

1 **History-dependent volcanic ground deformation from**
2 **broad-spectrum viscoelastic rheology around magma reservoirs**

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7 **Key Points:**

- 8 • New analytic framework for deformation from pressure forcing of a magma chamber
9 in a viscoelastic crust with temperature dependent viscosity
10 • Analytic transfer function between reservoir pressure and surface deformation depends
11 on frequency, viscoelastic model, and thermal profile
12 • Application of the transfer function reveals history dependence of deformation and elas-
13 tic/viscous transition surrounding magma reservoirs

Abstract

Long-duration, continuous geodetic timeseries suggest that volcanoes exhibit a wide range of deformation patterns that vary between episodes of unrest. Viscoelastic deformation around crustal magma storage zones is an expected contributor to such observations, but is challenging to characterize robustly. Here we present an analytic approach for modeling crustal deformation around magma reservoirs that highlights frequency-domain signatures of viscoelastic response for temperature-dependent crustal rheology. We develop a transfer function that links frequency spectra of chamber pressure to surface displacement, finding that properties of the magmatic system are encoded at periods where geodetic observations are routinely made. Inhomogeneous viscoelastic response is characterized by a frequency-dependent elastic-viscous transition around the reservoir. We explore the consequences of this frequency dependence by examining broadband forcing consisting of multiple impulsive pressurization episodes, and identify a history dependence of volcano deformation in which past activity influences the stress state and surface deformation of future episodes.

Plain Language Summary

Prior to eruption, magma is stored in crustal reservoirs. The mechanical evolution of such magmatic reservoirs can sometimes be inferred from timeseries of surface deformation by invoking deformation models. But such models often exhibit significant non-uniqueness, particularly over long timescales or with respect to spatially variable crustal rock properties. Here we develop a method which considers volcano deformation problem in the frequency rather than time domain. We focus on viscoelastic deformation and demonstrate that surface deformation patterns depend on the frequency of forcing as well as the prior history of deformation in the reservoir. This approach implies that aspects of the mechanical and thermal state of the crust around magma chambers may be encoded in characteristic frequency spectra of surface deformation.

1 Motivation and background

Modeling ground deformation timeseries at active volcanoes is one of the most often used approaches for inferring magma reservoir dynamics (e.g., Fernández et al., 2017; Townsend, 2022), magma properties (Hou Yip et al., 2022), and forecasting eruptions (Kilburn, 2018). While some active volcanoes exhibit deformation patterns that are well-approximated with the simplest of mechanical models for a pressurized magma chamber at depth in an elastic half-space (e.g., Mogi, 1958), additional factors are necessary to explain the spectrum of volcano deformation observed (Biggs & Pritchard, 2017). Crustal mechanical heterogeneity, surface topography and subsurface layering, and multiphase, multicomponent rheology of magma and fluids have been proposed, painting an increasingly complex picture of the shallow crustal magma transport system.

Unfortunately, many of these factors trade off when it comes to their surface expression, particularly because the deep magma flux entering reservoirs is typically unknown. Time-dependent deformation signals are challenging to interpret uniquely as due to rock creep or magma/fluid mass movements. It is an outstanding challenge in volcano geodesy therefore to characterize deformation timeseries in a self-consistent physical framework.

One general approach proposes a frequency dependent rheology of Earth materials (O'Connell & Budiasky, 1978; H. C. P. Lau et al., 2020) to account for the characteristic spectrum of viscoelastic response between post-seismic and isostatic adjustment timescales (Pollitz et al., 2000; Lambeck et al., 2017), as the mechanisms and scales of deformation vary. Here we examine some implications of such a spectral domain perspective on magmatic systems. Under an appropriate description of magma chamber deformation, for example, the factors mentioned above might be viewed as linear or nonlinear spectral 'filters', which modify an input signal

(e.g., a pressurization time sequence) to generate frequency and wavenumber spectra of output signals (e.g., crustal stresses, surface displacement, etc).

We derive an analytic transfer function between magma chamber pressure and maximum surface deformation, confirming the findings of Rucker et al. (2022) that frequency-dependent phase and amplitude are signatures of the viscoelastic filter. These metrics of the transfer function are shown to be sensitive to magma chamber geometry, host rock rheology, and crustal temperature field. This approach establishes a surprisingly simple link between analytic (e.g., Dragoni & Magnanensi, 1989; Segall, 2016) and numerical approaches (e.g., Del Negro et al., 2009; Gregg et al., 2013; Head et al., 2021) to viscoelastic magma chamber models.

We then demonstrate through two volcanologically-motivated examples that viscoelastic host rock response to broad-band magma chamber pressurization leads to history-dependence of surface deformation. This has implications for the interpretation of long volcano deformation timeseries, inference of crustal stress state, and eruption forecasting. We show that the elastic-ductile transition around magma chambers associated with temperature dependence of crust rheology arises via frequency-dependent partitioning of viscous and elastic crustal strains. This implies a spectral framework for investigating trans-crustal magmatic systems via ground deformation that leverages broad spectrum rheological considerations.

2 Frequency domain viscoelastic model for magma reservoir deformation

We consider a spherical magma chamber with radius r_o and depth d in a viscoelastic half space (Figure 1A). The magma chamber has a uniform interior temperature T_{in} . Steady state crustal temperature $T(r)$ is assumed radially symmetric (Figure 1A), determined by two boundary conditions $T(r_o) = T_{in}$ and $T(d) = 0$. This temperature field approximates a crustal geotherm dominated by the thermal perturbation of a magma reservoir, and becomes inaccurate at distances where the radial gradient dT/dr approaches the background vertical gradient. For a magma chamber with interior temperature of 1000–1200°C at depth of 5–10km and vertical geothermal gradient of 20–30°C/km, a radially symmetric temperature profile approximates an extended region above the chamber adequately to a radius equal to the depth for some cases (see Figure S1).

Rheology of the crust is assumed Maxwell viscoelastic, with temperature-dependent viscosity that increases exponentially away from the chamber (Figure 1A and Supplement) (Del Negro et al., 2009; Karlstrom et al., 2010; Degruyter & Huber, 2014). This rheological model has been used extensively in volcano and tectonic geodesy for understanding viscoelastic response (e.g., Tromp & Mitrovica, 1999; Segall, 2010). However it is not unique and likely oversimplifies the parameterization of microscale creep mechanisms that set the relative proportions of recoverable versus non-recoverable strains for given forcing (H. C. Lau & Holtzman, 2019). We use the Maxwell model for demonstrating a theoretical framework that is transparent and simply extended to more complex rheological models.

Mechanical response, such as surface ground deformation, to forcing associated with chamber pressurization is governed by the rheology of the magma reservoir plus crust system. Time-dependent pressure forcing is a boundary condition for radial stress at r_o , which, together with an implicit boundary condition of vanishing displacement at $r = \infty$, predict a unique displacement pattern. An approximate solution for surface displacement is found via first-order correction on the full-space solution to account for stress-free surface conditions (Mogi, 1958; Del Negro et al., 2009). This is accurate so long as chamber radius to depth ratio R/D is sufficiently small (Segall, 2010).

As a starting point for modeling active systems, it is often assumed that the geometry of magma reservoirs is fixed in time and that magmatic forcing arises from magma pressurization relative to lithostatic stress. With these assumptions, viscoelastic deformation around a magma reservoir is a Linear Time-Invariant system (Schetzen, 2003) and can be solved via transfer function in the frequency domain between the unknown forcing function as input sig-

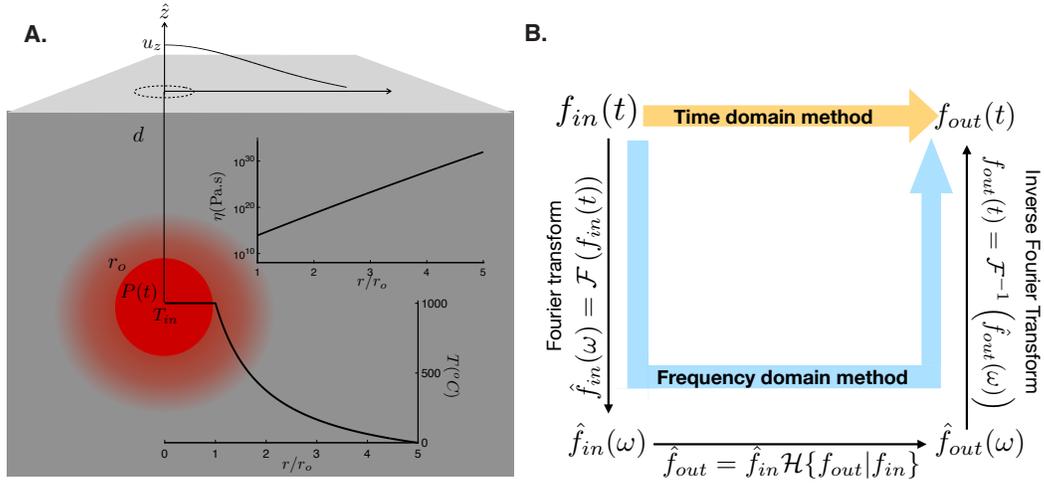


Figure 1. A. Geometry of the model, representative temperature, vertical surface deformation and viscosity profiles. B. Representation of the spectral method and transfer function approach for connecting general input and output signals f_{in} and f_{out} . The input signal is represented either in time domain (t) or frequency domain (ω), hats represent Fourier transform \mathcal{F} . Multiplication by transfer function $\mathcal{H}\{f_{out}|f_{in}\}$ is the frequency domain equivalent of time domain solution to the linear governing equations.

112 nal and any resultant scalar mechanical output such as vertical or horizontal displacement at
 113 a point on the Earth’s surface. Although in general this transfer function can be found numer-
 114 ically (Rucker et al., 2022), we develop an analytic transfer function for the model problem
 115 above (derived in the Supplement) to demonstrate key phenomenological outcomes of broad-
 116 spectrum viscoelastic deformation.

117 The transfer function $\mathcal{H}\{f_{out}(t)|f_{in}(t)\} = \hat{f}_{out}/\hat{f}_{in}$ linearly relates the frequency spec-
 118 trum of an unknown quantity \hat{f}_{out} (i.e., an output signal, where hat signifies Fourier transform)
 119 from the frequency spectrum of an input signal \hat{f}_{in} . This frequency domain method provides
 120 an equivalent approach to time-domain methods for forward and inverse problems (Figure 1B).
 121 While any input or output signals can be used to compute \mathcal{H} , we will assume for illustrative
 122 purposes that the chamber overpressure $P(t)$ relative to lithostatic is a known input signal, and
 123 the maximum surface displacement $u_z(t)$ is the output signal (Figure 1A).

For a spherical magma chamber in an elastic halfspace, the transfer function assuming first-order free surface corrections (McTigue, 1987) may be stated as

$$\hat{u}_z^{el}(\omega) = \mathcal{H}\{u_z^{el}(t)|P(t)\}\hat{P}(\omega) = \frac{r_o^3}{\mu d^2} \frac{3K + 4\mu}{6K + 2\mu} \hat{P}(\omega) \quad (1)$$

124 where superscript *el* refers to linear elastic rheology, μ is shear modulus and K is the bulk
 125 modulus. The elastic transfer function is hence real-valued and independent of frequency. We
 126 are interested in isolating viscoelastic effects, and henceforth normalize transfer functions by
 127 equation 1.

Applying the constitutive relations, boundary conditions, and Fourier transform (supple-
 ment), we obtain the normalized viscoelastic transfer function \mathcal{H} between chamber pressure

and maximum surface displacement

$$\bar{\mathcal{H}} = \frac{\mathcal{H}\{u_z|P\}}{\mathcal{H}\{u_z^el|P\}} = \left(1 - 3r_o^3 \int_{r_o}^{\infty} \frac{dr}{r^4 (iDe(r)/\zeta + 1)}\right)^{-1}, \quad \zeta = \frac{K}{K + \frac{4}{3}\mu}. \quad (2)$$

128 This equation introduces the Deborah number $De(r) = \omega\eta(r)/\mu$, a dimensionless product
 129 of characteristic cyclic strain rate ($\omega > 0$) or inverse period ($\tau = 2\pi/\omega$) associated with
 130 reservoir pressurization, and Maxwell time $\eta(r)/\mu$ that measures the relative importance of
 131 viscous versus elastic response in the system. De varies with space when material properties
 132 η and/or μ vary with space, here due to the Arrhenius relationship between viscosity and tem-
 133 perature (Figure 1A). In general the elastic moduli K and μ also vary with temperature, but
 134 for temperature difference between 0 and $800^\circ C$ K varies by 1% and μ varies by 10% (Bakker
 135 et al., 2016). This is small in comparison to the orders of magnitude of variation in viscosi-
 136 ty, so we assume uniform elastic bulk moduli K and μ to keep the model simple.

137 From equation (2) we see that the normalized transfer function $\bar{\mathcal{H}}$ is a viscoelastic correc-
 138 tion on the elastic displacement. The magnitude of this correction is determined by the spa-
 139 tial structure of Deborah number. If the crust is elastic, the viscosity is infinitely large and $De(r) =$
 140 0 for all frequencies; in this case the normalized transfer function becomes unity.

141 Because crustal magmatic systems are characterized by spatially localized temperature
 142 anomalies, the transfer function defines a localized region of viscous response and implies that
 143 a near-chamber elastic/viscous transition controls viscoelastic deformation. This is the moti-
 144 vation behind magma chamber models that assume a discrete viscoelastic shell of uniform vis-
 145 cosity (Dragoni & Magnanensi, 1989; Karlstrom et al., 2010; Degruyter & Huber, 2014), a
 146 simplification of continuous variation in material properties expected in spatially variable ther-
 147 mal field.

148 We find that the general response of a material with variable viscoelastic moduli can be
 149 precisely represented by that of a discrete and uniform viscoelastic shell with frequency de-
 150 pendent effective viscosity and temperature under monochromatic forcing at period τ . For such
 151 case, the outer radius of the viscoelastic shell R_{eff} defining a transition to elastic response,
 152 the uniform effective temperature T_{eff} and the resulting (constant) Deborah number De_{eff}
 153 associated with viscosity $\eta_{eff}(T_{eff})$ are found by requiring that the transfer function $\mathcal{H}^{eff} =$
 154 $(iDe_{eff} + \zeta)/(iDe_{eff} + \frac{r_o^3}{R_{eff}^3}\zeta)$ matches equation (2). Generic unsteady pressure forcing
 155 can be decomposed into superpositions of such harmonic forcing functions (Rucker et al., 2022).
 156 This result thus provides a bridge between classical analytic models and numerical approaches
 157 for magma chamber deformation.

158 3 Properties of the transfer function

159 Polar decomposition of the complex-valued $\bar{\mathcal{H}}$ calculated by (2) via $\bar{\mathcal{H}} = \mathcal{A}e^{i\varphi}$ allows
 160 for the identification of an amplification factor $\mathcal{A} = |\bar{\mathcal{H}}|$ and a phase delay of $-\varphi$. These quan-
 161 tities completely characterize the transfer function, and provide insight into the frequency de-
 162 pendence of viscoelastic deformation.

163 Both the amplification factor and the phase delay frequency spectra vary with the phys-
 164 ical properties of the system. Figure 2A-B shows dependence on the two parameters control-
 165 ling steady-state temperature of the crust, the chamber temperature and assumed background
 166 thermal gradient (defined using a radius contour associated with chamber depth below surface).
 167 As shown in Figure 2B, \mathcal{A} increases with forcing period due to increasing spatial extent of
 168 viscous response. In contrast, the frequency dependence of the phase lag is non-monotonic (Fig-
 169 ure 2A), and peaks at a value well below the viscous fluid phase lag of $\pi/2$ (Figure 2D). Time-
 170 domain delay between deformation and harmonic pressure forcing increases monotonically with
 171 period (Supplementary figure S5).

172 For short forcing periods, the crust becomes more elastic hence the phase lag decreases
 173 with forcing period. As forcing period $\tau = 2\pi/\omega$ increases, the phase lag reaches a max-

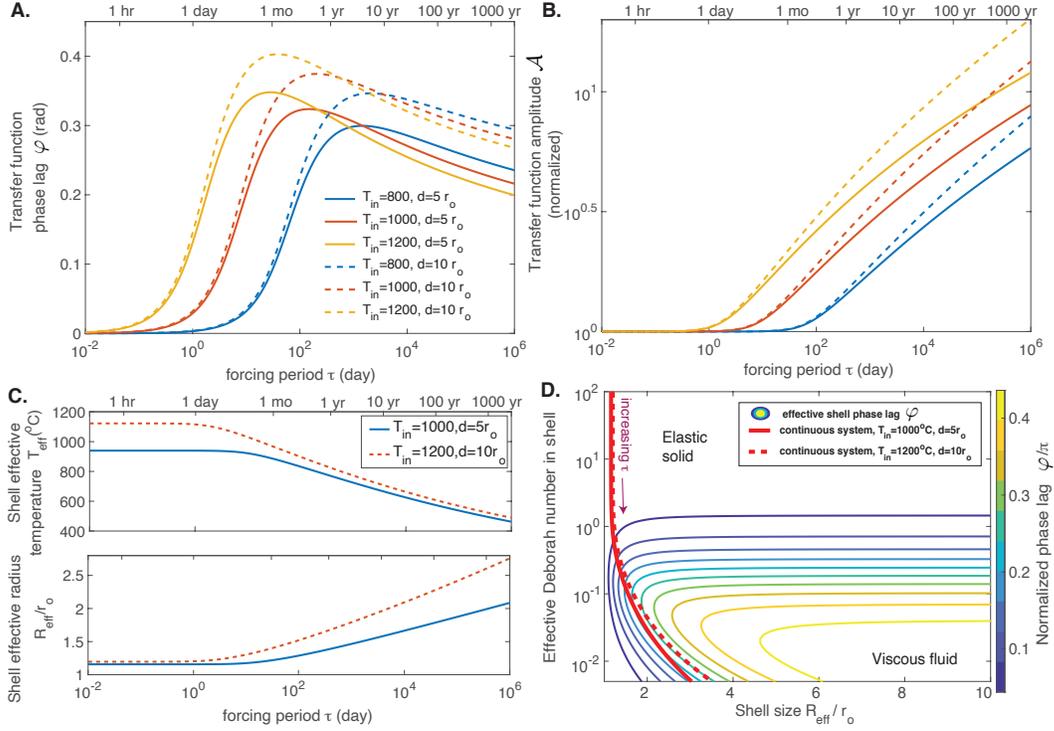


Figure 2. **A.** Phase lag φ and **B.** amplification factor \mathcal{A} of the normalized transfer function $\bar{\mathcal{H}}$ calculated according to equation (2) as functions of harmonic pressure forcing period ($\tau = 2\pi/\omega$), for different chamber temperatures and depths approximated from a thermal model. **C.** Effective outer radius R_{eff} and temperature T_{eff} of equivalent discrete viscoelastic shell for harmonic pressure forcing. **D.** Phase lag φ of the transfer function as function of effective discrete viscoelastic shell radius and Deborah number in the shell (De_{eff} , colored contours). The red curves are trajectories from variable coefficient models shown in (C), illustrating that the radial viscosity profiles result sample a range of phase lags with finite maximum. The viscous fluid limit ($\varphi = \pi/2$) is not reached because viscoelastic relaxation saturates in the variable coefficient system, with effective elastic response observed at small τ and approached as $\tau \rightarrow \infty$.

174 inum and drops to zero as $\tau \rightarrow \infty$. This behavior can be explained by a competition be-
 175 tween spatially confined viscous relaxation and cyclic pressure forcing. The spatial extent of
 176 viscous response R_{eff} is confined near the reservoir by the viscosity profile (set by temper-
 177 ature). As forcing period increases, effective temperature of the shell decreases while R_{eff}
 178 increases (Figure 2C). The timescale for viscoelastic stress relaxation over the shell $\eta_{eff}/\mu(R_{eff}/r_0)^3$
 179 (Dragoni & Magnanensi, 1989) thus increases with forcing period, although shell effective Deb-
 180 orah number is dominated by τ and decreases monotonically. The increase of \mathcal{A} with τ re-
 181 flects viscous strain across the growing shell, with maximum viscoelastic response implicated
 182 by a maximum phase lag φ . For fixed R_{eff} , maximum phase lag occurs where $De_{eff} = \zeta(R_{eff}/r_0)^{-3/2}$
 183 (supplement). Large forcing period becomes an effective elastic system (zero phase lag) with
 184 reservoir radius R_{eff} rather than r_0 (Karlstrom et al., 2010), within which viscous stresses
 185 are uniform. The spatial viscosity structure that gives rise to this behavior, perhaps a defin-
 186 ing feature of magma reservoirs, means that fully viscous crustal response is never realized
 187 in our model (red lines in Figure 2D). As shown in supplement section S1, if host rock vis-
 188 cosity is constant, \mathcal{H} does approach the viscous flow limit at large τ . Of course, at long forc-
 189 ing periods and spatial scales much larger than the reservoir we expect that the vertical vari-
 190 ation in temperature controls viscous response (e.g., Tromp & Mitrovica, 1999) and our model
 191 assumptions are no longer valid. Additional structure in the phase lag spectra may also arise
 192 from details of the problem not modeled here (Rucker et al., 2022). But our analytic model
 193 captures first-order frequency dependence of the reservoir-crust system effective geometry and
 194 bulk rheology on timescales of interest to volcano geodesy.

195 We also see that crustal thermal structure is imprinted on the transfer function. Cham-
 196 ber depth is approximated by the distance d between surface temperature and chamber bound-
 197 ary T_{in} . Larger T_{in} and d generally result in more pronounced phase lag, with chamber tem-
 198 perature being particularly sensitive (Figure 2A, Figure S3), and noting trade-offs in maximum
 199 phase lag between these parameters. Longer forcing periods (lower frequency) require larger
 200 effective shells with smaller effective temperatures. Likewise, a hotter crust requires a larger
 201 effective shell with larger effective temperature. Although not explored here explicitly, the tra-
 202 jectories in Figure 2D show how variable material coefficients and constitutive model inter-
 203 act: in this case, the background thermal field dictates the range of possible Maxwell viscoelas-
 204 tic response for harmonic forcing functions.

205 Of course, the discrete shell equivalence explored in Figure 2 is only precise when the
 206 pressure forcing is sinusoidal in time. For broadband pressure forcing with more than one fre-
 207 quency as will be explored in the next section, there does not exist a set of values (R_{eff}, T_{eff})
 208 that will allow the effective shell to yield the same response for all frequency components.

209 4 Signatures of viscoelastic volcano ground deformation

210 It is useful to demonstrate the utility of the spectral transfer function approach through
 211 application to synthetic time-series that mimic geodetic observations. In this section we show
 212 examples of maximum vertical surface displacement and crustal strains obtained using the spec-
 213 tral method for various pressurization episodes of a subsurface reservoir.

214 4.1 Isolated pressurization events

215 We consider a square pulse forcing time series, pressurizing the chamber for a given du-
 216 ration (episode) above some baseline. This could be considered a simplistic model for a recharge-
 217 driven eruption, for example. Elastic surface displacement would be proportional to this cham-
 218 ber pressure (Segall, 2010), however viscous creep causes the displacement be larger and last
 219 longer in our model (Figure 3a). These differences are directly evident in the displacement fre-
 220 quency spectra (Figure 3a). The transfer function increasingly amplifies the spectra at frequen-
 221 cies with periods longer than the characteristic time of the square pulse in this case. Such frequen-
 222 cy-dependent amplification results in larger displacement and continuing surface deformation af-
 223 ter the end of the episode. Despite the broadband forcing function, viscoelastic response in

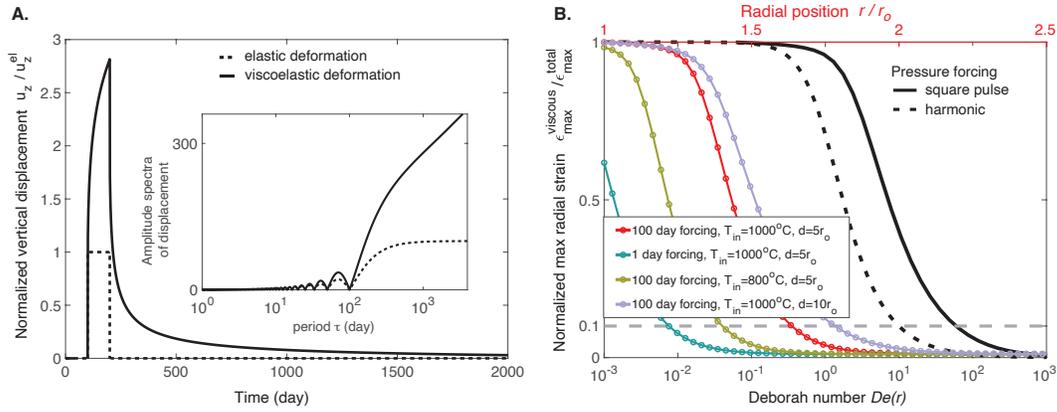


Figure 3. **A.** Maximum vertical ground displacement u_z associated with square pulse pressurization over 100 days with reference viscoelastic parameters (table S1 in Supplementary Material). Dashed lines show the corresponding elastic case. Insert shows amplitude spectra of the normalized displacement obtained from the transfer function as functions of period τ . **B.** Spatial extent of viscous relaxation for square pulse forcing measured by the ratio of maximum deviatoric viscous strain $\epsilon_{max}^{viscous}$ and maximum total deviatoric strain ϵ_{max}^{total} . Horizontal dashed line indicates $\epsilon_{max}^{viscous} / \epsilon_{max}^{total} = 10\%$, an elastic/viscous transition point. The ratio $\epsilon_{max}^{viscous} / \epsilon_{max}^{total}$ is shown as functions of radial position on the top x-axis for different parameters (colored lines and markers). These curves collapse (black curves, bottom x-axis) when plotted against spatially variable Deborah number $De(r)$. The elastic/viscous transition corresponds to $De \approx 65$ for square pulse forcing (solid black curve), compared to $De \approx 10$ for harmonic pressurization (dotted black curve).

224 surface displacement varies with the characteristic time of the pressure forcing: for a rapid pres-
 225 sure forcing event (e.g., a pressurization episode with duration of 1 day), the surface displac-
 226 e-ment is close to the elastic solution. Conversely for longer pressure forcing (e.g., pressuriza-
 227 tion episode of one year), the viscoelastic displacement is amplified and the relaxation spec-
 228 trum exhibits extended temporal lag from input pressure compared with the elastic prediction
 229 supplementary Figure S2).

230 Similar to the harmonic forcing case, the physical origin of this mechanical response can
 231 be understood by examining viscous strain around the chamber and the location of effective
 232 elastic transition. For linear viscoelastic rheology, the deviatoric strain is the sum of an elas-
 233 tic and a viscous component. We calculate the partition of the total viscous deviatoric strain
 234 in space $\epsilon_{max}^{viscous} / \epsilon_{max}^{total}$, which decreases away from the chamber with the background tem-
 235 perature of the crust (Figure 3b colored lines). Viscous relaxation is thus focused around the
 236 chamber, with effectively elastic deformation far from the chamber.

237 We characterize the point where $\epsilon_{max}^{viscous} / \epsilon_{max}^{total} < 10\%$ as an elastic/viscous transi-
 238 tion point for the variable coefficient mechanical response to chamber pressurization. With differ-
 239 ent parameters and different square pulse duration, $\epsilon_{max}^{viscous} / \epsilon_{max}^{total}$ appears to vary spatially (Fig-
 240 ure 3B colored curves, top axis). However, the partition between the viscous and elastic compo-
 241 nents collapses onto a single curve when plotted against local Deborah number (Figure 3B
 242 black solid lines, bottom axis). This data collapse indicates ‘thermorheologically simple’ behav-
 243 ior common in linear viscoelastic systems (Muki & Sternberg, 1961). Rucker et al. (2022)
 244 suggest that the extent of significant viscous strain is characterized by a contour associated with
 245 $De(r) \approx 10$. This is demonstrated for a single frequency forcing in Figure 3B (black dot-
 246 ted line). However, for broadband square pulse pressure forcing, the corresponding transition
 247 boundary is larger, $De \approx 65$ (Figure 3B black solid line).

248 The dependence of transfer function \mathcal{H} on control parameters suggest possible constraints
 249 on thermorheologic and geometrical aspects of the combined magma reservoir-crust system
 250 (defining the top of a transcrustal magma transport network, Sparks et al. (2017)) using fre-
 251 quency domain observations. With background temperature as an example, we see in Figure
 252 2 that the 1200°C chamber always amplifies the elastic displacement more strongly than the
 253 800°C chamber. However, the larger relative phase delay between models switches as forc-
 254 ing period increases. The maximum difference in phase delay between 1200°C chamber and
 255 800°C chamber occurs around 3.8 days (Figure S3). For broadband forcing such as the square
 256 pulse, such signatures imply specific relationships between deformation frequencies.

257 4.2 History dependence in event sequences

258 The frequency dependence of viscoelastic response also implies that sequences of im-
 259 pulsive pressure forcing functions with long period content may exhibit incomplete viscous
 260 stress relaxation and thus impart history dependence to the resulting deformation. We demon-
 261 strate this time-dependent stress build-up by considering vertical ground deformation response
 262 to square pulses of duration t_p in sequence (Figure 4). In the case shown in (Figure 4A), the
 263 repose time t_s (e.g., inter-event or hiatus time) between each pressure pulse increases through
 264 the sequence. The resulting surface uplift consists of repeated episodes, each with a different
 265 peak vertical uplift, despite identical forcing functions. Larger peak displacements occur when
 266 the repose time t_s is less than the pressurization pulse duration t_p . But even for the last event
 267 in the sequence, occurring after a repose time of twice the pulse duration (100 days), there is
 268 amplification relative to an isolated pulse (the amplitude of the first uplift event).

269 We explore this relationship in more detail in Figure 4B using two square pressure pulses,
 270 each with similar t_p but variable t_s . Peak ground deformation relative to an isolated pulse is
 271 greater than 1% even for t_s/t_p of 30 (for example, representing ~ 3 month episodes sepa-
 272 rated by ~ 8 years).

273 This history dependent behavior is connected again to the extent of viscous relaxation
 274 in the crust at the onset of each pressure forcing episode, which involves both the pressuriza-
 275 tion and repose history. For short repose time, the crust does not have sufficient time to re-
 276 lax before subsequent pressurization occurs, hence the pre-stressed crust results in larger dis-
 277 placement at the end of the second pressurization episode. For large t_s , crustal stress relaxes
 278 over a greater range of periods, hence the peak displacement is closer to the previous episode.
 279 For the two square pulse case (Figure 4B), the peak surface uplift in the second episode is al-
 280 ways higher than the peak uplift during the first episode, which corresponds to a zero-stress,
 281 fully-relaxed initial condition. The range of periods for which relaxation can occur is set by
 282 the spectrum of Maxwell relaxation times in the crust, determined by the thermal profile in
 283 our model. The product of forcing function by the transfer function \mathcal{H} at each period deter-
 284 mines its relaxation time.

285 Incomplete relaxation of forcing signals with significant long-period power is thus likely
 286 on timescales of repose times at active volcanoes (e.g., years to centuries). This history de-
 287 pendence implies that the absolute stress state of the crust – a key initial condition for cham-
 288 ber failure or eruption triggering – reflects concurrent magmatism but also magmatic and tec-
 289 tonic history.

290 5 Summary and Implications

291 The generality of the Fourier transform and linear superposition make the spectral method
 292 presented here attractive for studying time-dependent deformation in magmatic systems. This
 293 approach extends commonly used analytic techniques for obtaining viscoelastic solutions from
 294 corresponding elastic solutions (e.g., Dragoni & Magnanensi, 1989; Segall, 2016), as Laplace
 295 transforms (often used, Fung, 1965) and Fourier transforms agree if the imaginary axis is in
 296 the region of absolute convergence of the Laplace transform. As shown in Rucker et al. (2022),

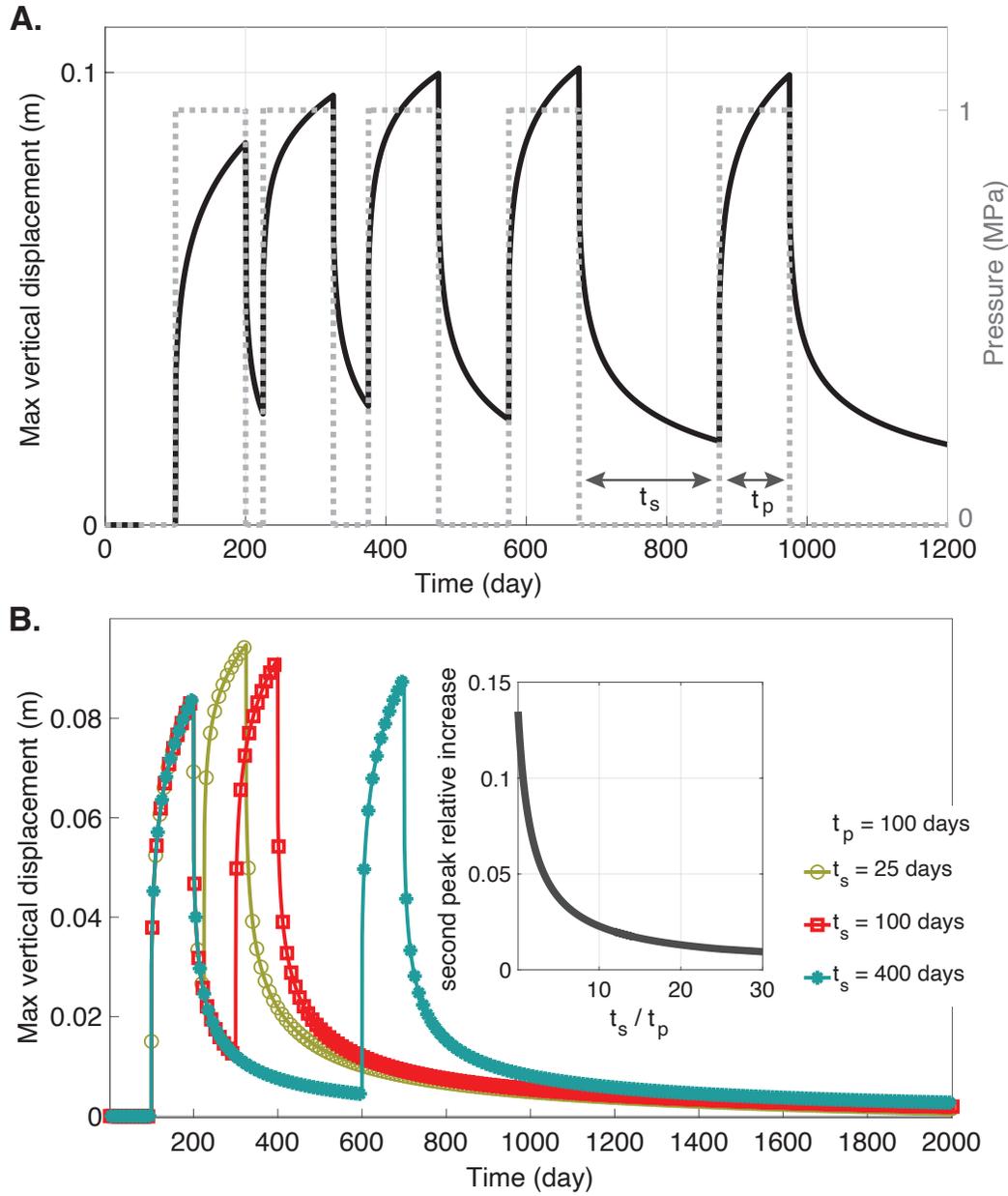


Figure 4. **A.** Maximum vertical ground displacement (solid line, left axis) as a function of time in response to pressure forcing (dash line, right axis) and reference model parameters. Each pressure forcing episode has duration $t_p = 100$ days. The duration of repose time between subsequent pulses are $t_s = 25, 50, 100,$ and 200 days. **B.** Ground displacement from two square pressure pulses with variable repose time t_s . Each pulse has a duration of $t_p = 100$ days. Insert shows the relative increase of the peak uplift in the second episode with regard to the peak uplift in the first episode and decreases with repose time.

transfer functions can be obtained numerically, which allows for arbitrary background thermal and material constant heterogeneity, chamber geometry, topography/layering, and tectonic stresses. The advantage of our analytic approach is its physical transparency and efficiency of implementation. Except in unusual cases (Patrick et al., 2019), pressure itself is an unknown quantity (Zhan et al., 2019; Anderson et al., 2020) so reservoir source-time forcing function as well as the transfer function must be inferred from observations. Multiphase magma mass balance and buoyancy impart additional complexity to viscoelastic deformation in general (Segall, 2019; Sigmundsson et al., 2020).

Of course, quantitative details of our results depend on assumed rheology and thermal structure. Here we use a simple radial temperature profile, which approximates expected steady near-surface gradients (supplementary Figure S1) and localized viscoelastic rheology associated with a thermal boundary layer around the chamber. But as numerical explorations show (e.g., Gregg et al., 2013; Head et al., 2021), spatially complex thermal field and specific form of constitutive model exert significant influence on viscoelastic deformation. Although Rucker et al. (2022) demonstrate that the frequency domain structure of transfer function $\mathcal{H}\{u_z|P\}$ found numerically is qualitatively similar to our analytic results, dependence on the spatial distribution of material parameters, domain geometry, and far-field boundary conditions have yet to be established. Additional time-dependent processes, such as poroelasticity (Liao et al., 2018; Mittal & Richards, 2019; Liao, 2022), likely contribute in some cases and could be incorporated into the spectral method developed here.

A more serious problem with this approach is our assumption of steady state geometry and background temperature. The thermal structure of magmatic systems is not steady state on timescales of magmatic evolution (Karakas et al., 2017). This is implied by active lifetimes of mature volcanic centers (100s kyr for stratovolcanoes, Hildreth, 2007), which is smaller than thermal conduction timescale between depths of magma storage and the surface ($d^2/\kappa \sim 800\text{kyr}$ for $d = 5\text{km}$ and thermal diffusivity $\kappa = 10^{-6} \text{ m}^2/\text{s}$) which provides an upper bound on variants in the thermal field. Temperature anomalies that precede eruptions (Girona et al., 2021) suggest far shorter timescales of thermal transience, mediated by fluid advection. Magma reservoir geometry also evolves on a wide range of timescales (e.g., Rivalta et al., 2019; Neal et al., 2019), although large changes in magma storage geometry may be linked to thermorheologic evolution of the crust (Karlstrom et al., 2017; Colón et al., 2018; Huber et al., 2019). Such temporal variations violate the Linear Time Invariant nature of the transfer functions presented here without generalization of the model. For example, evolution of temperature or other scalar fields in the system would require spectral treatment of a more complete set of governing equations.

These caveats aside, we believe that the frequency domain framework outlined here has potential both for observational validation of viscoelastic volcano models, and for enhancing understandings of the diverse deformation patterns seen at volcanoes globally. To argue the first point, we note that the most significant variation in the transfer function occurs in a range of frequencies (1–100s days) where geodetic observations are increasingly common. By leveraging the full displacement field (not just maximum vertical displacement presented here) we expect that a variety of transfer functions can be posed and validated with geophysical data. As for the second point, we note that the global distribution of active volcanoes represent diverse snapshots of slowly evolving transcrustal magmatic systems. Identifying quantitative ways in which, for example, a thermally immature versus mature volcanic system should deform as a function of frequency provides concrete predictions that can be used to design experiments and link with exhumed magmatic systems in the geologic record.

6 Open Research

The codes for realizing the results are being uploaded to the public data repository Dryad and will be completed upon resubmission. Codes (matlab) for realizing the results are uploaded as supplementary materials for review purpose.

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