### Using Vehicle-induced DAS Signals for Near-surface Characterization with High Spatiotemporal Resolution

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#### Key Points:

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8	•	We utilize a large number of vehicles transiting on city streets as non-dedicated
9		seismic sources for continuous near-surface monitoring.
10	•	Our method outperforms ambient noise interferometry in efficiency and resolu-
11		tion, leveraging selective cross-correlation of surface waves.
12	•	We observed rain-induced changes in seismic properties using time-lapse analy-
13		sis of kinematics and attenuation.

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#### 14 Abstract

Vehicle-induced seismic waves, generated as vehicles traverse the ground surface, carry 15 valuable information for imaging the underlying near-surface structure. These waves prop-16 agate differently in the subsurface depending on soil properties at various spatial loca-17 tions. By leveraging wave propagation characteristics, such as surface-wave velocity and 18 attenuation, this study presents a novel method for near-surface monitoring. Our method 19 employs passing vehicles as active, non-dedicated seismic sources and leverages pre-existing 20 telecommunication fibers as large-scale and cost-effective roadside sensors empowered 21 by Distributed Acoustic Sensing (DAS) technology. A specialized Kalman filter algorithm 22 is integrated for automated DAS-based traffic monitoring to accurately determine ve-23 hicles' location and speed. Then, our approach uniquely leverages vehicle trajectories 24 to isolate space-time windows containing high-quality surface waves. With known ve-25 hicle (i.e., seismic source) locations, we can effectively mitigate artifacts associated with 26 suboptimal distribution of sources in conventional ambient noise interferometry. Com-27 pared to ambient noise interferometry, our approach enables the synthesis of virtual shot 28 gathers with a high signal-to-noise ratio and spatiotemporal resolution at reduced com-29 putational costs. We validate the effectiveness of our method using the Stanford DAS-30 2 array, with a focus on capturing spatial heterogeneity and monitoring temporal vari-31 ations in soil seismic properties during rainfall events. Specifically, in non-built-up ar-32 33 eas, we observed an evident decrease in phase velocity and group velocity and an increase in attenuation due to the rainfall. Our findings illustrate our method's sensitivity and 34 resolution in discerning variations across different spatial locations and demonstrate that 35 our method is a promising advancement for high-resolution near-surface imaging in ur-36 ban settings. 37

#### <sup>38</sup> Plain Language Summary

Continuous monitoring of near-surface soil properties is important to various ap-39 plications, including identifying subsidence and monitoring groundwater levels. Vehicles 40 transiting in city streets excite seismic waves propagating in the subsurface, which can 41 be analyzed to gain insights into the structures beneath the surface. In this study, we 42 develop a novel near-surface monitoring method utilizing traffic recordings of Distributed 43 Acoustic Sensing (DAS) technology, transforming existing telecommunication cables into 44 extensive ground motion sensors. To harness the vibrations generated by vehicles, our 45 method employs a specialized algorithm, determining vehicle locations and speeds based 46 on the ground deformation they induce. The identified vehicle location is precisely uti-47 lized to select specific traffic-induced seismic waves to explore the subsurface. Our ap-48 proach allows for the acquisition of clearer and more precise insights into underground 49 structures in urban areas and is more computationally efficient than traditional meth-50 ods based on ambient noises. Tested at Stanford University in 2023, our method adeptly 51 identified variations in the seismic properties of the subsurface, particularly in non-built-52 up areas, during rainfall events. Such accurate detection is valuable for water resource 53 management and urban development, enabling enhanced understanding and management 54 of urban subsurface environments. 55

#### <sup>56</sup> 1 Introduction

In urban areas, it is useful to monitor continuously the near-surface for various purposes, including subsidence and pothole detection, as well as for improving seismic hazard analysis maps to include more site-specific effects. While traditional methods, such as controlled source surveys (Nazarian et al., 1983; Park et al., 1999; Stokoe et al., 2017), can provide high-quality near-surface images, repeatedly conducting such surveys on a large scale is challenging regarding logistics and operational expenses. To circumvent the need for expensive active source surveys, researchers have turned to ambient noise interferometry (Shapiro & Campillo, 2004; Wapenaar et al., 2010) that aims to extract coherent surface-wave signals by performing cross-correlation between passive ambient noise
recordings at virtual shot locations and virtual receivers at different offsets. Traditionally used with geophone arrays, this algorithm has proven effective for subsurface imaging in urban environments (Lin et al., 2013; Chang, 2018). However, deploying dense geophone arrays in urban settings on a large scale and a long-term basis presents its own
set of challenges, including high operational costs and significant logistical hurdles.

Distributed Acoustic Sensing (DAS) has emerged as a promising technology in re-71 72 sponse to these challenges. DAS-based monitoring is performed by connecting an interrogator to one end of a standard telecommunications-grade optical fiber. The interroga-73 tor sends short laser pulses into the optical fiber and measures the subtle phase shifts 74 of Rayleigh scattered light returning to the detector at a predicted two-way travel time (Posey, 75 2000; Masoudi & Newson, 2016). In this way, the strain field induced by natural pro-76 cesses (e.g., earthquakes) and urban activities (e.g., moving vehicles, construction, pumps) 77 acting on the fiber coupled to the Earth can be sampled at a meter-scale spatial reso-78 lution over tens of linear fiber kilometers. Notably, DAS technology has proven effective 79 on existing and growing "dark fiber" telecommunication infrastructure for earthquake 80 monitoring (Biondi et al., 2021), infrastructure monitoring (Yuan et al., 2021; Liu, Yuan, 81 Luo, et al., 2023), and near-surface imaging (E. R. Martin et al., 2017; Fang et al., 2020), 82 significantly reducing installation cost. Furthermore, by incorporating state-of-the-art 83 interrogators, such as OptaSense QuantX (Optasense, a Luna company, 2022), DAS can 84 record full waveform signals over distances up to 50 km, with a granular 1 m channel spac-85 ing, which makes DAS promising for continuous city-wide sensing. 86

Just as the geophone-based techniques, DAS often harnesses ambient noise inter-87 ferometry to sidestep active source surveys in subsurface characterization (E. R. Mar-88 tin et al., 2017, 2021). While the conventional interferometry approach has been success-89 ful in numerous applications, it has several limitations. Firstly, it is computationally ex-90 pensive because it requires cross-correlation of days or even weeks of noisy recordings 91 to reach convergence, depending on the relative strength of signals and noise. This com-92 putational burden intensifies when using DAS, given its abundance of channels. The lengthy 93 cross-correlation period also results in diminished temporal resolution, which may not 94 capture sudden subsurface changes caused by floods or construction. Secondly, passive 95 interferometry relies on the assumption that the incident azimuth of the wave field gen-96 erated by the sources is uniformly distributed, which may not hold in practice. The noise 97 sources may be localized, heterogeneous, and time-dependent, leading to inaccurate re-98 sults. Thirdly, capturing high-quality, high-frequency signals (above 10 Hz) using ambient noise interferometry presents a challenge due to the dominance of lower-frequency 100 vibrations in ambient noise. While passing vehicles can generate strong high-frequency 101 energy, this energy attenuates more rapidly as it propagates than lower frequencies. As 102 a result, the high frequencies often remain undetected when cross-correlating without 103 specific targeting. Therefore, the method may miss important subsurface information 104 in the high-frequency range that is relevant for detecting small-scale and shallow features, 105 such as fractures or cracks. 106

To overcome the aforementioned challenges associated with ambient noise inter-107 ferometry, we propose a novel approach that utilizes regular, everyday vehicles as active 108 and non-dedicated seismic sources in a roadside DAS array. Specifically, our approach 109 capitalizes on a prevalent urban dark fiber setup in which the DAS array is aligned par-110 allel to the roadway. This configuration enables the DAS to effectively record the seis-111 mic signals of vehicles as they transit along the road. The trajectories of the vehicles can 112 be automatically detected and tracked by the Kalman filter algorithm that we designed 113 for a DAS-based traffic monitoring system (Liu, Yuan, Dong, et al., 2023). Leveraging 114 these accurately identified trajectories, we can efficiently isolate high-quality, vehicle-induced 115 surface waves for advanced subsurface characterization. 116

The unique advantage of our method is its ability to leverage the knowledge of ve-117 hicle trajectories, from which we select space-time windows containing high-quality sur-118 face waves from isolated vehicles. Unlike ambient noise interferometry, which requires 119 cross-correlation of days or weeks of recordings from unknown ambient noise sources, we 120 streamline the process and only cross-correlate the data in these selected windows with 121 the benefits of known source locations. Our approach enables us to construct high signal-122 to-noise ratio virtual shot gathers efficiently, reducing computational costs significantly. 123 By stacking the results of hundreds of automatically tracked vehicles, we can obtain a 124 highly accurate virtual shot gather containing subsurface information with a temporal 125 resolution of one day, which is difficult to achieve with conventional interferometry. Fur-126 thermore, our method eliminates issues arising from uneven distribution of wave azimuth 127 angles, thanks to our knowledge of the source locations. Finally, by utilizing the precise 128 locations of the transiting vehicles, we are able to target and capture rapidly attenuated 129 high-frequencies excited by the vehicles, enabling effective imaging of shallow subsurface 130 structures. 131

Our method represents a generalized solution capable of providing high spatial-temporal 132 resolution for urban near-surface imaging. We demonstrate its efficacy via studies con-133 ducted using the Stanford DAS-2 array. Our primary aim is to capture spatial hetero-134 geneity and track temporal modifications in near-surface seismic properties — specifi-135 cally, phase and group velocity, and seismic attenuation — observed during the 2023 San 136 Francisco Bay Area rainfall events. Alterations in these seismic properties can serve as 137 indicators to estimate soil saturation levels with the application of rock physics princi-138 ples and assumptions. The results from the analyses highlight our method's robust ca-139 pability to accurately detect spatiotemporal variations in soil properties, thereby offer-140 ing an enhanced approach to urban subsurface characterization. 141

#### <sup>142</sup> 2 Existing work on continuous subsurface characterization with DAS

Surface waves, originating from traffic or other natural or anthropogenic sources, 143 can provide valuable insights into subsurface soil characteristics. Traditional interfero-144 metric methods allow the extraction of phase and group velocities of these waves, which 145 can then be inverted to reveal depth-dependent subsurface elastic parameters (Dou et 146 al., 2017; E. Martin et al., 2017). Several researchers have used the combination of DAS 147 and interferometry for continuous subsurface monitoring. Notably, Shen (2022) applied 148 DAS in a suburban setting, leveraging ambient noise data to explore subsurface water 149 content changes over a two-year span. Yang and Shragge (2023) deployed an urban DAS 150 array in Perth, Australia, and applied ambient seismic interferometry to detect subsur-151 face variations over a ten-month period. They recorded up to 9.4% seasonal variations 152 in depth-averaged S-wave velocity estimates, inversely correlated with local rainfall pat-153 terns, indicating changes in near-surface groundwater content. Despite these successes, 154 conventional "blind" interferometry can be computationally intensive and potentially skewed 155 due to the less-than-ideal positioning of seismic sources, such as vehicles, relative to the 156 sensors. In response, Yuan et al. (2020) proposed a cost-effective approach that capital-157 izes more efficiently on vehicle signals. By manually isolating signals from 33 distinct ve-158 hicles passing a section of the Stanford DAS-2 array and utilizing the directly excited 159 surface waves, they were able to invert a shear wave velocity  $(V_S)$  profile that corresponded 160 with an independent geotechnical survey, using only vehicle-induced signals. Importantly, 161 Yuan et al. (2020)'s approach delivers high-temporal resolution characterization as it achieves 162 imaging from vehicle signals within a 2-hour window, significantly shorter than the days 163 or weeks typically required for ambient noise interferometry. In addition, the known lo-164 cation of the sources (vehicles) bypasses the challenge presented in ambient noise inter-165 ferometry of not having waves from sources spanning all azimuths. This innovative strat-166 egy represents a notable advancement in efficient and accurate urban subsurface char-167 acterization. Our research extends the work of Yuan et al. (2020). The primary advance-168



Figure 1. Map view of a roadside section of the Stanford DAS-2 Array. Distances along the fiber are labeled on the map.

<sup>169</sup> ment we introduce is the automation of the previously manual and time-intensive vehi-<sup>170</sup> cle selection process. This enhancement allows for the incorporation of hundreds of ve-<sup>171</sup> hicles each day, markedly improving the reliability of subsurface monitoring.

#### <sup>172</sup> **3** Experimental setup

The Stanford DAS-2 experiment carried out at Stanford University has been con-173 tinuously recording data since December 10, 2019. Utilizing an OptaSense ODH-3 in-174 terrogator, the experiment operates at a sampling rate of 250 samples per second, with 175 a gauge length of 16 m. The array consists of 1250 channels in total, each spaced 8.16 176 m apart. Figure 1 illustrates a section of the fiber along Sand Hill Road. This section 177 was specifically chosen due to its complex and varied nature, which represents realistic 178 urban sensing scenarios. The fiber traverses locations with differing soil properties, such 179 as pavement and grass. This variation presents a comprehensive and challenging test bed 180 for our methodologies. The winter of 2023, characterized by recurrent atmospheric rivers 181 leading to heavy rainfall, posed an unusual weather pattern in the San Francisco Bay 182 Area. This scenario provided an excellent opportunity to evaluate both the spatial res-183 olution and the effectiveness of our method in detecting and analyzing changes in soil 184 saturation levels due to these rain events. 185

## 4 Proposed precision interferometry method for selective surface wave capture

The study introduces a precision interferometry method designed for the automated capture of traffic-induced surface waves and the synthesis of virtual shot gathers, facilitating continuous near-surface monitoring. We leverage a Kalman-filter-based vehicle tracking algorithm (Liu, Yuan, Dong, et al., 2023) to automatically select high-quality surface-wave windows, enhancing the methodology developed by Yuan et al. (2020). To improve the dispersion image quality and utilize signals from multiple vehicles, we construct virtual shot gathers leveraging the trajectory information of each passing vehicle and then stacking the amplitudes of the virtual shot gathers for hundreds of vehicles
to increase the signal-to-noise ratio (SNR). Time-lapse analyses are conducted based on
the virtual shot gather in a rainfall monitoring case study.

#### <sup>198</sup> 4.1 Proposed workflow

Our proposed workflow, illustrated in Figure 2, encompasses a series of steps de-199 signed to segregate and process traffic recordings, detect and track vehicle movements, 200 select time-space windows of surface waves, and finally, construct efficient virtual shot 201 gathers for advanced multi-channel analyses. The workflow starts with the separation 202 of full-bandwidth traffic recordings into quasi-static and surface wave components through 203 bandpass filtering. We then apply a Kalman filter algorithm to the quasi-static signals 204 to detect and track vehicles. Leveraging the output vehicle trajectories, we select time-205 space windows of the surface waves generated by isolated vehicles. By cross-correlating 206 only the selected windows, we can efficiently construct virtual shot gathers that enable 207 multi-channel analyses for time-lapse near-surface characterization. 208

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#### 4.2 Automatic surface-wave window selection based on vehicle-tracking

The Kalman filter algorithm (Liu, Yuan, Dong, et al., 2023), applied to quasi-static signals of moving vehicles, generates the trajectories of all detected vehicles. Figure 3 illustrates the selection process for surface-wave windows based on these tracking results. We've centered the tracking and selected surface wave windows around a pivot trace of 650 m in this example.

To prevent cross-talk among closely traveling vehicles, we select isolated vehicles by applying a time threshold parameter, denoted as  $\Delta \tau$ . Specifically, vehicles that reach the pivot trace within time differences smaller than  $\Delta \tau$  are considered too proximate and are therefore excluded. The yellow boxes in Figure 3 represent the surface-wave windows of these isolated vehicles, selected with a  $\Delta \tau$  value of 25 s.

A closer look at the surface waves from one of the selected yellow boxes is provided in Figure 4 (b). The zoomed-in view reveals the presence of two types of waves - forward and backward-propagating waves. The forward waves refer to the waves propagating in the same direction as the vehicle's movement. Conversely, the backward waves are seen propagating in the opposite direction to the vehicle's movement.



Figure 2. Workflow of the proposed vehicle-tracking imaging method.



Figure 3. An example of the selection of time-space windows of the vehicle-induced surface wave for a virtual shot location,  $x_0 = 650$ . Vehicle trajectories from the Kalman filter algorithm are indicated in red. Yellow boxes centered at  $x_0$  indicate isolated vehicles. The dashed orange box points to a vehicle that remains undetected because it enters Sand Hill Road from an intersection beyond the starting point of detection and tracking by the Kalman filter.



**Figure 4.** (a) Surface-wave component of one of the selected isolated vehicles. (b) A zoomedin view of the surface wave.

#### 4.3 Virtual shot gather synthesis

Utilizing surface waves, we construct virtual shot gathers via cross-correlation of 226 the pivot trace with other traces. This process is informed by the identified vehicle tra-227 jectories. A simplified illustration of surface waves generated by a vehicle is presented 228 in Figure 5, with forward-propagating waves denoted in yellow and backward-propagating 229 waves denoted in orange. Two snapshots, Figures 5 (a) and (b), depict the vehicle to the 230 left and right of the virtual shot, respectively. The color-filled receivers represent those 231 that are located on the same side as the virtual shot relative to the vehicle, with their 232 233 color matching the wavefield. By cross-correlating the recorded data at the virtual shot location with the data collected by the color-matched receivers, virtual shot gathers are 234 constructed. Receivers represented by empty circles are not used for cross-correlation, 235 as they are not within the same wavefield as the virtual shot. 236

To elaborate further, we start by defining a virtual shot at location  $x_s$ . Using the identified vehicle trajectory, we pinpoint the vehicle's arrival time at  $x_s$ , denoted as  $t_s$ . We then construct the virtual shot gathers utilizing both the forward and backward-propagating waves. Here, we first explain the assembly process of the virtual shot gather using backwardpropagating waves, which propagate in the opposite direction to the vehicle's movement.

The formation of the negative offset section of the virtual shot gather is achieved 242 by cross-correlating the recordings of the trace at virtual shot location with the receivers 243 situated to the left of  $x_s$  ( $x_r < x_s$ ). As can be seen in Figure 5, the virtual shot at  $x_s$ 244 encounters forward-propagating waves before the vehicle crosses  $x_s$ , i.e., when  $t < t_s$ . 245 After the point  $t \ge t_s$ , the vehicle has already traversed past  $x_s$ , and both the virtual 246 shot and the receivers to the left of  $x_s$  are exposed to the same backward-propagating 247 wavefields. Therefore, to implement the cross-correlation, we establish a time window 248 of length  $\Delta t$ , within the interval  $(t_s + \epsilon, t_s + \epsilon + \Delta t)$ . We introduce the additional term 249  $\epsilon$  to reduce the influence of near-field effects. This operation results in the negative-offset 250 portion of the virtual shot gather, which can be represented by the following equation: 251

$$C(\tau, x_r - x_s) = \int_{t_s + \epsilon}^{t_s + \epsilon + \Delta t} d(t + \tau, x_r) \cdot d(t, x_s) dt, \qquad (1)$$

where  $d(t, x_s)$  is the strain at the virtual shot location  $x_s$ ,  $d(t, x_r)$  is the strain at a virtual receiver location  $x_r$  situated to the left of  $x_s$  ( $x_s > x_r$ ), and  $\tau$  is the time lag.

Creating the positive-offset section from the backward propagating waves requires 254 cross-correlation of the receivers located to the right of the virtual shot  $(x_r > x_s)$ . This 255 process demands a different time window, expressed as  $(t_r + \epsilon, t_r + \epsilon + \Delta t)$ . Here,  $t_r$ 256 represents the vehicle's arrival time at a specific receiver location  $x_r$ , as informed by the 257 identified trajectory. This change is crucial because these receivers only experience the 258 backward-propagating wavefield once the vehicle, traversing its path, crosses  $x_s$  and reaches 259 the virtual receiver position, as visualized in Figure 5 (b). Additionally, since the waves 260 move from  $x_r$  to  $x_s$ , the time offset,  $\tau$ , is negated during cross-correlation to generate 261 causal virtual shot gathers. The modified equation for cross-correlation in the positive-262 offset section consequently becomes: 263

$$C(\tau, x_r - x_s) = \int_{t_r + \epsilon}^{t_r + \epsilon + \Delta t} d(t - \tau, x_r) \cdot d(t, x_s) dt.$$
<sup>(2)</sup>

Equations 1 and 2 together provide the complete virtual shot gather, including both the negative and positive offset sections, which are constructed utilizing the backward propagating wavefields.

In dealing with forward-propagating wavefields, our method reconfigures the crosscorrelation time windows. For synthesizing the negative-offset segment  $(x_r < x_s)$ , we opt for the time interval of  $(t_r - \epsilon - \Delta t, t_r - \epsilon)$ , where  $t_r$  denotes the vehicle's arrival times at  $x_r$  as determined by the Kalman filter trajectory. We select this time window because, within it, the vehicle hasn't yet reached  $x_r$ , and both  $x_s$  and  $x_r$  are subjected to the forward propagating wavefield. For the assembly of the positive-offset portion, we involve the receivers situated to the right of  $x_s$ . They intersect with the forward-propagating wavefields until the vehicle passes  $x_s$ . We select the time window  $(t_s - \epsilon - \Delta t, t_s - \epsilon)$ for cross-correlation, resulting in the positive-offset section of the virtual shot gather.

As a concrete example, Figure 6 panels (a) and (b) show the virtual shot gathers 276 277 obtained from the forward-propagating and backward-propagating wavefields depicted in Figure 4, respectively. Figure 6 panel (c) displays the virtual shot gather obtained by 278 combining panels (a) and (b). In this combined gather, the signals are amplified due to 279 the process of constructive interference, where signals of the gathers from the forward 280 and backward-propagating wavefields augment each other, leading to an increase in the 281 overall signal strength. This amplification enhances the SNR of the combined virtual shot 282 gathers. 283

4.4 Improving signal-to-noise ratio (SNR) through stacking virtual shot gathers

To enhance the quality of the constructed virtual shot gathers, our methodology employs daily detection and examination of between 150 to 250 unique vehicles. By leveraging the average of their individual virtual shot gathers, we increase the Signal-to-Noise



Figure 5. The diagram presents a simplified illustration of surface waves generated by a vehicle, with forward-propagating waves shown in yellow and backward-propagating waves shown in orange. Two snapshots are shown in panels (a) and (b), depicting the car to the left and right of the virtual shot, respectively. Color-filled receivers are located on the same side of the vehicle as the receiver at the virtual shot location. As such, they are subject to the same forward or backward propagating waves. To illustrate this, they are colored to match the respective waves. Virtual shot gathers can be constructed by cross-correlating the recorded data at the virtual shot location with the data collected by the color-matched receivers.

Ratio (SNR) due to the signal's constructive averaging and the noise's cancellation effects. Notably, the number of vehicles examined can vary depending on the required SNR and the time scale of the subsurface variation of interest. For a higher SNR or a longer time scale of interest, a larger number of vehicles can be utilized. Conversely, for capturing changes in soil properties at a finer temporal resolution, a smaller number of vehicles within a shorter time frame should be utilized.

The impact of this multi-vehicle virtual shot gather stacking approach can be seen 295 in Figure 7. It showcases averages of virtual shot gathers related to varying numbers of 296 297 passing cars at the same fiber location: 4 cars (panel a), 41 cars (panel b), and 173 cars (panel c). The corresponding dispersion images derived from negative-offset signals are 298 also displayed in panels (d), (e), and (f), respectively. The displayed dispersion images 299 are normalized at each frequency by the L-1 norm. This method of normalization is uni-300 formly applied to the dispersion images in all the figures throughout this paper. We can 301 see that with a stack of only 4 cars, both the virtual shot gather and the dispersion im-302 age are significantly noisy. However, when the stack includes hundreds of vehicles, the 303 quality visibly improves. Particularly, higher modes can be discerned more clearly. 304

In the ideal scenario, virtual shot gathers should be purely causal. However, upon examining Figures 7, one can notice faint yet coherent signals in the negative  $\tau$  region. This unexpected energy emanates from various sources: waves produced by undetected vehicles, such as the one highlighted in the dashed box of Figure 3; vehicles traveling in the distant opposing traffic lanes which were not explicitly used in our analysis due to their low amplitude and the challenges in accurately tracking them; waves resulting from other ambient noise sources with different kinematic patterns.

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#### 4.5 Comparisons with ambient noise interferometry: better resolution and less computational expense

Figure 8 offers a comparative analysis of our innovative method and the traditional ambient noise interferometry approach. Panels (a) and (c) respectively display the virtual shot gathers constructed from the same absolute eight-hour time window for DAS recording using ambient noise interferometry and our method. Panels (b) and (d) present the corresponding dispersion images.

From the virtual shot gathers, it is clear that while both methods yield waveforms with consistent moveouts, our approach recovers a significantly greater amount of highfrequency energy. The dispersion images further demonstrate that both the fundamen-



**Figure 6.** Panels (a) and (b) show the virtual shot gathers obtained using the forward-propagating and backward-propagating wavefields shown in Figure 4, respectively. Panel (c) is the virtual shot gather obtained by combining panels (a) and (b).

tal and overtone modes from our results are more sharply defined compared to those from 322 the ambient noise interferometry approach. It's noteworthy that ambient noise interfer-323 ometry does maintain superior signal quality below 5 Hz, which is advantageous for imag-324 ing deeper earth structures. In terms of computational costs, our method processed 200 325 isolated vehicles detected over the eight-hour period. For each vehicle, we cross-correlated 326 recording in a 20-second time window, amounting to roughly 1.1 hours of data process-327 ing. In contrast, ambient noise interferometry required cross-correlation of the entire eight-328 hour recording. These comparisons underscore the enhanced effectiveness and efficiency 329 of our novel approach, highlighting its potential to deliver superior results while reduc-330 ing computational demands. 331

#### <sup>332</sup> 5 Investigation of near-surface spatial heterogeneity

Leveraging the virtual shot gathers assembled along the fiber, we conduct an indepth spatial characterization of the near surface. This involves both kinematic and amplitude analyses. The kinematic analysis focuses on the phase- and group velocity, while the amplitude analysis is centered on the assessment of seismic attenuation.



Figure 7. Panels (a), (b), and (c) show the average of virtual shot gathers for 4, 41, and 173 passing cars, respectively, at a fixed fiber location. Panels (d), (e), and (f) show their corresponding dispersion images using the negative-offset signals. Each frequency in these images is normalized by the L-1 norm. This normalization method is consistently applied throughout all dispersion images in this paper. Shaded areas show spatial high-cut filters caused by finite gauge length (16 m).

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#### 5.1 Kinematic characterization: dispersion analyses and group velocity tomography

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#### 5.1.1 Spatial heterogeneity uncovered through dispersion analysis

For dispersion analysis, we use the frequency-wavenumber method (Louie, 2001) 340 to compute dispersion images from the virtual shot gathers to obtain phase velocities 341 for different frequencies. Figure 9 provides a series of maps and images. Panel (a) offers 342 a zoomed-in view of a map for a non-built-up area, with the virtual shot location indi-343 cated by a red arrow. Panel (b) shows the virtual shot gather for this area, and panel 344 (c) presents the corresponding dispersion image derived from the negative-offset signals. 345 In contrast, panel (d) provides a zoomed-in view of a built-up area's map, where the vir-346 tual shot location is also marked by a red arrow. Panel (e) presents the virtual shot gather 347 for this built-up area, and panel (f) shows the corresponding dispersion image using the 348 negative-offset signals. 349

Comparing the virtual shot gathers from these two locations, we observe faster wave propagation in the built-up region due to the greater compactness of the soil beneath the fiber in this constructed zone. The dispersion images confirm this increased speed in the built-up area. Notably, in panel (f), a bifurcation is evident between 10 and 15 Hz due to lateral heterogeneity. We note energy around 350 m/s, consistent with the ve-



Figure 8. Comparisons between ambient noise interferometry and our method using the same eight-hour time window of DAS recording. Panels (a) and (b) are, respectively, the virtual shot gather and the corresponding dispersion image obtained using the ambient noise interferometry approach. Panels (c) and (d) are the results obtained using our vehicle-tracking-based imaging approach. Both the fundamental and overtones are resolved much better than interferometry.

- locity in the non-built-up location, and a faster velocity of about 400 m/s, which could
- relate to the compacted soil at the building foundation in the built-up area.



**Figure 9.** (a) Zoomed-in view of the map of a non-built-up region. (b) is the virtual shot gather (virtual shot location is indicated with a red arrow in (a)). (c) is the dispersion image using the negative-offset signals. (d) shows a zoomed-in view of the map of a built-up region. (e) and (f) are the virtual shot gather (virtual shot location is indicated with a red arrow in (d)) and the dispersion image using the negative-offset signals. Bifurcation due to lateral heterogeneity can be observed between 10 and 15 Hz.

Phase-velocity dispersion analyses operate under the assumption of consistent lateral velocities. Yet, as Figure 9 (f) illustrates, such uniformity isn't always present along Sand Hill Road. The bifurcation can introduce errors in selecting the appropriate phase velocity. To offer a solution to this challenge, the next subsection explores group velocity tomography, aiming for a detailed estimation of group velocities along the fiber.

#### 5.1.2 Group-velocity tomography

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To capture spatial heterogeneity in imaging, the straight-ray tomography method 363 is presented by Shapiro et al. (2005); Lin et al. (2008); de Ridder and Dellinger (2011) 364 to generate high-resolution group velocity maps through arrival time measurements. We 365 adapt this concept to implement a method of 1-D group-velocity tomography that can 366 be performed in two steps: travel-time picking and interal velocity least-square fitting. 367 To perform travel-time picking, we use a continuous wavelet transform (CWT) approach 368 on multiple virtual shot gathers with sources at different locations to extract the travel 369 times of a dominant frequency. Next, we compute the local time derivative at each fiber 370 location to obtain a rough estimate of the group velocity. To obtain smoother estimates, 371 we employ an interval velocity inversion approach. We do this by matching the predicted 372 group velocity through a least squares approach and using a smoothing operator that 373 penalizes the second derivative of the predicted group velocity. This can be formulated 374 mathematically as minimizing: 375

$$|m - v||_2^2 + \lambda ||\nabla^2 m||_2^2, \tag{3}$$

where *m* represents the interval velocity model to estimate, and *v* represents the measured group velocity obtained from travel-time picking. The second term on the righthand side is a regularization term that penalizes the roughness of the estimated model. The parameter  $\lambda$  controls the trade-off between data fidelity and model smoothness.

To improve the accuracy and reliability of the travel-time estimates, we average vir-380 tual shot gathers from approximately 2800 vehicles over a two-week period for each fiber 381 segment. The group-velocity profile for each segment is then determined by solving the 382 least-squares fitting problem with the loss function in Equation 3. For each spatial lo-383 cation, we take the median of the estimated group velocity from all the virtual shot gath-384 ers that cover it. The group-velocity profiles for 6, 7, and 8 Hz along the fiber are de-385 picted in Figure 10. According to (Aki & Richards, 2002), group-velocity images pos-386 sess a depth-integrated sensitivity, peaking at approximately half the wavelength. For 387 the frequencies analyzed, the respective depth sensitivities are 30 m, 25 m, and 21 m. 388



Figure 10. Estimated group velocity profile along the fiber line for 6, 7, and 8 Hz. Depth sensitivities for these frequencies are approximately 30 m, 25 m, and 21 m, respectively.

By comparing these profiles with the map in Figure 1, a strong correlation can be 389 observed between the profile and the geotechnical conditions along the fiber. Particu-390 larly, an increase in group velocity from 380 m to roughly 540 m is evident, correspond-391 ing to the DAS fiber passing through areas from the lawn to the built-up zone. This tran-392 sition is marked by a paved parking lot around the 540-meter mark, as shown on the map. 393 Beyond this point, the group velocity begins to decline from approximately 540 m to 650 394 m as the fiber traverses from the constructed zone to a second lawn region. This obser-395 vation aligns with our understanding that higher group velocities suggest a more com-396 pact subsurface. Additionally, in lawn regions, the 6 Hz profile, which is more sensitive 397 to deeper depths, typically exhibits a higher group velocity—evident between 650 m and 398 720 m. This suggests a more stratified subsurface. Conversely, in the built-up area, es-399 pecially from 500 m to 600 m, the velocity profiles for all three frequencies are compa-400 rable. This similarity suggests a more uniform subsurface due to the homogenization and 401 compaction from construction activities. 402

#### 403 5.2 Amplitude Analysis: seismic attenuation

Our methodology utilizes the spectral ratio method to investigate the spatial het-404 erogeneity of the seismic attenuation level along the fiber, denoted as  $Q^{-1}$ . Our approach 405 aligns with the technique used by (Zhao et al., 2023). to extract seismic attenuation from 406 traffic signals using a single seismic station. However, we enhance the reliability of our 407  $Q^{-1}$  estimates by incorporating DAS technology, which allows us to leverage multi-channel 408 recordings. The first step of our method involves converting the virtual shot gather to 409 the frequency-distance domain via a Fourier Transform for each trace. According to the 410 equation 4, the logarithm of the spectral ratio between two traces is linearly related to 411 the distance separating these traces, with  $Q^{-1}$  being proportional to the slope. 412

$$ln\left(\frac{A_1}{A_2}\right) = C - \frac{\pi(x_2 - x_1)}{Qv}f,\tag{4}$$

where  $A_1$  and  $A_2$  represent the amplitudes of the spectrum for frequency f for traces 1 and 2, respectively. The constant C is the intercept term of the linear relationship. vstands for surface-wave velocity. We select the trace at  $x_0$  of a virtual shot gather as the reference trace and compute the spectral ratio of this reference trace to the traces at distance x. A linear line representing the logarithm of the spectral ratio versus x is fitted via a least squares method to estimate  $Q^{-1}$  for some dominant frequencies.

Figure 11 illustrates the  $Q^{-1}$  estimation process using a fiber subsection as an ex-419 ample. Panel (a) depicts the negative-offset virtual shot gather with the virtual shot's 420 position at 580 m. In panel (b), the variation in spectral amplitude with distance off-421 set is presented, derived from a trace-wise Fourier transform. It's evident that higher fre-422 quencies attenuate more rapidly than lower ones, aligning with our expectations. More-423 over, the majority of the energy is concentrated within the initial 50 m. Consequently, 424 our  $Q^{-1}$  estimation focuses on this first 50 m, as shown in panel (c). This panel depicts 425 the logarithmic spectral ratio between each virtual receiver and the virtual shot record-426 ing with dots, suggesting a linear relationship. Employing a least-squares fitting method. 427 we obtain the solid lines for frequencies 8 and 10 Hz. With the slopes of these lines and 428 surface-wave velocity extracted from the dispersion curve estimated in this fiber subsec-429 tion, we estimated the  $Q^{-1}$  factors to be 0.5 and 0.45 for 8 and 10 Hz, respectively. 430



Figure 11. Illustration of the  $Q^{-1}$  estimation process over a location range spanned by a fiber subsection. (a) Negative-offset virtual shot gather, with the virtual shot located at 580 m; (b) Spectral variation as a function of distance offset; (c) Dots depict the log spectral ratio of each virtual receiver relative to the virtual shot recording. The solid lines represent the least-square fitted trends, and their slopes are used to compute the  $Q^{-1}$  value.

We performed an analysis using the virtual shot gathers generated along the fiber 431 to study the  $Q^{-1}$  profile. To ensure reliable estimates, we averaged the virtual shot gath-432 ers from approximately 2800 vehicles detected over a two-week span for each fiber seg-433 ment. The  $Q^{-1}$  value derived from these recordings is assigned to the midpoint of each 434 fiber segment. Figure 12 displays the derived  $Q^{-1}$  profile based on recordings from two 435 consecutive dry weeks. Comparing this profile with the group velocity depicted in Fig-436 ure 10, it is clear that constructed areas with a higher group velocity tend to have lower 437 attenuation. In contrast, the two lawns show higher seismic attenuation than the paved 438 area. 439



Figure 12. Profile of  $Q^{-1}$  attenuation values along the fiber-optic cable. Elevated levels of seismic attenuation are observed in the non-constructed lawn areas, which are possibly linked to the high clay content in the subsurface soil.

#### <sup>440</sup> 6 Time-lapse analysis of soil property variations

In this section, we conduct both kinematic and amplitude analyses of virtual shot
 gathers constructed over a seven-month duration. This time-lapse study highlights the
 efficacy of our proposed method in tracking alterations in soil saturation caused by rain fall events.

445

#### 6.1 Phase velocity variation and rainfall correlation

We first investigate the influence of varying rainfall volumes on the phase velocity changes within two distinct sections of fiber optic cables from early December 2022 until the middle of July 2023. The first cable section, found underneath a paved road, extends from 490 m to 590 m. The second section, nested beneath a grassy terrain, spans from 610 m to 710 m. Figure 13 (a) and (b) showcase the phase velocities, specifically at frequencies of 6, 8, and 10 Hz, selected from the dispersion images of the daily constructed virtual shot gathers, corresponding to the paved and grassy regions, respectively.

An observable decline in phase velocity is evident in the grassy area correspond ing to Figure 13 (b) following substantial rainfall from the end of December to early January. During the comparatively drier period towards the end of January, there's a slight

resurgence in phase velocity. However, this increase is short-lived as the phase velocity
dips again with the onset of rain during February and March's wet conditions. From April
to July, characterized as drier months, a gradual recovery in phase velocity can be noted.
Comparatively, in the built-up area corresponding to Figure 13 (a), the impact of rainfall events on the phase velocity's temporal variation is not as pronounced, indicating
lesser sensitivity to precipitation changes.

The observed changes in the phase velocity of Rayleigh waves due to rainfall events stem from the fundamental principles of wave propagation in porous media. As the vadose zone becomes saturated, various seismic properties of the subsurface undergo substantial alterations.

A direct outcome of the water saturation is an increase in the soil's bulk modulus, 466 attributable to water's near incompressibility. This results in an elevated compressional 467 wave velocity  $(V_p)$ . However, Rayleigh waves exhibit a stronger sensitivity to shear wave velocity  $V_s$  as opposed to  $V_p$ . This sensitivity has been empirically supported by mul-469 tiple studies. Xia et al. (1999) showed that for the fundamental mode of high-frequency 470 Rayleigh waves in a layered model,  $V_s$  is the dominant property affecting the Rayleigh 471 wave's behavior. They reached this conclusion by comparing dispersion curves of mod-472 els with 25 percent changes in each model parameter, namely  $V_s$ ,  $V_p$ , density, and thick-473 ness. This finding was later extended to the higher modes by Xia et al. (2003). These 474 studies underline the important role of  $V_s$ , which is primarily influenced by shear strength, 475 in determining the changes in Rayleigh wave velocity. 476

The area under investigation predominantly features clayish soil, as documented 477 in a USGS technical report (Pampeyan, 1993). The shear strength of this type of soil 478 is governed by frictional resistance and particle interlocking, as well as interparticle forces (Stark 479 et al., 2005). One crucial factor influencing shear strength, and thereby  $V_s$ , is the elevation in pore pressure induced by rainfall events. Excess pore pressure is particularly 481 influential in clayey soils, leading to phenomena like hydroplaning, which substantially 482 reduces internal friction (Mohrig et al., 1998; Anderson & Sitar, 1995). This increased 483 pressure also reduces effective stress in the subsurface and can lead to the formation or 484 widening of existing fractures, increasing the soil's porosity (Anderson & Sitar, 1995; Iver-485 son, 1997). These alterations have direct implications on the shear strength of the soil, 486 consequently influencing its  $V_s$ . Previous hydrogeophysical investigations utilizing both 487 conventional broadband seismic and DAS technologies have reported consistent observations, notably a decrease in  $\Delta v/v$  that correlates with elevated water table levels or 489 seasonal rainfall patterns (Clements & Denolle, 2018; Lecocq et al., 2017; Rodríguez Trib-490 aldos & Ajo-Franklin, 2021; Mao et al., 2022; Shen, 2022; Yang & Shragge, 2023). Ad-491 ditionally, the saturation process also modifies the subsurface's density. As water, pos-492 sessing a greater density than air, fills the pore spaces, the bulk density of the soil or rock 493 medium inherently rises. This augmentation in density typically results in a decrement 494 in  $V_s$  (Knight & Nolen-Hoeksema, 1990). 495

496

#### 6.2 Group-velocity tomography

In Figure 10, I presented the group velocity profiles derived from vehicles over two dry weeks. To discern the impact of rainfall on the group velocity along the fiber, we generated additional group-velocity profiles. These are based on averages of virtual shot gathers during a rainy two-week period in January for the frequencies of 6, 7, and 8 Hz. Figure 14 contrasts the profiles from dry and wet periods.

Two primarily non-built-up stretches, spanning 430 to 480 m and 650 to 670 m, exhibit a marked reduction in group velocity. In contrast, the constructed region near the 530-meter point manifests a subtler decrease. The substantial reduction in group velocity in less developed areas during rainfall can be ascribed to their enhanced perme-



Phase velocity variation corresponding to different volumes of rainfall for two Figure 13. distinct fiber optic sections. (a) The section under the paved road, ranging from 490 m to 590 m; (b) The section under the grass, extending from 610 m to 710 m. The figure illustrates the influence of rainfall on the propagation characteristics in these distinct settings.

ability. This allows for more extensive water infiltration, leading to significant changes 506 in subsurface characteristics. 507

In Figure 15, we show the temporal fluctuations of group velocity at the 430 m point 508 within the lawn area1 for frequencies of 6 Hz and 7 Hz. These variations are plotted against 509 the daily volume of rainfall within the same time span as depicted in Figure 13. The trend 510 we observe aligns with the changes seen in phase velocity - a distinct reduction during 511 the wetter months. Notably, towards the end of January, in the presence of reduced rain-512 fall, a modest uptick in group velocity is evident. However, this resurgence is brief, as 513 the group velocity diminishes once more with the commencement of rain in the wetter 514 conditions of February and March. From April onward, during the drier months, we no-515 tice a steady recovery in the group velocity. 516

517

#### 6.3 Seismic attenuation analyses

This subsection investigates the rain-induced property changes from an amplitude 518 perspective. To investigate the influence of rainfall on seismic attenuation across the DAS 519 array, we derived a  $Q^{-1}$  profile from recordings on both dry and wet days. In Figure 16, 520 the blue curve represents the  $Q^{-1}$  profile deduced from dry day recordings, while the or-521 ange curve corresponds to those from wet days. It's noteworthy that heightened atten-522 uation levels are evident in lesser-developed regions, particularly between the stretches 523 of 430 - 500 meters and 650 - 750 meters. 524

Figure 17 exhibits the temporal  $Q^{-1}$  variations plotted against the daily rainfall 525 volume at the 465 and 675-meter marks in the two lawn areas. This observation period 526 aligns with the timeframes depicted in Figures 13 and 15. During rainfall events, there 527 is a substantial increase in attenuation. Towards the end of January, when rainfall was 528 less frequent, we notice a slight decrease in attenuation. However, during the rainfall events 529 in February and March, the attenuation increases again. From April onward, we observe 530



**Figure 14.** The group-velocity profile along the fiber. The blue curves in (a), (b), and (c) represent the profiles derived from averaging the virtual shot gathers over a dry two-week period in December for frequencies of 6, 7, and 8 Hz, respectively. The orange curves illustrate the profiles obtained by averaging virtual shot gathers over a wet two-week period in January for the same frequencies. These curves show a notable drop in group velocity at two relatively non-built-up areas, while the drop in the built-up region is less pronounced, indicating the influence of rainfall on group velocity along the fiber.



Figure 15. This figure displays the temporal variations in group velocity at the 430m mark within the lawn area1, as highlighted in Figure 14. The observed trend, characterized by a significant reduction in group velocity during the wetter months, shows a subtle resurgence in group velocity towards the end of January with reduced rainfall. The trend aligns with the variations observed in phase velocity, followed by recovery in group velocity during subsequent drier periods.

that attenuation gradually decreases during dry periods. This suggests that seismic waves 531 are more strongly scattered and absorbed due to increased water content. One plausi-532 ble explanation for this heightened attenuation during wet conditions is the increased 533 pore pressure induced by rainfall. According to A. I. Best and McCann (1995); A. Best 534 et al. (1994), the compliant and microporous nature of clay minerals in the soil allows 535 for the phenomenon of squirt flow, which becomes more active with higher pore-fluid pres-536 sure. Squirt flow, involving rapid movement of fluids between tiny pores, effectively at-537 tenuates seismic waves as they pass through the medium. Therefore, the increased at-538 tenuation levels during rainfall events provide a sensitive measure of changes in soil sat-539 uration and pore pressure. 540

#### 541 7 Conclusions

In this study, we introduce an innovative near-surface monitoring approach that 542 uses vehicles as non-dedicated seismic sources. Our method enhances the traditional am-543 bient noise interferometry by improving high-frequency sensitivity, boosting computa-544 tional efficiency, and offering superior spatiotemporal resolution in subsurface monitor-545 ing. We have demonstrated the efficacy of our technique in monitoring rainfall-induced 546 soil seismic property changes along a roadside DAS array at Stanford, achieving a level 547 of spatiotemporal resolution previously impractical with traditional active source sur-548 veys and ambient noise interferometry. Our observations reveal significant alterations 549 in phase and group velocity during rainfall events, as well as increases in seismic atten-550 uation, particularly in non-built-up areas. These findings can potentially enhance urban 551 water resource monitoring, including the early detection of water leakages. 552



**Figure 16.**  $Q^{-1}$  profiles for dry and wet days. Higher attenuation due to the rain can be observed for 10 Hz.



Figure 17. Temporal variations of the  $Q^{-1}$  parameter (estimated at 10 Hz) in correlation with the estimated daily rainfall volume at fiber ranges centered at 465 m and 675 m within the two lawn areas, over a timeframe consistent with Figures 13 and 15. A pronounced increase in attenuation is evident during rainfall events, whereas towards the end of January, a slight decrease in attenuation is observed due to reduced rainfall. This attenuation pattern then gradually reduces in drier periods following.

#### 553 Data and Software Availability Statement

The data supporting the conclusions of this study are derived from continuous DAS recordings captured by the Stanford DAS-2 array. Due to the extensive size of the dataset, we selected ten days' recordings from December 15th to December 24th, 2022, during dry conditions. This data is publicly available at https://premonition.stanford.edu/syyuan/stanforddas-2-data-for-near-surface-characterization.

Separately, recordings from wet days in February 2023 have been published in line with the Global DAS Month initiative (NORSAR, 2023). This data set can be retrieved via the Globus platform, targeting the PubDAS endpoint (Spica et al., 2023). Navigate to the DAS-Month-02.2023/Stanford-SandHill/ directory for the DAS recordings. Direct access to the PubDAS Globus endpoint at the University of Michigan is facilitated through the following link: https://tinyurl.com/PubDAS.

The software for the proposed precision interferometry method introduced in the paper is publicly available in https://github.com/syyuan93/das\_veh.

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