where a majority of slip occurred by removing the  
262 edges of the finite fault model that have a mean slip less than half the entire model's mean

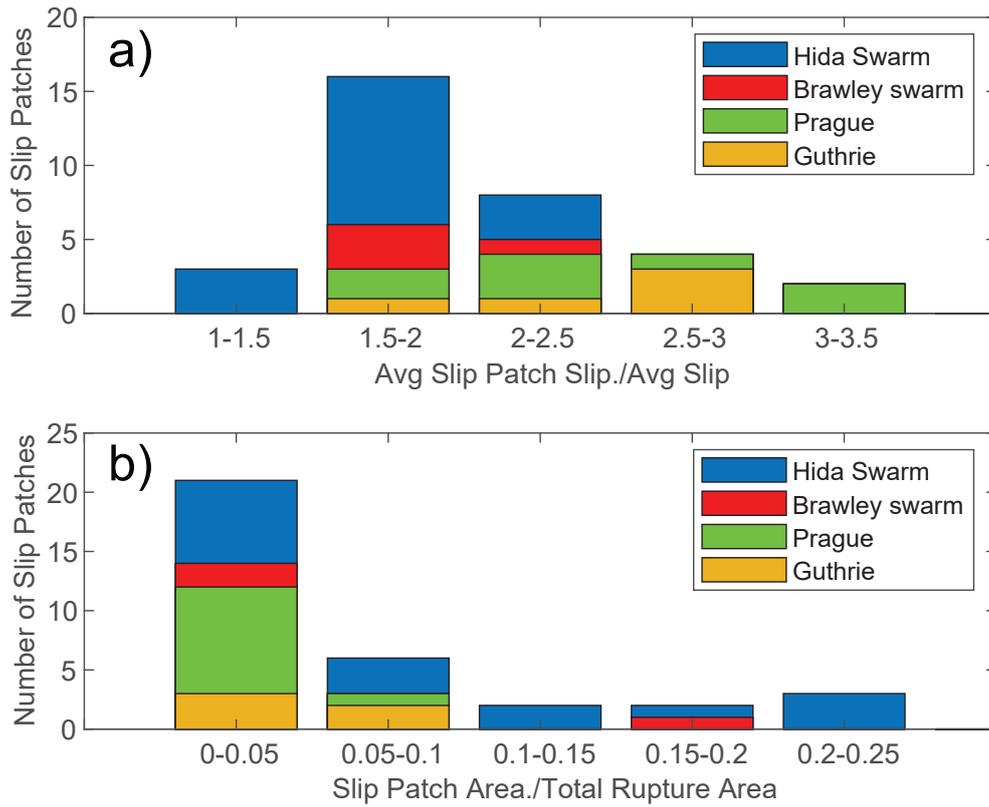
263 slip. Next, we isolate the grid points that have slip values greater than or equal to the  
264 80 percentiles of the slip distribution of the trimmed fault. We then group these grid points  
265 using the method of Haralick and Shapiro (1992) and a criterion of 4-way connectivity,  
266 which means that if grid points are connected either vertically or horizontally, they are  
267 grouped together. Of the final groups we remove those with fewer than 2 grid points.

268 The number of slip patches observed for each earthquake can be found in supple-  
269 mental Table S1 and their individual plots in supplemental Figure S1. In each region,  
270 the average number of slip patches observed per earthquake is roughly 7, 2, 2 for Ok-  
271 lahoma, Brawley Swarm and the Hida-Mountain Swarm, respectively. For each slip patch  
272 we calculate its area as a fraction of the total area of the trimmed model (normalized  
273 area), and its slip as a fraction of the average slip over the trimmed fault (normalized  
274 slip). In Oklahoma, the normalized area of the slip patches is significantly smaller than  
275 what is observed in Hida and Brawley (Figure 4b). The normalized slip of the slip patches  
276 is highest for Oklahoma (2 to 3), while relatively smaller for Brawley (1.5 to 2.5) and  
277 Hida (1 to 2) (Figure4a). This suggests that the slip for Hida and Brawley earthquakes  
278 is more diffuse and covers more of the rupture area. In contrast, Oklahoma earthquakes  
279 tend to have slip concentrated in small or isolated patches. These differences between  
280 induced intraplate earthquakes in Oklahoma and induced/natural earthquakes at plate  
281 boundaries suggest that the dormant faults in intraplate regions might exhibit different  
282 behavior from plate boundary regions, and ruptures in intraplate regions may be more  
283 complex than similar magnitude interplate events. We should note that the sample size  
284 is relatively small due to limited slip models for M4-5 strike-slip earthquakes and res-  
285 olution of the models differs between studies, the latter of which could limit the num-  
286 ber of isolated slip patches (L. Brown et al., 2015). Future studies of more systematic  
287 comparisons can further address this hypothesis.

## 288 **6 Conclusion:**

289 The finite slip inversion indicates that moderate sized earthquakes in Oklahoma  
290 have complex ruptures with multiple slip patches. Our analyses find the following:

- 291 • The Guthrie earthquake, high slip patches are surrounded by prior seismicity, in-  
292 dicating that the slip patches likely represent relatively stronger asperities.



**Figure 4.** Histogram of the normalized slip (a) and normalized area (b) for the asperities observed in each region. Note that Prague and Guthrie have higher concentrations of slip in within asperities (a) and they also have smaller asperities (b).

- 293 • Both of the two Oklahoma earthquakes analyzed here exhibit higher levels of slip  
 294 heterogeneity compared to other regions.
- 295 • The heterogeneity of slip observed in Oklahoma can be attributed to both fault  
 296 characteristics, prior seismicity, and to injection.

297 We find that both pore pressure perturbations, earthquake interactions, and fault char-  
 298 acteristics control rupture propagation in moderate size earthquakes in Oklahoma. In  
 299 order to properly understand the potential magnitude ranges we could expect from a fault  
 300 a full understanding of that fault's geometry and characteristics is required.

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 304 tained from the IRIS Data Management Center (<https://ds.iris.edu/ds/nodes/dmc/>).  
 305 The finite fault slip inversions of the Hida and Brawley earthquakes are downloaded from  
 306 the SRCMOD Earthquake Finite Fault Database (Mai & Thingbaijam, 2014). The Prague  
 307 earthquakes finite fault model was obtained directly from Sun and Hartzell (2014). The  
 308 datasets for relocated catalog and stress drop estimates are available from Chen et al.  
 309 (2018) and Chen and Abercrombie (2020).

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Figure1\_Mapview.

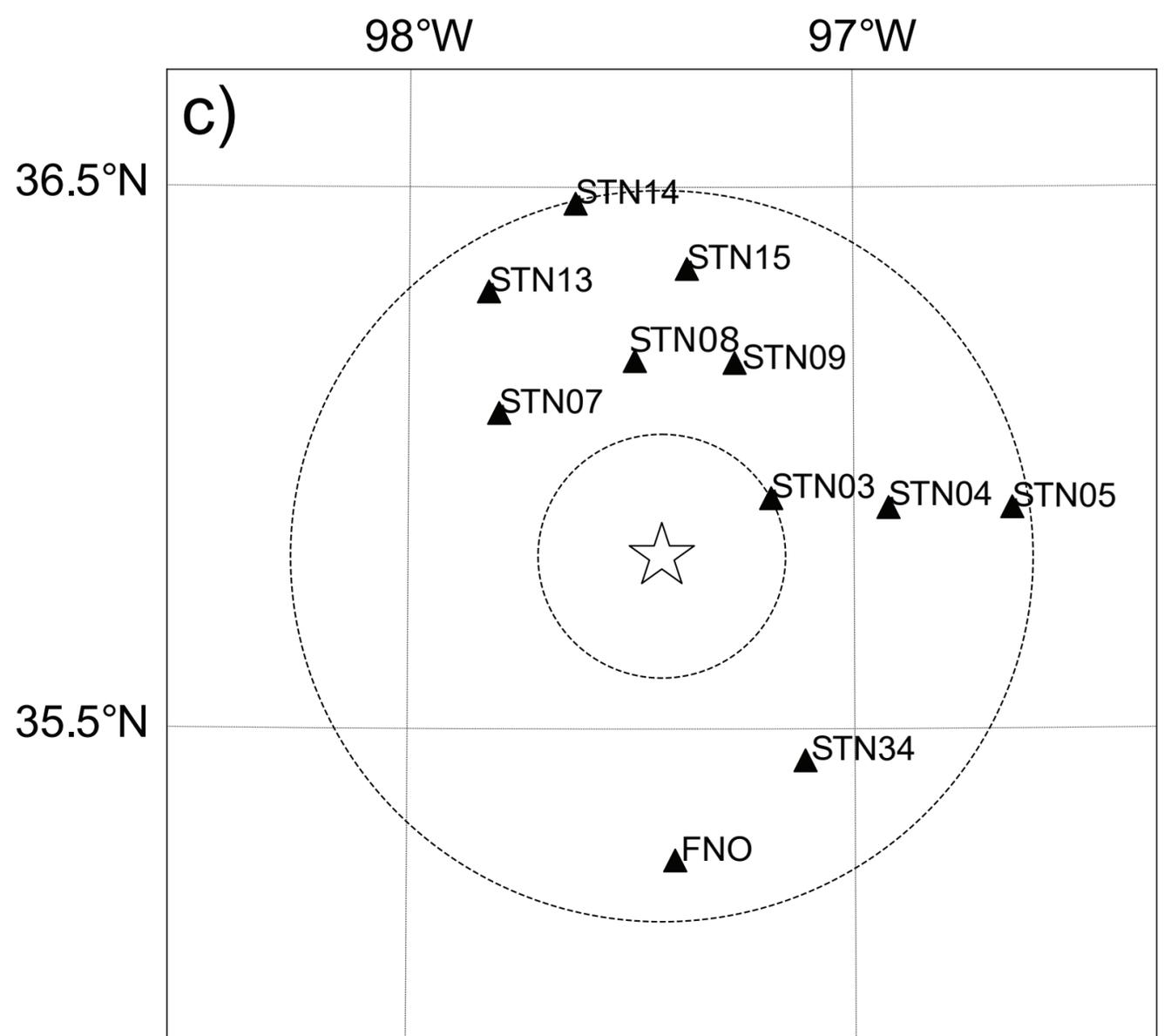
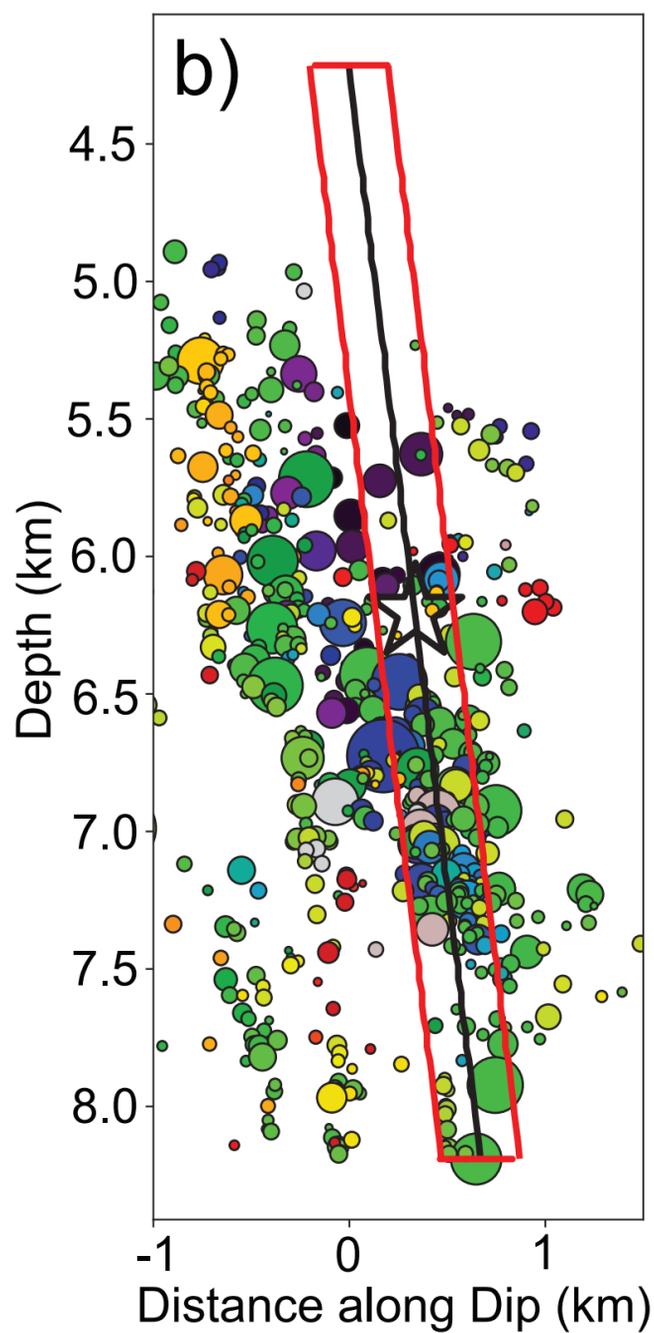
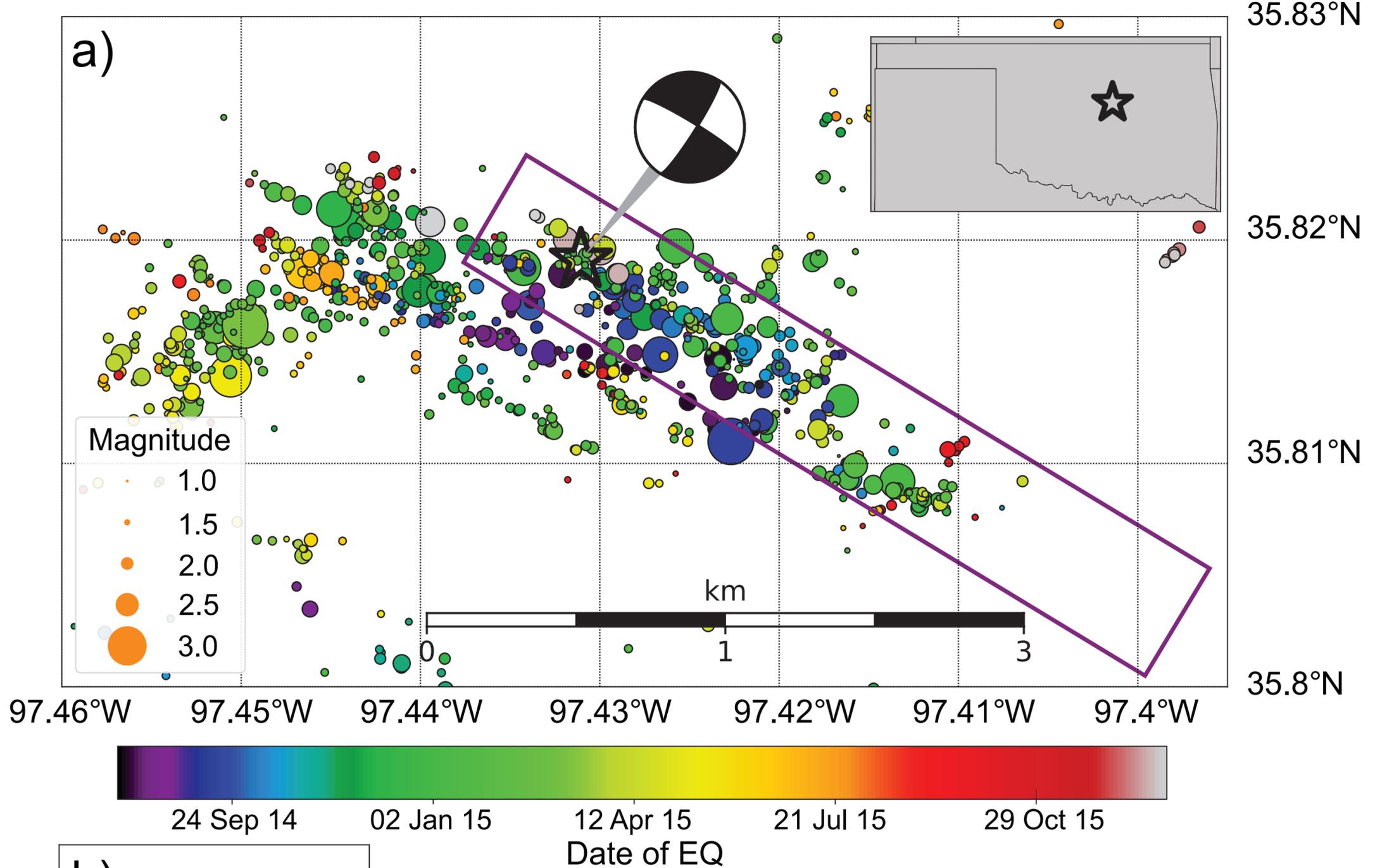


Figure2\_inversion.

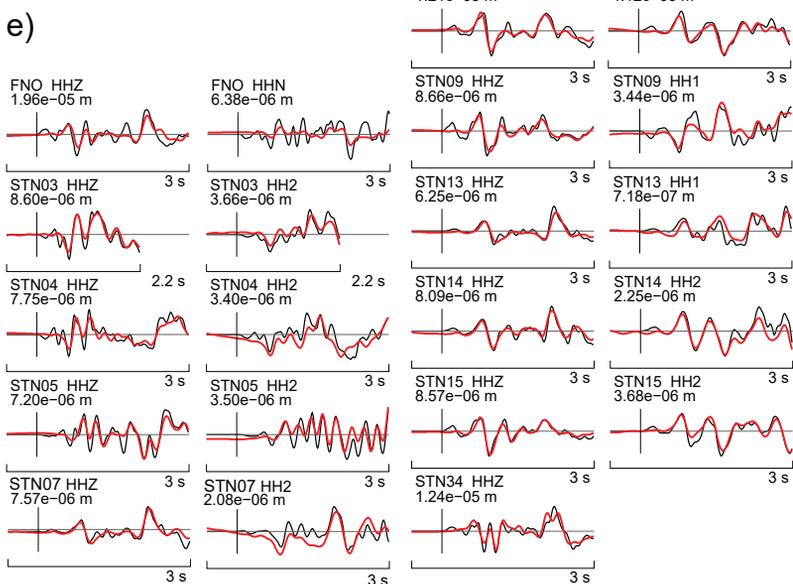
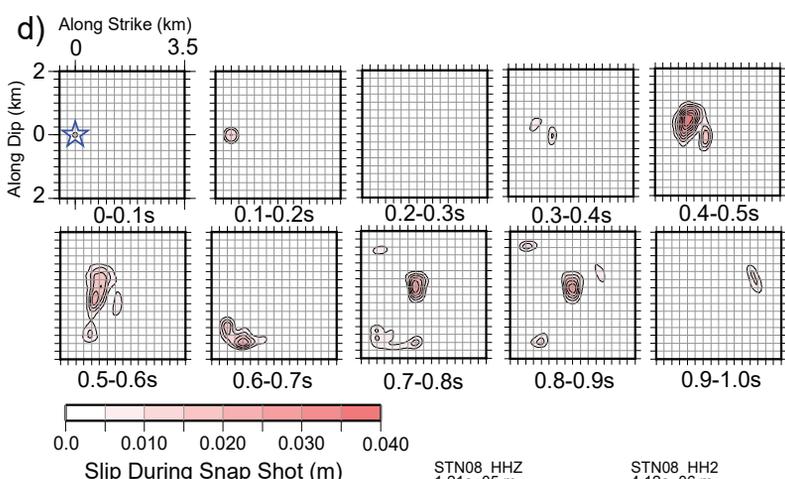
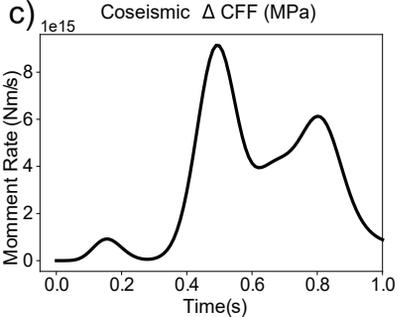
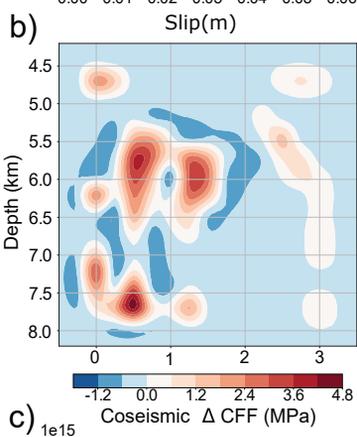
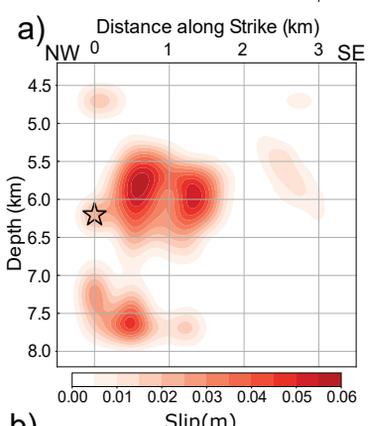


Figure3\_Prior\_slip.

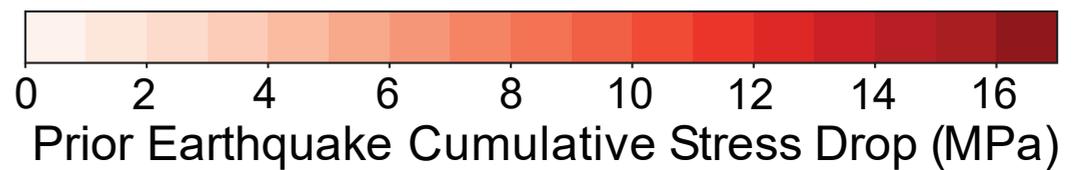
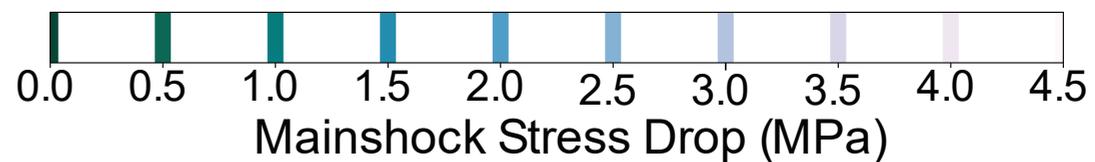
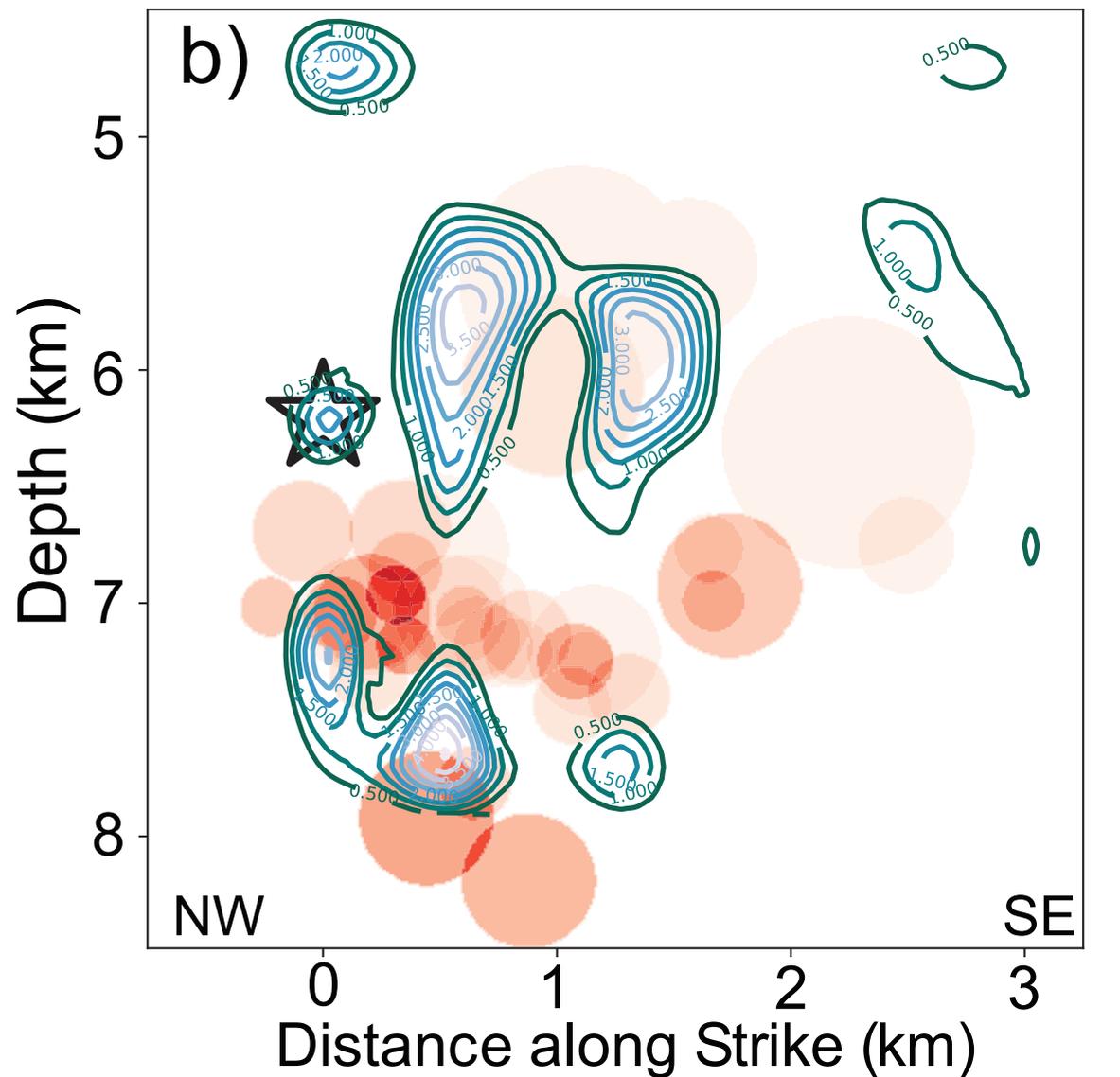
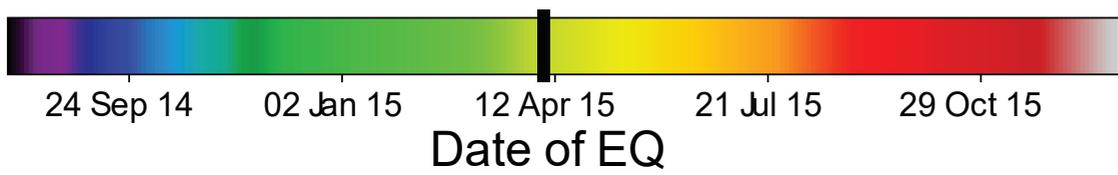
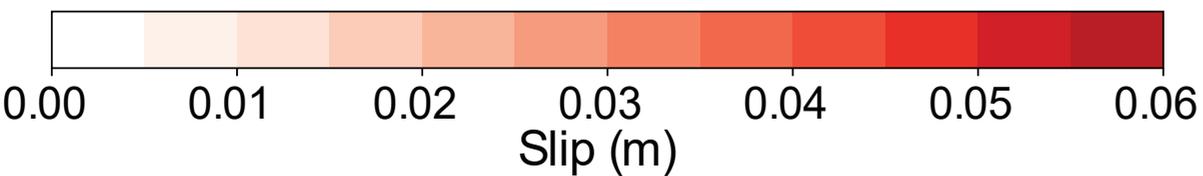
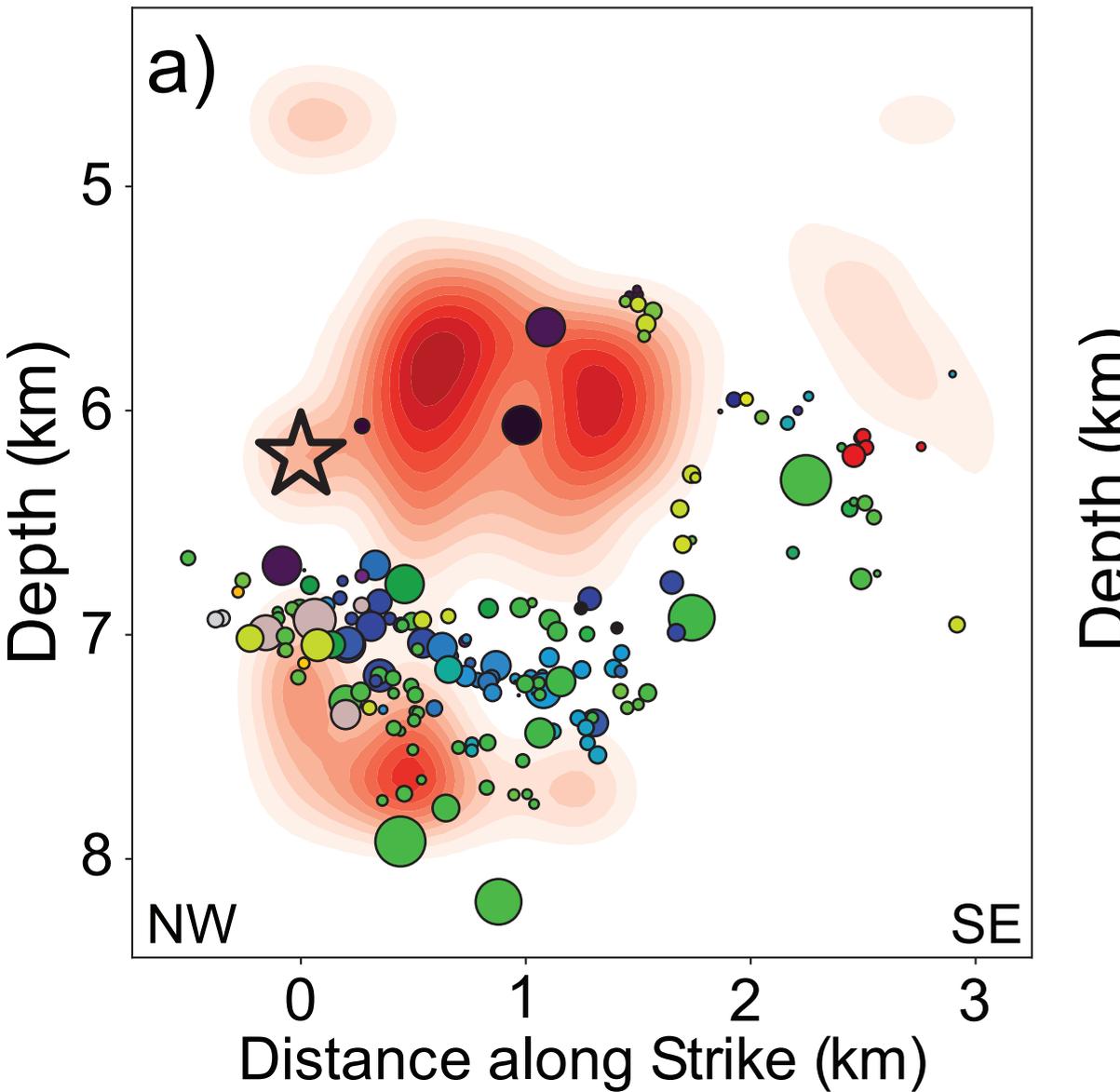


Figure4\_other\_regions.

