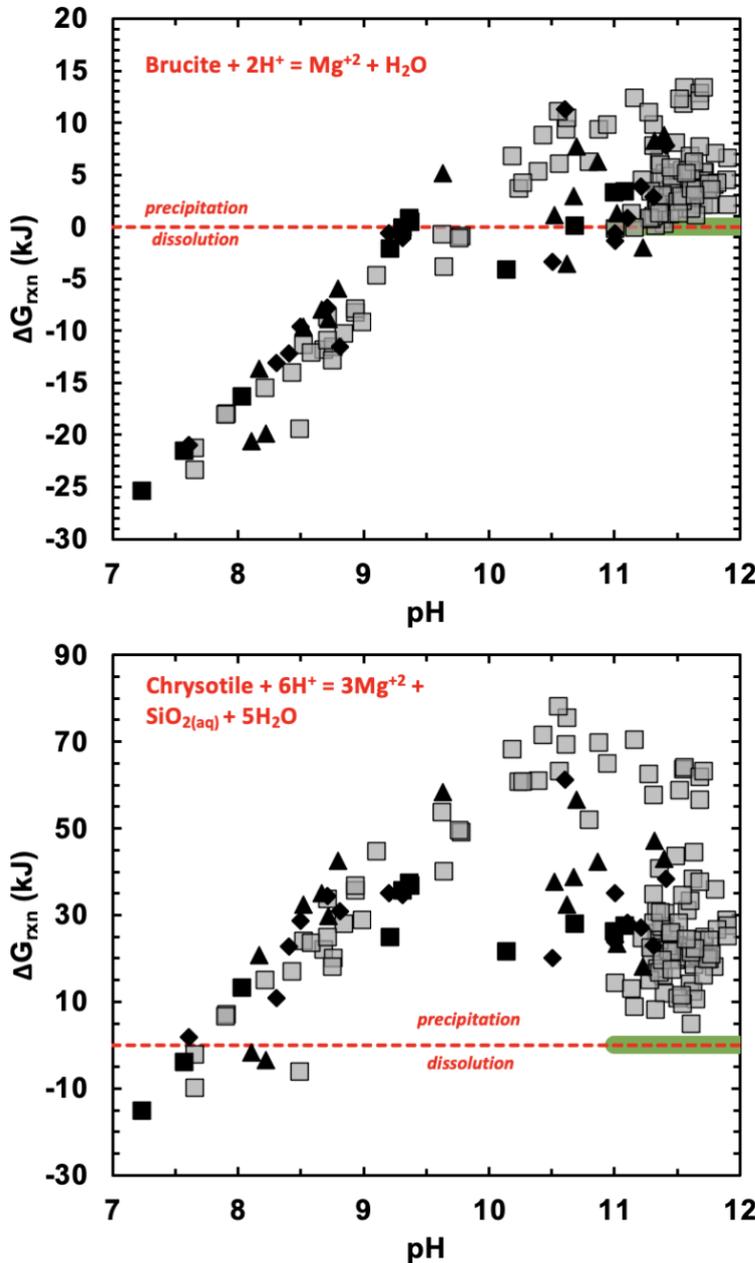


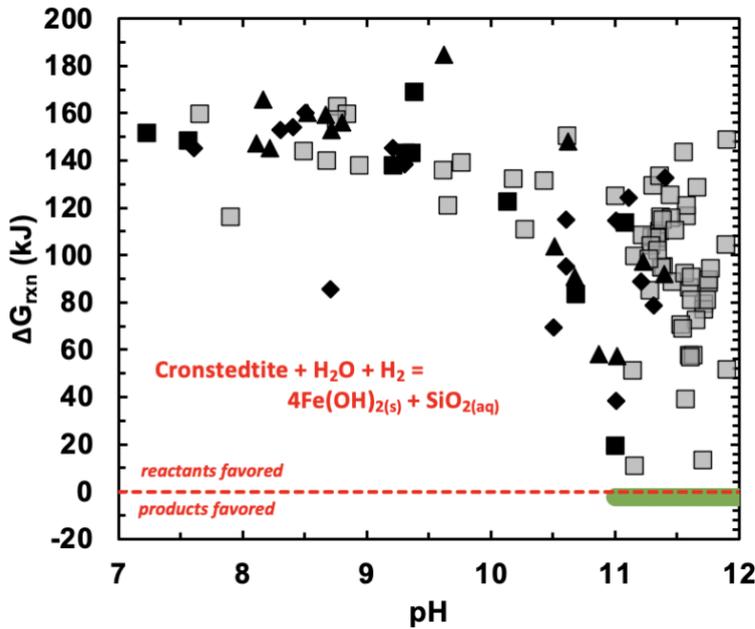
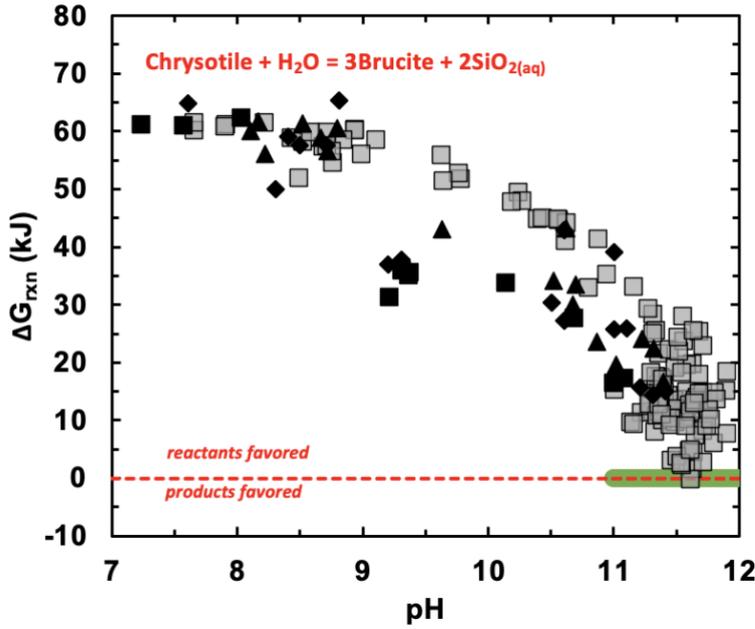
Supplementary Information

Supplementary Section 1: Results of thermodynamic calculations for equilibria involving Oman fluids, serpentine and brucite.

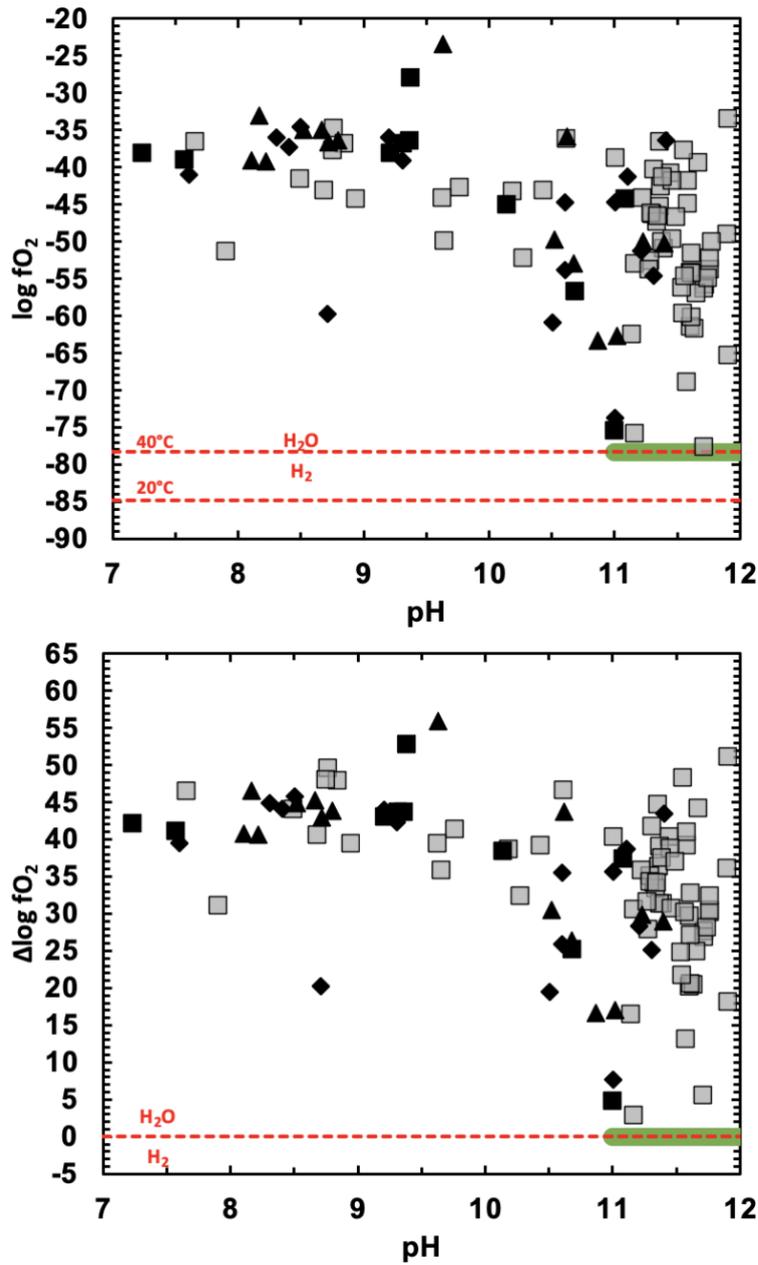


Methods used for these calculations, and general results, are described in the main text, [Section 2.5](#).

**Supplementary Figure S1:** Extent of disequilibrium (in kilojoules per reaction) for the brucite (top panel) and chrysotile (bottom panel) dissolution reactions in various peridotite-hosted Samail ophiolite fluid compositions reported in previous studies. Horizontal green line depicts fluid with pH ranging from 11 to 12, at 40 °C, the pressure of sampling (1 bar for surface samples) and  $f\text{O}_2$  at the  $\text{H}_2\text{O}-\text{H}_2$  stability limit, in equilibrium with chrysotile and brucite. Surface fluids in grey squares: Paukert et al. ([Paukert et al., 2012]), Canovas et al. ([Canovas et al., 2017]), Leong et al. ([Leong et al., 2021]). Borehole fluids in black symbols: diamonds, Rempfert et al. ([Rempfert et al., 2017]); squares, Paukert Vankeuren et al. ([Paukert Vankeuren et al., 2019]); triangles, Nothaft et al. ([Nothaft et al., 2021a; Nothaft et al., 2021b]). Positive  $\Delta G$  indicates that the fluid is saturated in brucite or chrysotile; negative values indicate that the fluid is undersaturated in brucite or chrysotile.

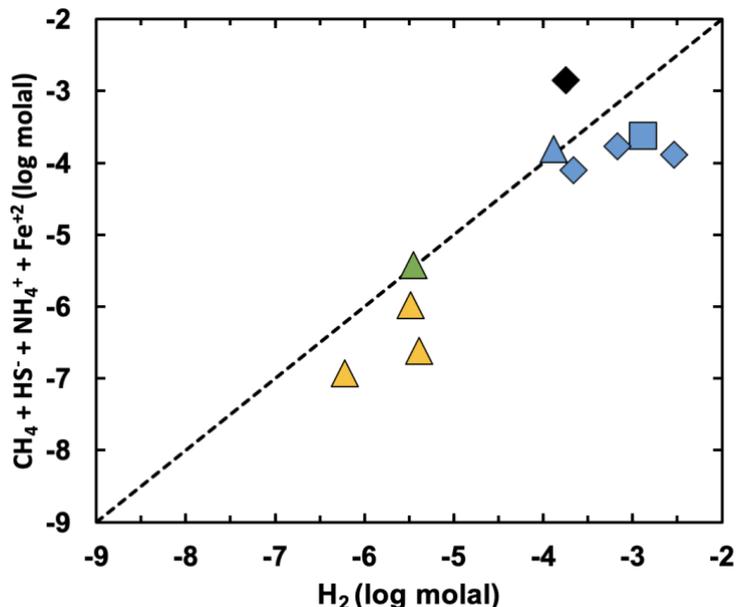


**Supplementary Figure S2: Extent of disequilibrium (in kilojoules per reaction) provided by the serpentine breakdown or brucite silicification (top panel) and brucite oxidation or cronstedtite reduction (bottom panel) reactions in various peridotite-hosted Samail ophiolite fluid compositions reported in previous studies. Data sources and symbols as for Supplementary Figure S1. Positive  $\Delta G$  indicates that SiO<sub>2</sub> in the fluid will react with brucite to form chrysotile or cronstedtite. Thus, brucite is metastable with respect to serpentine in all analyzed fluids from peridotite-hosted alkaline springs and boreholes in the Samail ophiolite.**



**Supplementary Figure S3:** Top panel: Oxygen fugacity ( $f_{O_2}$ ) calculated from measured Eh, pH and temperature of Oman fluids. Bottom panel: Difference in  $f_{O_2}$  from the calculated values in the top panel relative to the  $H_2O$ - $H_2$  limit at 40°C and 1 bar. Data sources and symbols as for Supplementary Figure S1. Based on these estimates, all analyzed fluids from peridotite-hosted alkaline springs and boreholes in the Samail ophiolite are undersaturated in  $H_2$  gas. Indeed, this is consistent with measured dissolved  $H_2$  contents in gas tight borehole samples to date (Hoelher, pers. comm. 2021). However, it is also apparent that some fluid compositions closely approach the  $H_2O$ - $H_2$  limit (on a log scale!), again consistent with some borehole sample data.

**Supplementary Section 2: Concentration of dissolved H<sub>2</sub> in borehole water samples compared to the sum of concentrations of other redox-sensitive solutes**



**Supplementary Figure S4:** Concentration of dissolved H<sub>2</sub> vs the sum of concentrations of all other redox sensitive, dissolved species (CH<sub>4</sub>, HS<sup>-</sup>, NH<sub>4</sub><sup>+</sup>, Fe<sup>+2</sup>) measured in discrete samples recovered from >50 m depth in MBO boreholes. Yellow, green, blue, and black symbols correspond to samples from BA1A, BA1D, NSHQ14 (nearby BA3A), and NSHQ04, respectively. Triangle, diamond, and square symbol represent data from Nothaft et al. [2021a; 2021b], Rempfert et al. [2017], and Paukert Vankeuren and co-workers [Paukert et al., 2012; Paukert Vankeuren et al., 2019], respectively.

**Supplementary Section 3: Propagation of uncertainty for estimates of fO<sub>2</sub> based on measurements of Eh, pH and temperature**

Methods for calculating fO<sub>2</sub> from measurements of Eh, pH and temperature are described in Section 2.6, with results described in the text and illustrated in Figures 24, 28 and 30, as well as Supplementary Figure S3. We developed formalism for propagation of uncertainty for these calculated fO<sub>2</sub> values, which is presented here.

The formal uncertainty of log(fO<sub>2</sub>) and log(fO<sub>2(limit)</sub>) in equations 5 and 6 in the main text can be calculated by assuming that the uncertainty in the measured E<sub>h</sub> (σ<sub>Eh</sub>) was 10 mV, the uncertainty in pH (σ<sub>pH</sub>) was 0.1, the uncertainty in temperature (σ<sub>T</sub>) was 0.05 K, and the uncertainty in pressure (σ<sub>P</sub>) was 5 bars. These were determined by multiplying the manufacturer specifications for uncertainty of the instruments **by a factor of 10** for a conservative estimate of the real uncertainty in the field. These errors were propagated through the calculations above by taking the partial derivative with respect to Eh, pH, T, and P, multiplying by the corresponding uncertainty, and adding in quadrature, i.e.:

$$\sigma_{\log(fO_2)} = \sqrt{\left(\frac{\partial \log(fO_2)}{\partial E_h}\right)^2 \sigma_{E_h}^2 + \left(\frac{\partial \log(fO_2)}{\partial T}\right)^2 \sigma_T^2 + \left(\frac{\partial \log(fO_2)}{\partial pH}\right)^2 \sigma_{pH}^2}$$

$$\sigma_{\log(fO_{2(limit)})} = \sqrt{\left(\frac{\partial \log(fO_{2(limit)})}{\partial T}\right)^2 \sigma_T^2 + \left(\frac{\partial \log(fO_{2(limit)})}{\partial P}\right)^2 \sigma_P^2}$$

Which reduces to:

$$\sigma_{\log(fO_2)} = \sqrt{\left(\frac{20159.1}{T}\right)^2 \sigma_{E_h}^2 + \left(\frac{19174 - 20159.1 E_{measured}}{T^2}\right)^2 \sigma_T^2 + 16 \sigma_{pH}^2}$$

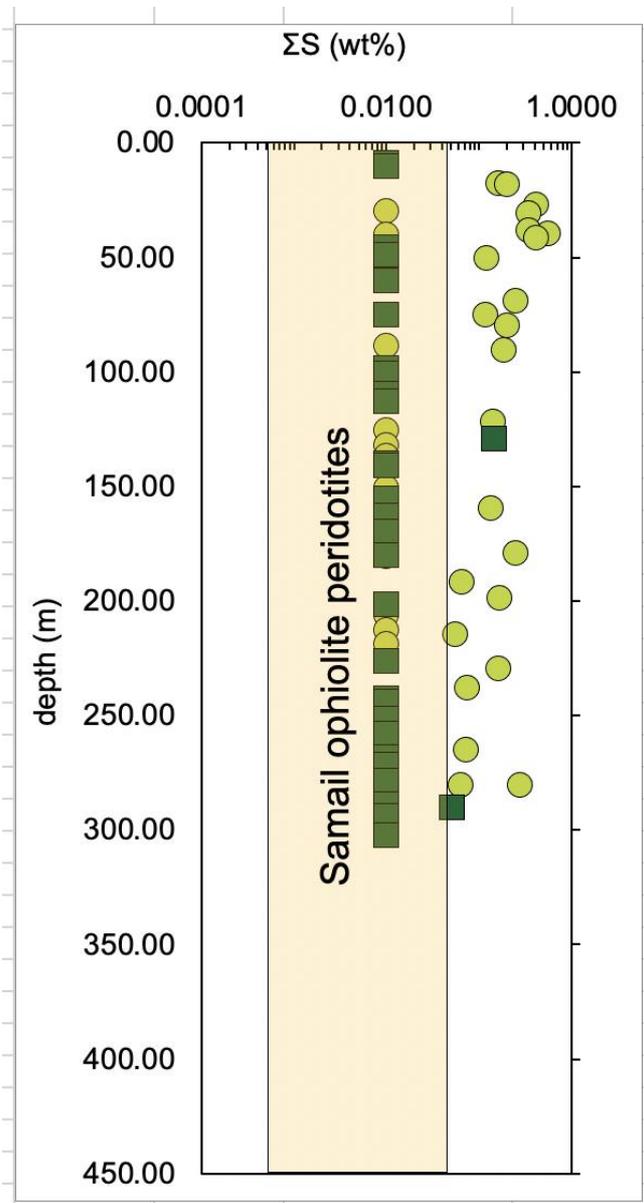
$$\sigma_{\log(fO_2(\text{limit}))} = \sqrt{\left(\frac{29433.8}{T^2}\right)^2 \sigma_T^2 + \left(\frac{-2}{\ln(10)P}\right)^2 \sigma_P^2}$$

Finally, the uncertainty in  $\Delta \log(fO_2) = \log(fO_2) - \log(fO_2(\text{limit}))$  is:

$$\sigma_{\Delta \log(fO_2)} = \sqrt{\sigma_{\log(fO_2)}^2 + \sigma_{\log(fO_2(\text{limit}))}^2}$$

Again, we assumed that actual measurement errors in field conditions were **about** ten times larger than the formal uncertainties arising from formal propagation of the manufacturer-provided uncertainties in measurements. As a result, these calculations yield estimates of uncertainty that are  $\leq \pm 1$  log unit of (fO<sub>2</sub>) in bars. Also, as noted in Section 2.6, the fO<sub>2</sub> values calculated from Eh, pH and temperature measurements should be regarded as approximate because the fluids may contain multiple, redox sensitive solutes that are not in mutual equilibrium. Thus, there are several qualitative elements contributing to the actual uncertainty of the fO<sub>2</sub> estimates. As a result, we have not tabulated or illustrated the specific uncertainties for each fO<sub>2</sub> value. Instead, we infer and illustrate uncertainty bounds of  $\pm 1$  log unit of fO<sub>2</sub> in Figure 30.

#### Supplementary Section 4: Sulfur concentration vs depth in Hole BA4A

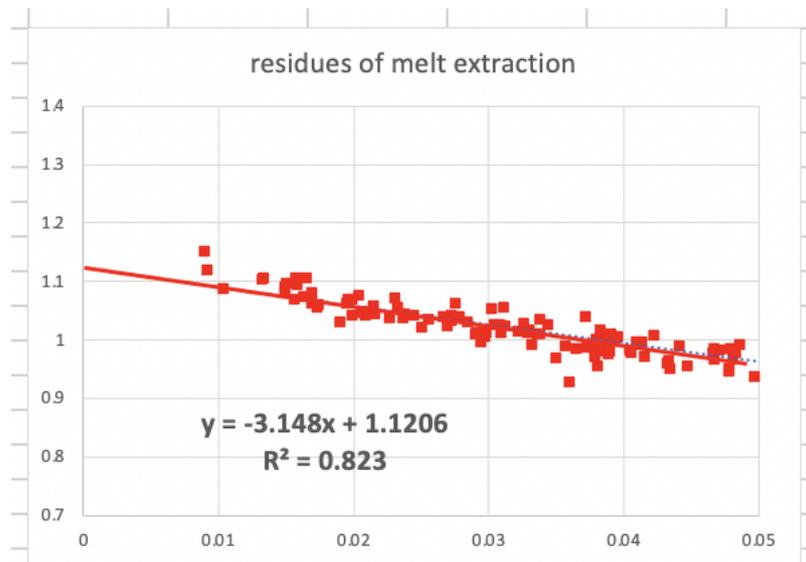


**Figure S5:** Sulfur concentration versus depth in core from Hole BA4A [Kelemen et al., 2021]. Sulfur concentrations below the detection limit of shipboard analyses were assigned a value of 0.01 wt% (100 ppm). Orange bar illustrates previously measured range of sulfur concentration in mantle harzburgites and dunites in the Samail ophiolite, from 5 to 500 ppm [Hanghøj et al., 2010; Oeser et al., 2012]. Dunites: light green circles; harzburgites: dark green squares.

### Supplementary Section 5: Evaluation of the hypothesis that addition of igneous minerals to residual mantle harzburgites produced low Mg/Si at a given Al/Si in core samples from the MBO

As shown in [Figure 26](#) and discussed in [Section 4.3](#) in the main body of the paper, core samples of harzburgite from Holes BA1B, BA3A and BA4A have low wt% MgO/SiO<sub>2</sub> at a given wt% Al<sub>2</sub>O<sub>3</sub>/SiO<sub>2</sub> (hereafter, Mg/Si and Al/Si for brevity) compared to the residues of partial melting and melt extraction from the mantle. The discussion in the main text mentions three possible reasons for low Mg/Si at a given Al/Si in these samples: (1) Mg dissolution and removal from the rocks (2) Si addition, and (3) igneous “impregnation”, for example by crystallization of small amounts of relatively Al-rich, Si-rich, Mg-free plagioclase feldspar in pore space in residual peridotites in the shallow mantle. This section of the Supplementary Information evaluates, and rejects, the third of these hypotheses. We do this primarily graphically, with a minimum of explanatory text.

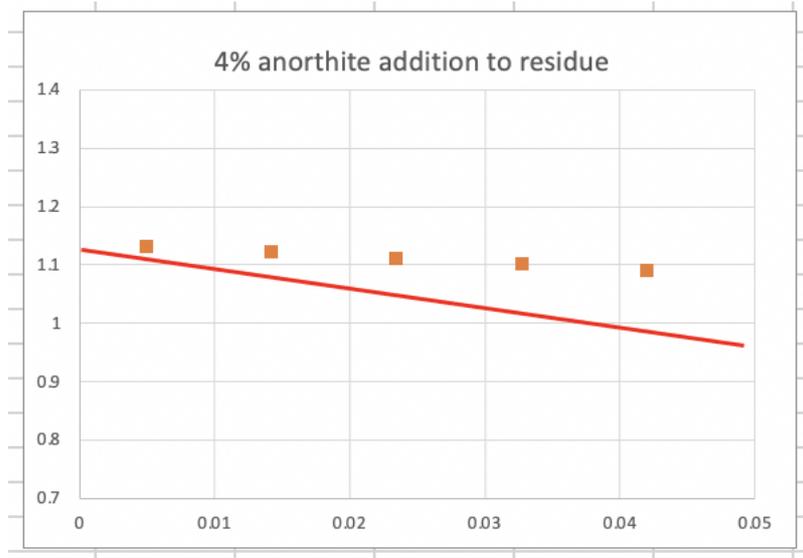
The terms “impregnated peridotite”, “impregnated dunite”, and sometimes (usually, erroneously) “troctolite” are used to refer to rock with added, igneous minerals precipitated during migration of melt through pre-existing, residual mantle peridotites and dunite conduits, as outlined in [Sections 1.2 and 4.1](#) of the main text. 100% crystallization of added melt would produce a geochemical trend more or less identical to the melt extraction trend illustrated by the red symbols in [Figure 26](#). However, commonly the minerals added to impregnated peridotites are “cumulate”, in the sense that they are precipitated by partial crystallization of a melt, after which the remaining melt is removed from the rock. In various cases, the presence of individual minerals (typically, calcium-rich pyroxene, cpx, and/or plagioclase, but in some cases Ca-poor pyroxene, opx), or mixtures of these minerals, are attributed to impregnation.



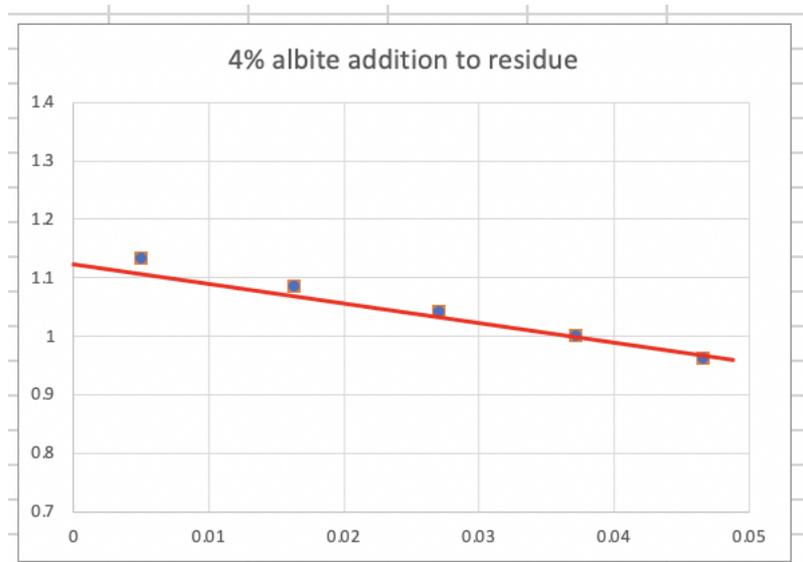
**Figure S6:** For reference the residues of melt extraction from [Figure 26](#) are plotted again here.

As an end-member residual peridotite, we use a harzburgite with 10 wt% opx, 90 wt% olivine, a molar Mg# (molar Mg/(Mg+Fe)) of 0.9, and Al/Si of 0.005 (perhaps with Al in spinel), ~ 42.6 wt% SiO<sub>2</sub>, 0.2 wt% Al<sub>2</sub>O<sub>3</sub>, 9.0 wt% FeO and 48.2 wt% MgO.

The mineral plagioclase is a solid solution primarily composed of end-members anorthite (CaAl<sub>2</sub>Si<sub>2</sub>O<sub>8</sub>) and albite (NaAlSi<sub>3</sub>O<sub>8</sub>). Neither addition of 4 wt% anorthite, nor addition of 4 wt% albite, reproduces the compositions of MBO harzburgites illustrated in [Figure 26](#).

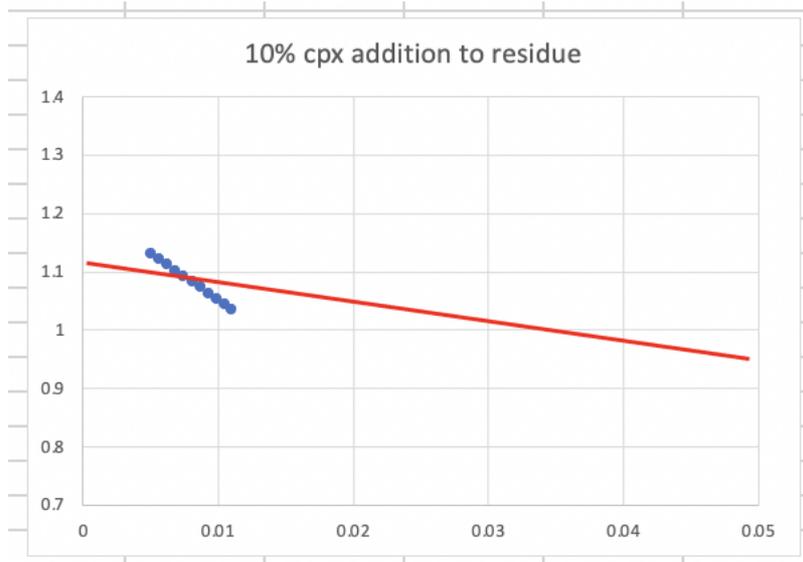


**Figure S7**



**Figure S8**

There are many sources of data on mineral compositions in peridotites from the Samail ophiolite. For brevity and simplicity, here we simply use averages from the extensive data of Monnier et al. [2006]. Neither 10 wt% addition of cpx, nor 10 wt% addition of opx, reproduces the compositions of MBO harzburgites illustrated in Figure 26. Addition of more than 10 wt% either pyroxene would produce CaO and/or SiO<sub>2</sub> concentrations much higher than in most MBO harzburgites, and optically evident, high pyroxene abundances that are not observed in MBO core.

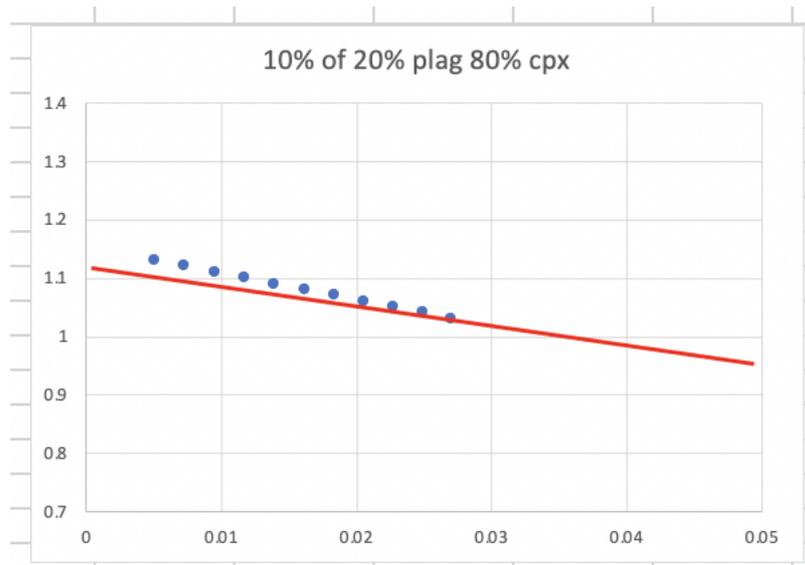


**Figure S9**

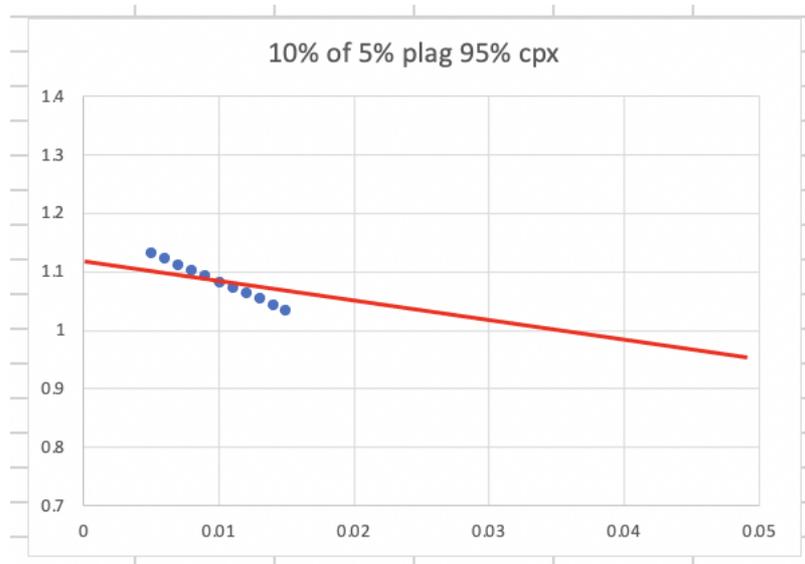


**Figure S10**

We also tested various mixtures of minerals, which also failed to reproduce the compositions of MBO harzburgites illustrated in [Figure 26](#).



**Figure S11**

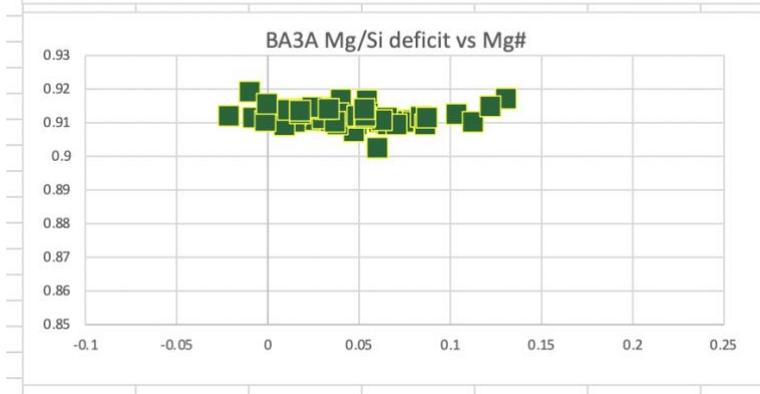
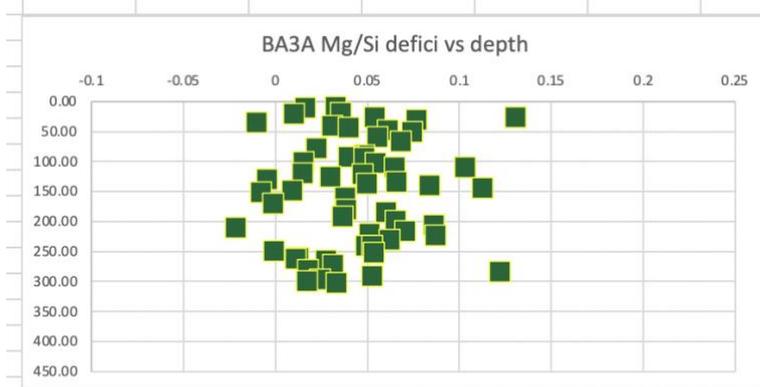
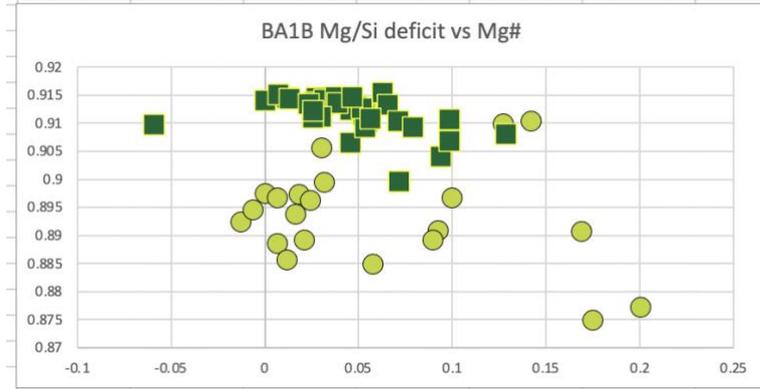
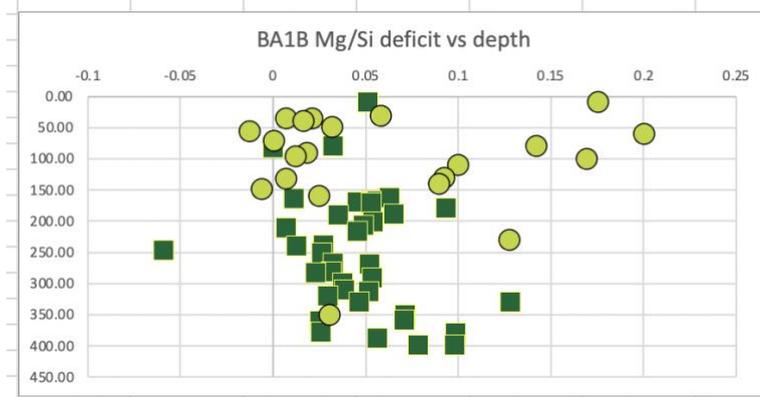


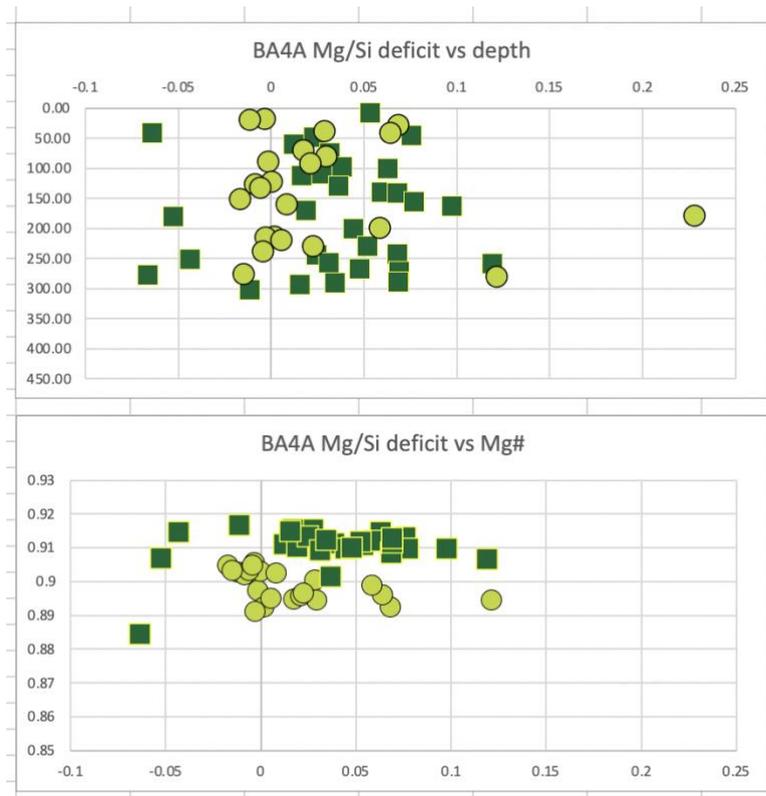
**Figure S12**

As a result of these and several other, related calculations, we conclude that igneous impregnation cannot explain the low Mg/Si at a given Al/Si observed in MBO harzburgites (Figure 26).

#### **Supplementary Section 6: Plots of Mg/Si deficit vs Mg# and depth**

As noted in Section 4.3 of the main text, if the observed low Mg/Si in MBO harzburgites were due to Mg extraction, one would expect to see a correlation between the Mg/Si deficit (equation 9) and Mg# (molar Mg/(Mg+Fe)). In Figure S12, we show that such correlations are not observed, and further that there is no correlation between the Mg/Si deficit with depth in the cored MBO Holes.

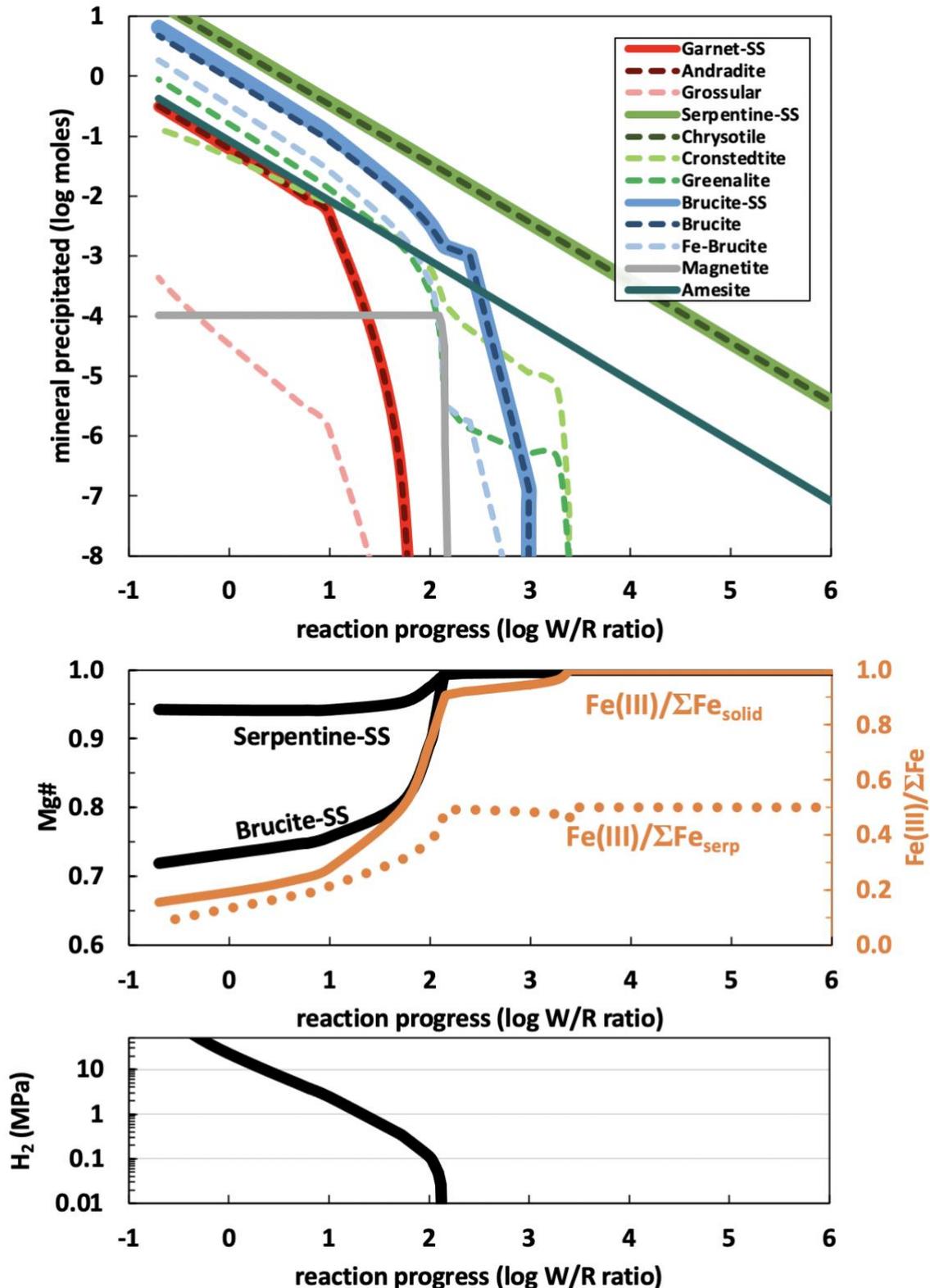




**Figure S14:** Plots of Mg/Si deficit vs Mg# and depth for the three cored MBO Holes.

### Supplementary Section 6: Additional results of reaction-path modeling

Figure 29 in the main text presents results of reaction path modeling at 35°C and 50 MPa. The righthand panels in that figure illustrate results from Step 2 of the modeling, involving reaction of Type 1, Mg-HCO<sub>3</sub> rich waters with peridotite, isolated from the atmosphere, as described in Sections 2.5 and 4.6. Here, in Figure S13, we provide a few more results from Step 2. We invite readers to look at the caption for Figure 29 to aid in understanding Figure S13.



**Figure S13:** Additional results from reaction path modeling at 35°C and 50 MPa, as described in Sections 2.5 and 4.6, and presented in Figure 29. Here we provide some details of phase proportions and compositions, as well as the calculated partial pressure of dissolved H<sub>2</sub> produced in the model. In addition to results described in the text and the caption for Figure 29, the main point to take from this figure is information about the composition of precipitating brucite and serpentine solid solutions. Initially, at water/rock ratios greater than 100, precipitating serpentine is composed almost entirely of (Mg,Fe<sup>2+</sup>)<sub>2</sub>Fe<sup>3+</sup>SiFe<sup>3+</sup>O<sub>5</sub>(OH)<sub>2</sub> - Mg-Fe<sup>2+</sup>-cronstedtite, with molar Mg/(Mg+Fe<sup>2+</sup>), or Mg#, close to 1. With increasing reaction progress, at water/rock ratios less than 100, brucite begins to crystallize, with increasingly large proportions of Fe<sup>2+</sup> (lower Mg#) and no Fe<sup>3+</sup>, while the serpentine solid solution contains increasingly large amounts of greenalite and chrysotile components. Both of these factors lead to increasingly low Fe<sup>3+</sup>/(Fe total) in the crystallizing phase assemblage. Thus, Fe<sup>3+</sup>/(total Fe) in the serpentine solid solution drops by a factor of about 5, and Fe<sup>3+</sup>/(total Fe) in the total crystallizing assemblage drops by a factor of ~ 10. However, meanwhile, the mass of crystallized serpentine + brucite increases by more than a factor of 100 during reaction progress from water/rock ratio of ~ 100 to 10<sup>-0.8</sup>. As a result, as shown in Figure 29, the total amount of Fe<sup>2+</sup> that is oxidized to form Fe<sup>3+</sup> continues to increase throughout the reaction path, together with decreasing fO<sub>2</sub> and an increasing partial pressure of H<sub>2</sub>.

To reiterate, (déjà vu all over again!) the reaction path modeling was done at a pressure 50 MPa, whereas the maximum pressure at the bottom of MBO boreholes is ~ 4 MPa. At 4 MPa and 35°C, the partial pressure of H<sub>2</sub> would not increase above 4 MPa, fO<sub>2</sub> would be limited to a maximum value of ~ 10<sup>-8.3</sup>, but oxidation of Fe<sup>2+</sup> to Fe<sup>3+</sup> would proceed, together with formation of H<sub>2</sub> gas.

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