

Geoengineering's role in reducing future Antarctic mass loss is unclear

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Key Points:

- Idealised geoengineering is unable to prevent significant loss from Antarctica regardless of emissions pathway or year of implementation
- Geoengineering in 2050 under high emissions reduces sea level contribution compared to stabilisation but geoengineering in 2100 increases it
- Surface mass balance gains initially offset loss under stabilisation, but this may be negated in future by accelerating dynamic loss

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Abstract

Using the BISICLES ice sheet model, we compare the Antarctic ice sheet's response over the 22nd century in a scenario where idealised large scale, instantaneous geoengineering is implemented in 2100 or 2050 (geoengineering), with scenarios where the climate forcing is held constant in the same year (stabilisation). Results are highly climate model dependent, with larger differences between models than between geoengineering and stabilisation scenarios, but show that geoengineering cannot prevent significant losses from Antarctica over the next two centuries. If implemented in 2050, sea level contributions under geoengineering are lower than under stabilisation scenarios. If implemented in 2100, under high emissions, geoengineering produces higher sea level than stabilisation scenarios, as increased surface mass balance in the warmer stabilisation scenarios offsets some of the dynamic losses. Despite this, dynamic losses appear to accelerate and may eventually negate this initial offset, indicating that beyond 2200, geoengineering could eventually be more effective.

Plain Language Summary

Sea level will keep rising well into the next century as oceans and ice sheets take decades to respond to atmospheric temperature changes, even if aggressive greenhouse gas reduction policies were immediately implemented. Consequently, geoengineering has been proposed as a more rapid measure. Geoengineering refers to the manipulation the climate system to lessen the impacts of human induced warming. We use an ice sheet model to predict Antarctica's response to geoengineering in 2200, as it is one of the most uncertain sea level contributors. We find that, although the results depend strongly on which climate model is used to drive the ice sheet model, geoengineering cannot prevent sea level contribution from Antarctica. However, implementing geoengineering in 2050 produces smaller sea level rises compared with a scenario where the climate is stabilised in the same year. If geoengineering is delayed to 2100, sea level rise is worse under geoengineering, because stabilising the climate in 2100 creates a warmer climate where the air can hold more moisture, increasing snowfall on Antarctica and offsetting some mass loss. However, stabilising the climate also produces progressively bigger increases in ice discharge compared with geoengineering. This suggests that geoengineering may be more effective in future.

1 Introduction

The Antarctic ice sheet is the largest ice mass on the planet, containing the equivalent of 58m of sea level rise (Morlighem et al., 2020). It is also the most uncertain sea level contributor. Projected sea level contributions for Antarctica from the IPCC Sixth Assessment Report are 0.03-0.27m to 0.03-0.34m for 2100 for the low and high emission scenarios (SSPs: Shared Socioeconomic Pathways) SSP1-2.6 and SSP5-8.5, respectively (IPCC, 2021). Beyond 2100, projections for the ice sheet become even more uncertain, in part due to a relative lack of projections, but also due to remaining uncertainties in ice loss mechanisms, solid earth feedbacks, ice shelf rheology, and others (Bulthuis et al., 2019; Lowry et al., 2021).

An ice sheet's contribution to sea level is dictated by the difference between its surface mass balance (SMB) and ice dynamics. Surface mass balance processes encompass all gains and losses on the ice sheet's surface, including snow deposition, surface melting, runoff, and evaporation, and are primarily controlled by atmospheric changes (Hanna et al., 2013). Ice dynamics refer to losses through the calving and melting of ice shelves into the ocean, and are driven by oceanic changes. The combination of SMB and ice discharge make up an ice sheet's total mass balance. A positive mass balance indicates a net gain in ice mass, while a negative value indicates net mass loss and therefore a contribution to sea level. Currently, mass loss is primarily driven by ocean interactions (Pattyn

67 & Morlighem, 2020). In particular, upwelling of circumpolar deep water (CDW), a water
68 mass over 4°C warmer than the freezing point at the base of an ice shelf, is widely
69 accepted as a key driver of current basal melting in the Amundsen Sea (Jacobs et al.,
70 2011; Pritchard et al., 2012; Rignot & Jacobs, 2002). Understanding the impacts of future
71 climate change is difficult as ocean and atmospheric warming can produce contrasting
72 effects (Payne et al., 2021; Edwards et al., 2021). Ocean warming amplifies mass loss
73 through increased ice discharge, and while atmospheric warming increases the moisture
74 holding capabilities of the air, leading to more precipitation and mass gain, it can also
75 increase ice discharge through melting and runoff, which can lead to ice shelf breakup
76 (Kittel et al., 2020).

77 Even if stringent emissions reduction policies were immediately implemented, sea
78 level rise is projected to continue beyond 2200 due to the delayed response of the oceans
79 and cryosphere to atmospheric temperature changes (climate inertia (IPCC, 2021)). To
80 try and ameliorate some of these lagged climate responses, geoengineering has been pro-
81 posed as a more extreme measure. Geoengineering describes a deliberate modification
82 of the climate system to help mitigate the impacts of anthropogenic warming (Lockley
83 et al., 2020). Geoengineering methods are broadly comprised of two types; carbon diox-
84 ide removal (CDR) and solar radiation management (SRM). CDR removes carbon diox-
85 ide from the atmosphere and stores it in long term sinks, while SRM increase the earth's
86 albedo (Irvine et al., 2018). While SRM does not target the source of anthropogenic warm-
87 ing, its impacts would be felt more rapidly than CDR methods.

88 Geoengineering experiments are essential for understanding whether Antarctic mass
89 losses would be irreversible, and if implementation could prevent the crossing of criti-
90 cal thresholds such as the initiation of marine ice sheet instability (MISI). MISI refers
91 to the mechanism by which marine ice sheets could rapidly retreat via a destabilising
92 of their grounding lines (Weertman, 1974). It can only occur in marine ice sheets where
93 the bedrock in the interior is more depressed than the coasts, resulting in a retrograde
94 slope (Pattyn & Morlighem, 2020). If an ice shelf thins, its buttressing capabilities on
95 the ice sheet are reduced, accelerating ice flow and causing grounding line retreat (Schoof,
96 2007). As ice flux is a function of ice thickness at the grounding line, the retreat of the
97 grounding line to deeper portions of the bed leads to a higher ice flux (Weertman, 1974).
98 This creates a positive feedback of mass loss which can only be stabilised when the bed
99 slope reverses or buttressing increases (Weertman, 1974; Gudmundsson, 2013).

100 Few studies have been done regarding geoengineering's impact on Antarctic mass
101 loss. Garbe et al. (2020) show with equilibrium experiments that regrowth of the Antarc-
102 tic ice sheet is much slower than deterioration (i.e. hysteresis), suggesting slow imple-
103 mentation of CDR may be ineffective. DeConto and Pollard (2016) showed that for high
104 emission scenarios, implementing CDR in 2500 could reduce the sea level contribution
105 from Antarctica more effectively than a natural reduction of CO₂ begun in the same year,
106 but sea level rise remained very high: at 9.55m and 4.7m for high and mid emissions sce-
107 narios, respectively, even after 5000 years. These experiments were limited in scope, how-
108 ever, with a very late drawdown of CO₂, no ocean cooling, and were driven by a model
109 that includes a mechanism of sustained ice front retreat known as marine ice cliff insta-
110 bility (MICI) and thus loses ice more rapidly than other models (IPCC, 2021, 2019). Sutter
111 et al. (2023) find that SRM cannot prevent a collapse of the West Antarctic Ice Sheet
112 under a high emissions scenario due to committed warming in the Southern Ocean, but
113 that under a mid emission scenario, if implemented by mid century, collapse could be
114 prevented.

115 Under an earlier application of CDR, DeConto et al. (2021) still show sustained
116 sea level contribution from Antarctica. They see a distinct increase in contribution be-
117 tween CDR deployment in 2060 and 2070, suggesting the existence of a critical thresh-
118 old of ice sheet loss. The authors attribute this to marine ice instabilities being triggered

119 due to the deterioration of ice shelves that cannot recover, even with rapid CDR, due
120 to the ocean’s slow response time.

121 Here, we also perform idealised CO₂ drawdown experiments to mimic an instan-
122 taneous application of geoengineering, but using an ice sheet model that does not invoke
123 MICI processes. We compare the Antarctic ice sheet’s response to a scenario where ide-
124 alised, large scale CDR is immediately implemented in either 2100 or 2050 by instantly
125 returning the climate to present day forcing, with ones where the climate is held con-
126 stant in the same year. In doing so, we aim to improve understanding of reversibility and
127 long term commitments of mass loss from Antarctica.

128 **2 Methods**

129 **2.1 The BISICLES ice sheet model**

130 This study used the Berkeley Ice Sheet Initiative for Climate at Extreme Scales (BISI-
131 CLES) (Cornford et al., 2013). This model was chosen due to its adaptive mesh refine-
132 ment capabilities, allowing it to better capture ice dynamics around grounding lines and
133 ice streams. Modelling ice sheets requires fine spatial resolution (<1km) for these pro-
134 cesses, but as interior changes are slower and on larger spatial scales, they do not require
135 such high resolution. By using adaptive mesh refinement, high resolution is only used
136 where it is necessary, reducing computational costs and allowing more simulations. Here,
137 we apply a finest spatial resolution of 1km, reducing down to 8km in the interior.

138 **2.2 Forcing scenarios**

139 This work is based on extending Antarctic projections from the Ice Sheet Model
140 Intercomparison Project for CMIP6 (ISMIP6), which compared a range of stand-alone
141 ice sheet models to provide the most up to date understanding of ice sheet response to
142 the climate system for the Climate Model Intercomparison Project Phase 6 (CMIP6) (Nowicki
143 et al., 2016; Seroussi et al., 2019; Payne et al., 2021; J. O’Neill et al., 2024). Five exper-
144 iments (experiments 5-8 and B7) were chosen to extend beyond 2100 from O’Neill et al.
145 (2024). Three experiments are high emission scenarios under RCP8.5, and use GCMs
146 NorESM1-M (*NorESM1 8.5*), MIROC-ESM-CHEM (*MIROC 8.5*) and CCSM4 (*CCSM4*
147 *8.5*). The other two experiments are low emission scenarios forced by NorESM1-M un-
148 der RCP2.6 (*NorESM1 2.6*) and CNRM-CM6-1 under SSP1-2.6 (*CNRM 1-2.6*). These
149 GCMs were selected for ISMIP6 via a thorough analysis process (Barthel et al., 2020),
150 based on their ability to simulate present day Antarctic climate, in addition to sampling
151 a range of atmospheric and ocean forcings, and the availability of both RCP8.5 and RCP2.6.
152 CNRM was selected due to availability only, to provide an additional low forcing scenario
153 (Payne et al., 2021).

154 The ice sheet model experiments were driven by both atmospheric and ocean forc-
155 ing, both of which were provided by ISMIP6 directly from GCM output. The atmospheric
156 projections consist of yearly SMB and surface temperature anomalies relative to a ref-
157 erence period of January 1995 to December 2014. Oceanic projections consist of ther-
158 mal forcing anomalies (calculated from temperature and salinity) relative to 1995-2014,
159 which were then added to an observed climatology (1995-2017) in order to calculate basal
160 melt rates using the ISMIP6 melt parameterization (Jourdain et al. (2020)).

161 Climate forcings were extended beyond 2100 to 2200 by either repeating the cli-
162 mate forcing between 2091-2100 (simulating a stabilisation scenario with no geoengineer-
163 ing), or instantly returning to present day forcing of 2015-2024 (simulating an instant,
164 large scale geoengineering application scenario). A second set of scenarios was generated
165 using the same method but extending the climate forcing from 2050, to understand the
166 effects of an earlier geoengineering implementation. In this case, the repeated time pe-

167 riod for the stabilisation scenario was 2051-2060. We refer to these as the 2100/2050 sta-
 168 bilisation and geoengineering scenarios, respectively.

169 3 Results

170 3.1 Total sea level contribution

171 Figure 1 shows the projected Antarctic sea level contribution for all experiments.
 172 Total sea level contribution is the change in volume above flotation (VaF) for grounded
 173 ice, calculated by

$$V_{af} = \left(\min((Z - S), 0) \times \frac{\rho_{ocean}}{\rho_{ice}} + H \right) dx dy$$

174 where Z is topography, S is sea level, $\rho_{ocean} = 1028 \text{ kg m}^{-3}$ and $\rho_{ice} = 910 \text{ kg}$
 175 m^{-3} are the densities of ocean water and ice respectively, and H is ice thickness. Table
 176 B1 summarises the projected changes for key variables at 2200 relative to 2012 for all
 177 experiments.

178 Regardless of scenario, Antarctica will contribute considerably to sea level rise over
 179 the next two centuries: up to 172mm. There is no clear distinction between high and low
 180 emission scenarios, with a large range in sea level contributions between models for the
 181 same scenario, indicating that the results are highly model dependent (Figure 1). For
 182 instance, in the 2050 scenarios, *NorESM1 2.6* stabilisation has a sea level contribution
 183 almost 70mm higher than *CCSM4 8.5* stabilisation.

184 Under RCP2.6/SSP1-2.6, geoengineering results in marginally lower sea level con-
 185 tributions than stabilisation for both 2050 and 2100 implementation. The difference in
 186 sea level contribution between the models' geoengineering and stabilisation scenarios (G-
 187 S difference) is smaller for the 2100 scenarios (<1-4mm) than the 2050 scenarios (3-11mm,
 188 B1).

189 The 2050 RCP8.5 scenarios show that, with the exception of *CCSM4 8.5*, geoen-
 190 gineering would result in a smaller sea level contribution than stabilisation. For *CCSM4*
 191 *8.5*, geoengineering increases sea level by 2200, though the trajectory indicates that there
 192 may be recovery in future decades (Figures 1 and B1). G-S differences are higher than
 193 for low emissions, between 14-24mm (Figure B1).

194 The 2100 RCP8.5 emission experiments have more disagreement between models
 195 on the effectiveness of geoengineering. Geoengineering has a higher sea level contribu-
 196 tion than stabilisation for *NorESM1 8.5* and *CCSM4 8.5* by 2200. However, both geo-
 197 engineering trajectories appear to slow, while the stabilisation scenarios accelerate, sug-
 198 gesting that post 2200, geoengineering could eventually be more effective, with their G-
 199 S differences peaking and beginning to decrease (Figure B1). *MIROC 8.5* also initially
 200 shows a higher sea level contribution under geoengineering, but this reverses in ~ 2185 .
 201 *CCSM4 8.5* has a much larger G-S difference than the other two models.

202 In the following two sections, the two components that make up total sea level con-
 203 tribution (SMB and ice dynamics) are discussed.

204 3.2 Surface Mass Balance

205 Table B1 shows the integrated SMB sea level contribution in 2200. Values are neg-
 206 ative as the data is shown in terms of sea level contribution. As with total sea level con-
 207 tribution, there is overlap between RCP8.5 and RCP2.6/SSP1-2.6 scenarios and a large
 208 spread in model projections. *NorESM1* consistently shows the weakest increases in SMB.

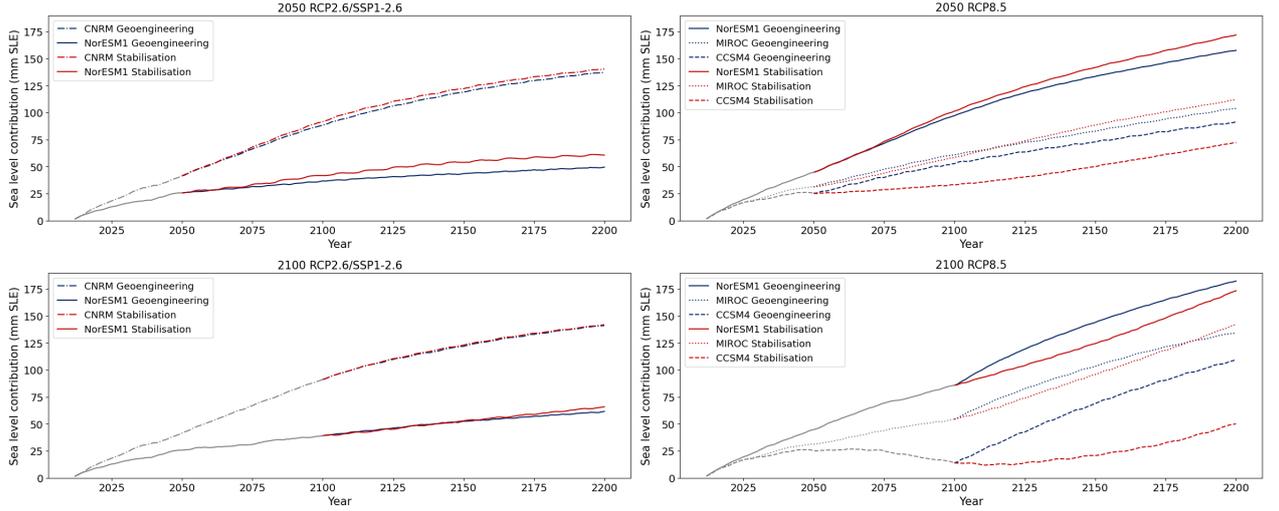


Figure 1. Total sea level contribution relative to 2012 shown in SLE (mm) for 2050 (top) and 2100 (bottom) for RCP2.6/SSP1-2.6 (left) and RCP8.5 (right) emission scenarios. Line types show different model experiments. *NorESM1*: solid line, *MIROC*: dotted line, *CCSM4*: dashed lined, *CNRM*: dash dotted line. Red lines indicate stabilisation scenarios, blue lines indicate geoengineering scenarios.

209 Figure 2a-d shows the G-S differences for SMB. Under low emissions, *CNRM 1-*
 210 *2.6* shows that geoengineering results in smaller SMB gains (negative G-S difference).
 211 In contrast, *NorESM1 2.6* has higher SMB under geoengineering for the 2050 scenario
 212 (positive G-S difference) and a negligible difference for the 2100 scenario. All show smaller
 213 G-S differences and the largest differences are between the models themselves.

214 All high emission simulations show smaller SMB gains under geoengineering than
 215 stabilisation. SMB gains and G-S differences are larger in the 2100 simulations. The 2100
 216 scenarios also have a clearer distinction between geoengineering and stabilisation as there
 217 is no overlap between scenarios. *CCSM4 8.5* has the strongest SMB response, showing
 218 the largest gains for both the 2050 (991mm) and 2100 (1116mm) experiments under sta-
 219 bilisation, as well as the largest G-S differences (85mm and 156mm).

220 3.3 Ice Dynamics

221 Estimates of ice dynamics sea level contribution were calculated by subtracting the
 222 integrated SMB from the total sea level contribution, to better understand changes in
 223 Antarctic ice sheet volume not directly due to SMB. This calculation produces an ice
 224 dynamics contribution that can be attributed to both grounding line retreat and increased
 225 flux across across the grounding line.

226 Figure 2 (panels e-h) shows the G-S differences for ice dynamics. Under RCP2.6/SSP1-
 227 2.6, *NorESM1 2.6* has negligible G-S differences for both 2050 and 2100 scenarios. *CNRM*
 228 *1-2.6* has G-S differences of 18mm and 14mm respectively, with geoengineering produc-
 229 ing a smaller sea level contribution from ice dynamics than stabilisation. Both models
 230 have higher ice dynamics contributions for the 2100 experiments (Table B1).

231 Under RCP8.5, geoengineering results in smaller ice dynamics sea level contribu-
 232 tions, whether implemented in 2050 or 2100, shown by the negative G-S differences. For
 233 the 2050 experiments, *CCSM4* has the largest G-S difference of 67mm, with *NorESM1*

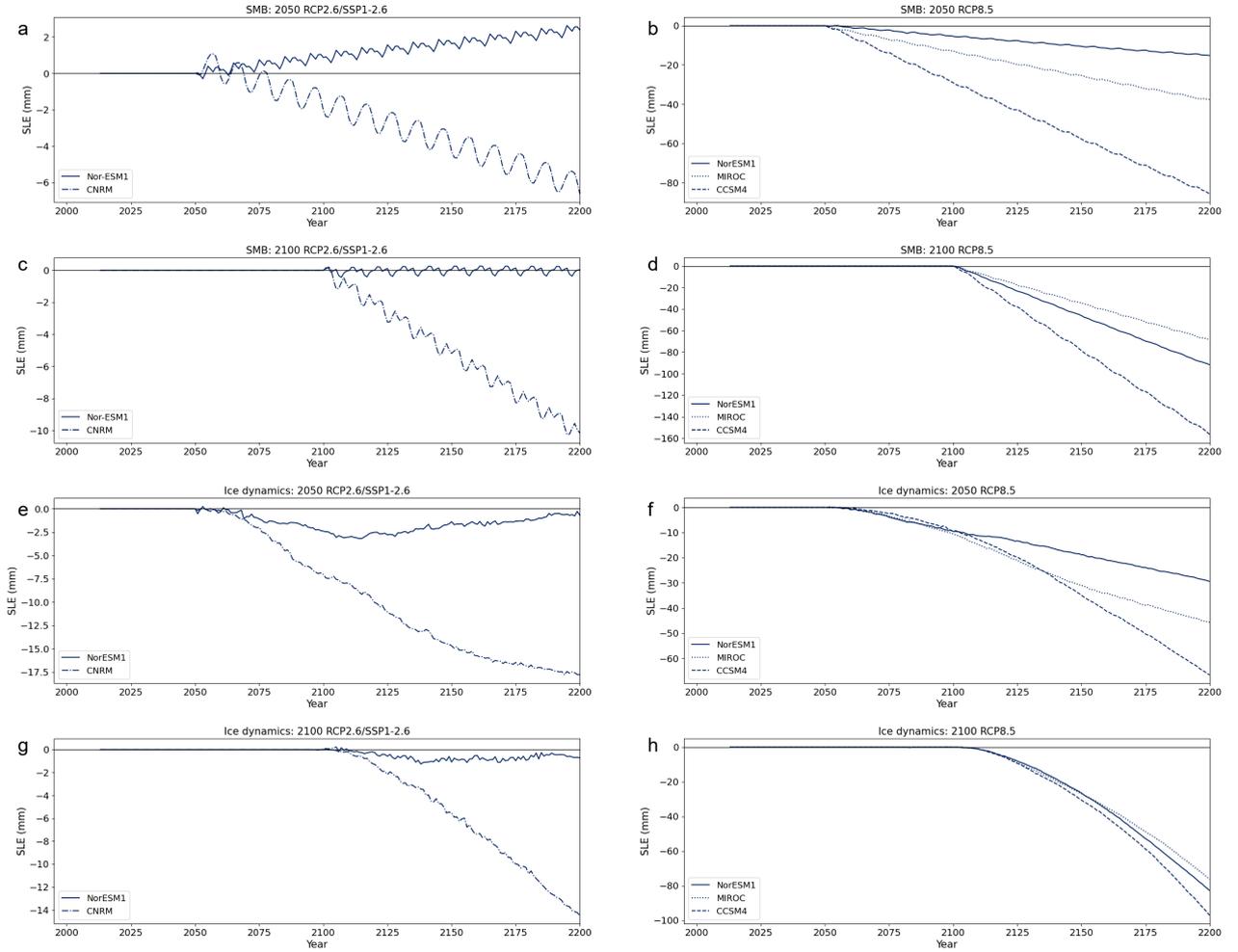


Figure 2. Difference between geoenineering and stabilisation scenarios (geoenineering minus stabilisation) for cumulative SMB (panels a-d) and ice dynamics (e-h). RCP2.6/SSP1-2.6 scenarios are shown in the left panels, and RCP8.5 scenarios are shown on the right. Line types show different model experiments. *NorESM1* – solid line, *MIROC* – dotted line, *CCSM4* – dashed lined, *CNRM* – dash dotted line. Positive (negative) values indicate that geoenineering has a larger (smaller) SMB or ice dynamics value than stabilisation.

234 having the smallest G-S difference of 30mm. For the 2100 experiments, the G-S differ-
 235 ence is more pronounced for all models (76-97mm), and the ice dynamic sea level con-
 236 tribution is greater than compared with the 2050 experiments. G-S differences also ap-
 237 pear to increase at an accelerating rate compared with the 2050 experiments' more lin-
 238 ear response (with the exception of *CCSM4 8.5*). The acceleration in G-S difference is
 239 due to the sea level contribution from ice dynamics increasing at a faster rate under a
 240 stabilisation scenario than under geoengineering.

241 3.4 Spatial patterns of mass loss

242 Figure 3 presents spatial patterns of G-S differences for ice thickness. Geoengineer-
 243 ing is helpful in reducing mass loss for the Amery and West ice Shelves, the Amundsen
 244 Sea Embayment, and Totten Glacier. The Ross and Ronne-Filchner ice shelves are more
 245 model dependent. All models show greater thickening in the interior under stabilisation
 246 compared with geoengineering. Though geoengineering does prevent some thinning, there
 247 are still large losses in these regions, under both geoengineering and stabilisation (B2)

248 Similar results are observed in the 2100 simulations, with losses observed in the same
 249 areas but with greater severity (Figure B3). The north coast of Queen Maud Land also
 250 experiences significant losses. The G-S difference is larger in the 2100 experiments (Fig-
 251 ure 3), as is the inland thickening under stabilisation because of the increased SMB, and
 252 there is strong model agreement on geoengineering being beneficial to the Ross ice shelf.

253 Losses are smaller under RCP2.6/SSP1-2.6, but spatial patterns of thinning are sim-
 254 ilar (Figures B2 and B3). Though there is some thickening in the interior, G-S differ-
 255 ences are much smaller for RCP2.6/SSP1-2.6 than under RCP8.5, indicating smaller SMB
 256 changes (Figure B4). All simulations demonstrate that geoengineering is less effective
 257 for the Ross ice shelf but is otherwise useful in many similar regions as the RCP8.5 ex-
 258 periments.

259 4 Discussion

260 All models agree that regardless of scenario, Antarctica will contribute consider-
 261 ably to sea level over the next two centuries. SMB plays an important role in driving
 262 changes across all scenarios, with ice dynamics also contributing significantly to the 2100
 263 RCP8.5 emissions scenarios.

264 Scenarios with most warming show the largest SMB gains as warmer climates lead
 265 to increased precipitation. This is seen in the forcings (Figures A1 and A2), where for
 266 all models, the repeated decadal SMB forcing under stabilisation is higher than under
 267 geoengineering. This difference in climate forcing produces the large negative G-S dif-
 268 ferences for SMB seen for the RCP8.5 emissions scenarios, particularly for the 2100 sim-
 269 ulations, indicating that geoengineering tends toward smaller SMB increases due to the
 270 reduced warming. For the 2100 RCP8.5 stabilisation scenarios, this increased SMB par-
 271 tially offsets some of the losses from Antarctica, resulting in smaller sea level contribu-
 272 tions compared with geoengineering. This contrasts to what is seen in the 2050 RCP8.5
 273 scenarios and all RCP2.6/SSP1-2.6 emission scenarios, as here the small forcing differ-
 274 ence between geoengineering and stabilisation does not produce a SMB increase large
 275 enough to partially offset dynamic losses. *CCSM4 8.5* however, has a very large SMB
 276 increase, which is why this is the only 2050 experiment where sea level contribution un-
 277 der geoengineering is higher than under stabilisation: geoengineering dampens the SMB,
 278 while dynamic losses continue.

279 Though the 2100 RCP8.5 scenarios initially show larger sea level contributions un-
 280 der geoengineering, all geoengineering trajectories begin to slow, while the stabilisation
 281 trajectories accelerate (Figure 1), leading to the possibility of the scenarios eventually

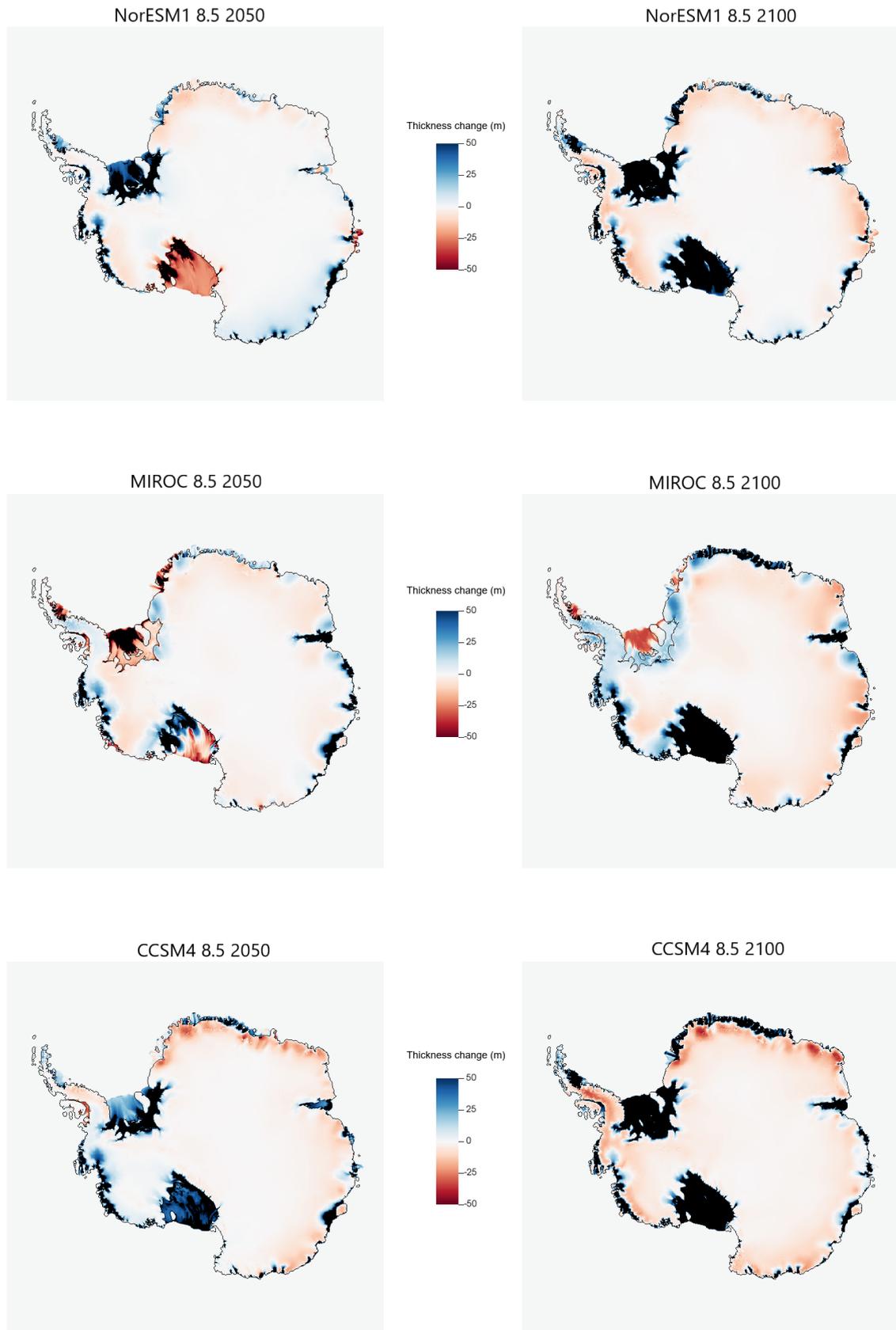


Figure 3. Spatial patterns of ice thickness difference in meters between geoengineering minus stabilisation for RCP8.5 experiments at 2050 and 2100. Experiments are shown on the left and 2100 shown on the right. Where values are negative (red), geoengineered ice thickness is less than the stabilisation experiments. Where values are positive (blue), geoengineered ice thickness is more than stabilisation experiments. Values higher than 50m or lower than -50m are shown in black.

282 converging. G-S differences peak and then decline (Figure B1), with *MIROC's* sea level
283 contribution under stabilisation overtaking geoengineering in ~ 2185 (Figure 1). Initially,
284 increased SMB from warmer atmospheric temperatures in the stabilisation scenarios com-
285 pensates for some of the losses: however, over time, the ice dynamic contribution increases
286 substantially relative to the geoengineered scenarios. At this point, SMB increases are
287 no longer enough to compensate for the dynamic losses. This has been found in previ-
288 ous work (Winkelmann et al., 2015; Golledge et al., 2015) and is seen here in Figure 2,
289 where the 2100 RCP8.5 scenarios show an accelerating increase in G-S difference for ice
290 dynamics, while the SMB G-S difference increases linearly.

291 The large rise in sea level contribution from ice dynamics under the high emission
292 stabilisation scenarios is explained by the basal melt (Figure B5), which greatly increases
293 compared to geoengineering. Figure 3, also shows thinner ice shelves under stabilisation,
294 reducing buttressing and increasing ice flow. The G-S difference for the grounded area
295 also accelerates because the grounded area under stabilisation continues to decrease, while
296 it begins to plateau under geoengineering (Figure B6). All other scenarios show a sta-
297 bilisation for both geoengineering and stabilisation. The 2100 RCP8.5 stabilisation sce-
298 narios could therefore point to a possible instability in grounding line retreat being trig-
299 gered, which geoengineering could help to mitigate.

300 The Amery ice shelf, Totten and Amundsen Sea Embayment glaciers appear to be
301 more unstable than others, as they continue to thin even when ocean thermal forcing re-
302 verts to present day under both low and high emissions scenarios. Observed rates of thin-
303 ning and grounding line retreat are highest in the Amundsen and Bellingshausen Sea ar-
304 eas and around Totten Glacier, and several Amundsen Sea Embayment glaciers have been
305 stated as being compatible with the onset of MISI, though this is still uncertain (IPCC,
306 2021, 2019)

307 The lagged response of the ice sheet to past warming means that geoengineering
308 is unable to prevent mass loss, even in this idealised case where ocean forcing is instantly
309 decreased. In reality, sea level contributions would likely be even higher as the additional
310 ocean inertia would mean that ocean thermal forcing would remain at 2050 or 2100 lev-
311 els for decades, even if atmospheric temperatures were immediately reduced. CDW, for
312 example, is a relatively old (Matsumoto, 2007) and deep (Jacobs et al., 2011) water mass.
313 This means it is not in frequent contact with the atmosphere, and that these deeper wa-
314 ters take time to adjust to atmospheric changes as they penetrate down from the sur-
315 face. The ocean's lagged response time has been previously proposed as the reason Antarc-
316 tica will have committed sea level rise, even if atmospheric temperatures were stabilised
317 (DeConto et al., 2021).

318 The models show little agreement on sea level contribution, and high and low emis-
319 sion scenarios overlap between models in many cases. Figures A1 and A2 show that SMB
320 and ocean thermal anomalies have large interannual variability, meaning these results
321 depend strongly on the decade chosen to repeat. Particularly for the low emission sce-
322 narios, there is considerable overlap between stabilisation and geoengineering input forc-
323 ings, which may explain why smaller changes are seen between the two, and why the largest
324 differences are seen between models. The model and decade chosen therefore play a com-
325 parably large role in determining Antarctic sea level contribution. As these scenarios are
326 highly idealized, we do not focus on projecting absolute sea level contribution. Instead,
327 we focus on understanding whether geoengineering leads to more effective sea level rise
328 mitigation than stabilising climate at 2050 or 2100. The simulations also provide insight
329 into the reversibility of mass loss from Antarctica: that while idealised, large scale geo-
330 engineering can mitigate some loss, it cannot reverse it.

5 Conclusion

Although the Antarctic ice sheet will contribute substantially to sea level rise in all cases, implementing geoengineering in 2050 generally results in decreases in sea level contribution compared with stabilising the climate at 2050 or 2100. The climate model *CCSM4* under an RCP8.5 scenario is an exception, as its strong SMB response offsets some sea level contribution in the stabilisation scenario. If geoengineering methods are deployed in 2100, outcomes are more uncertain, and under high emission scenarios, geoengineering often initially contributes more to sea level rise than stabilising climate in 2100, due to increased SMB offsetting some of the mass loss. Beyond 2200, however, sea level contribution under stabilisation appears to accelerate, likely as a result of increased losses due to ice dynamics, whilst the geoengineering scenarios' sea level contribution decelerates. This could indicate that in future, geoengineering may eventually be more effective.

Sea level contributions differ widely between models for the same scenario, with this difference often being larger than the difference between the geoengineering and stabilisation scenarios. Under RCP8.5, models do not all agree that geoengineering in 2050 would be more effective than stabilising the climate. The model uncertainty therefore makes it difficult to quantify the effectiveness of geoengineering, however the results still highlight that Antarctic mass loss is irreversible for the next two centuries due to its delayed response to climate forcings.

More work is needed to understand Antarctica's response to more realistic geoengineered scenarios, but the results presented here indicate that geoengineering would not be a complete solution to mitigating sea level contribution from the ice sheet, nor reverse it on multi-century timescales. Deployment would be more effective if implemented earlier, and if delayed until the end of the century, would initially be more harmful than stabilising the climate. As substantial mass losses are still seen under a 2050 implementation, it is likely that even an earlier implementation of geoengineering would not be able to fully prevent further sea level contribution. Additional mitigation and adaptation strategies will therefore still need to be investigated.

6 Open research

We use BISICLES version 1.3, revision number 4311 of the public branch, accessible at <https://anag-repo.lbl.gov/svn/BISICLES/public/trunk/>. BISICLES is written in a combination of C++ and FORTRAN and is built upon the Chombo AMR software framework. More information about Chombo can be found at <http://Chombo.lbl.gov>.

ISMIP6 atmosphere and ocean forcing data is stored on the University of Buffalo's CCR transfer server, accessed at <sftp://transfer.ccr.buffalo.edu/projects/grid/ghub/ISMIP6>. Instructions for accessing the server can be found at: https://www.climate-cryosphere.org/wiki/index.php?title=ISMIP6-Projections-Antarctica#A2.2.Retrieving_dataset_and_Uploading_your_model_output

The data that support the findings of this study are openly available at <https://data.mendeley.com/preview/y3vg6c68th?a=d675fa69-5403-40ec-8422-96f347654d63>.

Figures were created using Matplotlib version 3.7 and Pandas version 1.5.3. Maps were creating using VisIt version 3.1.0, available at <https://sd.llnl.gov/simulation/computer-codes/visit/executables>

376

Appendix A Climate forcing inputs

377

Appendix A shows all input forcings used, illustrating the repeated decadal timescales.

378

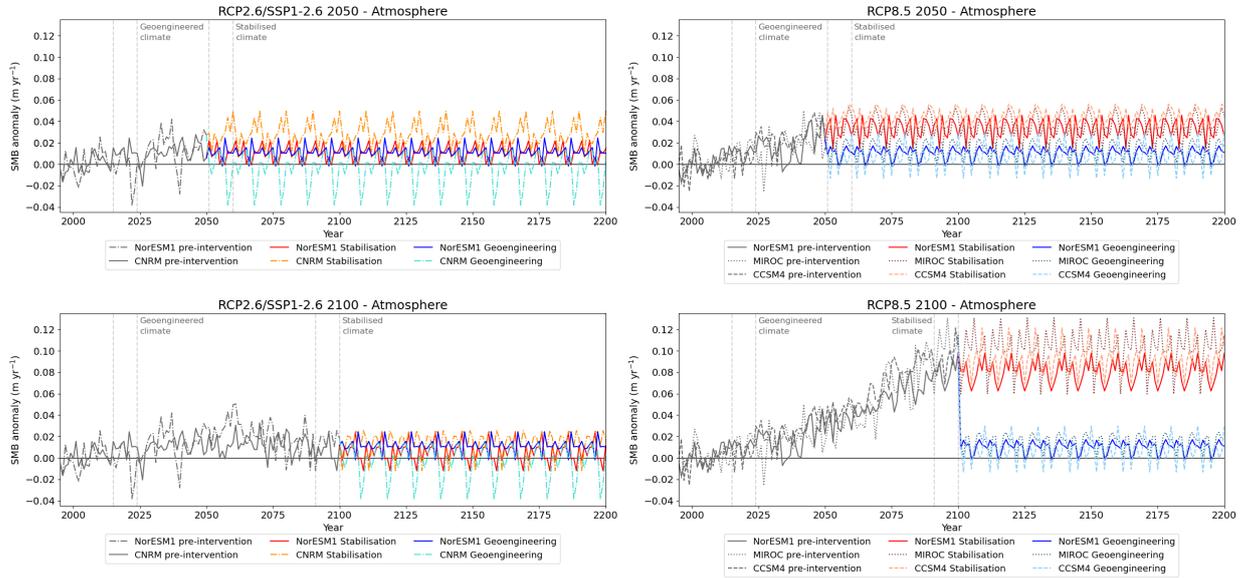


Figure A1. SMB anomalies for 2050 (top) and 2100 (bottom) for RCP2.6/SSP1-2.6 (left) and RCP8.5 (right) emission scenarios. Different line types show different model experiments. *NorESM1* – solid line, *MIROC* – dotted line, *CCSM4* – dashed lined, *CNRM* – dash dotted line. Red/orange lines indicate stabilisation scenarios, blue lines indicate geoengineering scenarios. The grey vertical dashed lines show the repeated time periods of geoengineered (2015-2024) and stabilisation (2051-2060/2091-2100) climates.

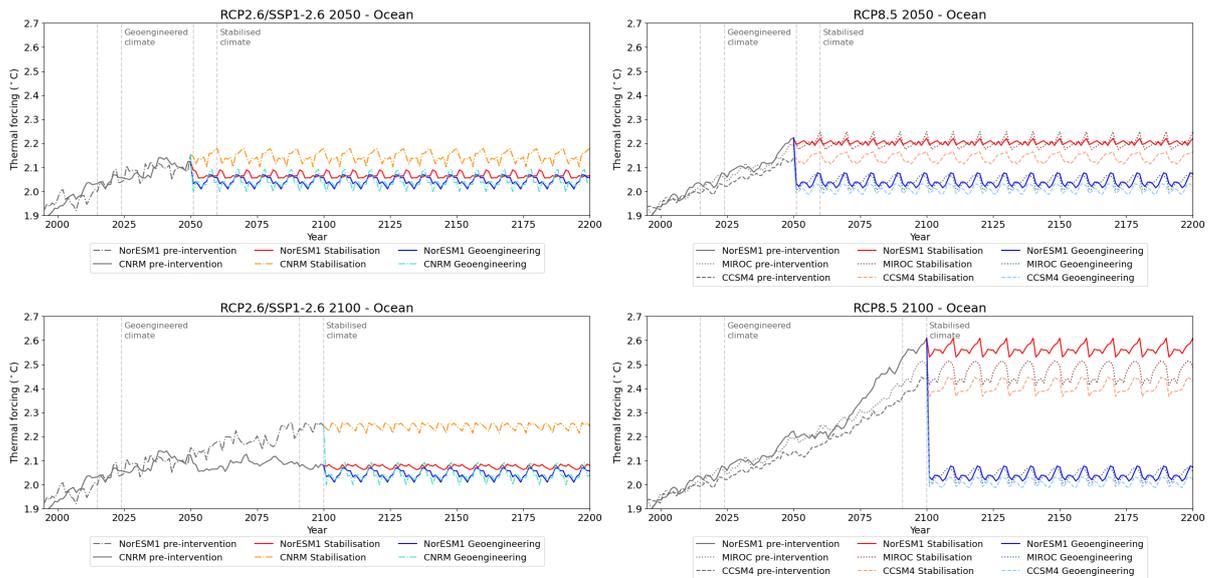


Figure A2. As A1 but for ocean thermal forcing.

379 **Appendix B Further results and variables**

380 Appendix B contains a table of all 2200 values relative to 2012 for total sea level
 381 contribution, SMB, ice dynamics, total melt, and grounded area change (Table B1). It
 382 contains timeseries showing the G-S difference for total sea level contribution (B1), ab-
 383 solute sea level contribution from melt (B5) and grounded area change (B6), and spa-
 384 tial patterns of mass loss (B2, B3 and B4).

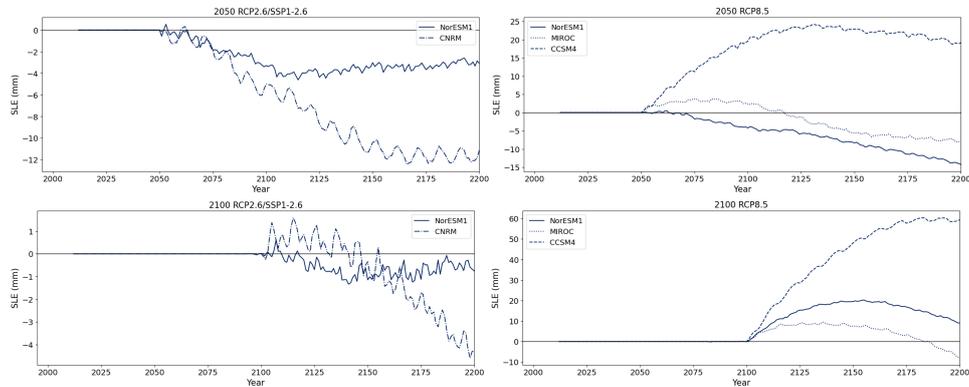


Figure B1. Difference between the geoengineering and stabilisation scenarios (geoengineering minus stabilisation) for total sea level contribution, for 2050 (top) and 2100 (bottom) for RCP2.6/SSP1-2.6 (left) and RCP8.5 (right) emission scenarios. Different line types show different model experiments. *NorESM1* – solid line, *MIROC* – dotted line, *CCSM4* – dashed lined, *CNRM* – dash dotted line. Where the value is positive, geoengineering has a larger sea level contribution than stabilisation, i.e. that geoengineering is worse than fixing the climate at that point. If the value is negative, then geoengineering has a smaller sea level contribution than stabilisation.

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Table B1. Projections in 2200 relative to 2012 for total sea level contribution, integrated SMB, integrated ice dynamics, integrated basal melt, and grounded area change, for all experiments, shown in mm sea level equivalent

	Stabilisation 2050	Geoengineering 2050	Stabilisation 2100	Geoengineering 2100
Total sea level contribution (SLE mm)				
NorESM1 8.5	171	157	172	181
MIROC 8.5	111	103	142	134
CCSM4 8.5	72	91	50	109
NorESM1 2.6	140	137	141	141
CNRM 1-2.6	60	49	65	61
SMB cumulative sum (SLE mm)				
NorESM1 8.5	-879	-859	-976	-885
MIROC 8.5	-946	-908	-997	-928
CCSM4 8.5	-991	-905	-1116	-959
NorESM1 2.6	-873	-875	-875	-875
CNRM 1-2.6	-966	-960	-974	-964
Ice dynamics cumulative sum (SLE mm)				
NorESM1 8.5	1051	1021	1154	1071
MIROC 8.5	1058	1012	1139	1063
CCSM4 8.5	1063	997	1166	1069
NorESM1 2.6	1013	1012	1017	1017
CNRM 1-2.6	1027	1009	1040	1025
Melt cumulative sum (SLE mm)				
NorESM1 8.5	358	253	926	466
MIROC 8.5	474	291	1267	504
CCSM4 8.5	424	211	981	390
NorESM1 2.6	153	184	180	191
CNRM 1-2.6	284	314	366	335
Grounded area change (km ² /1000)				
NorESM1 8.5	-215	-186	-302	-234
MIROC 8.5	-217	-188	-293	-227
CCSM4 8.5	-222	-171	-319	-226
NorESM1 2.6	-150	-170	-156	-168
CNRM 1-2.6	-148	-180	-162	-176

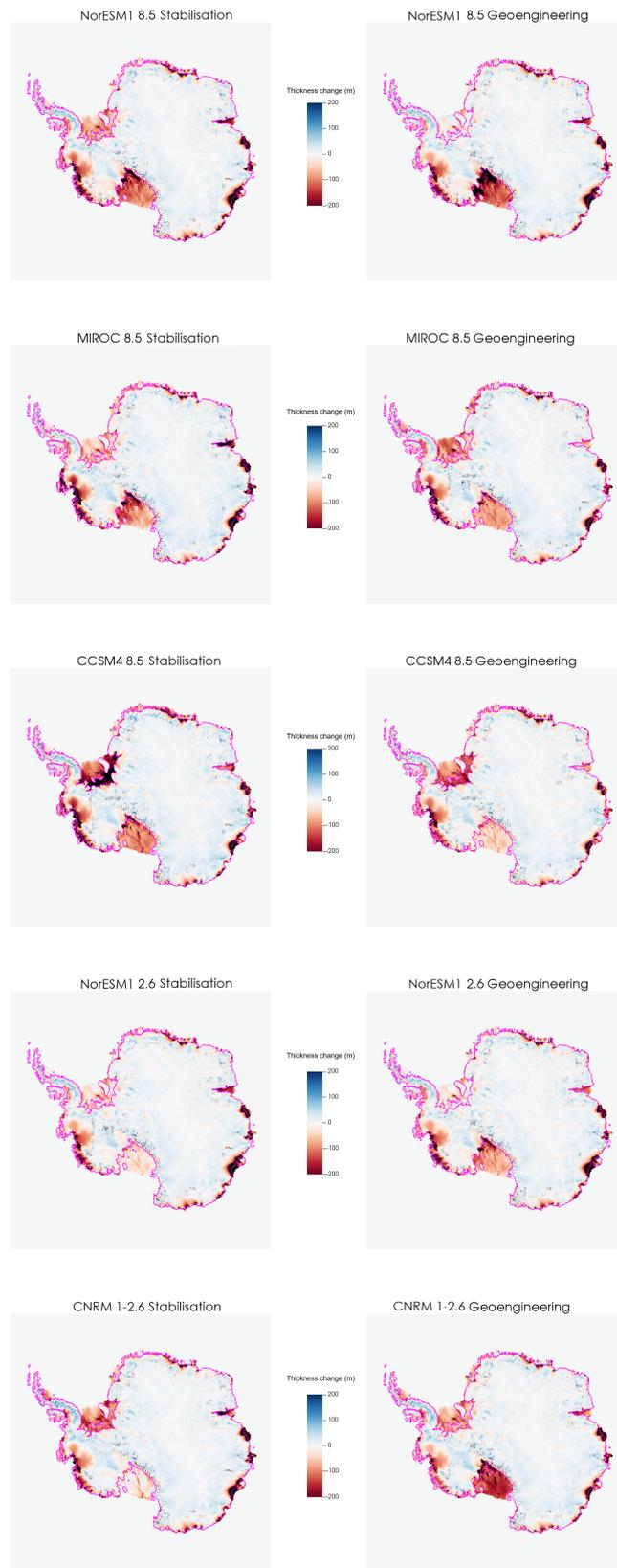


Figure B2. Thickness change in meters between 2012 and 2200 for the 2050 experiments. Pink line denotes the grounding line. Red areas represent areas where ice thickness is lower in 2200 compared with 2012. Values higher than 200m or lower than -200m are shown in black.

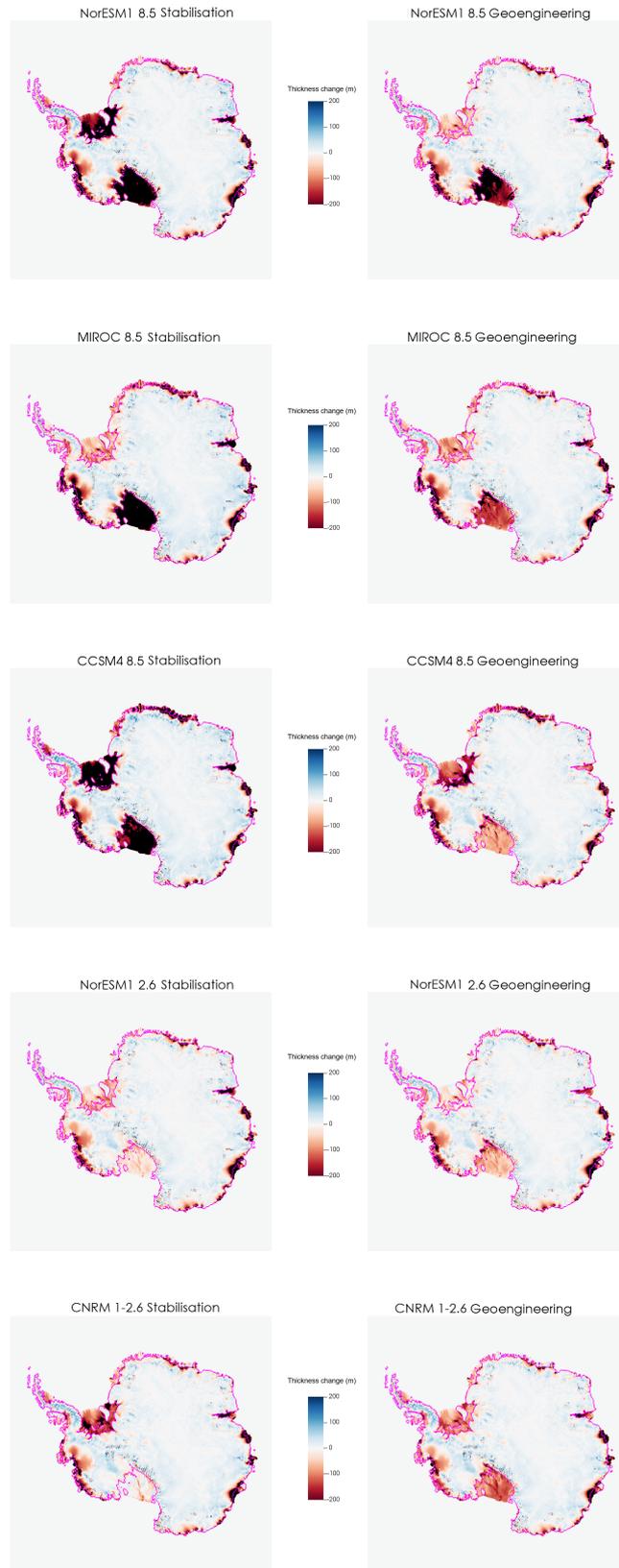


Figure B3. As B2 but for the 2100 scenarios.

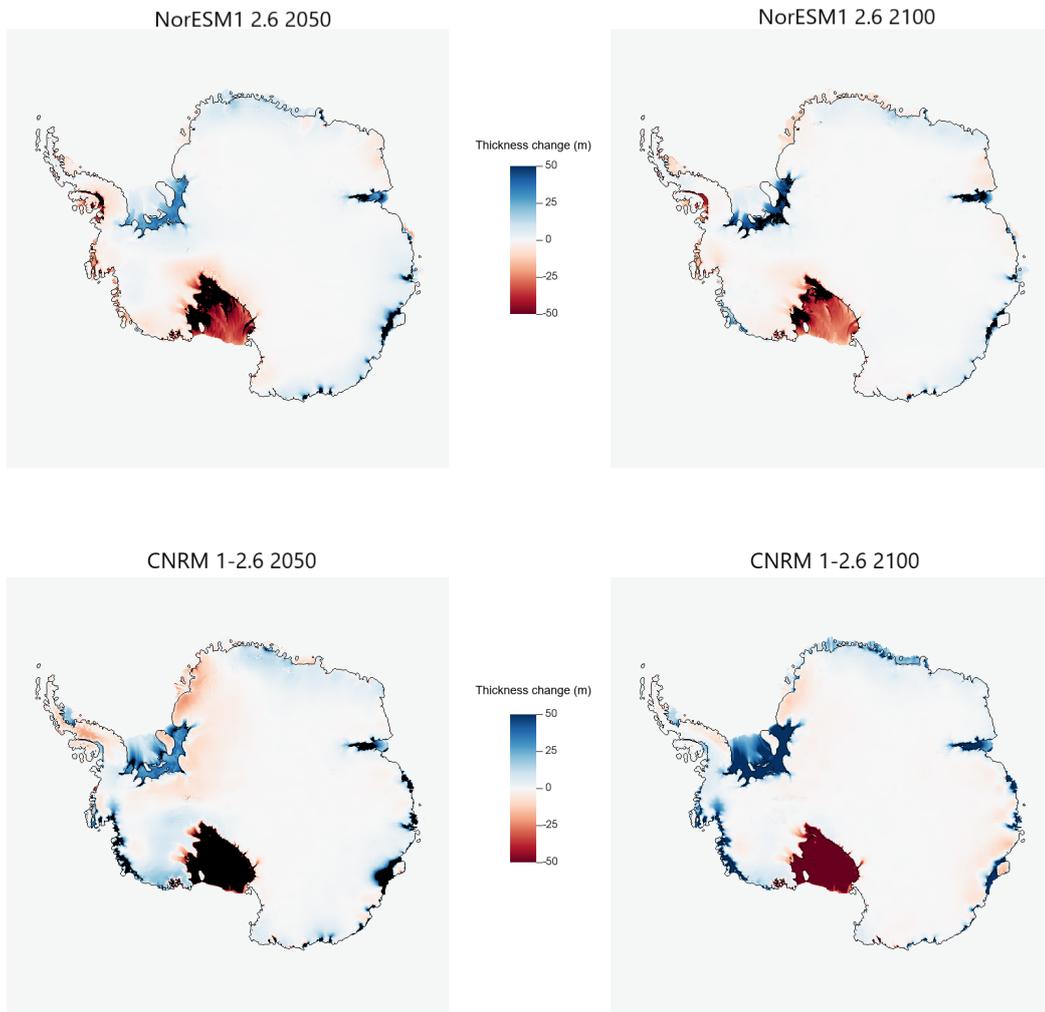


Figure B4. Spatial patterns of ice thickness difference between geoengineering minus stabilisation for RCP2.6/SSP1-2.6 experiments at 2200. Thickness difference shown in meters. 2050 experiments are shown on the left and 2100 shown on the right. Where values are negative (red), geoengineered ice thickness is less than the stabilisation experiments. Where values are positive (blue), geoengineered ice thickness is more than stabilisation experiments. Values higher than 50m or lower than -50m are shown in black.

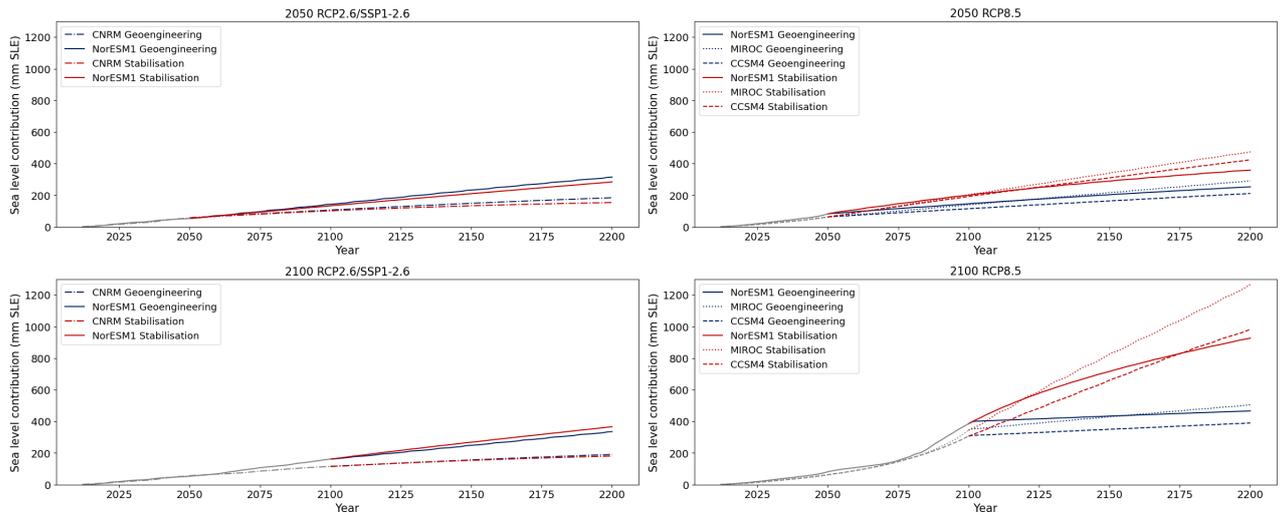


Figure B5. Cumulative sum of total melt relative to 2012 shown in SLE for 2050 (top) and 2100 (bottom) for RCP2.6/SSP1-2.6 (left) and RCP8.5 (right) emission scenarios. Different line types show different model experiments. *NorESM1* – solid line, *MIROC* - dotted line, *CCSM4* - dashed lined, *CNRM* - dash dotted line. Red lines indicate stabilisation scenarios, blue lines indicate geoengineering scenarios.

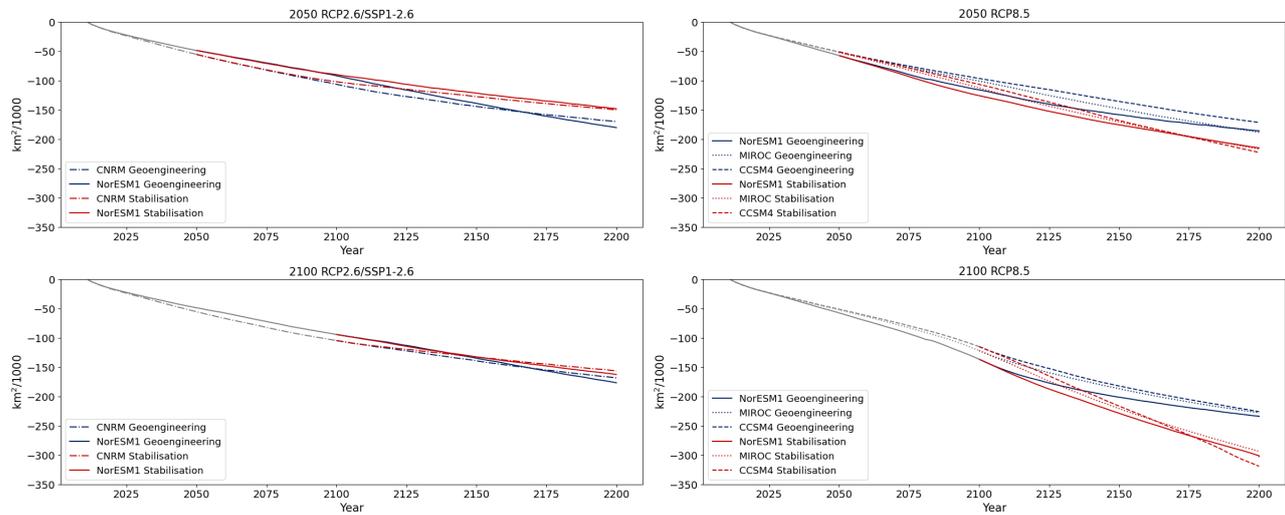


Figure B6. Grounded area change relative to 2012 for 2050 (top) and 2100 (bottom) for RCP2.6/SSP1-2.6 (left) and RCP8.5 (right) emission scenarios. Different line types show different model experiments. *NorESM1* – solid line, *MIROC* - dotted line, *CCSM4* - dashed lined, *CNRM* - dash dotted line. Red lines indicate stabilisation scenarios, blue lines indicate geoengineering scenarios.

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