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24 Decoupling parameter based daily evapotranspiration fraction algorithm

26

27 **Abstract**

28 Evapotranspiration (ET) is the major component of the hydrology cycle. Satellites
 29 provide a convenient way for gathering information to estimate regional ET . The
 30 most widely applied method for converting the instantaneous satellite measurement to
 31 daily scale assumes that evaporative fraction (EF), defined as the ratio of ET to the
 32 available energy, is constant during the daytime. However, this method was proved to
 33 underestimate the daily ET . This study implemented a theoretically improved EF
 34 algorithm to calculate daily ET with the decoupling factor method based on the
 35 Penman-Monteith and McNaughton-Jarvis equations. Seven improved algorithms
 36 were developed by assuming that various parameters remain constant during the day.
 37 The satellite-based ET estimates were compared with seven local flux tower
 38 measurements in China. The results showed that: (1) The original ET method
 39 calculated the daily evaporation more accurately than the other algorithms. However,
 40 the good fit was based on two compensating inaccuracies. Compared to the flux tower
 41 measurement, the original ET method underestimated the daily EF by 26% and
 42 overestimated the daily net radiation by 30%. (2) Six of the seven proposed
 43 algorithms underpredicted the daily ET by 30-60%, mainly due to the inaccurate
 44 daily net radiation. (3) The algorithm that assumed that the instantaneous decoupling
 45 parameter Ω^i was equal to its daily value method calculated EF and ET with the
 46 relative errors of 8% and 10% when the inaccurate estimated daily net radiation was
 47 replaced by the observed flux tower data.

48 **Plain Language Summary**

49 The water that evaporates from the land surface sustains the hydrological cycle that
 50 replenishes the world's freshwater resources. Scientists and water managers are
 51 therefore interested in quantifying the water that evaporates each day. It is especially
 52 true for China that has one of the lowest water reserves in the world. Satellites that
 53 provide coverage of all the land surface would be ideal for recording evaporation if
 54 we could scale up the instantaneous satellite measurements to a daily scale. The

current scale-up methods available have not been widely tested. In this manuscript, we test the available methods and show how they can be improved for China.

1 Introduction

In the seventeenth century, the first water balance was made for the Seine by Perrault (1674). Since that time, it became apparent that evapotranspiration (*ET*) sustains the hydrologic cycle and replenishes the world's freshwater resources (Katul and Novick, 2009). Today, evaporation is a critical component of the short-term numerical weather predication, long-term climate simulations, and diagnoses of climate change (Brutsaert et al., 2019; Jung et al., 2019; Wang & Dickinson, 2012).

Products of actual evaporation are usually from ground measurements, climate (or hydrology) model output, or satellite-based estimates. Ground measurements like flux towers and lysimeters can make ground or point scale evaporation measurements. Pan evaporation can be used for point scale but needs to be adjusted for the soil moisture content using a model such as the Thornthwaite Mater Procedure (Portela et al., 2019; Steenhuis & van der Molen, 1982). The climate and hydrology models could provide large-scale and long-time *ET* estimates, but they often have coarse resolutions and assuming the land cover was fixed, leading to large uncertainties. Satellite measurements can calculate regional-scale evaporation at low-cost (Miranda et al., 2017), and unlike the climate models, they have higher resolution and more realistic land parameters. Moderate Resolution Imaging Spectroradiometer (MODIS) (Ait Hssaine et al., 2020; Faisol et al., 2020; Mu et al., 2007, 2011; Zhang et al., 2019), Advanced Very High-Resolution Radiometer (AVHRR) (Dile et al., 2020; Zhang et al., 2009, 2010) and Landsat (Allen Richard G. et al., 2007; Bastiaanssen, Menenti, et al., 1998; Bastiaanssen, Paul, et al., 2020) have tabulated over the past 20 years, and they provided pioneering satellite-based regional *ET* estimates models.

Evapotranspiration for large basins or countries by remote sensing methods is calculated by extrapolating instantaneous remotely sensed satellite measurements (usually taken around midday) over daily or more extended periods (Hou et al., 2019; Zou et al., 2018). Several published methods convert the instantaneous *ET*

measurements to the daily evaporation: constant evaporative fraction method (Brutsaert & Sugita, 1992), reference evaporative fraction method (Tang et al., 2017), constant ET -radiation ratio methods, including the ET -top-of-atmosphere irradiance (Cammalleri et al., 2014), ET -extraterrestrial solar irradiance (Ryu et al., 2012) and ET -insolation method (Knipper et al., 2020). These methods vary for the various climates, and land uses, in almost cases, require calibration when applied to a different region (Alfieri et al., 2017; Chen & Liu, 2020; Delogu et al., 2012).

The most widely used method to convert instantaneous satellite measurements to daily values is called the evaporation fraction (EF) method. The EF is defined as the ratio of ET to the available energy flux, Q which is the sum of ET and sensible heat flux (Brutsaert & Sugita, 1992; Shuttleworth, 1989; Sugita & Brutsaert, 1991). This method assumes that the EF remains constant during the day (Nichols & Cuenca, 1993) and thus the daily latent heat flux (e.g., evaporation) is calculated as the product of the daily mean available energy Q and EF (Chen & Liu, 2020; Hu et al., 2019).

Researchers have, however, shown the EF is not constant during the daytime (Gentine et al., 2007; Liu et al., 2020; Panwar et al., 2020; Sobrino et al., 2007). Using the instantaneous constant EF during the midday as its daily mean value will underestimate the daily ET by 5%-30% (Farah et al., 2004; Van Niel et al., 2011, 2012; Yang et al., 2013). The EF depends on several environmental factors including saturation deficit above the well-mixed layer (Lhomme & Elguero, 1999), the solar radiation intensity, friction velocity, water availability, relative humidity, cloudiness, and boundary layer entrainment (Gentine et al., 2011)

To avoid underestimating the daily ET with the EF method, Tang & Li (2017) introduced a new method to calculate the ET based on an extra Penman-Monteith's expanded form Priestley-Taylor equation. They expressed the EF as a function of ratios of daily and instantaneous measured values of the slope of the saturated vapor pressure, the psychrometric constant, and a decoupling factor representing the relative contribution of the radiative and aerodynamic terms to the overall ET . Tang & Li (2017) tested their method in the cropped and irrigated North China Plain using

113 instantaneous satellite measurements and ground-based daily observations. They
 114 found that the daily ET calculated by their method was more robust and accurate than
 115 the constant EF method.

116 Our objective is to improve daily evaporation accuracy from instantaneous
 117 satellite measurements by adapting Tang & Li (2017) method for land uses other than
 118 irrigated cropland. The improved method is tested by comparing the flux tower
 119 measurements in China with evapotranspiration and several intermediate variables
 120 calculated with datasets of the Moderate Resolution Imaging Spectroradiometer
 121 (MODIS) Land Product and China Meteorological Forcing. The intermediate tested
 122 variables are instantaneous and daily air temperature and net radiation, and the daily
 123 EF . The MODIS Land Product has a spatial resolution of 0.05 degree and the China
 124 Meteorological Forcing data has a resolution of 0.1 degrees.

125 2. Theory

126 2.1 Evaporative fraction

127 Satellites provide only instantaneous data at fixed intervals that can range from
 128 several times a day to once in several days. To extend the instantaneous data to daily
 129 values, Nishida et al. (2003) assumed that the instantaneously measured evaporation
 130 fraction, EF^i during the satellite overpass around noon time was equal to the daily
 131 evaporation fraction EF^d . The EF , that was originally introduced by Brutsaert &
 132 Sugita, (1992) for calculation of evaporation in Kansas with weather balloons, is
 133 defined for both instantaneous and daily measurements as the ratio of latent heat flux
 134 (ET) to available energy flux, Q ($W\ m^{-2}$):

$$135 \quad EF = \frac{ET}{Q} \quad (1)$$

136 where ET is the actual evapotranspiration ($W\ m^{-2}$); Q is the sum of the latent heat flux
 137 and sensible heat flux, also called the available energy ($W\ m^{-2}$). The
 138 evapotranspiration, ET , can be calculated as the sum of the transpiration from the
 139 vegetation and the evaporation from the bare soil surface when the energy transfer
 140 from the vegetation to the soil surface can be neglected (Nishida et al., 2003), i.e.,

$$ET = f_{veg} ET_{veg} + (1 - f_{veg}) ET_{soil} \quad (2)$$

where the subscript "veg" means full vegetation cover and subscript "soil" indicates the soil exposed to solar radiation (called bare soil); ET_{veg} is the transpiration from the full vegetation cover ($W m^{-2}$), ET_{soil} is the evaporation from the soil ($W m^{-2}$), f_{veg} is the portion of the area with the vegetation cover. The equation and the method for

calculating f_{veg} is given in Appendix A. The available energy Q ($W m^{-2}$) is expressed by Nishida et al. (2003) as:

$$Q = f_{veg} Q_{veg} + (1 - f_{veg}) Q_{soil} \quad (3)$$

where Q_{veg} is the available energy for the vegetation ($W m^{-2}$) and Q_{soil} is the available energy for bare soil ($W m^{-2}$). Equations 1-3 are valid over any period, including instantaneous and daily times.

The instantaneous evaporation fraction, EF^i may be found by combining Eqs. 1, 2, and 3 as:

$$EF^i = f_{veg} \frac{Q_{veg}^i}{Q^i} EF_{veg}^i + (1 - f_{veg}) \frac{Q_{soil}^i}{Q^i} EF_{soil}^i \quad (4)$$

where the superscript i stands for the instantaneous value of the parameter, EF_{veg}^i and

EF_{soil}^i are the instantaneous evaporation fractions for the vegetation and bare soil, respectively. Combining the complementary relationship as described by Bouchet (1963), Morton (1978), Brutsaert and Stricker (1979), and Nishida et al. (2003):

$$ET + PET = 2 ET_0 \quad (5)$$

PET is the potential ET ($W m^{-2}$), described by the Penman-Monteith potential ET equations, ET_0 is the ET when ET equals to the potential ET ($W m^{-2}$), described by

the Priestley-Taylor equation, the EF_{veg}^i can be expressed as a function of instantaneously measured parameters as:

$$EF_{veg}^i = \frac{\alpha \Delta^i}{\Delta^i + \gamma (1 + r_{cveg}^i / 2r_{aveg}^i)} \quad (6)$$

where α is the Priestley-Taylor parameter which was set to 1.26 (De Bruin, 1983); Δ^i is the slope of the saturated vapor pressure, which is a function of the temperature (Pa K⁻¹); γ is the psychrometric constant (Pa K⁻¹); r_{cveg}^i is the instantaneous surface resistance of the vegetation canopy (s m⁻¹); r_{aveg}^i is the instantaneous aerodynamics resistance of the vegetation canopy (s m⁻¹). Expressions for the surface and the aerodynamic resistances and slope of the saturated vapor pressure can be found in Appendices B and D.

Assuming that the evaporation fraction of bare soil is constant during the day, EF_{soil}^i was expressed by Nishida et al. (2003) as a function of the instantaneous soil temperature and the available energy based on the energy balance of the bare soil:

$$EF_{soil}^i = \frac{T_{soilmax}^i - T_{soil}^i}{T_{soilmax}^i - T_a^i} \frac{Q_{soil0}^i}{Q_{soil}^i} \quad (7)$$

where $T_{soilmax}^i$ is the instantaneous maximum possible temperature at the surface reached when the land surface is dry (K), T_{soil}^i is the instantaneous temperature of the bare soil (K), T_a^i is the instantaneous air temperature, Q_{soil0}^i is the instantaneous available energy when T_{soil}^i is equal to T_a^i (W m⁻²).

2.2 Daily evaporation fraction values based on decoupling parameter

Huang et al. (2017) observed that the Nishida (2003) instantaneous midday evaporative fraction, EF^i underestimated the daily EF^d . To correct for the underprediction, Tang & Li (2017) introduced a new expression based on the Penman-

184 Monteith equation and McNaughton-Jarvis equation to calculate the daily EF^d that is
 185 more generally known as the decoupling factor method:

$$186 \quad EF^d = EF^i \frac{\Delta^d}{\Delta^d + \gamma} \frac{\Delta^i + \gamma}{\Delta^i} \frac{\Omega^{\dot{i}}}{\Omega^{\dot{d}}} \frac{\Omega^d}{\Omega^i} \quad (8)$$

187 where superscript "d" means daily; the EF^i is the midday instantaneous evaporation
 188 fraction; Ω is decoupling factor that represents the relative contribution of radiative
 189 and the aerodynamic terms to the overall evapotranspiration (McNaughton & Jarvis,
 190 1983), $\Omega^{\dot{i}}$ is the value of the decoupling factor, Ω , for wet surfaces. According to
 191 Pereira (2004), Ω and $\Omega^{\dot{i}}$ can be expressed as:

$$192 \quad \Omega = \frac{1}{1 + \frac{\gamma}{\Delta + \gamma} \frac{r_c}{r_a}} \quad (9)$$

$$193 \quad \Omega^{\dot{i}} = \frac{1}{1 + \frac{\gamma}{\Delta + \gamma} \frac{r^{\dot{i}}}{r_a}} \quad (10)$$

$$194 \quad r^{\dot{i}} = \frac{(\Delta + \gamma) \rho C_p VPD}{\Delta \gamma (R_n - G)} \quad (11)$$

195 where r_c is the surface resistance (s m⁻¹); r_a is the aerodynamic resistance (s m⁻¹); $r^{\dot{i}}$
 196 is the critical surface resistance when the actual evapotranspiration equals the
 197 potential evaporation, (called equilibrium evapotranspiration, s m⁻¹); ρ is the air
 198 density (kg m⁻³); C_p is the specific heat of the air (J kg⁻¹ K⁻¹); VPD is the vapor
 199 pressure deficit of the air (Pa). The method to calculate the slope of the saturated
 200 vapor pressure Δ is specified in Eq. B1; the calculation of vapor deficit, VPD , from
 201 satellite data is described in Appendix B with Eqs B2- B5. The resistance factors are
 202 further detailed in Appendix D.

203 The decoupling method (Eq. 8) performed well for irrigated cropland (Tang et al.,
 204 2017; Tang & Li, 2017). In this study, we were interested in finding the evaporation of
 205 all landscapes. Thus, we need to adapt Eq. 8 for other land uses such as grassland and
 206 forest. To do this, the constant EF_{veg} in Eq. 6 and EF_{soil} in Eq. 7 are reformulated
 207 similarly to the decoupling method in Eq 8:

208

$$EF_{veg}^d = \frac{\alpha \Delta^i}{\Delta^i + \gamma \left(1 + \frac{r_{cveg}^i}{2r_{aveg}^i} \right)} \left(\frac{\Delta^d}{\Delta^d + \gamma} \frac{\Delta^i + \gamma}{\Delta^i} \frac{\Omega_{veg}^{i,i}}{\Omega_{veg}^{i,d}} \frac{\Omega_{veg}^d}{\Omega_{veg}^i} \right) \quad (12)$$

209

$$EF_{soil}^d = \frac{T_{soilmax}^i - T_{soil}^i}{T_{soilmax}^i - T_a^i} \frac{Q_{soil0}^i}{Q_{soil}^i} \left(\frac{\Delta^d}{\Delta^d + \gamma} \frac{\Delta^i + \gamma}{\Delta^i} \frac{\Omega_{soil}^{i,i}}{\Omega_{soil}^{i,d}} \frac{\Omega_{soil}^d}{\Omega_{soil}^i} \right) \quad (13)$$

210 Substituting EF_{veg}^d (Eq. 12) and EF_{soil}^d (Eq. 13) into Eq. 4:

211

$$EF^d = f_{veg} \frac{Q_{veg}^i}{Q^i} EF_{veg}^d + (1 - f_{veg}) \frac{Q_{soil}^i}{Q^i} EF_{soil}^d \quad (14)$$

212 According to Eq. 1, the daily evaporation ET^d is:

213

$$ET^d = EF^d Q^d \quad (15)$$

214 In practice, the instantaneous parameter value for calculating EF^d and ET^d in Eqs
 215 12-15 are often not very precise when derived from the available satellite
 216 measurements. We, therefore, introduced eight approximations to determine the daily
 217 averaged evaporation fraction EF^d and evaporation ET^d and then tested how well
 218 these approximations could reproduce independently measured EF and ET values
 219 with flux tower data (Table 1). The first method in Table 1, named ETd, computed the
 220 evaporation with all the daily and instantaneous parameters in Eq. 12 and 13. The
 221 subsequent methods in Table 1, named ET0-ET7, used various approximations to find
 222 daily parameters. The second approximation, ET0, in Table 1 is Nishida's method
 223 (2003, Eq 6). It assumed that the daily values were equal to the instantaneously
 224 measured values during satellite overpass. Other methods used various ways to
 225 approximate the daily values. They included the slope of saturated vapor pressure vs.
 226 air temperature, ET1, the surface resistance, aerodynamic resistance, decoupling
 227 parameter resistance ET2-ET4, and decoupling factors, ET5 - ET7 (Table 1).

228 **Table 1.** Equations for the complete methods using all instantaneous values. EFd, the
 229 Nishida (2003) method EF0, and seven approximations EF1-EF7 for calculating the
 230 daily values EF^d from the instantaneous evaporation fraction EF^i , based on Eqs 11-14
 231 The superscript d indicates a daily value and the superscript i the instantaneous value.

EF	Assumption	Equation	ET
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<i>EFd</i>	<i>No assumptions</i>	$EFd = EF^i \frac{\Delta^d}{\Delta^d + \gamma} \frac{\Delta^i + \gamma}{\Delta^i} \frac{\Omega^{i,i}}{\Omega^{i,d}} \frac{\Omega^d}{\Omega^i}$	<i>ETd</i>
<i>EF0</i>	$EF^i = EF^d$	$EF0 = EF^i$	<i>ET0</i>
<i>EF1</i>	$\Delta^i = \Delta^d$	$EF1 = EF^i \frac{\Omega^{i,i}}{\Omega^{i,d}} \frac{\Omega^d}{\Omega^i}$	<i>ET1</i>
<i>EF2</i>	$r_c^i = r_c^d$	$EF2 = EF^i \frac{\Delta^d}{\Delta^d + \gamma} \frac{\Delta^i + \gamma}{\Delta^i} \frac{\Omega^{i,i}}{\Omega^{i,d}} \frac{\Omega^d}{\Omega^i}$	<i>ET2</i>
<i>EF3</i>	$r_c^i = r_c^d$	$EF3 = EF^i \frac{\Delta^d}{\Delta^d + \gamma} \frac{\Delta^i + \gamma}{\Delta^i} \frac{\Omega^{i,i}}{\Omega^{i,d}} \frac{\Omega^d}{\Omega^i}$	<i>ET3</i>
<i>EF4</i>	$r^{i,i} = r^{i,d}$	$EF4 = EF^i \frac{\Delta^d}{\Delta^d + \gamma} \frac{\Delta^i + \gamma}{\Delta^i} \frac{\Omega^{i,i}}{\Omega^{i,d}} \frac{\Omega^d}{\Omega^i}$	<i>ET4</i>
<i>EF5</i>	$\Omega^i = \Omega^d$	$EF5 = EF^i \frac{\Delta^d}{\Delta^d + \gamma} \frac{\Delta^i + \gamma}{\Delta^i} \frac{\Omega^{i,i}}{\Omega^{i,d}}$	<i>ET5</i>
<i>EF6</i>	$\Omega^{i,i} = \Omega^{i,d}$	$EF6 = EF^i \frac{\Delta^d}{\Delta^d + \gamma} \frac{\Delta^i + \gamma}{\Delta^i} \frac{\Omega^d}{\Omega^i}$	<i>ET6</i>
<i>EF7</i>	$\frac{\Omega^{i,i}}{\Omega^{i,d}} \frac{\Omega^d}{\Omega^i} = 1$	$EF7 = EF^i \frac{\Delta^d}{\Delta^d + \gamma} \frac{\Delta^i + \gamma}{\Delta^i}$	<i>ET7</i>

3 Material, methods and data

This section presents the data and the methods used in calculating the satellite-based daily evaporation fraction, EF^d and the daily evaporation ET^d , using Eqs 11-14 with and without the simplifying approximations listed in Table 1. A description of the data available for seven flux towers in China closes this section (Table 2). Note that the MODIS satellite data are available for 250 m, 500 m, and 0.05 degree (approximately 5 km) grids. While the smallest grid size would likely be more representative of the grid tower measurements used for validation, we chose to use the larger size because we intended to develop a method for large areas such as China. Even with the computer capabilities, using the two smallest grids as input would result in excessive amounts of data and computer time. For that reason, we chose the 0.05-degree grid data as input.

3.1 Data used for calculating satellite-based daily EF and ET

The schematic to calculate the evaporation fraction, EF (Eq. 14), and the evaporation ET (Eq. 15) is shown in Figure 1. The input consists of the MODIS Land Product and China Meteorological Forcing datasets (Table 2).

248 The MODIS data for China were downloaded for 2001 to 2018 from the website
249 <https://modis.gsfc.nasa.gov/>. The input data consisted of the following instantaneously
250 measured data each day around noon (Figure 1, Table 2a): the surface reflectance
251 (MOD09CMG), surface temperature/emissivity (MOD11C1), albedo (MCD43C3),
252 16-day NDVI (MOD13C1), and yearly land cover classes compiled from MODIS
253 data by the International Geosphere-Biosphere Programme, IGBP (MCD12C1). In
254 addition, the China Meteorological Forcing solar radiation dataset was downloaded
255 from <http://data.tpdc.ac.cn/en/data/> (Table 2). The solar radiation had a resolution of
256 0.1 degree and a 3-hour time step and was described in detail in (He et al., 2020; Yang
257 et al., 2006, 2010) and Huang et al. (2017).

258

259 **Table 2a** Input data used in this study

Input data (2001-2018)				
Data source	Data name	Used parameter	Time step	Spatial resolution
MODIS Land Product http://data.tpdc.ac.cn/en/data/	MOD11C1	Land Surface Temperature	daily	0.05 degree
	MOD09CMG	Surface Reflectance	daily	0.05 degree
	MCD43C3	Albedo	daily	0.05 degree
	MOD13C1	NDVI	16-day	0.05 degree
	MCD12C1	Land cover	yearly	0.05 degree
China Meteorological Forcing	Srad	shortwave radiation	3-hourly	0.1degree
Dataset				
https://modis.gsfc.nasa.gov/data/				

260 **Table 2b** Data for verification

Flux tower	Lon. (°E)	Lat. (°N)	Altitude (m)	Land cover	Footprint (m)	Climate	Time period
Changbaishan	128.1	42.4	738	Forest	181 to 3070	Monsoon temperate continental climate	2003-2005
Qianyanzhou	115.06	26.74	102	Forest	120 to 1655	Subtropical monsoon climate	2003-2005
Dinghushan	112.53	23.17	240	Forest	129 to 1908	Monsoon humid climate	2003-2005
Yucheng	116.57	36.83	28	Cropland	16 to 190	Semi-humid monsoon climate	2003-2005
Haibei	101.32	37.62	3190	Grassland	19 to 195	Plateau continental climate	2003-2005
Neimeng	116.67	43.53	1200	Grassland	19 to 195	Temperate arid and semiarid continental climate	2004-2005
Dangxiong	91.07	30.5	4350	Grassland	27 to 163	Plateau monsoon climate	2004-2005
Wujiaqu	87.67	44.41	438	Grassland	400	Temperate arid and semiarid continental climate	2020.2.7- 2020.12.17

261 3.2 Procedures for calculating satellite-based daily EF and ET

262 Figure 1 shows how to obtain the variable values to calculate the EF using the
263 data described in section 3.1. The vegetation fraction, f_{veg} (Eq 13) was calculated with
264 Eq. A1 in Appendix A based on the Normalized Difference Vegetation Index, NDVI,
265 derived from the reflectance data in the MOD09CMG product (Eq. A2). When the
266 daily reflectance data was not available, the MOD13C1 (measuring NDVI with a 16-
267 day interval) was used as an auxiliary data source (Nishida et al., 2003). The actual
268 available energy for the bare soil surface, Q_{soil} (Eq 13), was calculated by the radiation
269 energy budget with the data of the MOD11C1 product using Eqs C1-C3 in Appendix
270 C (Figure 1). The available energy for the vegetation Q_{veg} (Eq 13), was obtained by
271 using the air temperature with Eq. C3 in Appendix C. The air temperature was

determined in Appendix F with the Nishida's Vegetation Index – temperature, VI-T_s diagram using the NDVI (MOD09CMG and MOD13C1), and the surface temperature tabulated in the MOD11C1 product with the diagram. The VI-T_s diagram was based on the assumption that dense vegetation has the minimum surface temperature and that dry, bare soil has the maximum temperature. Thus, there is a negative correlation between vegetation coverage and surface temperature. The calculation of the slope of the vegetation coverage, the surface temperature (also called the warm edge), and the intercept of them (also called the minimum surface temperature) is shown in Appendix F.

The instantaneous and daily equations were of the same form (Appendices D and E). The aerodynamic resistance of the bare soil, $r_{a\ soil}$ was determined with the equation D1 in appendix D originally proposed by Nishida (2003). The surface resistance of the bare soil, $r_{c\ soil}$ was found by subtracting the aerodynamic resistance of the bare soil from the total aerodynamic resistance (Eq. D2). The total aerodynamic resistance was computed with Eq. D3 (Griend and Owe, 1994 and Mu, 2007). The canopy surface resistance, $r_{c\ veg}$ was obtained with the method developed by Jarvis (1976, Eq. E1-E3 in Appendix E). The aerodynamic resistance of the forest cover was obtained with Eq. E4 and of both grassland and cropland with Eq. E5 (Kondo, 2000). The wind speed, which was input in Eqs E4 and E5, is given in Eq E6-E8. Then, the instantaneous and daily surface and aerodynamic resistance were computed with the equations provided in Appendices D and E using a combination of all available MODIS and Meteorological products as shown in Figure 1. Finally, these resistances were used to calculate the EF_{veg} in Eq. 5 and EF_{soil} in Eq. 6

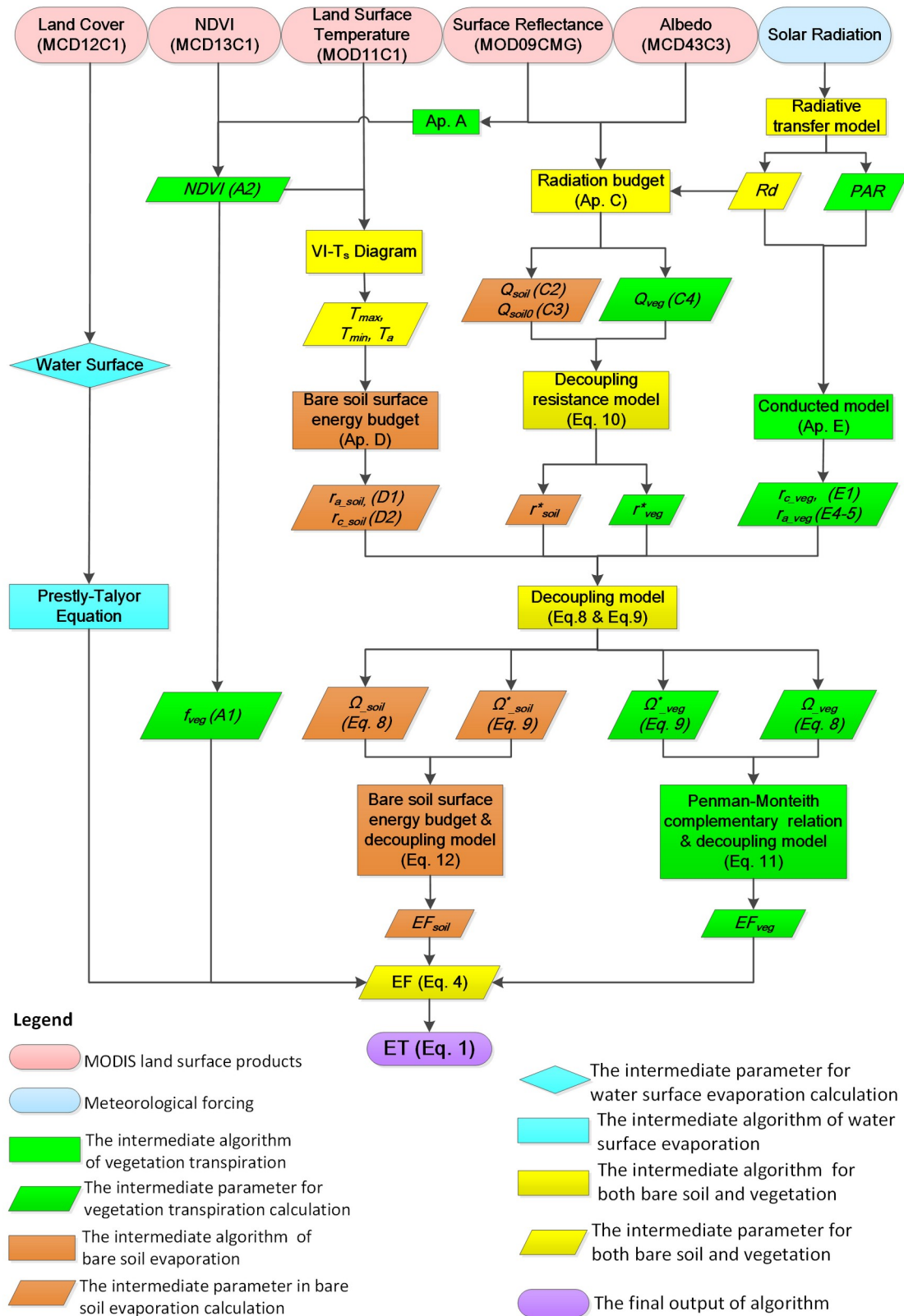


Figure 1: Schematic to calculate the evaporation fraction, EF (Eq. 13) and evaporation (Eq. 14). The ovals in the top row are the databases, and the square boxes are the algorithms, and parallelograms are the parameters. The numbers in the parenthesis are the equation to determine the parameters.

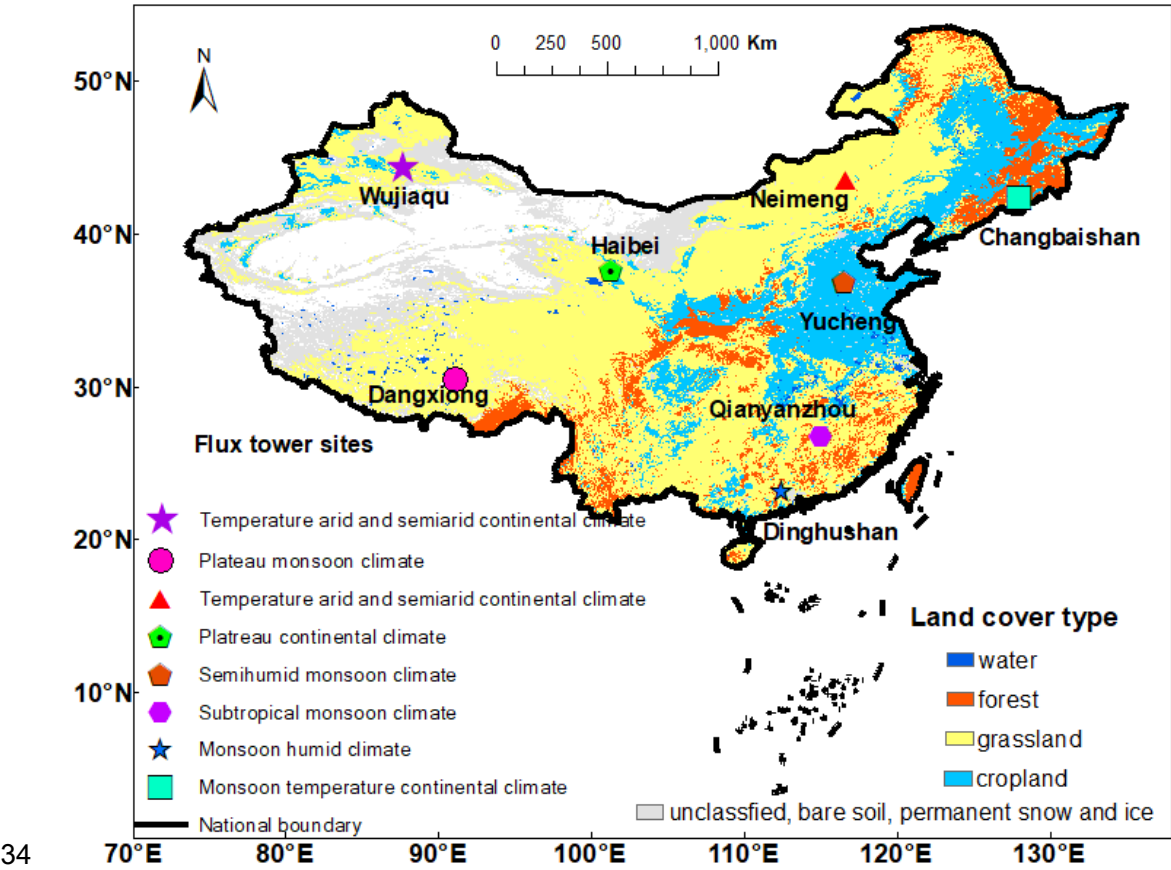
3.3 Data used for ground-truthing EF , ET and its components

The validity of the methods in Table 1 for calculating the actual ET was examined with data from seven flux towers from the Chinese FLUX Observation and Research Network (ChinaFlux): ChangBaiShan (CBS), QianYanZhou (QYZ), DingHuShan (DHS), YuCheng (YC), Haibei (HB), Neimeng (NM) and Dangxiong (DX) (Yu et al., 2006, 2008, 2013). These 7 flux towers are situated throughout China in different climate zones. CBS is in the monsoon temperate continental climate; QYZ and DHS are in the humid monsoon climate; YC is in the monsoon semi-humid climate; NM is in the temperate arid and semiarid continental climate; HB and DX sites are in the plateau continental climate, and land use, including forest, alpine, and grassland, as shown in Figure 2. The period considered was from 2003 to 2005 for CBS, QYZ, DHS, YC, and HB, and from 2004 to 2005 for the NM and DX sites. The sensible heat flux, latent heat flux, air temperature, and solar radiation observations are measured with a sampling frequency of 10 Hz with the open-path eddy covariance (3-D Sonic Anemometer of Campbell, and Li7500CO₂/H₂O analyzer of LI-COR) and standard meteorology equipment observations are aggregated every 30 minutes. The solar radiation, air temperature, and latent heat flux data at the closest 30-minute time interval to the MODIS Terra overpass time were used for instantaneous time scale validation. Daily temperatures were the average of the half-hour temperatures from 6:00 to 18:00. The Wujiaqu site is in the temperate arid and semiarid continental climate, and the measurement period was from Feb.7, 2020 to Dec. 17, 2020. The albedo measurements in the Wujiaqu site were used for diurnal albedo ground-truthing.

Several factors can cause discrepancies between satellite predicted EF and ET and flux tower measurements. These discrepancies may be due to the mismatch in the flux tower and the satellite footprint, the unsuitability of the satellite methods to the environmental conditions at the flux tower site (specifically high altitude sites with frozen soils and deserts), inaccuracies in the underlying assumptions of the theory, etc. We assumed the underlying assumptions were at fault when there was a

330 consistent difference for most flux towers. When the mismatch between our estimates
331 and the flux tower measurements was for only a few of the flux towers, environmental
332 factors and the particular site's footprint were likely the cause.

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334

335 **Figure 2.** The location of the seven flux tower sites of the FLUX Observation and
336 Research Network (ChinaFlux): ChangBaiShan (CBS), QianYanZhou (QYZ),
337 DingHuShan (DHS), YuCheng (YC), Haibei (HB), Neimeng (NM), WuJiangQu
338 (WJQ) and Dangxiong (DX). The 5 land cover types include water, forest, grassland,
339 cropland, unclassified, bare soil, permanent snow, and ice, are shown in Figure 2.

340 3.4 Statistical methods

341 To compare the daily satellite evaporation (ET_{MOD}^d) calculation with the flux
342 tower observed ET_{Obs}^d , the Pearson's correlation coefficient (r) and Root Mean Square
343 Error (RMSE) were calculated.

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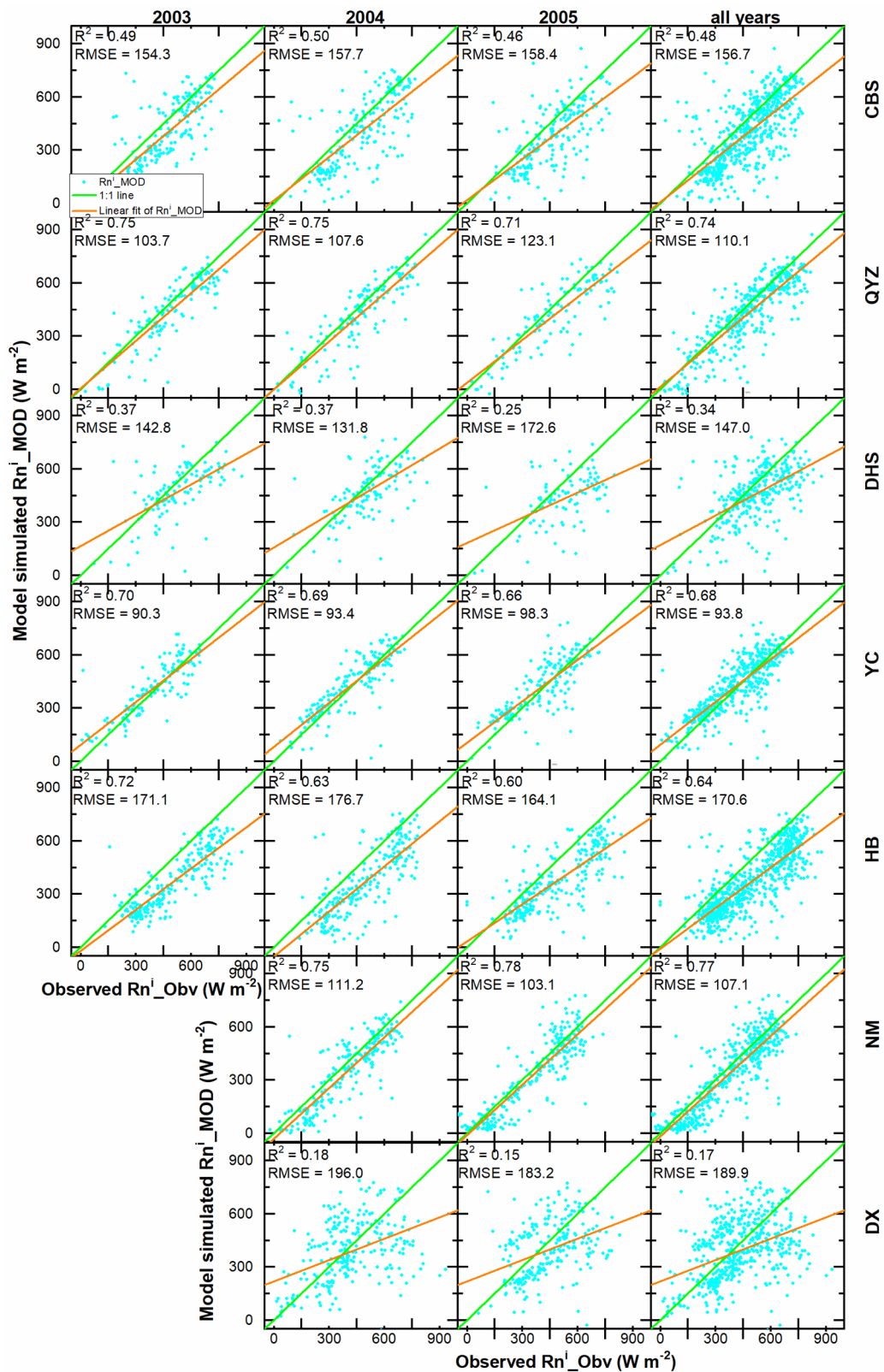
363

shortwave radiation ranged from 0.77 to 0.92, and RMSE varied between 27.1 and 40.4 W m⁻¹ (Figure H2 in Appendix H). The discrepancy between the two measurement techniques was the largest for the Dinghushan(DHS), Haibei(HB), and Dangxiong(DX) sites. The observed incoming shortwave radiation for the DHS site located in southeast China with a monsoon climate was greater than that of the CMFD because the albedo was overestimated during the rainy phase (Huang et al., 2017). The HB and DX sites are both situated at high elevations. According to Yang et al. (2006), shortwave radiation was underestimated.

4.2 Net radiation

4.2.1 Instantaneously net radiation

The satellite-based model simulated instantaneous net radiation Rn_{MOD}^i was calculated by Eq C1 and C2 in Appendix C. In Figure 3, R_c^i shows a good agreement with the instantaneous net radiation for four of the seven flux towers at the time of the satellite overpass. This is consistent with the generally good fit of the instantaneous incoming shortwave radiation (Appendix H1). Although Rn_{MOD}^i are consistently underestimated in the CBS, QYZ, YCand NM four sites, it has satisfactory regression coefficients, R^2 , ranging from 0.25 to 0.75, and root mean square error (RMSE) from 90.3 W m⁻² to 158.4 W m⁻² (Figure 3). Three remaining three sites (DHS, DX, and HB) perform poorly with RMSEs ranging from 103.1 to 198.9 W m⁻². The main reason for the weak performance of these three sites are the inadequate quality of the downloaded incoming shortwave radiation in the CMFD data base (section 4.1, Appendix H1 and H2)



Figure

re 3. Scatter plots of satellite based model simulated instantaneous (during MODIS Terra overpass) net radiation Rn^i_{MOD} against flux tower observed instantaneous air temperature (Rn^i_{Obv}) in an individual year and entire period of 2003 to 2005 at

393 Changbaishan (CBS), Qianyanzhou (QYZ), Dinghushan (DHS), Yucheng (YC),
 394 Haibei (HB), Neimeng (NM) and Dangxiong (DX) sites.

395 4.2.2 Daily net radiation

396 The daily net radiation Rn_{MOD}^d , calculated by the equation C3 in the Appendix by

397 assuming the longwave outgoing radiation term $\varepsilon\sigma T_s^4$ equals to the

398 $\varepsilon\sigma T_a^4 + 4\varepsilon\sigma T_a^3(T_s - T_a)$ in Eq. C1. Rn_{MOD}^d is consistently overestimated the observed

399 net radiation of the seven flux towers as shown in Figure 4, similar to that found by

400 Tang et al. (2009) employed the same algorithms. Despite that the R^2 for most flux

401 sites is good (R^2 ranges from 0.68 to 0.81) but the intercept with the y-axis is positive

402 indicating a systematic error in the calculations. The daily net radiation for QYZ and

403 DHS sites located in the south and southeast China (Figure 4) with a wet and warm

404 climate with dense plant cover is relatively close. The daily net radiation for the other

405 five sites (located in northern China, in colder, more arid, or semiarid climate) with

406 less dense vegetation have a greater offset from the observed values. Especially, the

407 DX site has the poorest fit R^2 of 0.29. We first hypothesized that the systematic error

408 causing the overestimation of the calculated satellite the net energy was related in part

409 to the vegetation density through the longwave radiation term in Eq C1 in appendix C.

410 Because we assumed that for daily scale, the longwave outgoing radiation term

411 $\varepsilon\sigma T_s^4 \approx \varepsilon\sigma T_a^4 + 4\varepsilon\sigma T_a^3(T_s - T_a)$ (Appendix C3), but we compared the $\varepsilon\sigma T_s^4$ and

412 $\varepsilon\sigma T_a^4 + 4\varepsilon\sigma T_a^3(T_s - T_a)$, and found they are very close (the difference is lower than

413 1%). Then, we found that assuming the instantaneous albedo as its daily value may be

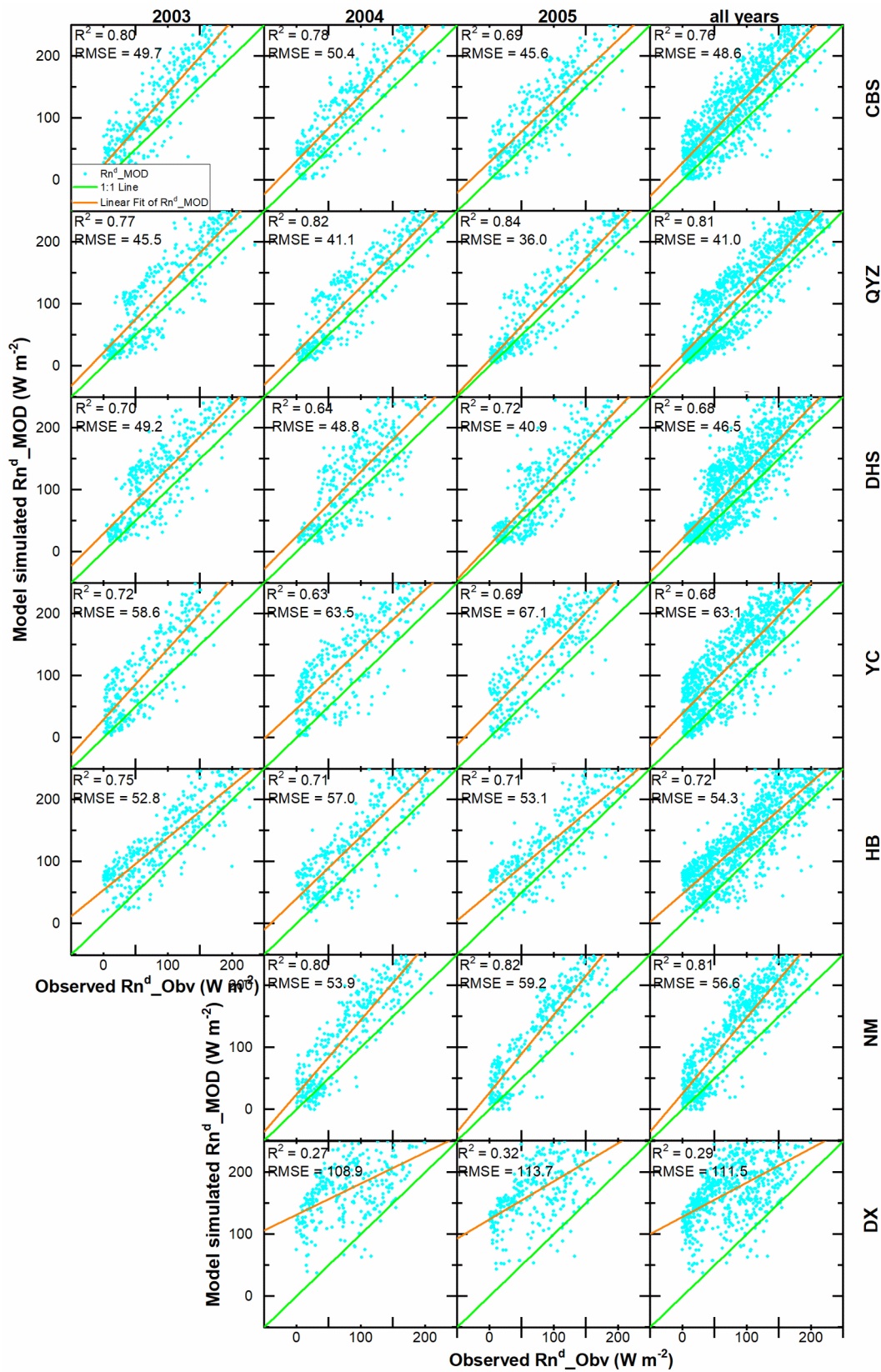
414 the main reason. Studies (Cierniewski et al., 2015; Jääskeläinen & Manninen, 2021;

415 Wang et al., 2015; Zhang et al., 2020) have shown that the albedo has a distinct

416 diurnal variation and it has the minimum values during the noon time during the

417 satellite overpass. Grant et al. found that the instantaneous albedo for a grass cover in

418 Australia was about 30% lower at noon than at 7 AM or 5 PM (Grant et al., 2000) as
419 the diurnal albedo measurements of Wujiaqu site in Appendix I.



Fig

Figure 4. Scatter plots of satellite-based model simulated daily net radiation (Rn_{MOD}^d) calculated with Eq. C1 plotted against the observed flux tower measurements (Rn_{Obs}^d) for an individual year and the entire 2003 to 2005 period. The abbreviation for the flux tower sites are in Figure 3, and the locations in Figure 1.

4.3 Air temperature

4.3.1 Instantaneous air temperature

Instantaneous air temperature T_{ϵ}^i was calculated by the MODIS land surface data and NDVI data combined with the VI-Ts method in Appendix F. The comparison of the satellite-based instantaneous daytime air temperatures, T_{ϵ}^i with the observed temperature T_{ϵ}^i at the seven flux towers during the satellite overpass is shown in Figure 5. The predicted air temperature is in general agreement with the flux tower measurements with R^2 ranging from 0.50 to 0.84 and root mean square (RMSE) from 3.0 K to 15.9 K. The three sites Haibei, (HB), Neimeng (NM), and Dangxiong (DX) that are located at high elevations with an annual average of 0 °C and grass ground cover, deviated most (i.e., low R^2 and large RMSE). For these sites at high elevations, a distinct relationship between the NDVI and air temperature does not exist when the grass is frozen or snow-covered. Hence the underlying assumptions of the VI diagram (Appendix F) are violated and resulted in poor estimates of air temperature, as shown in Figure 5. When the NDVI has large spatial differences (e.g., forests in northeast China at the Changbaishan (CBS) site and cropland in North China Plain at the Yucheng (YC) site), the air temperature calculated with the VI-T_s diagram is comparable to the flux tower (Figure 5).

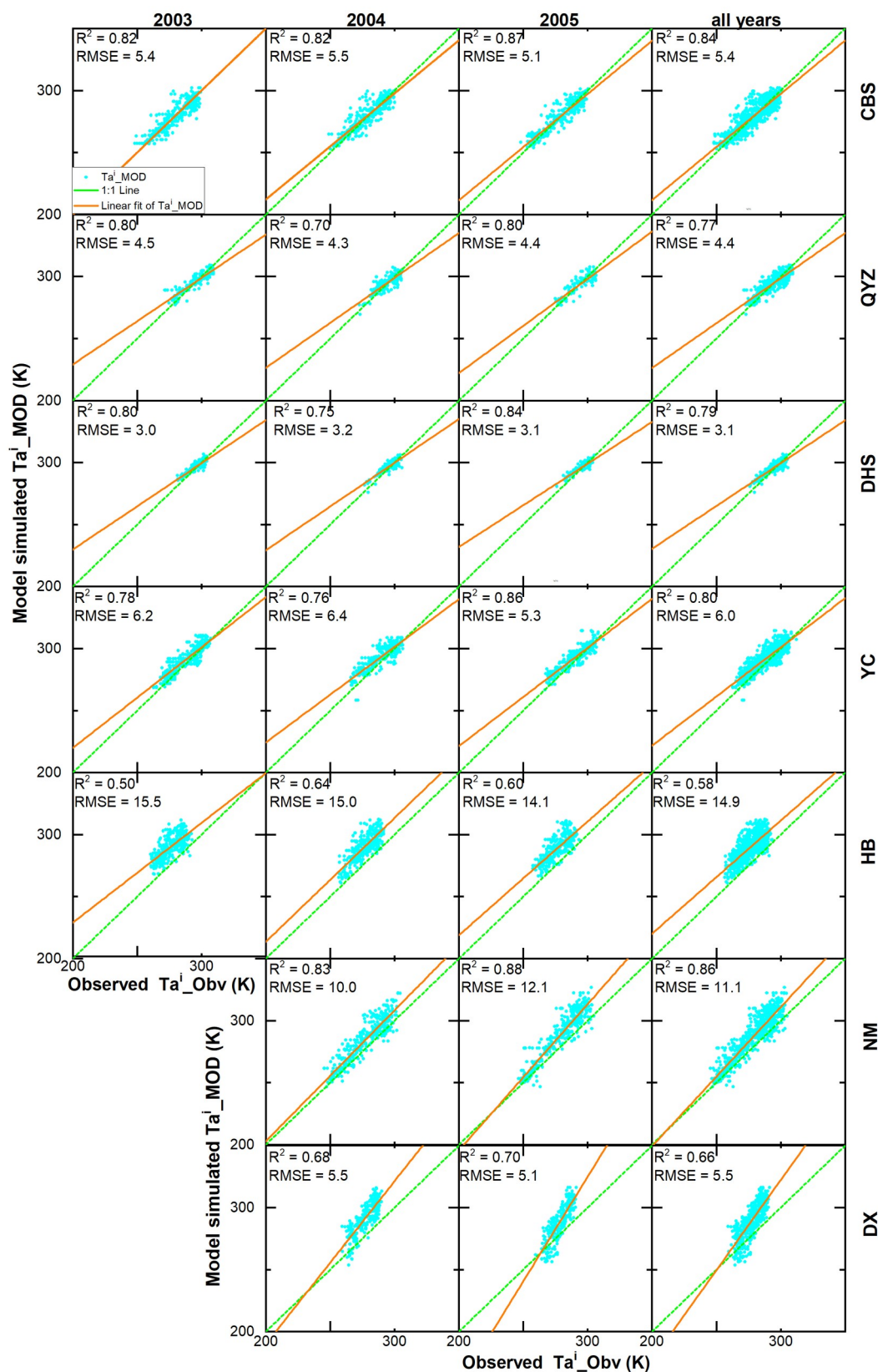


Figure 5. Scatter plots of satellite based model simulated instantaneous (during MODIS Terra overpass) air temperature Ta^i_{MOD} against flux tower observed instantaneous air temperature (Ta^i_{Obv}) in an individual year and entire period of 2003 to

447 2005. The flux tower abbreviations are in Figure 3, and the locations in Figure 1.

448 4.3.2 Daily air temperature

449 The model simulated daily mean air temperature, T_{a}^d was calculated by extending
 450 the daytime and nighttime instantaneous air temperature with a sine and cosine
 451 method in Appendix G. T_{a}^d was compared with the daily averaged air temperatures
 452 seven flux towers observations T_{a}^d in Figure 6. In general, the fit of the daily
 453 temperatures in Figure 6 is either equal or better than the instantaneous temperatures
 454 in Figure 5, with the R^2 ranging from 0.64 to 0.95 and RMSE ranging from 3.1 K to
 455 6.4 K. Especially for the DX, NM, and HB sites, the fit is much better because 1) the
 456 random biases of flux tower measurements were reduced for the daily scale; 2) the
 457 calculation of the daily air temperature involved the high air temperature that was
 458 calculated by setting the satellite measured land surface temperature equal to the air
 459 temperature and did not involve the problems encountered with the VI-Ts diagram for
 460 these three sites (Appendix F). For the remaining four sites, the daily air temperatures
 461 based on the satellite measurements slightly underestimate the flux tower
 462 measurement (Figure 6). Therefore, the RMSE do not improve significantly over the
 463 instantaneous air temperatures in Figure 5.

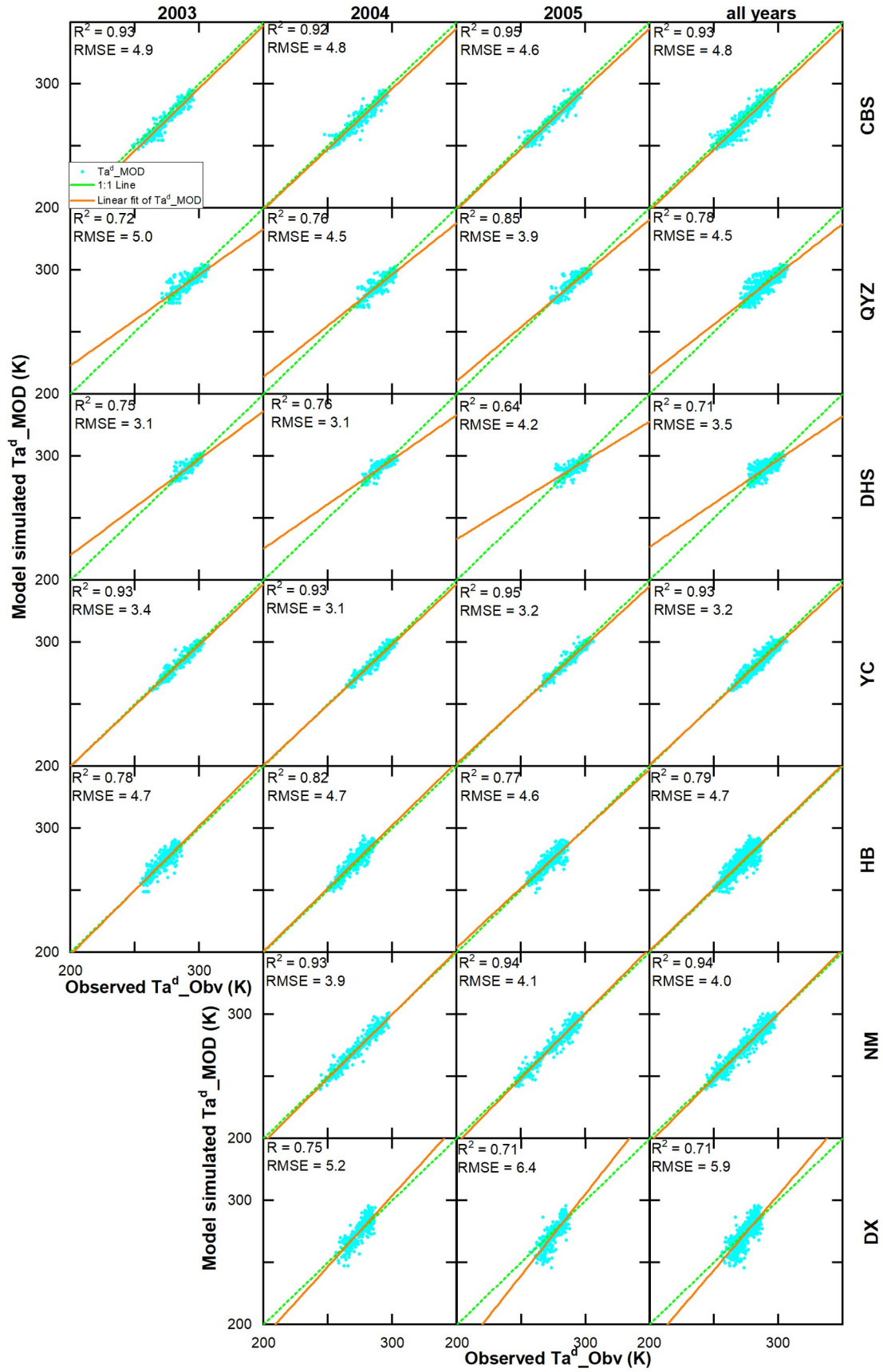


Figure 6. Scatter plots of satellite-based model simulated daily air temperature T^d_i against flux tower observed instantaneous air temperature (T^d_i) in an individual year and entire period. Figures 1 and 3 give the location and abbreviations.

4.4 Evaporation fraction (EF)

The satellite-based evaporative fraction (EF) using the approximations in Table 1 for Eqs 12-15 was averaged over the observation period (Figure 7). As expected, the greatest daily evaporation fractions are observed for the QYZ, DHS, and YC sites which either have the highest rainfall or are irrigated and thus have ample water to satisfy the evaporative demand (Figure 7). The other sites have limited rainfall, and thus evaporation is less than the potential evaporation and consequently greater amounts of incoming solar radiation converted into sensible heat. The calculated EF values for the Dangxiong (DX) site in southwest China for all approximations in Table 1 are much lower than the observed EF values (Table 3). The main reason is the difference in vegetative cover for the flux tower's footprint and the grid cell on which the satellite measurements. Sixty-five percent is vegetated in the flux tower footprint, but only 13 % of the grid cell had vegetation. The DX site will therefore not be considered further. The remaining EF values for the 6 flux tower sites are averaged in Table 3.

The expressions of daily evaporation fractions in Table 1 can be divided into the EF_d method and the remaining methods consisting of EF_0 - EF_7 . For EF_d , all daily parameter and instantaneously parameter values were calculated, and for EF_0 - EF_7 , one or more of the daily parameters were substituted for the instantaneous parameter values. As can be seen in Table 3, when no substitutions were made, the daily evaporation fraction, EF^d for the EF_d method resulted in a 50% underprediction of the observed flux tower EF^d of 45%. The second group in which substitutions were made of instantaneous values for daily parameters, EF_0 , in which the daily EF^d equaled to the instantaneous EF^i during satellite overpass, performs relatively well and provides a better estimate for the observed flux tower value than the EF_d . For EF_1 in Table 3, the slope of the saturated vapor pressure for the day Δ^d was set equal to the instantaneous value. The average value of EF_1 for $EF^d = 0.23$ and is similar to the EF_d , which is half of the observed value. Next is the set of EF_2 - EF_4 in which the

495 daily aerodynamic, surface and decoupling parameter resistances were replaced by
 496 their instantaneous values. None of the three approximation predict the observed EF^d
 497 very well (Table 3). Finally, the last set consists of EF5-EF7, in which the daily
 498 decoupling parameters were equated with the instantaneous values. Interestingly the
 499 EF^d values vary widely in this group and have the lowest performance for EF 5 with
 500 and an average value of $EF^d=0.17$ and the best performance for EF6 with $EF^d=0.41$.
 501 The latter is closer to the observed value of 0.45 than any other approximations,
 502 including the original method (EF0) proposed by Nishida and EFd that uses the
 503 complete equation (Eqs 11-14) without substitution Table 3.

504 The EF6 (as well as EF0 and EF7) method predicted the observed value EF^d
 505 value most accurately because in all the three methods the $\Omega^{i,d}$ was replaced by the
 506 instantaneous value $\Omega^{i,i}$ in some form (as can be seen from Table 1). Both $\Omega^{i,d}$ and $\Omega^{i,i}$
 507 were calculated with Eq.10 in which either daily or instantaneous values were used of
 508 the following independent parameters: the slope of the saturated vapor pressure, the
 509 psychrometric constant, the aerodynamic resistance and r^{ℓ} . Considering these four
 510 independent parameters in Eq 10, we note that critical surface resistance r^{ℓ} in Eq 11 is
 511 a function of the net radiation. As shown in Figure 4, the instantaneous net radiation is
 512 predicted much more accurately than the daily net radiation in Figure 5, which is
 513 overestimated by 20-40% using MODIS parameters. It means since the net radiation
 514 is the denominator in Eq 11, the instantaneous critical surface resistance $r^{i,i}$ is
 515 estimated relatively well, while the daily critical surface resistance $r^{i,d}$ is too small. In

516 turn, this calculates $\Omega^{i,i}$ correctly and gives a too large $\Omega^{i,d}$, thus, the $\frac{\Omega_i^{\ell}}{\Omega_d^{\ell}}$ is too small.

517 In the calculation of the daily evaporation fraction, EF^d , in Eq 9, the $\frac{\Omega_i^{\ell}}{\Omega_d^{\ell}}$ term is in the
 518 denominator, and hence the EF^d is underestimated for all approximations (i.e., EF1-

519 EF5) that use the calculated $\frac{\Omega_i^c}{\Omega_d^c}$ value.

520

521

Table 3. The comparison of the flux tower observed daily mean evaporative fraction (EF_{Obs}) and the satellite-based estimated EF with various methods (ET0-ET7 and ETd) during 2003 to 2005 at Changbaishan (CBS), Qianyanzhou (QYZ), Dinghushan (DHS), Yucheng (YC), Haibei (HB), Neimeng (NM) and Dangxiong (DX) sites.

Site	Observed	EF0	EF1	EF2	EF3	EF4	EF5	EF6	EF7	EFd
CBS	0.38	0.25	0.22	0.22	0.17	0.20	0.16	0.33	0.23	0.20
QYZ	0.63	0.53	0.39	0.39	0.41	0.34	0.34	0.57	0.50	0.38
DHS	0.60	0.52	0.35	0.34	0.37	0.33	0.21	0.81	0.49	0.33
YC	0.57	0.31	0.19	0.18	0.21	0.18	0.14	0.34	0.28	0.18
HB	0.28	0.20	0.10	0.10	0.08	0.08	0.05	0.21	0.15	0.08
NM	0.25	0.17	0.13	0.11	0.10	0.11	0.09	0.17	0.14	0.12
Average	0.45	0.33	0.23	0.22	0.22	0.21	0.17	0.41	0.30	0.22
DX	0.43	0.11	0.06	0.06	0.03	0.04	0.03	0.12	0.08	0.04

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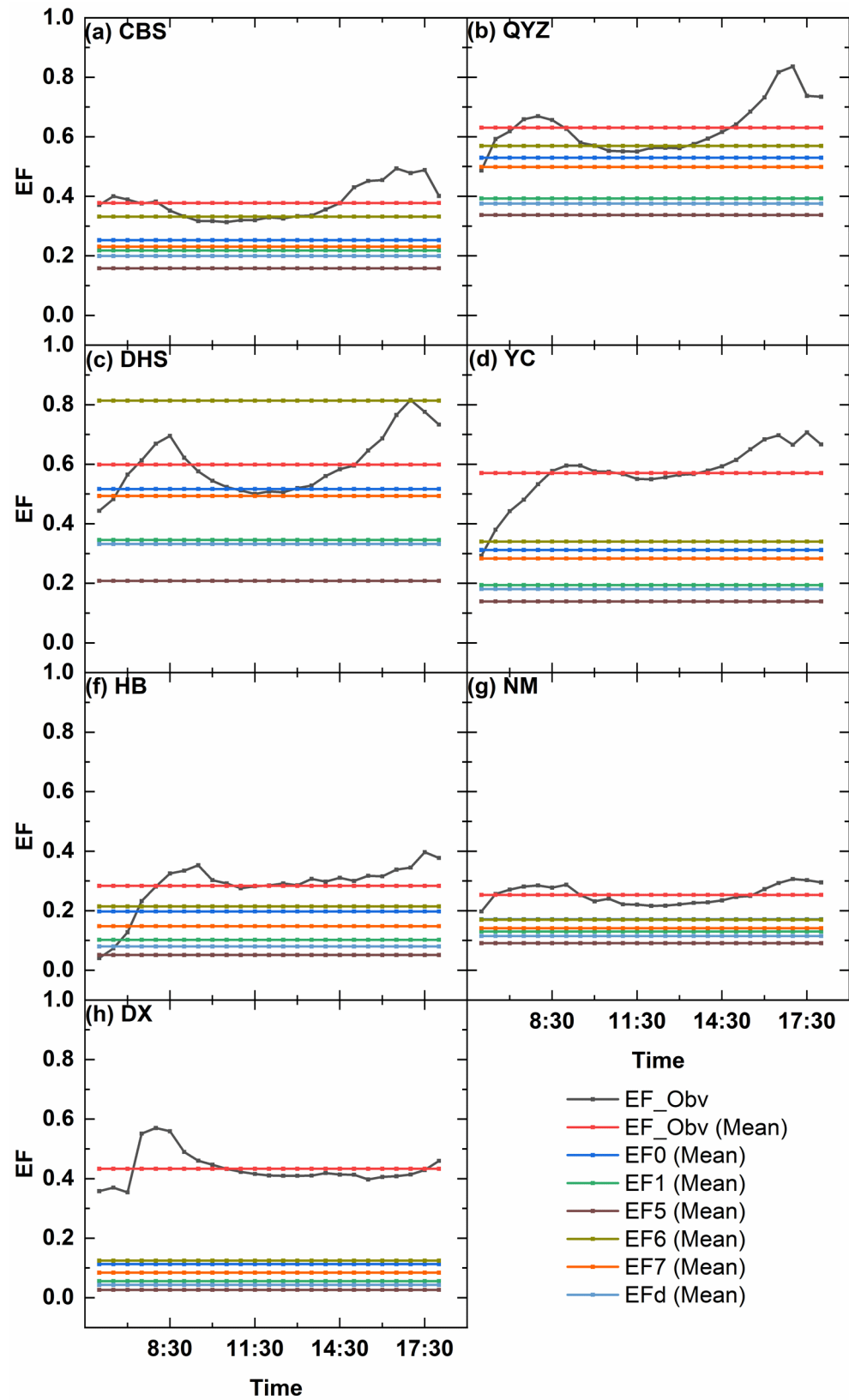


Figure 7. Comparison of multiyear averaged observed diurnal evaporation fraction, EF (EF_Obv) and estimated daily mean EF ($EF0$, $EF1$, $EF2$, $EF3$, $EF4$, $EF5$, $EF6$, $EF7$, and EFd) during 2003 to 2005 at Changbaishan (CBS), Qianyanzhou (QYZ), Dinghushan (DHS), Yucheng (YC), Haibei (HB), Neimeng (NM) and

533 Dangxiong (DX)

534 4.5 Evapotranspiration

535 The daily evapotranspiration calculated with the decoupling factor method (ET1
536 to ET7 and ETd in Table 1) is plotted against the flux tower measurements in Figure
537 8. The daily evaporation was obtained with Eq 15 by multiplying the evaporation
538 fraction EF^d (Table 3) with the daily available energy, Q (Appendix C). In each plot
539 in Figure 8, the daily evaporation calculated with the Nishida method (ET0 in Table 1)
540 is also plotted for comparison. The averaged daily measured and calculated
541 evaporation over the measurement period for each flux tower observation are shown
542 in Table 4. Similar to the evaporation fraction depicted in Table 3, the satellite-based
543 ET for Changbiashan, CBS (in the plot of (a)-(h) of Figure 8a), with the R^2 around
544 0.55 and RMSE 1.1 mm day⁻¹ and Haibei, HB (in the plot of (i)-(p) of Figure 8b),
545 with R^2 around 0.65 and RMSE 1.1 mm day⁻¹ agree most closely with the flux tower
546 measurements. The Dinghushan, DHS (in the plot of (q)-(x) of Figure 8a), with the R^2
547 around 0.25 and RMSE 1.5 mm day⁻¹ and Dangxiong, DX (Figure 8c) with the R^2
548 around 0.35 and RMSE 1.5 mm day⁻¹ deviate the farthest. Unlike the EF results in
549 Table 3, ET0 predicted most closely the flux tower measurements with the greatest R^2 ,
550 lowest RMSE (Figure 8a-8c, and Table 4). The ET6 method that most closely
551 matched the observed EF^d value in Table 3 overpredicted the observed flux tower
552 measurements significantly with RMSE 1.1 to 2.2 mm day⁻¹ (Figure 8a-8c, and Table
553 4). Of the other methods that calculated the ET from the satellite data, ET1-ET4
554 underestimated the daily ET by nearly 50% and ET7 underestimated the daily ET
555 by 30% (Table 4).

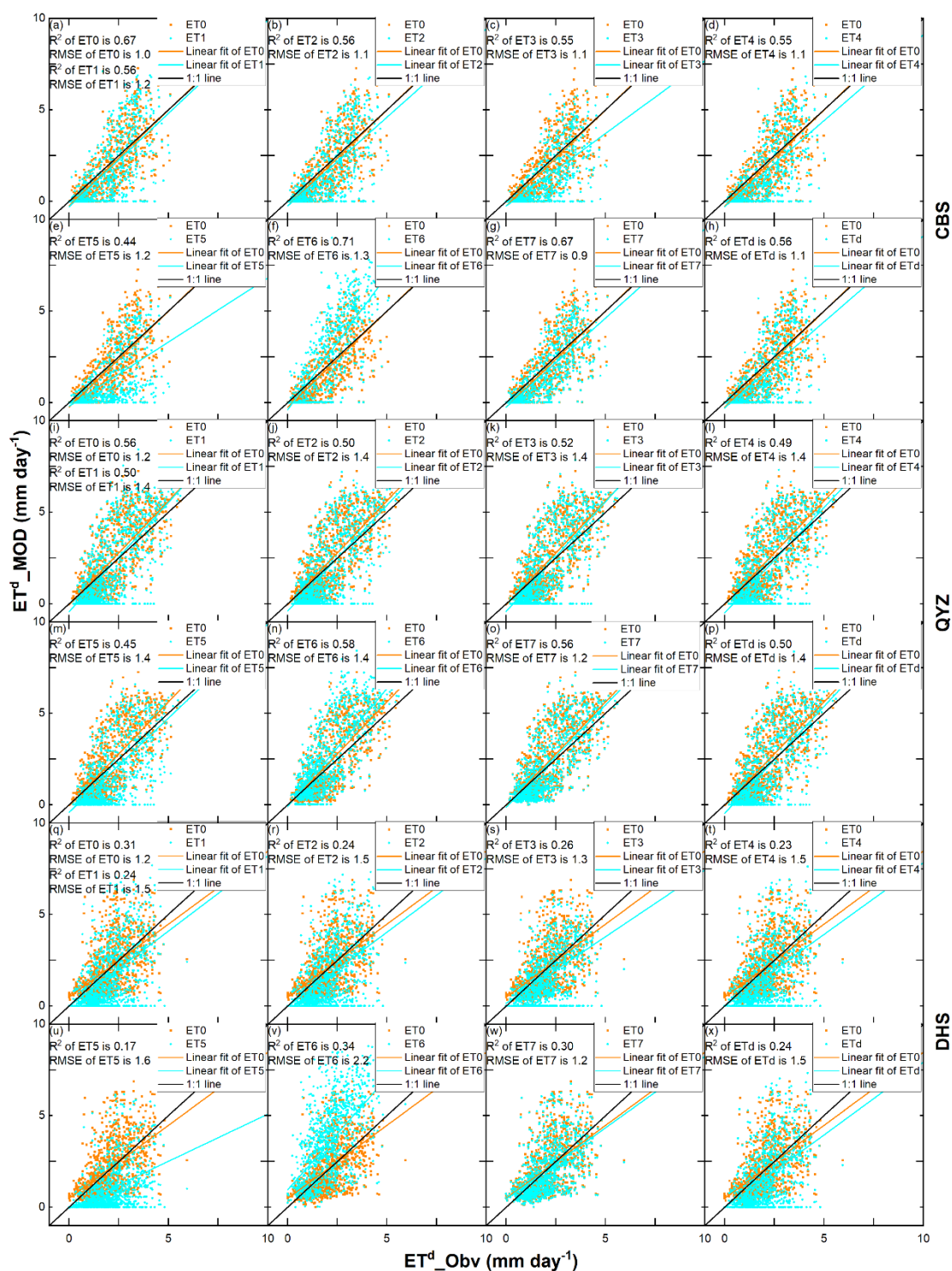


Figure 8a. Scatter plots of daily estimated ET data ET^d_MOD (ET_0 , ET_1 , ET_2 , ET_3 , ET_4 , ET_5 , ET_6 , ET_7 and ET_d) against flux tower daily observed ET data (ET^d_Obv) at entire period of 2003 to 2005 at Changbaishan (CBS), Qianyanzhou (QYZ), Dinghushan (DHS) sites.

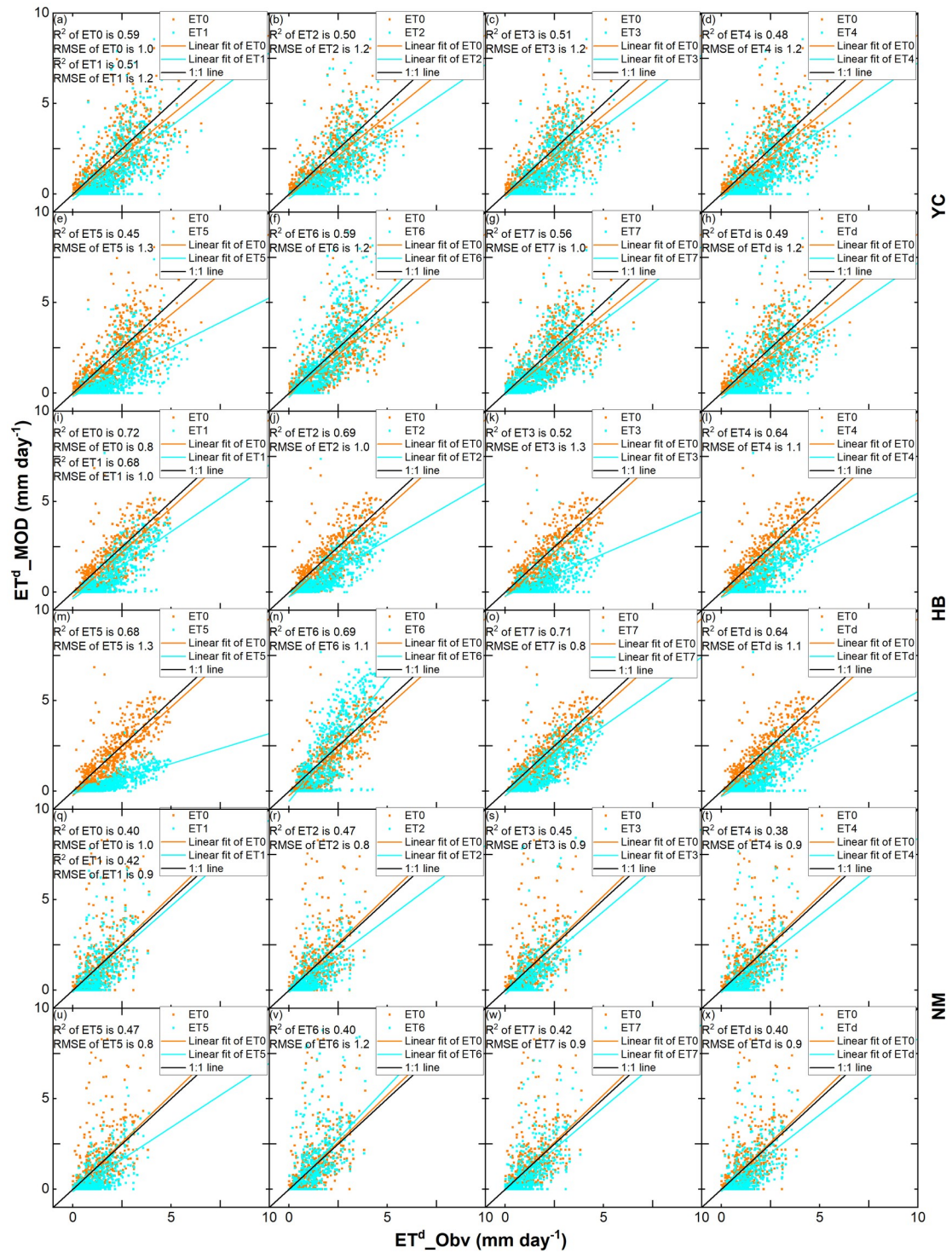
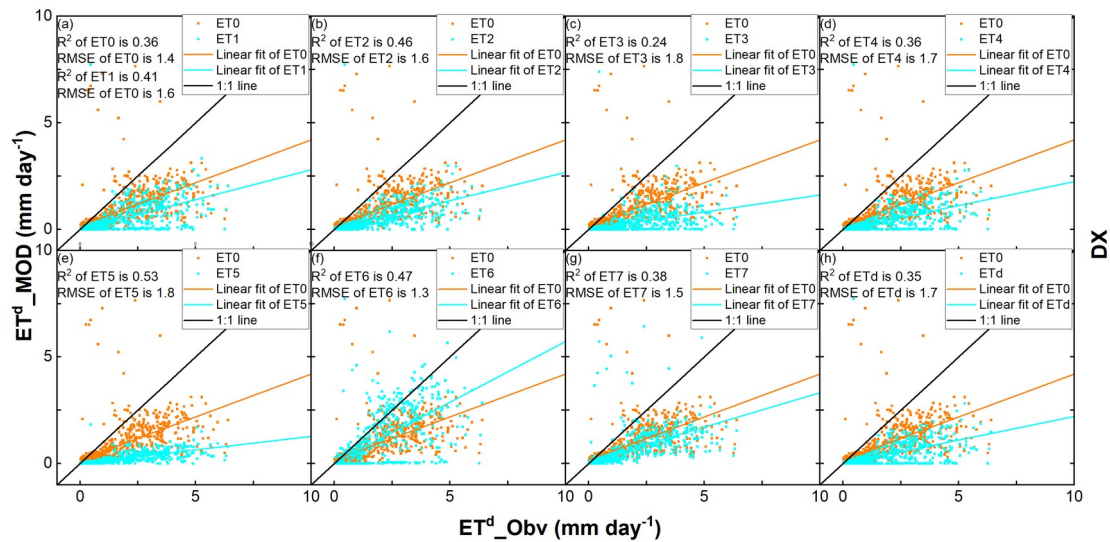


Figure 8b. Scatter plots of daily estimated ET data ETd_MOD ($ET0$, $ET1$, $ET2$, $ET3$, $ET4$, $ET5$, $ET6$, $ET7$ and ETd) against flux tower daily observed ET data (ETd_Obv) at entire period of 2003 to 2005 at Yucheng (YC), Haibei (HB) and 2004 to 2005 at Neimeng (NM) sites.



566

567 **Figure 8c.** Scatter plots of daily estimated ET data (ET0, ET1, ET2, ET3, ET4, ET5
 568 ET6, ET7 and ETd) against flux tower daily observed ET data (ET_Obv) at entire
 569 period of 2004 to 2005 a) at Dangxiong (DX) site.

570 **Table 4.** The comparison of the flux tower observed daily mean ET (ET_Obv) and
 571 the satellite-based estimated ET with various methods (ET0-ET7 and ETd, ET6_new
 572 was calculated by the EF6 and the observed net radiation) during 2003 to 2005 at
 573 Changbaishan (CBS), Qianyanzhou (QYZ), Dinghushan (DHS), Yucheng (YC),
 574 Haibei (HB), Neimeng (NM) and Dangxiong (DX) sites.

Site	ET_Obv	ET0	ET1	ET2	ET3	ET4	ET5	ET6	ET7	ETd	ET6_new
mm day ⁻¹											
CBS	1.44	1.25	1.16	1.14	0.87	1.05	0.80	1.71	1.14	1.05	1.65
QYZ	2.05	2.27	2.01	1.97	2.03	1.86	1.70	2.55	2.16	1.93	2.35
DHS	2.06	2.13	1.68	1.65	1.65	1.61	0.99	3.47	2.05	1.61	3.24
YC	1.64	1.36	1.03	0.97	1.06	0.96	0.71	1.63	1.24	0.95	1.46
HB	1.37	1.09	0.65	0.60	0.43	0.50	0.31	1.28	0.82	0.51	1.18
NM	0.96	0.92	0.74	0.62	0.64	0.64	0.49	1.03	0.77	0.65	0.61
Average	1.59	1.50	1.21	1.16	1.11	1.10	0.83	1.95	1.36	1.12	1.75
DX	1.50	0.80	0.43	0.43	0.27	0.34	0.20	0.93	0.60	0.34	0.53

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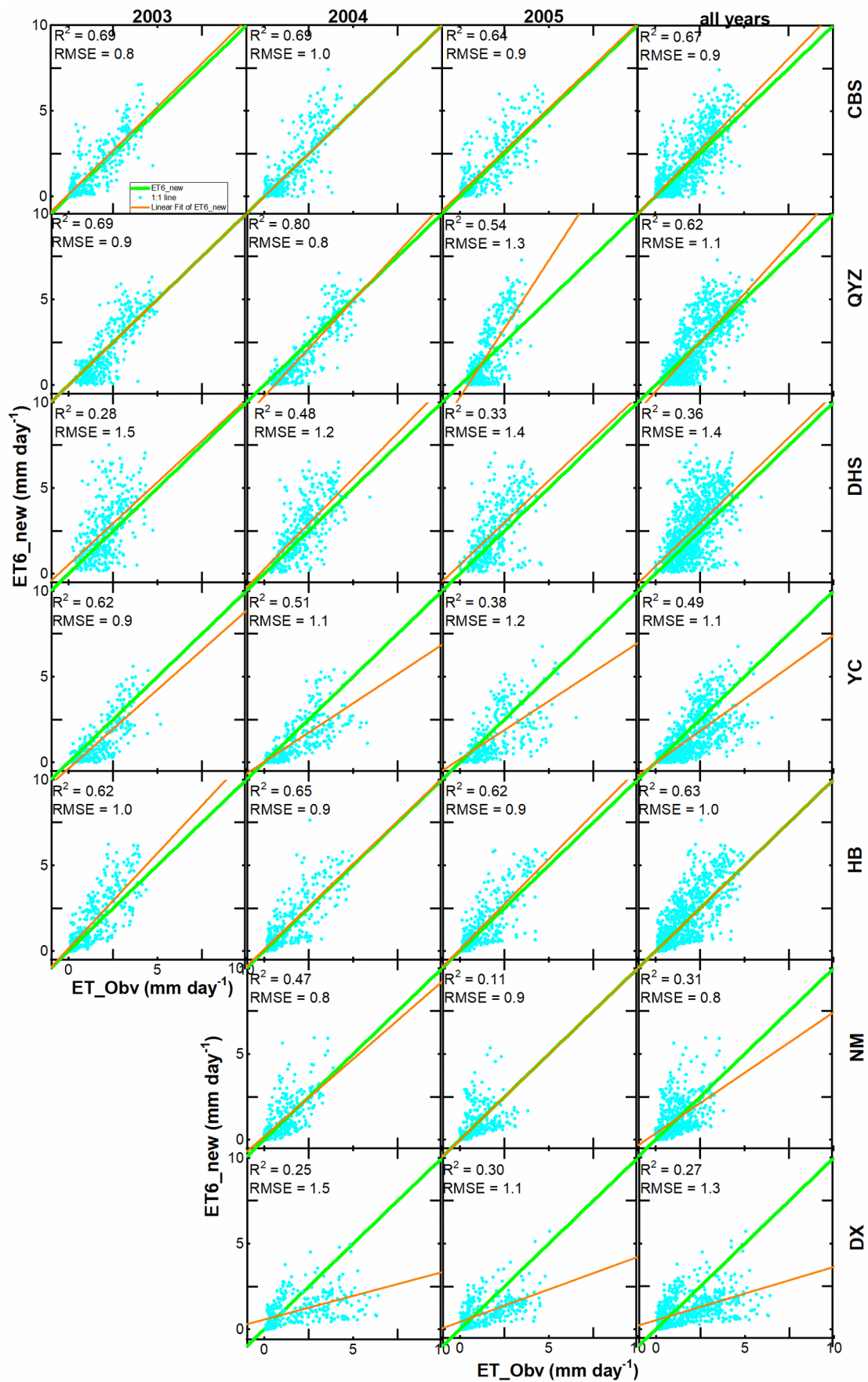
576 Considering the intermediate results in Fisections 4.1 to 4.4, the calculated EF
 577 with the method of Nashida (2003), EF0, was on the average 25% less than the
 578 observed flux tower EF (Figure 7 and Table 3). While the daily net radiation was 30%
 579 greater than the flux tower measurement (Figur 4). Thus, the daily ET0 was predicted
 580 more accurately than any other methods in Table 1. as it is the product of these two
 581 variables (Eq. 15) fortuitously provided the correct answer. Conversely, the EF6

method predicted the EF most closely to the flux tower measurements but overpredicted the daily evaporation, because of the 30% overestimates of the daily net radiation (Figur 4).

To reduce the impact of the overestimated daily net radiaiton on the daily ET estimates and examine whether the ET6 method would accurately predict the evaportation, we used EF6 method and the observed flux tower net radiation to recalculate the ET. The results are shown in Figure 9. The calculated ET generally match the observations with R^2 ranging from 0.27 to 0.67 and RMSE ranging from 0.9 to 1.4 mm day⁻¹. Compared to the ET0 method, the ET6 methad was generally more precise. For example, in the CBS site, the RMSE of ET6_new and ET0 is 0.9 mm day⁻¹ and 1.0 mm day⁻¹ respectively; in the QYZ site, the R^2 is 0.62 (ET6_new) and 0.56 (ET0), RMSE is 1.1 mm day⁻¹ (ET6_new) and 1.2 mm day⁻¹ (ET0); in the YC site, the R^2 is 0.49 (ET6_new) and 0.31(ET0), RMSE is 1.1 mm day⁻¹ (ET6_new), and 1.2 mm day⁻¹ (ET0); in the HB site, the R^2 is 0.63 (ET6_new) and 0.59 (ET0) respectively.

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599 **Figure 9.** As Figure 3, but for daily estimated ET ($ET6_new$) which was based on
 600 the EF6 and observed net radiation against flux tower daily observed ET data

601 (ET_Obv).

602 **5 Discussion and Conclusion**

603 This study converted the instantaneous satellite observation into daily evaporation
 604 fraction and actual evapotranspiration, for forests, grassland, cropland, and deserts for
 605 large-scale applications in China. Our approach was based on the decoupling
 606 parameter method introduced by Tang & Li (2017) for irrigated winter wheat and
 607 summer maize cropland in the North China Plain. The decoupling parameter method
 608 is based on the relative contribution of radiative and aerodynamic terms to the overall
 609 evapotranspiration. We introduced eight different ways to calculate the daily
 610 evaporation from instantaneous satellite observation by replacing none, one, or
 611 several of the daily calculated intermediate variables by their instantaneous values
 612 (EFd, EF1-EF7 in Table 1). In this way, we were able to check the validity of the
 613 proposed conversions of instantaneous to daily values.

614 The MODIS 0.05-degree grid cell data, rather than the 250m or 500 m, was used
 615 as input because our focus was on determining the *ET* for China. A better agreement
 616 could have been obtained between flux tower measurement and satellite-based
 617 calculations of evaporation and its intermediate calculated values by calibrating the
 618 vegetation coverage (f_{veg}) in Eq. 2 using the same footprint MODIS data and flux
 619 tower surroundings. For example, for the DX site, the f_{veg} for the 0.05 grid cell is 0.13,
 620 and the f_{veg} for the flux tower footprint is 0.65. This resulted in a mismatch of satellite
 621 and flux tower evaporation. For this reason, the DX site was excluded from further
 622 consideration.

623 In evaluating the original Nishida method, we found that despite underestimating
 624 the evaporation fraction of the flux towers by 26% on average, the daily evaporation
 625 was more accurate than any of the eight methods based on the original Nishida
 626 method. The Nishida method assumed that the instantaneous evaporation was equal
 627 to the daily evaporation. By checking the intermediate values, we found that the daily
 628 net radiation was 30% too large. This too-large value with the 26% lower evaporation
 629 fraction made the daily *ET* estimates of the Nishada method came out well.

In calculating the daily net radiation, the diurnal albedo was assumed remained constant during the day. Studies (Cierniewski et al., 2015; Jääskeläinen & Manninen, 2021; Wang et al., 2015; Zhang et al., 2020) have proven that the albedo has a distinct diurnal variation with the minimum values during the noon when the satellite overpass (Grant et al., 2000). Observations at the Wujiaqu site (Appendix I) in Northwest China confirmed the findings. Thus, assuming that the albedo was constant resulted in the overestimation of the daily net radiation. It affected the intermediate calculated values such as the daily decoupling resistance $r^{i,d}$ in Eq. 11, where the daily net radiation is in the denominator. Other variables such as the daily decoupling parameter $\Omega^{i,d}$, depended on the value $r^{i,d}$ (Eq. 12). Ultimately the 30% error in the daily net radiation caused about 50% and 30% or higher underestimates of daily EF and ET respectively for six of the eight methods of the decoupling parameter method in Table 1.

Once we dropped the decoupling parameter $\Omega^{i,d}$ in determining the daily EF and used the correct daily net radiation, we found that the Tang & Li (2017) method as adapted by us and provided both reasonable daily EF and ET estimates with the relative error of 8% and 9% respectively. Thus using the decoupling parameter method should be tried in other locations as well for predicting the ET over large areas.

Acknowledgments

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659 **Appendix A: Vegetation fraction (f_{veg}) and Normalized Difference Vegetation** 660 **Index (NDVI)**

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662 The vegetation fraction coverage (f_{veg}) is calculated as (Figure 1)

$$663 \quad f_{veg} = \frac{NDVI - NDVI_{min}}{NDVI_{max} - NDVI_{min}} \quad (A1)$$

664 where the NDVI is the Normalized Difference Vegetation Index and can be calculated
665 as:

$$666 \quad NDVI = \frac{R_{nir} - R_{\bar{r}}}{R_{nir} + R_{\bar{r}}} \quad (A2)$$

667 where $NDVI_{min}$ is the NDVI of the bare soil without plants and $NDVI_{max}$ is the NDVI
668 of the full vegetation cover, R_{nir} is the near-infrared reflectance and $R_{\bar{r}}$ is the red
669 reflectance. The daily reflectance R_{nir} and $R_{\bar{r}}$ were measured by MODIS reflectance
670 data MOD09CMG (Figure 1). Based on Tang (2009), we have set $NDVI_{min}=0.22$ and
671 $NDVI_{max}=0.83$. Missing observation for the daily NDVI data was filled with the 16-
672 day averaged NDVI values in the MOD13Q1data product (Fig. 1, Table 2).

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Appendix B: The calculation of the slope of the saturated vapor, and the vapor pressure deficit of the air VPD

The slope of the saturated vapor (Δ),

$$\Delta = 4098 \frac{1}{T_a} \quad (B1)$$

where T_a is the air temperature ($^{\circ}\text{C}$) that can be calculated by the VI-Ts method in Appendix F with the NDVI and land surface data. VPD is the vapor pressure deficit of the air (kPa)

$$VPD = e^0(T_a) - e_a \quad (B2)$$

$$e^0(T_a) = 0.6108 \exp \left(\frac{17.27 T_a}{T_a + 237.3} \right) \quad (B3)$$

$$e_a = e^0(T_{dew}) \quad (B4)$$

$$e^0(T_{dew}) = 0.6108 \exp \left[\frac{17.27 T_{dew}}{T_{dew} + 237.3} \right] \quad (B5)$$

where the parenthesis indicates the independent variable, $e^0(T_a)$ is the saturation vapor pressure (kPa) at the air temperature T_a ($^{\circ}\text{C}$); e_a is the actual vapor pressure (kPa);

$e^0(T_{dew})$ is the saturation vapor pressure (kPa) at the dew point temperature T_{dew} ($^{\circ}\text{C}$).

T_{dew} is set to the minimum air temperature during the day ($^{\circ}\text{C}$) for the forest, water surface, and cropland. In arid areas like bare soil and non-irrigated grassland, T_{dew} maybe 2-3 $^{\circ}\text{C}$ lower than T_{min} . For this reason, 2 $^{\circ}\text{C}$ is subtracted from the T_{min} in arid and semiarid areas to obtain the T_{dew} . Although these simplifications might introduce a bias in the final calculated ET value, our initial results showed that the effect was small.

Appendix C: Determining the net radiation (R_n), available energy of bare soil (Q_{soil}) and vegetation cover (Q_{veg}).

710

711 The net radiation was calculated by the land surface energy balance equation (Tang et
712 al., 2009):

$$R_n = (1 - albedo) R_d + \varepsilon \sigma (T_a - 20)^4 - \varepsilon \sigma T_s^4 \quad (C1)$$

714 where *albedo* is obtained from the MODIS 16-day albedo data (MCD43C3); R_d is the
715 3-hourly incoming shortwave radiation from the China Meteorological Forcing
716 Datasets (CMFD) (W m^{-2}) with a resolution of 0.1 degrees; ε is the emissivity from
717 the MODIS daily surface temperature/emissivity data (MOD11C1); σ is the Stefan-
718 Boltzmann constant $5.6704 \times 10^{-8} \text{ W m}^{-2} \text{ K}^{-4}$; T_a is the air temperature (K); T_s is the

719 surface temperature (K); $\varepsilon \sigma (T_a - 20)^4$ is the incoming long-wave radiation (W m^{-2}),

720 $\varepsilon \sigma T_s^4$ is the upward long-wave radiation (W m^{-2}).

721 We follow Nishida (2003) to estimate the net radiation of vegetation R_{veg} (W m^{-2}) by
722 assuming $T_s = T_a$

$$R_{veg} = (1 - albedo) R_d + \varepsilon \sigma (T_a - 20)^4 - \varepsilon \sigma T_a^4 \quad (C2)$$

724 And we estimate the net radiation of bare soil R_{soil} (W m^{-2}) following Nishida (2003),

725 assuming $\varepsilon \sigma T_s^4 = \varepsilon \sigma T_a^4 + 4 \varepsilon \sigma T_a^3 (T_s - T_a)$

$$R_{soil} = (1 - albedo) R_d + \varepsilon \sigma (T_a - 20)^4 - \varepsilon \sigma T_a^4 - 4 \varepsilon \sigma T_a^3 (T_s - T_a) \quad (C3)$$

727 The available energy for the bare soil Q_{soil} (W m^{-2}), and for fully vegetated surfaces,
728 Q_{veg} (W m^{-2}) and the maximum available energy for evaporation of bare soil, Q_{soil} (W
729 m^{-2}) can be determined according to Nishida, (2003) as:

$$Q_{soil} \approx (1 - C_G) (R_{n0} - 4 \varepsilon \sigma T_a^3 (T_{soil} - T_a)) \quad (C4)$$

$$Q_{veg} = R_{n0} \quad (C5)$$

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123

732 where the C_G is an empirical coefficient ranging from 0.3 (wet soil) to 0.5 (dry soil)
733 (Idso et al., 1975); R_{n0} is the net radiation assuming T_{soil} equals T_a (W m^{-2}); T_{soil} is the
734 surface temperature of bare soil (K) calculated with the VI-Ts diagram (Appendix F);

Appendix D: determining the aerodynamic and surface resistance of bare soil from satellite data

737

738 The aerodynamic resistance of the bare soil, $r_{a\ soil}$ (m s^{-1}), was calculated by Nishida,
 739 (2003), assuming that the maximum surface temperature of bare soil $T_{soil\ max}$ (K)
 740 occurs when the sum of latent heat flux and the sensible heat flux of the bare soil,
 741 namely, the available energy of bare soil Q_{soil} (W m^{-2}) is used as sensible heat flux and
 742 the latent heat flux is zero:

$$r_{a\ soil} = \frac{\rho C_p (T_{soil\ max} - T_a)}{Q_{soil}} \quad (D1)$$

744 $r_{a\ soil}$ is the aerodynamic resistance of the bare soil, (s m^{-1}), ρ is the air density, kg m^{-3} ;
 745 C_p is the specific heat of the air, ($\text{J kg}^{-1} \text{K}^{-1}$); $T_{soil\ max}$ is the maximum surface
 746 temperature of bare soil (K), calculated by the VI-Ts method in Appendix F, T_a is the
 747 air temperature (K), Q_{soil} is the available energy of bare soil (W m^{-2}).

748 For the calculation of canopy surface resistance of bare soil $r_{c\ soil}$ (s m^{-1}), we
 749 follow the studies of Griend and Owe (1994), and Mu (2007):

$$r_{c\ soil} = r_{tot} - r_{a\ soil} \quad (D2)$$

$$r_{tot} = \frac{1.0}{\left(\frac{T_a}{293.15}\right)^{1.75} \frac{101300}{P}} * 107.0 \quad (D3)$$

752 where r_{tot} is the total aerodynamic resistance (s m^{-1}); $r_{a\ soil}$ is the aerodynamic
 753 resistance over the bare soil (s m^{-1}); P is the atmospheric pressure (Pa), which was set
 754 to 101300 Pa.

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Appendix E: Determining the surface resistance and aerodynamic of a vegetation canopy from satellite data

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759 Jarvis (1976) found that the inverse of surface resistance of the canopy $\frac{1}{r_{cveg}}$ is equal
760 to:

$$\frac{1}{r_{cveg}} = \frac{f_1(T_a) f_2(PAR) f_3(VPD) f_4(\phi) f_5(CO_2)}{r_{cMIN}} + \frac{1}{r_{cuticle}} \quad (E1)$$

762 where r_{cMIN} is the minimum resistance ($s\ m^{-1}$); $r_{cMIN} = 33$ ($s\ m^{-1}$) for cropland and
763 $r_{cMIN} = 50$ ($s\ m^{-1}$) for all other vegetation (Tang, 2009); $r_{cuticle}$ is the canopy resistance
764 related to diffusion through the cuticle layer of leaves ($s\ m^{-1}$). The value used in the
765 Biome-BGC model is $r_{cuticle} = 100,000$ ($s\ m^{-1}$, White et al., 2000), which is used by us.

766 The functions of air temperature T_a , $f_1(T_a)$ and photosynthetic active radiation PAR ,
767 $f_2(PAR)$ can be written as (Jarvis, 1975):

$$f_1(T_a) = \left(\frac{T_a - T_n}{T_o - T_n} \right) \left(\frac{T_x - T_a}{T_x - T_o} \right)^{\left(\frac{T_x - T_o}{T_o - T_n} \right)} \quad (E2)$$

769 where T_n , T_o and T_x are the minimum, optimal and maximum temperature for
770 stomatal activity. According to Tang (2009), $T_n = 275.85$ K, $T_o = 304.25$ K and $T_x =$
771 318.45 K. The function $f_2(PAR)$ is expressed as:

$$f_2(PAR) = \frac{PAR}{PAR + A} \quad (E3)$$

773 where PAR is photosynthetic active radiation per unit area and time ($\mu\ mol\ m^{-2}\ s^{-1}$)
774 calculated by incoming solar radiation multiplied by 2.05 (Campbell and Norman,
775 2000); A is a parameter related to photon absorption efficiency at low light intensity,
776 which was set to $152\ \mu\ mol\ m^{-2}\ s^{-1}$ (Tang, 2009); Nishida (2003) found that in Eq. E1
777 the following functions can be omitted without great loss of accuracy: the functions
778 depending on vapor pressure deficit, $f_3(VPD)$, leaf water potential $f_4(\phi)$ and carbon

779 dioxide vapor pressure, $f_5(CO_2)$.

780 Instantaneous and daily aerodynamic resistance of the canopy $r_{a\ veg}$ ($s\ m^{-1}$) is
 781 calculated by the empirical formulae of Kondo (2000) for forest cover, grassland, and
 782 cropland:

$$783 \quad \frac{1}{r_{a\ veg(forest)}} = 0.008 U_{50m} \quad (E4)$$

784 where U_{50m} is the wind speed at 50 m height above the canopy ($m\ s^{-1}$). The
 785 aerodynamic resistance grassland and cropland is Kondo (2000)

$$786 \quad \frac{1}{r_{a\ veg(grassland \wedge cropland)}} = 0.003 U_{1m} \quad (E5)$$

787 where U_{1m} is the wind speed 1m above the canopy ($m\ s^{-1}$). The wind speed as a
 788 function of the height z , $U(z)$ can be calculated by the logarithm profile of wind. As
 789 the $r_{a\ veg}$ has two variety calculation equations (E4 and E5) in the forest canopy (E4),
 790 grassland and cropland (E5), thus, we used the land cover classes from the yearly
 791 International Geosphere-Biosphere Programme (IGBP) (MCD12C1) to identify the
 792 land cover and choice the different equation of $r_{a\ veg}$. U_{50m} and U_{1m} were calculated by
 793 the logarithm profile of wind:

$$794 \quad U(z) = U_{shear} \ln \left[\frac{(z-d)}{z_0} \right] / k \quad (E6)$$

795 where U_{shear} is the shear velocity ($m\ s^{-1}$); z is the height (m); d is the surface
 796 displacement (m); z_0 is the roughness length, we followed Kondo (2000), set as 0.005
 797 m for bare soil and 0.01 m for grassland; k is the von Karman's constant and set as 0.4
 798 following Nishida (2003). The shear velocity U_{shear} was calculated as:

$$799 \quad U_{shear} = U_{1msoil} \frac{0.4}{\ln \left(\frac{1}{0.005} \right)} \text{ where the } U_{1msoil} \text{ is the wind speed of bare soil at 1 m height}$$

800 ($m\ s^{-1}$), it was calculated as:

$$801 \quad U_{1msoil} = 1/0.0015 r_{a\ soil} \quad (E7)$$

802 The instantaneous air temperature can be calculated by the Vegetation Index-
 803 surface Temperature (VI-T_s) diagram (Nishida et al., 2003) using MODIS
 804 instantaneous surface temperature/emissivity data (MOD11C1) and daily calculated

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805 NDVI as inputs (Appendix F).

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813 **Appendix F Calculating instantaneous air temperature based on the VI-Ts**

814 **diagram**

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816 The calculation progress of instantaneous air temperature is shown in Appendix

817 (a), the scatter plot of vegetation index (VI) versus land surface temperature (Ts) is

818 drawn like Appendix (b). The slope of the warm edge can be calculated according to

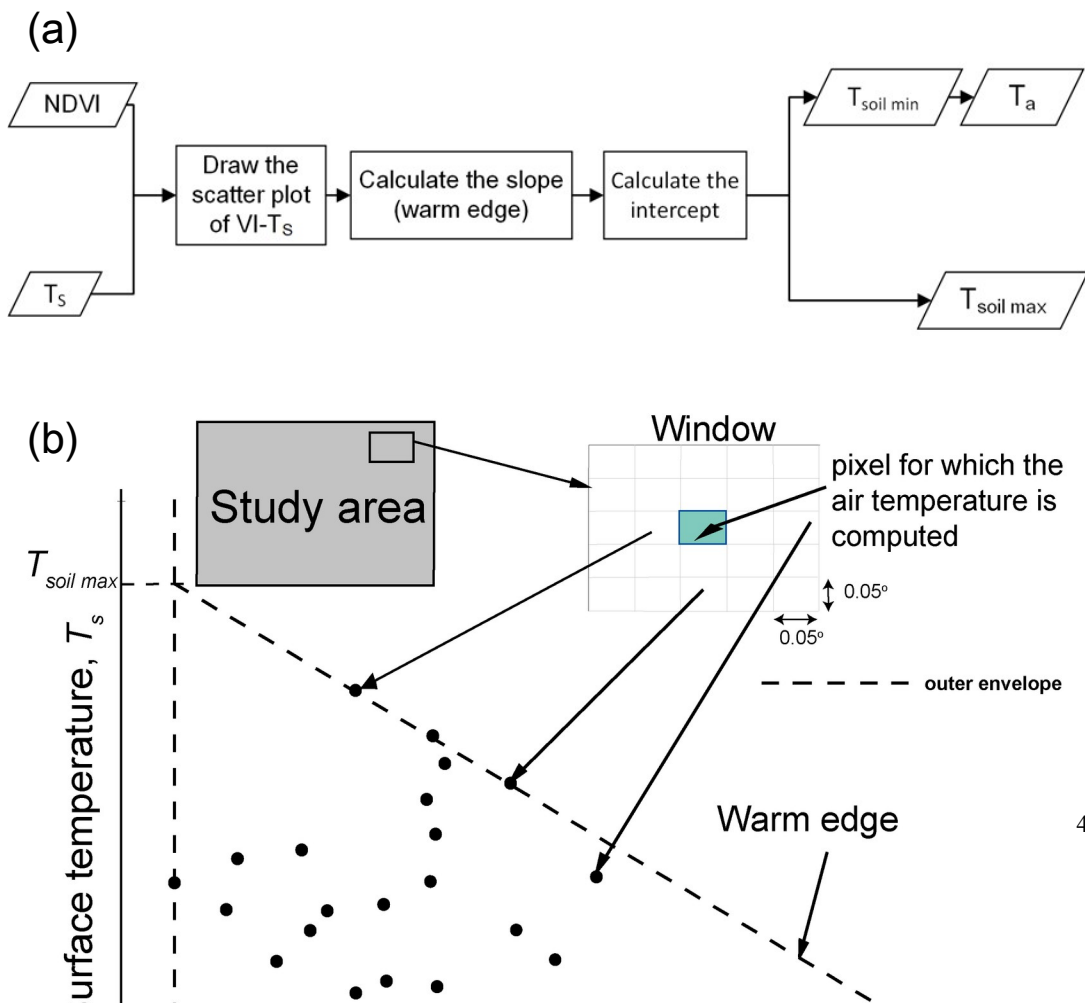
819 the slope and the maximum and minimum NDVI, by which, we can get the $T_{soil\ min}$ and

820 $T_{soil\ max}$ as the intercept of the slope. At last, we assumed that the $T_{soil\ min}$ equals to the

821 instantaneous air temperature T_a^i .

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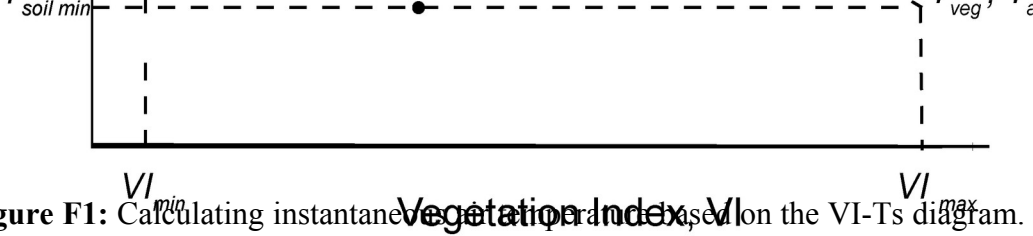
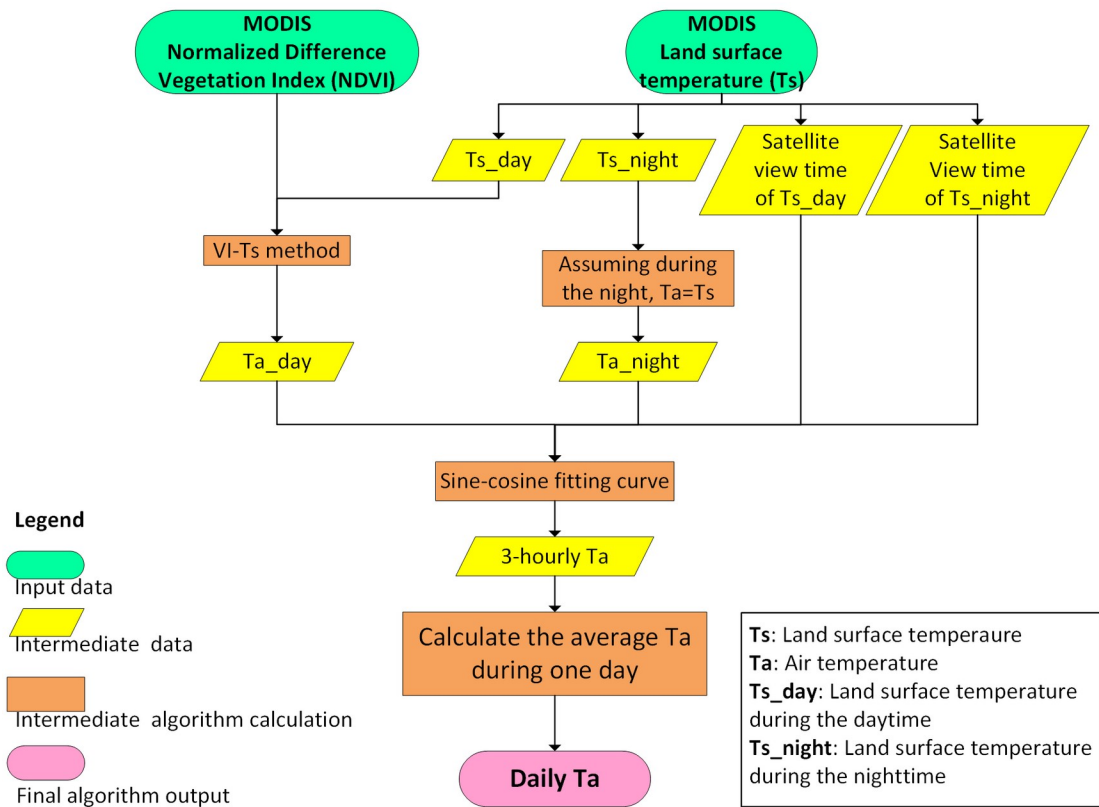


Figure F1: Calculating instantaneous air temperature based on the VI-Ts diagram. (a) is the calculation progress of the instantaneous air temperature and (b) is the scatter plot of the vegetation index and the surface temperature.

Appendix G. The flowchart daily air temperature of calculation

The daily mean air temperature T_a^d (K) was calculated as the average of 8 3-hourly air temperature estimates (Figure G1). These 3-hourly air temperature estimates were interpolated by the instantaneous air temperature T_a^i and the instantaneous night air temperature (which was assumed to be equal to the MODIS land surface temperature during the night) based on a sine-cosine fitting curve.



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845 **Figure G1:** The flowchart daily air temperature of calculation.

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855 **Appendix H: shortwave radiation validation**

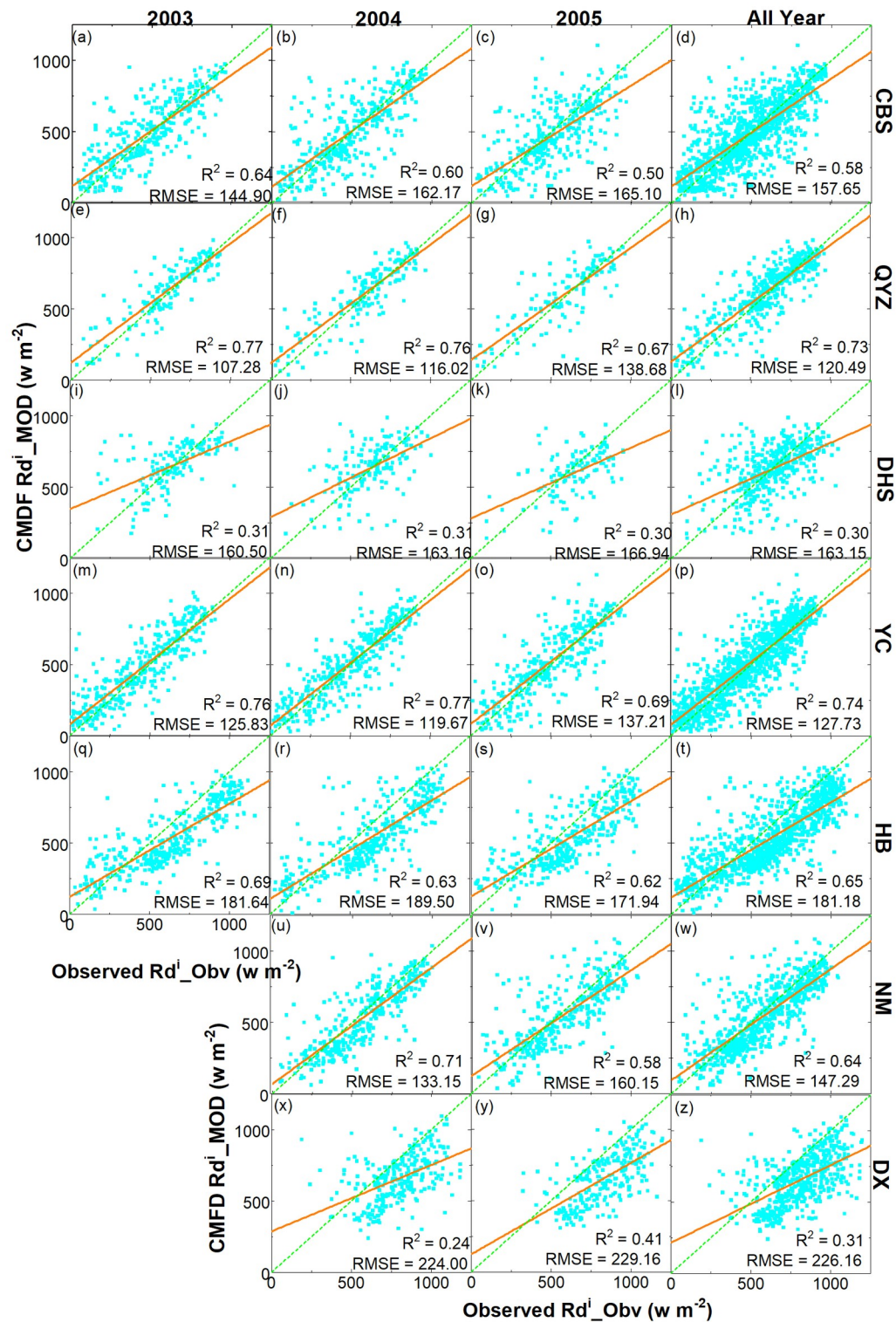


Figure H1. Instantaneous satellite-based shortwave radiation from the China Meteorology Forcing Dataset (CMFD), Rd^i_MOD against flux tower observed instantaneous download, shortwave radiation Rd^i_Obv . From <https://www.spiedigitallibrary.org/journals/Journal-of-Applied-Remote-Sensing/volume-11/issue-02/026019/Evaluation-of-satellite-based-evapotranspiration-estimates-in-China/10.1117/1.JRS.11.026019.full>. Reprinted with permission.

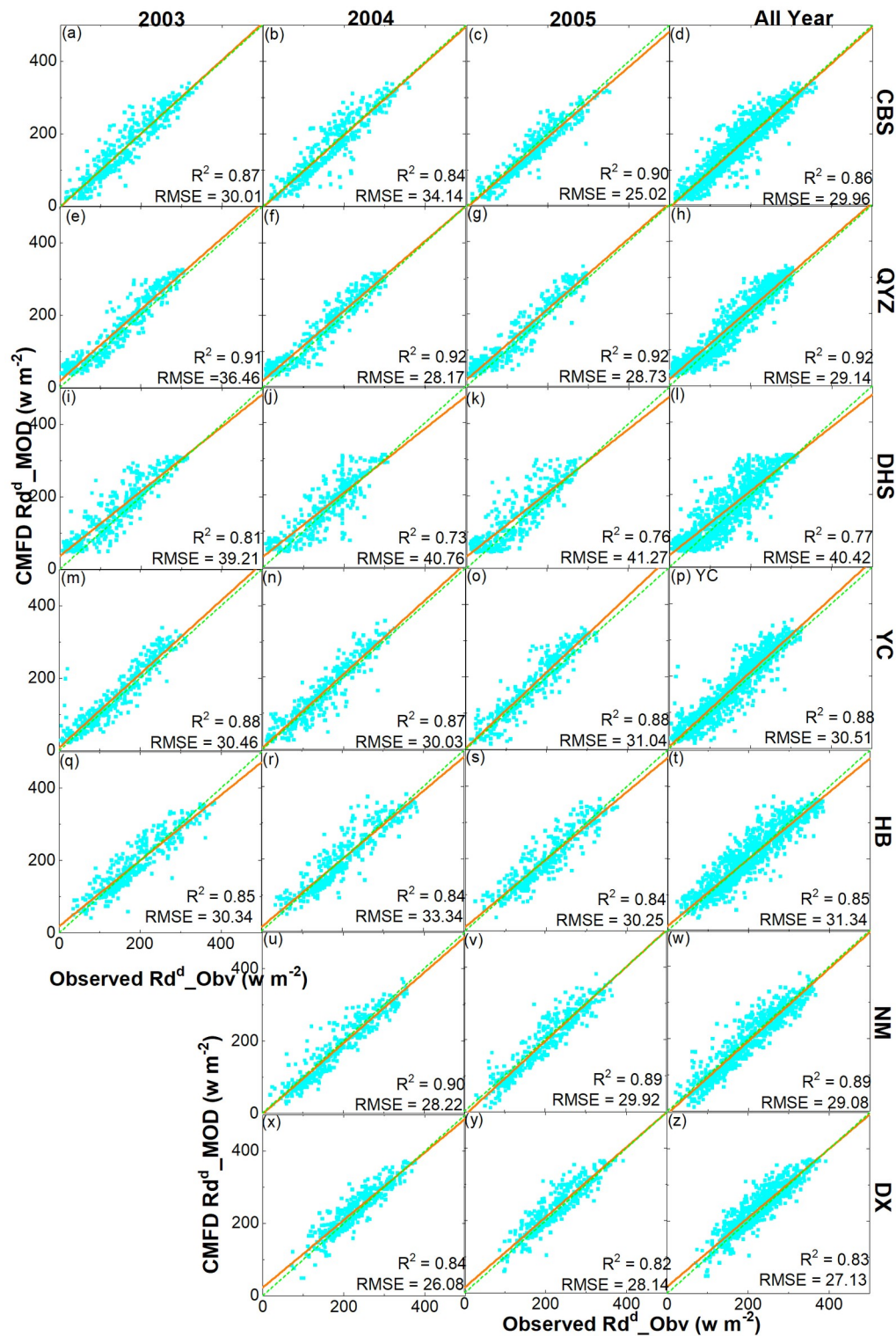
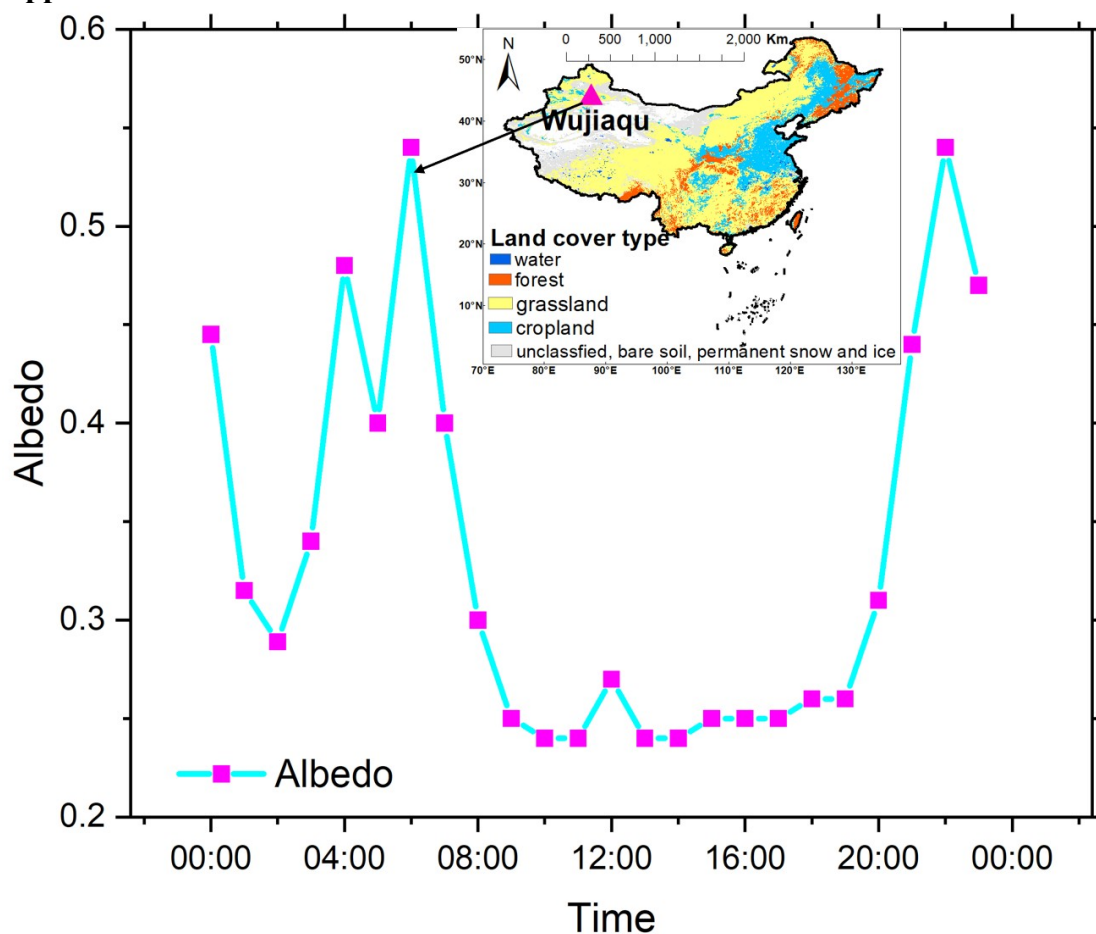


Figure H2 Daily mean download shortwave radiation from the China Meteorology Forcing Dataset (CMFD) Rd^d_MOD against flux tower observed daily mean download shortwave radiation (Rd^d_Obv). From <https://www.spiedigitallibrary.org/journals/Journal-of-Applied-Remote-Sensing/volume-11/issue-02/026019/Evaluation-of-satellite-based-evapotranspiration-estimates-in-China/10.1117/1.JRS.11.026019.full>. Reprinted with permission.

Appendix I: The diurnal variation of albedo



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Figure I: The multimonth averaged observed diurnal albedo during Feb.2 to Dec.27 2020 at Wujiaqu flux tower site.

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