Complex multi-scale preparatory processes of stick-slip events on rough laboratory faults

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¹ Intermittent criticality multi-scale processes

² leading to large slip events on rough

a laboratory faults

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18 Key points:

- 19 We study preparatory processes preceding large slip events on rough laboratory faults using seismo-
- 20 mechanical features derived from AE data
- The analysis highlights multi-scale rapidly evolving damage, roughness and stress changes along thefault surface
- 23 Intermittent criticality marked by evolving stress correlations on different length scales can explain
- 24 the observed patterns leading to large labquakes

25 Abstract

26 We discuss data of three laboratory stick-slip experiments on Westerly Granite samples performed 27 at elevated confining pressure and constant displacement rate on rough fracture surfaces. The 28 experiments produced complex slip patterns including fast and slow ruptures with large and small 29 fault slips, as well as failure events on the fault surface producing acoustic emission bursts without 30 externally-detectable stress drop. Preparatory processes leading to large slips were tracked with an ensemble of ten seismo-mechanical and statistical parameters characterizing local and global 31 32 damage and stress evolution, localization and clustering processes, as well as event interactions. We 33 decompose complex spatio-temporal trends in the lab-quake characteristics and identify persistent effects of evolving fault roughness and damage at different length scales, and local stress evolution 34 35 approaching large events. The observed trends highlight labquake localization processes on different 36 spatial and temporal scales. The preparatory process of large slip events includes smaller events 37 marked by confined bursts of AE activity that collectively prepare the fault surface for a system-wide 38 failure by conditioning the large-scale stress field. Our results are consistent overall with an evolving 39 process of intermittent criticality leading to large failure events, and may contribute to improved 40 forecasting of large natural earthquakes.

⁴¹ Plain language summary

42 We discuss failure events in laboratory experiments on a rough fault performed at pressures existing 43 in the Earth's crust. The laboratory faults were subjected to constant displacement resulting in short-44 lasting slips of their fault surface. We observe complex slip patterns including fast/slow ruptures 45 with large/small fault slips. Very small slips on the fault surface were observed only with acoustic 46 emission (AE) activity, representing tiny earthquakes of sub-mm size that produce elastic waveforms 47 that can be recorded with piezo sensors. Using parameters derived from AE data, we analyzed physical processes leading to large slip events of the lab fault surface, an equivalent of a large 48 earthquake in nature. Our parameters characterize local and global damage, stress, as well as 49 interactions of small fractures before the labquake. We identify evolving fault roughness at different 50 51 length scales, and find that the preparatory processes preceding lab quakes are facilitated by small 52 earthquakes marked with bursts of AE activity. These bursts indicate ruptures of individual fault 53 patches, which then interact and collectively prepare the fault surface for the labquake. Our results 54 provide a set of physics-based parameters describing complex processes leading to lab slip events 55 that may allow to improve earthquake forecasting along natural faults.

56 1 Introduction

57 Fault processes leading to large earthquakes have occasionally been observed to produce foreshock 58 activity and aseismic transients, sometimes lasting months or even years prior to the main shock 59 (Kato et al., 2012; Bouchon et al., 2013; Schurr et al., 2014; Durand et al., 2020; Meng and Fan, 2021; 60 Kwiatek et al., 2023). Seismic and aseismic precursors signifying fault damage evolution and 61 progressive localization towards large dynamic ruptures are not well understood due to limited availability and resolution of seismic data and widely varying structures and properties of fault zones 62 63 (e.g., Ben-Zion, 2008, and references therein). The role of precursory observables during the 64 preparatory process before earthquakes and their potential use for forecasting remain controversial (Geller et al., 1997; Bakun et al., 2005; Ogata and Katsura, 2012; Wu et al., 2013; Mignan, 2014). 65 66 Existing physical models describing the preparation and nucleation process on large pre-existing faults motivated by field and laboratory studies (Dieterich, 1978; Ohnaka, 1992; Ellsworth and 67 Beroza, 1995; McLaskey, 2019; Kato and Ben-Zion, 2021) converge towards a combination of 68 69 processes including accelerating preslip and, in some cases, cascading foreshocks. However, fault 70 heterogeneity and structural variability of fault zones result in rich and varying observational 71 phenomena, that often defy clear interpretation. Thus, seismic hazard assessment and earthquake 72 forecasting still largely rely on probabilistic approaches (Ogata, 1999; Lippiello et al., 2019; Hirose et 73 al., 2021; Mizrahi et al., 2023). The observation of a plethora of physical preparatory processes 74 requires high-resolution monitoring of both seismic and aseismic failures using frequency bands that 75 are hardly achievable in nature.

Laboratory experiments performed on intact and faulted rock samples with varying loading 76 77 conditions have provided a wealth of observations characterizing the effects of roughness, gouge 78 material, loading rate, effective normal stress, and stiffness ratio of the fault and loading system on 79 long-term deformation leading to failure (Latour et al., 2013; Mclaskey and Yamashita, 2017; 80 Leeman et al., 2018; Guérin-Marthe et al., 2019; Scuderi et al., 2020; Gounon et al., 2022; Morad et 81 al., 2022). Motivated by experimental results, various studies (Ohnaka, 1992; Dieterich and Kilgore, 82 1996; Ben-Zion and Rice, 1997; Ohnaka and Shen, 1999; Latour et al., 2013) have suggested to separate the preparatory phase into a quasi-static phase and an accelerating phase producing 83 84 dynamic slip (e.g. Okubo and Dietrich, 1984). This transition is often only loosely defined by the 85 onset of a local or system-wide decrease in shear stress leading to an abrupt stress drop or transition in rupture velocity, and an overall change of energy flux into the rupture front tip. In a complex and 86 87 heterogeneous fault zone, the preparation phase may be long-lasting. The transition towards 88 nucleation of a large rupture involves a localization process, distributed creep transients and

collective failure of a range of asperities (de Geus et al., 2019; Lebihain et al., 2021; Yamashita et al.,
2021; McBeck et al., 2022). These processes lead to redistribution of stresses along the fault zone at
different length scales, reflecting the multi-scale evolution of roughness at the level of granular
material forming the fault zone, cm-scale asperities and large-scale structural inhomogeneities.

93 These multi-scale preparatory processes before large laboratory slip events are typically 94 accompanied by Acoustic Emission (AE) activity that allows monitoring key seismo-mechanical 95 processes and local stress evolution during the deformation cycle. Parameters derived from AE data 96 showed changes in clustering and localization of AE hypocenters, AE magnitude-frequency 97 distributions, ultrasonic velocities, inter-event triggering and other statistical attributes approaching 98 failure (Bolton et al., 2023; Main, 1991, 1992; Lockner, 1993; Zang et al., 1998; Goebel et al., 2012, 2013, 2014; Kwiatek et al., 2014b; Davidsen et al., 2017, 2017, 2021; Scuderi et al., 2017). Typically, 99 100 AE-derived parameters from stick-slip cycles exhibit general trends, which are punctuated and 101 partially reversed by large failure events. Although the observed trends for some parameters during 102 the preparatory slip indicate progressive damage and localization, estimating time-to-failure is still 103 challenging.

104 Forecasting the origin time of future large earthquakes remains a challenge if not an impossible task. 105 In recent years, earthquake forecasting made a leap using new opportunities provided by Artificial 106 Intelligence (AI) techniques. These techniques demonstrated an ability to predict time-to-failure in 107 direct shear laboratory tests on smooth faults (Johnson et al., 2021), as well as on analog models, natural and induced seismicity, and synthetic modeling (e.g. Corbi et al., 2019; Johnson et al., 2021; 108 109 McBeck et al., 2021). Such studies use a number of potential precursory parameters derived from 110 seismic waveforms or earthquake catalogs (see e.g. Rouet-Leduc et al., 2017; Lubbers et al., 2018; 111 Hulbert et al., 2019; Picozzi and Iaccarino, 2021). Johnson et al. (2021) noted that successful cross-112 scale earthquake forecasting requires generalization of predictive models and a better physical understanding of input and output parameters. The former involves extension of the predictive AI-113 114 aided modeling to studies of rough faults, whereas the latter requires a clear linking of AE-derived 115 precursory parameters with observable damage and stress evolution on different spatio-temporal 116 scales.

117 In this study we employ large AE datasets from laboratory stick-slip experiments involving a series of 118 tests performed on rough pre-fractured faults (e.g. Goebel et al., 2012;2013; 2014). The experiments 119 produced complex slip patterns including large and small slips of the fault surface (characterized by 120 large and small stress drops), and confined slips (with stress drops not measurable with the internal 121 load cell) accompanied by AE data bursts. The multi-scale preparatory processes preceding systemwide slip events are analyzed with a set of physics-motivated AE-based features characterizing the seismo-mechanical spatio-temporal processes occurring on the fault. These include parameters describing damage and stress evolution, localization and clustering, event interactions, and local micromechanics and stress heterogeneity. We decompose the observed trends and discuss them in the context of roughness evolution at different spatial scales, a crossplay of local and global damage, and multi-scale stress evolution when approaching a system-size event.

128 2 Data and methods

129 2.1 Experimental setup and acoustic emission monitoring

130 Three triaxial stick-slip tests WgN04, WgN05 and WgN07 were conducted on cylindrical samples of 131 Westerly Granite with dimensions of 40 mm diameter × 107 mm length (Goebel et al., 2012, 2013, 2014, 2015). Samples were prepared with a 2.5 cm deep notch inclined at 30° to the cylinder axis to 132 133 guide formation of a shear fracture. The samples were first oven-dried at 100°C and subsequently 134 encapsulated in a rubber sleeve to prevent the intrusion of the confining medium (oil). The 135 specimens were fractured at 75 MPa confining pressure creating naturally fractured rough fault surface. To perform a series of subsequent stick-slip experiments, the faults were locked by 136 137 increasing the confining pressure to 150 MPa. For the initial fracture and subsequent stick slip tests, 138 the samples were loaded axially using a constant displacement rate of 0.02 mm/min = 0.33μ m/s. 139 Subsequent axial loading cycles were applied by advancing the piston at constant displacement rate resulting in an axial strain rate 3×10⁻⁶ s⁻¹. Displacement and axial force were recorded using a linear 140 variable displacement transducer fixed to the piston and external/internal load cells, respectively. 141

142 We performed a series of tests on the three different Westerly granite samples WgN04, WgN05 and 143 WgN07 containing rough faults (Goebel et al., 2012, 2013, 2014, 2015) but here we present data 144 from an illustrative stick-slip test (WgN05) that was further studied in greater detail in Dresen et al. 145 (2020) and Blanke et al. (2021). The recorded AE data, mechanical data and output parametric data from all three experiments are available in the associated data publication (Kwiatek and Goebel, 146 147 2023; see also Supplementary Information Figs. S5-S6 and Open Data section). The fault roughness in these experiments caused a complex stick-slip pattern with a variety of stress drops including five 148 large slip events with large stress drops (LSD) of > 100 MPa preceded by a varying number of events 149 with smaller slip and small stress drops (SSD), as determined from the axial stress data in Goebel et 150 151 al. (2013 2015). They are shown in Figure 1 and Figs. S5-S6. Both LSDs and SSDs are accompanied by 152 a large clipped signal on the AE data, representing relatively large laboratory events (see e.g. Fig. 3 in Goebel et al., 2012). 153

154 Loading and stick-slip events produced AEs, here indicating ~mm-scale fracturing and frictional 155 processes occurring on the grain scale (cf. Blanke et al., 2021). AE activity was recorded by sixteen AE 156 sensors with resonant frequency 2 MHz embedded in brass housings and glued directly to the 157 specimen surface, securing an almost complete azimuthal coverage of AE events. The event 158 waveforms were recorded in triggered mode at 10 MHz sampling rate with 16-bit amplitude 159 resolution. Throughout the experiment, repetitive P-wave velocity measurements were performed using ultrasonic transmission providing a time-dependent velocity model composed of five equally-160 161 spaced horizontal layers (with associated velocity) and single measurement of averaged vertical velocity (Stanchits et al., 2006). The velocity model was updated every 30 s during the course of the 162 163 experiment.

164 2.2 Mechanical behavior and AE response

165 We now describe the evolution of mechanical parameters and associated AE response for an 166 illustrative sample WgN05 following the conventions presented already and discussed in Goebel et 167 al. (2012, 2013, 2014, 2015). Mechanical evolution for samples WgN04 and WgN07 is presented in 168 the supplementary information (Figs. S5-S6), and the input catalog data are available in the 169 associated data publication (Kwiatek and Goebel, 2023). Sample WgN05 displayed large axial stress 170 drops measured in the S1 direction of $\Delta \sigma > 100$ MPa, slip duration of 0.2 - 0.4 s and slip velocity (corrected for machine stiffness) of at least 1.2 - 1.6 mm/s, which is at least 1000 times larger than 171 172 the applied loading rates (cf. section 2.1, Fig. 1, Supplementary Table S1). Note that peak slip 173 velocities for LSDs were not resolved due to the limited sampling rate of the geomechanical data (10 174 Hz). All LSDs were followed by rapid initial reloading lasting ca. 50 s and a longer period of almost 175 linear stress increase lasting typically no more than 1000 s. Further axial displacement beyond a yield point was accommodated by plastic deformation along the fault zone and in its surroundings 176 177 (cf. Dresen et al., 2020). We attribute most of the deformation during this part of the loading to shear-enhanced compaction of the granular material forming the fault gouge (Kwiatek et al., 2014b; 178 179 Goebel et al., 2017), as illuminated by the AE activity spreading over the whole fault surface (Fig. 1e, 180 h).

181 Cm-scale roughness of the fault surface (cf. Fig. S7) results in multiple small slip events with low 182 stress drops (SSDs), as defined in e.g. Goebel et al. (2012), which typically occur at elevated axial 183 stress with $S_1 > 400$ MPa. The AE activity associated with these SSDs is distributed over significant 184 parts or the entire fault surface (Fig. 1d, g). Stress drops of SSDs range $1<\Delta\sigma<20$ MPa and slip 185 velocities range <0.05-0.2 mm/s (Supplementary Table S1). The lower observable limit of SSDs' stress drops and slip velocity is due to the periodic noise of stress measurements caused by the servo-controlled MTS loading system.

188 The macroscopic displacement and stress drop recordings of LSDs and SSDs indicate detectable and 189 relative movement of fault-bounding blocks across the entire fault surface (Supplementary Movie 190 S1). The nucleation of both LSDs and SSDs is associated with extremely large AE events with clipped 191 waveforms following the first P-wave arrival (e. g. Goebel et al., 2012, Fig. 3, Goebel et al., 2015, 192 Fig. 5) and followed by a long coda wave indicating slip over the surface. This coda leads to a 193 temporally higher AE event detection threshold due to low-frequency noise resulting from 194 comminution and shearing of granular material and debris forming the fault surface while the fault is 195 slipping (gray area in Fig. 1e). The duration of the AE system saturation time period lasts 20-120 ms 196 and qualitatively scales with the duration of macroscopic slip and stress drop magnitude (cf. 197 Supplementary Table S1). The enhanced low-frequency noise is expected to mask very early AE 198 events directly following the LSDs.

199 In addition to LSD and SSD events resulting in externally measurable axial stress drops, we visually 200 identified short-lasting bursts in AE activity due to slips confined in the sample that were mostly not 201 recorded in the mechanical data (i.e. the externally measured axial stress drop is below $\Delta\sigma < 1$ 202 MPa). These local confined slips with no externally measured stress drop (CSD) were attributed to 203 local asperity failures providing a significant AE footprint with very localized AE activity that is most 204 prominent in the early stick-slip cycles (cf. Fig. 1c, f; Supplementary Movie S1; see also Goebel et al., 205 2012, 2015). Like LSD and SSD, each CSD is also associated with a large AE event followed by smaller 206 AEs (AE aftershocks) and occasionally preceded by increasing AE activity (AE foreshocks, see results 207 section for details).

208 2.3 AE Catalog Development

The development of an AE catalog from the experimental data is an upgraded procedure originally developed by Stanchits et al., (2006). Here, we summarize key and new processing steps relevant for evaluating the time-dependent AE characteristics.

The first P-wave arrivals of AE events were picked automatically using the Akaike Information criterion followed by pick refinement using the modified Convolutional Neural Network picker (Ross et al., 2018) trained on past AE data sets. Based on a time-dependent quasi-anisotropic velocity model, the resolved picks were used to invert for hypocenter locations and origin time using a grid search algorithm paired with the Coyote optimization algorithm (Pierezan and Dos Santos Coelho, 2018). The hypocenter location accuracy is estimated to be about ±2 mm, constrained, in part, by the selected Root-Mean-Square Deviation (RMSD) of travel time residuals (for the following analysis we selected locations with RMSD < 0.5 μ s). Then, the first *P*-wave amplitudes were corrected for hypocentral distance and incidence angle and for the coupling quality of AE sensors using an ultrasonic calibration technique (Kwiatek et al., 2014a). The average AE amplitude and AE magnitude were calculated from first P-wave amplitudes (Zang et al., 1998):

223
$$\underline{A_{AE}} = \frac{1}{n} (\sum_{i=1}^{n} (A_i R_i)^2)^{0.5}, \tag{1}$$

224
$$M_{AE} = log_{10}(A_{AE}),$$
 (2)

where A_i and R_i are corrected first P-wave amplitude and source-receiver distance for sensor *i*, respectively (cf. Dresen et al., 2020). The here used AE magnitude estimate reveals relative size differences between AE events but it is not directly calibrated to the physical size of the events (cf. Goodfellow and Young, 2014; McLaskey et al., 2014; Yoshimitsu et al., 2014; Blanke et al., 2021).

229 For each AE event, a full moment tensor (FMT) inversion was performed using the hybridMT software and first P-wave amplitudes and durations of the first P-wave pulses (Kwiatek et al., 2016; 230 231 Martínez-Garzón et al., 2017) corrected for coupling quality and incidence angle (Kwiatek et al., 232 2014a). The resulting FMTs were decomposed into isotropic and deviatoric parts (e.g. Vavryčuk, 233 2001; 2014). From the deviatoric part of the FMTs, we extracted the P-, T-, and B- axes directions (azimuths and plunges) and slip directions. A P- (T-, B-) axis plunge equal to 90° and 0° corresponds 234 235 to the direction of maximum compression S_1 and the direction perpendicular to it, respectively. The 236 two sets of nodal plane parameters (strike, dip, rake) were extracted from the deviatoric part of the 237 seismic FMT of each AE event.

238 The analyzed catalog form WgN05 sample contains N=310,815 located AEs with 239 $N(M_{AE} > M_{C,AE}) = 169,825$ above the magnitude of completeness $M_{C,AE} = 1.5$ estimated using the 240 goodness-of-fit method (Wiemer and Wyss, 2000) assuming that 95% of the catalog is explained by the Gutenberg-Richter power law. The FMTs were strongly quality-constrained, first at the input 241 242 data selection (we only accepted input data where amplitude could be measured at all sensors), and then using as an uncertainty measure the maximum value of the diagonal elements of the 243 244 covariance matrix normalized by the average AE amplitude, ε (see details hybridMT documentation, Kwiatek et al., (2016). Assuming, $\epsilon < 0.1$ and $N_{\text{stations}} = 14$, this resulted in a strongly reduced 245 246 number of N(FMT)=17,963 high-quality FMTs. The resulting catalog containing origin time, AE location in the local Cartesian coordinate system of the sample, AE magnitude, FMT parameters 247 248 including strike, dip, rake, the MT decomposition and orientation of P-, T- and B- axes, as well as associated location and MT inversion uncertainties is available in an associated data publication(Kwiatek and Goebel, 2023).

251 2.4 Time series of AE parameters

For all three samples we analyzed the temporal evolution of a total of 10 parameters (features) 252 253 derived from the AE catalog and defined onsets of informative changes of these parameters with 254 regard to global damage and stress evolution and potential cross-correlations between different 255 proxies. The selected parameters were utilized to characterize the development of local damage and 256 stress evolution on and around the fault during the preparatory phases of five LSDs. The predictive 257 AE-modeling of the time-to-failure, aggregating the input data from all three experiments, as well as 258 unsupervised classification of the preparatory phase are subjects of separate manuscripts 259 (Karimpouli et al., 2023a, b).

The temporal evolution of all AE parameters was calculated using sliding time windows of different lengths (ranging 1%-12% of the average length between consecutive LSDs, see Table 1) to better represent the development of short- and long-term processes. The calculated parameter values were assigned to the origin time of the last AE event included in each time window. We ignored time windows which overlap with the occurrence of LSDs to avoid mixing precursory AEs with those following LSD. In the following, we describe the 10 different AE parameters listed in Table 1 and subsequently used for tracking the preparatory processes.

267 **(1) AE event rate:** The AE event rate \dot{N} (unit: [1/s]) has been calculated for the catalog of events with 268 $M_{AE}>M_{AE,C}$ as the number of AEs divided by the duration of the moving time window. It represents 269 the intensity of seismic activity across the whole fault surface and characterizes the damage (cf. 270 Goebel et al., 2014).

271 **(2) b-value:** The slope from the magnitude-frequency Gutenberg-Richter (GR) relation indicates the 272 proportion between the number of small and large AE events in a selected population. The *b*-value is 273 calculated from AE events with magnitudes above the magnitude of completeness $M_{AE}>M_{AE,C}$ using 274 the maximum likelihood method while including a correction for the histogram bin size (e.g. Lasocki 275 and Papadimitriou, 2006). Changes in *b*-values are thought to be governed by rock damage evolution 276 (e.g. Main, 1991), changes in local stress (Scholz, 1968; Schorlemmer et al., 2005), and geometric 277 complexity and roughness (Goebel et al., 2013; 2017).

(3) d-value: The fractal dimension *d* from a population of AE hypocenters has been calculated using
 the boxcount algorithm (i.e. Minkowski–Bouligand dimension, see Moisy, 2022). We used

hypocentral locations [X, Y, Z] of AEs with location quality constrained by the RSMD<0.5 [μs]. The *d*value characterizes the geometry of the AE spatial distribution of AE with *d*=3, *d*=2, and *d*=1 corresponding to volumetric, planar and linear Euclidean distribution of AE hypocenters, respectively. Contrary to the *d*-value estimated using correlation integral, which is sensitive to point-clustering of the hypocentral locations, the box-counting method solely responds to the bulk geometry of AE hypocenter distribution.

286 **Clustering of AE events in space, time and magnitude domain:** We identified clusters of AE events 287 according to their space-time-magnitude nearest-neighbor proximity (Zaliapin et al., 2008; Zaliapin 288 and Ben-Zion, 2013a; 2013b). Specifically, we investigated the proximity of an event *j* to an earlier 289 event *i* in a combined space-time-magnitude domain (Baiesi and Paczuski, 2004) defined as:

290
$$\eta_{ij} = \{t_{ij}(r_{ij})^a 10^{-bm_i}\}, t_{ij} > 0, \infty, t_{ij} \le 0,$$
 (3)

where $t_{ij} = t_j - t_i$ and r_{ij} are the temporal and spatial distances between the earthquakes *i* and *j*, respectively, *b* is the *b*-value from the GR distribution, *d* is the fractal dimension, both estimated as described above, and m_i is the magnitude of the earlier event in time. The scalar proximity η_{ij} between events can be expressed as the product of its temporal and spatial components scaled by the magnitude of the earlier event *i*:

$$296 \qquad \eta_{ij} = T_{ij} \cdot R_{ij}, \tag{4}$$

with $T_{ij} = t_{ij} 10^{-qbm_i}$ and $R_{ij} = (r_{ij})^d 10^{-(1-q)bm_i}$, $0 \le q \le 1$. We fixed q = 0.5, providing equal 297 magnitude weights to the scaled temporal and spatial distances. To estimate the spatial distance 298 between events we used hypocentral locations. We denote η_i the shortest of the proximities 299 between event j and all earlier events. The distributions of the nearest-neighbor proximities η_i in 300 301 earthquake catalogs tend to be bimodal (Zaliapin and Ben-Zion, 2013a, Zaliapin and Ben-Zion, 2016; 302 Martínez-Garzón et al., 2019). The mode with larger event proximities η_i corresponds to *background* 303 Poissonian-like seismicity, while potentially appearing mode with smaller event proximities η_i 304 indicates *clustered* events, i.e. foreshocks and aftershocks (Zaliapin et al., 2008). The separation 305 threshold between these two modes is estimated by fitting a Gaussian mixture model 306 (Supplementary Figure S2).

307 Using the above method, we identify AE clusters that are connected by proximity links smaller than 308 the estimated threshold. Each AE connected to the parent by a link longer than the threshold is 309 considered a *background* event and starts a new cluster. A *single* is a cluster that consists of one 310 background event with no associated foreshocks or aftershocks, while multiple-event clusters are called *families*. The largest event in each cluster is called *mainshock*; all events within the cluster before or after the mainshock are called *fore/after-shocks* (see Fig. 6 of Zaliapin and Ben-Zion, 2013a). Due to the short-term saturation of the AE recording system during large slip events LSD1-LSD5 (see more details in the results section), the clustering analyses have been performed separately for each phase P1-P5 (Fig. 1a). This means that early aftershocks from previous slip for phases P2-P5 are not well resolved, biasing the separation between foreshocks, aftershocks, mainshocks and singles shortly after the LSDs.

The temporal changes in AE clustering properties occurring on grain-scales have been analyzed using a sliding time window. We calculated temporal evolution of four parameters, including the **(4) median proximity** parameter η :

$$321 \quad \hat{\eta} = median\{\eta_j\},\tag{5}$$

defined as a median of the decimal logarithm scalar proximities (eq. 4) of AEs, and the fraction of AE (5) foreshocks (p_{FO}), (6) aftershocks (p_{AF}), and (7) background (mainshocks and singles altogether) (p_{MA}) in each examined time window (with $p_{AF}+p_{FO}+p_{MA}=1$).

The **(8) median fault plane variability** $\widehat{\psi_f}$ characterizes the level of heterogeneity in the distribution of the focal mechanisms (Martínez-Garzón et al., 2016; Goebel et al., 2017; Dresen et al., 2020). This is a generalization of rotation angle between pairs of focal mechanisms (Kagan, 2007) applied to an ensemble of pairs of AEs with focal mechanism solutions located nearby. A small 3D rotation angle (<20°) between the P/T/B axes of two mechanisms indicates a high degree of similarity, and 0° means they are identical.

We compute the spatial variability of focal mechanism similarity across the laboratory fault and rock sample. Spatial variability is determined from 20 nearest AE neighbors located within R<10 mm of the specific AE event by calculating the respective median 3D rotation angle between all focal mechanism pairs (e.g. for 20 AE focal mechanisms there are 190 pairs). This procedure was repeated for each AE event to resolve the spatial heterogeneity/similarity of focal mechanism variability across the whole fault plane. The focal mechanism variability for a particular time window was then estimated as the median of locally calculated values.

(9) Plunge of local maximum principal stress $\delta_{\sigma 1}$ and (10) local stress (orientation) variability $\widehat{\Psi_{\sigma ij}}$: Using calculated MTs we performed a linear stress tensor inversion using the STRESSINVERSE package (Vavryčuk, 2014). We follow the sign convention that compressive stress σ is positive with $\sigma_1 > \sigma_2 > \sigma_3$. Similarly to median fault plane variability $\widehat{\Psi_f}$, for each time window, we first

calculated the spatial distribution of local stress tensors for each location where at least 40 focal mechanisms were available within a 10 mm distance. The input focal mechanism data were resampled and then inverted 200 times by randomly selecting either of the two nodal planes for each focal mechanism, suppressing the problem of fault plane ambiguity (e.g. Martínez-Garzón et al., 2014) in the input focal mechanism data. From this we obtained the spatial distribution of local stress tensors for a particular time window.

In the following, for each local stress tensor, we extracted the plunge of maximum principal stress $\delta_{\sigma 1}$ which is given by the eigenvector corresponding to the largest eigenvalue of the input stress tensor. Finally, we averaged maximum principal stress plunges from the whole fault surface. For plunges of $\delta_{\sigma 1}$ = 90° the local principal stresses averaged over the sample surface are aligned with the macroscopic vertical loading stress direction S₁.

The second parameter describing the local stress tensors is the tensor variability $\Psi_{\sigma ij}$, which was calculated with the same procedure as for the focal mechanism variability estimation. For each time window, we calculated the median out of an ensemble of rotation angles between all possible pairs of local stress tensors. Low values of $\Psi_{\sigma ij}$ suggest that local stress tensor orientations over the fault surface are similar.

358 3 Results

Here we present and describe representative time series for each of the above parameters describing the evolution of the fault system in sample WgN05. The results for samples WgN04 and WgN07 are presented in the supplementary information (Figs. S5-S6).

362 3.1 AE Rates

363 The AE rates display a short-term (within each phase P1-P5 leading to the LSD) as well as a long-term (across whole experiment) evolution with progressive deformation of the sample (Figure 2b). The 364 long-term evolution is characterized by an overall decrease of peak AE rates \dot{N} (Fig. 2b). The 365 individual phases P1-P5 preceding LSD1-LSD5 display exponentially increasing \dot{N} when approaching 366 367 failure (Fig. 2b). The LSD nucleation point is illuminated by a large AE event located using P-wave 368 arrivals. Once the elevated noise from saturation of the AE system drops to background level, AE aftershocks become visible, displaying a 1/T^p (Omori-type) decrease of AE rates typically lasting no 369 370 more than about 20 seconds following the actual stress drop (cf. Supplementary Figure S1). The 371 aftershock rates then decrease with consecutive LSDs suggesting bulk smoothing of the fault surface.

372 The increase of AE rates N during each phase P1-P5 is punctuated by multiple short-lasting bursts of AE activity following SSDs and CSDs characterized by AE rates decreasing as 1/T^p over a short period 373 374 of time (typically < 10 s, Figure S1). All SSDs and all but one CSD show no acceleration of AE rates up 375 to failure (cf. Supplementary Figure S1). Only the second CSD (T=3672.8 s) that occurred in phase P1 376 show a visible acceleration of AE rates (Supplementary Figure S1b). The SSDs and CSDs tend to 377 reduce the overall long-term AE rates in phases preceding LSDs (Figure 1b). AE rates are closely 378 related to slip rate at any spatial scale (i.e. at long-scale representing the sample size and the short-379 scale representative of asperity size). However, there is no clear relation of peak AE rates with stress 380 drop magnitude.

381 3.2 Gutenberg-Richter *b*-value

The temporal evolution of the *b*-value (Fig. 2c) displays low *b*-values associated with CSD and SSD events (cf. Goebel et al., 2013) through all phases P1-P5, but especially during P1 and P2. This suggests that the change in *b*-value acts as a proxy generally indicating small- (cm-scale) local ruptures confined in the sample at high levels of stress. In general, a decrease in *b*-value indicates an approach to system-wide failure (LSD).

387 From phase P3 onwards, CSDs and SSDs are less prominent and the temporal trends of the *b*-value 388 become somewhat more uniform and gradual. This may reflect a global conditioning process of the 389 whole fault surface, progressive localization and overall reduction of the fault roughness at the scale 390 of the whole sample. In P3-P5, prior to the LSDs, the *b*-values visibly decrease, and then recover to 391 b=1.4-1.6 during the initial part of the subsequent loading cycle. The amplitude of the *b*-value 392 recovery following the LSD is likely affected by the saturation of the AE acquisition system which 393 masks smaller aftershocks immediately following LSD, presumably reducing the jump in b-value in 394 early post-slip phases. The decreasing *b*-value before some of the CSDs and SSDs typically becomes 395 more evident if the AEs are additionally spatially constrained to those related to the activation of 396 specific patches (see e.g. Goebel et al., 2012). Overall, the localized slips (CSDs and SSDe) tend to be 397 preceded by a *b*-value decrease irrespective of the amplitude of macroscopic slip, thus the *b*-value is 398 predominantly sensitive to the long-term temporal evolution (sample-wide) as well as cm-scale 399 (asperity size) changes throughout the first phases P1-P2.

400 3.3 Fractal dimension

The *d*-values derived with the boxcounting method are primarily sensitive to the spatial distribution of AEs, and less sensitive to AE density, as for example *d*-value estimations based on the correlation

403 integral. A *d*-value of about 2.0 corresponds to an AE hypocenter distribution across the fault 404 surface. In contrast, *d*-values < 2.0 indicate formation of distinct AE lineaments or clusters within the 405 fault zone. The evolution of the *d*-value during individual stick-slip cycles leads to a general increase 406 of the *d*-value ahead of each major LSD, signifying the overall increase in the AE activity across the 407 entire fault surface as a consequence of the increased contact area between the two faces of the 408 fault. The AE activity immediately following the LSDs is characterized by higher *d*-values that quickly decrease within the first 50-100 seconds following the LSD. This may be due to fault dilation 409 410 associated with large slip and a destruction of small-scale asperities in contact reducing AE activity to 411 linear or isolated clusters indicating larger asperities. As loading and shear-enhanced compaction 412 across the fault resumes, the *d*-value increases again.

Interestingly, over stick-slip phases P1-P5 the *d*-values decrease. Local peak *d*-values are typically reached just prior to LSDs and they decrease from about 2.0 to 1.7 with consecutive LSDs. Concurrently, we observe development of a diagonal step-over (cf. Fig. S7) that in the later phases hosts the majority of AE activity forming a quasi-linear distribution of activity and depletion in AE activity elsewhere. Our observation suggests that *d*-value is primarily sensitive to changes over the length of the whole sample, collecting information from the geometrical distribution of AE events across the whole fault surface.

420 3.4 Clustering properties

421 The spatial distribution of AE hypocenters allows identifying transient AE clusters forming at small-422 scale mm- to cm-scale asperities characterizing the rough topography of the fault surfaces (Figure 423 S7, see also Goebel et al., 2012, 2015). All phases P1-P5 show generally similar trends in the 424 evolution of the median event proximity $\hat{\eta}$ parameter (Figure 3b), which signifies the level of event 425 clustering in the combined space, time and magnitude domain. During the initial part of each stick-426 slip cycle at low axial stress, the median event proximity $\hat{\eta}$ is relatively large. This indicates a 427 dominance of diffuse background activity suggesting random distribution of events in time, space 428 and magnitude domains over the surface. This agrees with the high proportion of mainshocks and 429 singles in the AE catalog observed during the initial portion of each stick-slip cycle (Fig. 3c).

With progressive loading and when approaching LSD failure, the AE rates increase and the median event proximity $\hat{\eta}$ displays a transient decrease, indicating a progressive localization of AE activity (Fig. 3b). This observation is consistent with other laboratory studies (e.g. Bolton et al., 2023; Marty et al., 2023). Concurrently, we observe a decreasing proportion of mainshocks and singles that are superseded by aftershocks and occasionally by foreshocks (Fig. 3c). The progressive localization and

435 increasing size of AE clusters before LSD failures agree with observed patterns before several Mw > 7
436 earthquakes in Baja and southern California (Ben-Zion and Zaliapin, 2020). The proportion of
437 foreshocks clearly does not increase ahead of the LSD, and are instead correlated with the SSD and
438 CSD occurrence. Likewise, an increase in AEs classified as aftershocks with progressive loading ahead
439 of the LSD appears to be linked to the more frequent occurrence of SSDs and CSDs at higher axial
440 stresses, rather than directly with the run-up to LSD.

441 Some SSDs and CSDs are preceded by a visible short-term drop in the median event proximity $\hat{\eta}$ 442 signifying increased clustering, and all CSDs and SSD display strong space-time localization within up 443 to 20 seconds after the slip followed by a transient $\hat{\eta}$ recovery (Figure 3c, Supplementary Figure S3). 444 The amplitudes of temporal $\hat{\eta}$ changes before the CSD or SSD do not seem to correlate with the macroscopic stress drop that follows (cf. Fig. S3 and Table SS1). Accordingly, the short-lasting 445 446 clustering episodes framing SSDs and CSDs are sometimes preceded by an increased proportion of 447 AE events that are classified as foreshocks, especially in later loading phases. The SSDs and CSDs are 448 always followed by an increased proportion of AE events classified as aftershocks (Supplementary 449 Figure S4). The proportions of foreshocks, mainshock and aftershocks do not substantially evolve 450 across several stick-slip cycles, despite the fact that the number of visible SSDs and CSDs responsible 451 for clustered seismicity seem to reduce with time (cf. Fig. 3a with Fig. 3c).

452 Time periods directly following LSDs display strong clustering with complete lack of AE foreshocks replaced with AEs classified as mainshocks/singles and aftershocks. The proportion of clustered to 453 background events (e.g. Martínez-Garzón et al., 2018) seems lower on average in comparison to that 454 455 in the time periods following SSD and CSD, which reflects problems with classification of events in 456 these time periods due to the saturation of the AE system. Nevertheless, in the time period 457 following a LSD, the initially localized AE activity progressively delocalizes within 50-100 s and the 458 next cycle starts, initially dominated by background seismicity. In summary, the evolution of 459 clustering properties is associated predominantly with the life cycle of cm-scale asperities (cf. Fig. 460 S7).

461 3.5 Fault plane variability

The observed AEs result from fracturing and frictional processes occurring on the grain scale (<mm scale). Consequently, the observed temporal evolution of fault plane variability $\widehat{\psi}_f$ (Figure 4) reflects the complex grain-scale (mm) micromechanics. This is because the parameter compares faulting kinematics of individual AE events located close by. In general, high $\widehat{\psi}_f$ values are observed during the entire experiment, reflecting a broad orientation distribution of focal mechanisms that

467 comprise mostly normal (parallel to fault dip) to strike-slip faulting mechanisms across the whole 468 fault surface. During loading, fault variability mostly increases or fluctuates around a high level but, in some cases, $\widehat{\psi_f}$ decreases before LSD. The latter agrees with earlier observations of Dresen et al. 469 (2020) and Goebel et al. (2017) indicating an increasing alignment of microslip planes ahead of LSD. 470 471 However, in rough faults the process is far less prominent than observed for saw-cut faults (e.g. Goebel et al., 2017) In addition, $\widehat{\psi_f}$ seems largely unaffected by the occurrence of CSD or SSD 472 473 events and does not show fundamental long-term evolution across many stick-slip phases. This 474 suggests that the grain-scale roughness is largely preserved during the experiment.

475 3.6 Maximum principal stress orientation and stress variability

476 Stress tensor inversion from AE-derived focal mechanisms allows inferring the local orientation of 477 the deviatoric stress tensor and a relative measurement of its eigenvalues. Changes in principal 478 stress orientation in response to loading, averaged over the whole fault plane, are recorded with the 479 $\delta_{\sigma 1}(t)$ (plunge) parameter, whereas heterogeneity of the local stress tensors is reflected in $\Psi_{\sigma ij}(t)$ 480 parameter.

481 During the initial phase P1 the plunge of the maximum principal stress orientation $\delta_{\sigma 1}(t)$ resolved 482 locally stays close to vertical. Subsequently, $\delta_{\sigma 1}(t)$ progressively deviates from the vertical direction 483 as loading increases. Ignoring some short-period outliers, local plunges of the maximum principal 484 stress roughly vary between 90° and 40° with respect to the vertical sample axis during loading and 485 unloading. Excluding the stick-slip cycle associated with LSD4, we find a progressive rotation of the 486 maximum principal stress during loading while approaching remaining LSDs. This rotation is likely 487 due to shear-enhanced compaction and build-up of shear stress during loading near the fault 488 surface, causing a local rotation of the stress tensor. The increasing local shear stresses are released during slip events, leading to back rotation of the local stresses towards the initial stress state that is 489 490 observed in early part of the phases P2-P4, following the LSD1 and LSD3, respectively. The rotation 491 of the principal stress axes in each stick-slip cycle is associated with a slow reduction in spatial heterogeneity of the local stress, as indicated by the decreasing stress variability coefficient $\widehat{\Psi_{\sigma_{ij}}}$. 492

493 **4 Discussion**

Various large earthquakes were observed to be preceded by precursory deformation and foreshock seismicity on varying scales in space and time, but the observed patterns are diverse and do not always occur (e.g. Kanamori, 1981; Wu et al., 2013; Kato and Ben-Zion, 2021; Sykes, 2021; Kwiatek et al., 2023). Recent studies of laboratory data showed that the use of AI techniques and features derived from AEs can open up new avenues towards forecasting laboratory earthquakes on smooth faults. However, the range of observable physical processes involved in the run-up to dynamic rupture and how they interact remain not well-understood, regardless of the scale (Ben-Zion, 2008, and references therein). Likewise, there is a need for physical understanding of the extracted data features used by AI techniques and assessment of their effectiveness in describing the run-up to failure, especially for rough faults (see overview in Karimpouli et al., 2023a, Johnson et al., 2021; Bolton et al., 2019; Lubbers et al., 2018; Picozzi and Iaccarino, 2021).

505 In this paper, we employ data from laboratory experiments and use AE-derived seismo-mechanical 506 and statistical parameters to characterize the evolution of local damage, roughness, and stress in the 507 immediate vicinity of a rough fault surface. In particular, we investigate whether our parameters 508 contain information on the preparation process leading to large stress drops (LSD). The sizes of AEs 509 recorded in laboratory experiments analyzed in this study range from M_W -7 to M_W -9 (Dresen et al., 510 2020; Blanke et al., 2021), being at least 3 units lower than the estimated magnitude of the large 511 stick-slips (Dresen et al., 2020). A meta-analysis by Mignan (2014) suggested that such AE activity 512 may include key precursory information related to large laboratory earthquakes. Field observations 513 of processes leading to large earthquakes have been categorized as pre-slip, cascade, or localization 514 phenomena, but recent studies point towards a case-specific combination of processes (see Cattania 515 and Segall, 2021, and reviews in McLaskey, 2019; Kato and Ben-Zion, 2021). The physically-516 motivated parameters used in this study are shown to (I) collectively capture the deviation from long-lasting stable deformation towards a preparatory process of large unstable failure, and (II) 517 518 enable high-resolution monitoring of local damage, roughness, and stress at different temporal and 519 length scales. This allows us to identify the time in which the fault enters a critical stage during which 520 a system-size dynamic rupture may seemingly occur at any time.

521 The stick-slip experiments are performed on a naturally fractured rock sample (Goebel et al., 2014, 522 2015). The fault surface (e.g. Fig. S7 for WgN05) displays high initial roughness representing a 523 strongly segmented and juvenile fault in nature. This is in contrast to a smooth saw-cut surfaces 524 which may be more representative of a fault with large displacement (cf. Goebel et al., 2017). As in 525 many past experiments (see e.g. Harbord et al., 2017), slip events on a rough fault show a rich 526 mechanical behavior. The large (LSD) and small (SSD) macroscopic slips of the whole or significant 527 portions of the surface display varying durations and amplitudes reflecting fast and slow slip 528 velocities as well as large and small stress drops (cf. Supplementary Table S1). Smaller slips confined 529 within the fault surface (CSD) are highlighted solely by AE activity, but not with external readings. In 530 consequence, the seismo-mechanical behavior generally shows much stronger or fractal-like

fluctuations compared to saw-cut faults in triaxial stick-slip experiments (cf. Goebel et al., 2015, 2017), and double-direct shear experiments containing gouge (e.g. Scuderi et al., 2017; Bolton et al., 2021). This highlights the need for a careful extraction of meaningful features/parameters from AE data describing the processes leading to system-size failure to enrich information on preparatory processes.

4.1 Fault roughness, damage and stress evolution

537 The complex evolution of fault damage, roughness and stress across multiple stick-slip cycles with 538 progressive shearing is related to *grain-scale* comminution, gouge production and destruction of 539 small-scale asperities that ultimately lead to generation of the persisting large-scale topography (cf. 540 Goebel et al., 2012, 2015, 2017; Kwiatek et al., 2014b). Development of roughness at these different 541 spatial scales has always some AE response (cf. Goebel et al., 2014). The length scale of the 542 roughness/damage evolution processes may be captured with AE source parameters via their 543 collective seismo-mechanical and statistical proxies (cf. Dresen et al., 2020; Blanke et al., 2021). In 544 this study, grain-scale roughness behavior is represented by the fault plane variability, which 545 captures the difference between focal mechanisms of neighboring events. The *small-scale* roughness 546 evolution of small cm-scale asperities is observed with collective properties of AE activity such as 547 event rates, and predominantly with (spatio-)temporal features including clustering and local-stress 548 field orientation and variability. Finally, the development of the *large-scale* (>cm) topography is 549 captured by long-term trends in the temporal evolution of global properties including d-value, b-550 value and event rates $\dot{\eta}$.

551 The complex long-term (across many stick-slip cycles) evolution of fault roughness is primarily 552 documented in the spatio-temporal AE distribution (d-value) and localized damage indicators (b-553 value, AE rate, cf. Fig. 2), as presented in past studies (Goebel et al., 2013, 2017; Kwiatek et al., 554 2014b; Dresen et al., 2020). A decrease in local stress variability (Fig. 4c), the new parameter 555 calculated using AE stress tensor inversion, confirms progressive smoothing of the large-scale fault 556 surface. These parameters signify that fault roughness evolves substantially up to LSD2 but less in 557 P3-P5. This is likely because after multiple slip events, small-scale asperities are progressively 558 destroyed but a *large-scale* fault topography remains, as revealed by the post-mortem inspection of deformed samples (Fig. S7). Consequently, the later P3-P5 AE activity is focused on these larger 559 560 asperities at the expense of a more uniform distribution on the fault. This results in a general d-561 value decrease across many stick-slip cycles converging towards d=1.6 close to the peak stresses for the last cycles. 562

The AE rate and *d*-value evolution towards higher values in each phase preceding LSD imply 563 564 spreading of AE events across the fault (Fig. 2d) imposed by enhanced contact area between the 565 granular material forming the fault zone at elevated normal load (Dieterich and Kilgore, 1996) (cf. 566 Supplementary Movie S1). This is associated with a general *b*-value decrease within the stick-slip 567 cycle, interpreted as a signature of increased stress (Schorlemmer et al., 2005; Goebel et al., 2013) 568 or damage accumulation (e.g. Main, 1991). Anti-correlations of *b*- and *d*-values, as observed in our 569 study, have been reported in similar experiments (Main, 1991, 1992). However, the d-values and b-570 values are also frequently linearly related through D = 2b (Aki, 1981; King, 1983) as found in some studies of natural earthquakes (Wyss et al., 2004) and other laboratory experiments (e.g. Goebel et 571 al., 2017). It is therefore conceivable that interpretation of b- and d-value correlations and trends 572 573 should be considered case-dependent (see also Legrand, 2002) and sensitive to the methodology 574 used. The evolution of the used parameters within one cycle towards the LSD is superposed with 575 high-frequency variations. These originate from activation of short-scale asperities at high levels of 576 axial load, visible as CSD and SSD events and associated transient clusters of AEs (cf. Supplementary 577 Movie S1-S4).

578 Post-mortem surface observations suggest that *small-scale* asperities causing clustered AE activity 579 have been progressively erased (cf. Goebel et al., 2012, 2015) but grain-scale roughness remained 580 unchanged. The former is supported by general decrease of the local stress variability (small-scale) 581 over several slips (Fig. 4c), although we do not observe significant evolution of the fault plane 582 variability that is governed by grain-scale fracturing. High values of fault plane variability observed 583 during the whole experiment, especially if compared with saw-cut faults (cf. Dresen et al., 2020), 584 reflect complex, inter-granular processes related to shear-enhanced compaction of the granular 585 material forming the fault zone (Kwiatek et al., 2014b). This indicates persistence of grain-scale sub-586 mm roughness of the stress field. The micromechanical grain-scale roughness evolution leads 587 effectively to smoothing of the short-scale asperities, and the short-scale stress field, as indicated by 588 the decreasing local stress variability.

Beyond P2 we note that fewer and smaller SSDs occur prior to LSDs. Our observations suggest that with progressive slip and smoothing of small-*scale* fault heterogeneities, the stress field across the whole fault surface becomes more uniform, as the length scale of large heterogeneities becomes more prominent. Increased contact area, and smoothing of the *small-scale* asperities responsible for local stress concentrations result in *large-scale* homogenization of the stress field while approaching the LSD. This agrees with findings from numerical modeling (Ben-Zion et al., 2003) as discussed further in the next section.

596 To summarize, we find that *grain-scale* (<mm) and *large-scale* (>cm) roughness remain largely 597 unchanged across many slip events in contrast to the *small-scale* (mm-to-cm) roughness involving 598 asperities distributed initially across the surface that are progressively erased with repeating slips.

599 4.2 Multi-scale preparatory process and intermittent criticality

600 Within single stick-slip cycles, the evolving space-time-magnitude correlation η_i of AEs indicates 601 formation of distinct clusters (Fig. 3b). Together with progressive b-value decrease and increased 602 event rates, the combined parameter evolution implies accelerating deformation and localization 603 ahead of the LSDs, in agreement with observations from lab tests and field data across different 604 scales (Das and Scholz, 1981; see e.g. Lei and Ma, 2014; Ben-Zion and Zaliapin, 2020; McBeck et al., 605 2022). Moreover, the exponentially increasing AE rates indicates accelerated seismic release (ASR), 606 which is a non-universal earthquake precursory behavior (e.g. Bufe et al., 1994; Ben-Zion and 607 Lyakhovsky, 2002; Mignan, 2011). However, the discussed set of parameters does not unequivocally 608 signify the proximity to system-size events (LSDs), as similar trends are observable at smaller spatio-609 temporal scales before individual SSDs or even CSDs.

610 At about 85-90% of the maximum axial stress (i.e. hundreds of seconds before LSD, corresponding to 611 the yield stress of the fault), the examined parameters tend to mostly fluctuate around a saturation 612 level with occurrence of SSDs and CSDs. Such saturation level is already observed in the first cycle P1 613 starting with the first CSD (ca. 1500 seconds before the LSD1) at about 85% peak stress and 75% of 614 failure time t_f . In addition, we observe that the length of the saturation period prior to failure 615 shortens with each stick-slip cycle, suggesting that the duration over which stress and seismic 616 parameters fluctuate depends on the temporal evolution of fault roughness and associated stress 617 heterogeneity. At the saturation level, b-values and $\hat{\eta}$ remain mostly low as both tend to drop 618 significantly in the last part of the loading cycle. Likewise, the clustered AE activity including AE 619 foreshock-mainshock-aftershock sequences increases, resulting in a reduced proportion of 620 background events (Fig. 3c). Clustered AE activity clearly associated with SSDs and CSDs typically 621 consists of aftershocks and few foreshocks framing the mainshock, suggesting active stress 622 interaction between events as stress transfer occurs across mm- to cm- length scales of the stress 623 field associated with asperities (see next section).

The external axial stress S_1 fluctuates around a critical state between ~85% and peak stress. This has been described previously as intermittent criticality and was observed in nature and numerical models in combination with accelerated seismic release and decreasing *b*-value (cf. Ben-Zion et al., 2003; Bowman and Sammis, 2004). In particular, Ben-Zion et al. (2003) showed in simulations of 628 stress and seismicity on a large heterogeneous fault that towards the end of a seismic cycle, a critical 629 (fractal-like) disorder of the stress field heterogeneity is reached over a broad range of scales. This is 630 found in a representative model for the brittle crust (model F, see Ben-Zion et al., 2003), which is 631 characterized by realistic dynamic weakening. In agreement with our results, any stress perturbation 632 at a high stress level may trigger a small or system wide seismic event. The ultimate size of the event 633 is conditioned on whether the stress level is sufficiently high over a large portion of the fault surface and smooth over this length scale, allowing the event to propagate. Other models of nucleation of 634 large events on rough faults were proposed using, e.g., models of progressive depinning of local 635 asperities collectively reaching the critical nucleation length (Lebihain et al., 2021) and partitioning 636 637 of seismic and aseismic slip and their collective influence on asperities failure and ultimate 638 nucleation (e.g. Cattania and Segall, 2021).

639 Following Ben-Zion et al., (2003), large-scale correlation of elevated stresses enables the generation 640 of large events over a smoothed portion of the stress field. However, the nucleation of such 641 instability remains a statistical event, as it can be in principle triggered by a small *small-scale* or even 642 a grain-scale stress perturbation at the right location. The statistical fluctuations before triggering of 643 large lab earthquakes involve CSD and SSD events. These events lead to local stress relaxation across 644 limited portions of the fault and stress transfer to the surrounding regions (Fig. 5). The concentrated 645 stress transfer near previous failure events is evidenced by significant clustering of AE activity 646 forming foreshocks and aftershock sequences at high axial stresses once CSDs and SSDs become more frequent. The redistribution of stress and the stress drops due to CSDs and SSDs may cause the 647 648 fault to temporarily retreat from the critical stress level. As loading continues, stress recovers and 649 long-range stress correlations are reestablished leading eventually to a system size (LSD) event.

4.3 Earthquake interaction on different length scales

At the beginning of a stick slip cycle, distributed background activity represents >90% of the total AE activity (Fig. 3c). As loading increases, activity rates increase, background activity and *b*-values decrease and there is a progressive spatio-temporal localization of AE events approaching LSDs (Fig. 3b). This is accompanied by increasing slip along the fault. The observed evolution of event proximity and mainshock aftershock distribution may signal AEs triggering close to larger slip events.

656 Compared to smooth saw-cut faults where shear strain is localized and off-fault damage is minor, 657 increasing fault roughness results in significant off-fault damage and a relatively broad damage zone 658 (Goebel et al., 2017). As a result, shear strain is less localized compared to smooth faults and fault 659 slip starts at lower shear stress. Therefore, precursory slip displays a larger fraction of aseismic 660 deformation compared to smooth faults that unlock only at significantly higher stresses (e.g. Dresen et al., 2020). For rough faults, the increase in shear stress, compaction and contact area of the fault 661 662 surfaces results in activation of a growing number of asperities leading to CSDs and LSDs. High local 663 stress concentrations ahead of CSDs and SSDs, as well as local stress redistribution following these 664 events, produces observable event clustering/triggering (see e.g. Schoenball et al., 2012; Davidsen et 665 al., 2017, 2021; Martínez-Garzón et al., 2018). In agreement with Davidsen et al., (2017, 2021), the local stress concentrations produce AE event interactions. This highlights the importance of local 666 stress intensities that control the evolution of the investigated parameters and the role of inter-667 event triggering (Meredith and Atkinson, 1983; Davidsen et al., 2017). 668

669 AE aftershocks following LSDs are controlled by residual elastic strain energy, and also depend on 670 differences in fault roughness and slip stability (Goebel et al., 2023). However, aftershocks are relatively scarce in the examined data with respect to those framing SSDs and CSDs. This is partially 671 because very early AE aftershocks following LSD or SSD are masked by the saturation of the AE 672 system with continuous noise consisting of abundant overlapping AEs lasting up to 100 ms (see 673 674 Supplementary Table S1). However, in large slip events the entire fault blocks are displaced and 675 strength across the interface is reduced to sliding friction. Since the LSD rupture reaches the sample 676 size, no stress redistribution beyond the rupture periphery is possible, which is in contrast to the 677 confined or some small-scale (SSD) ruptures where the stress is redistributed internally. This is visibly 678 reducing the aftershock productivity after LSDs, as the stress associated with large rupture is effectively unloaded in the triaxial machine. This difference in behavior of LSD and SSD/CSD in terms 679 680 of stress transfer poses some challenges for the analysis of aftershocks following LSD/SSD and CSD. 681 This observation needs to be considered while training models forecasting the time-to-failure of 682 laboratory tests. However, Karimpouli et al. (2023) showed that training machine learning models 683 forecasting time-to-failure using carefully framed data is possible, and the effects of boundary 684 conditions can be minimized.

⁶⁸⁵ 5 Potential applications to earthquake forecasting

686 Many studies attempted to characterize precursory deformation preceding large earthquakes using 687 changes in seismicity rate, accelerated release of seismic moment and energy, changes of *b*-values, 688 and other parameters calculated from geodetic and seismic data along with other measurements 689 (e.g. Varnes, 1989; Bolton et al., 2021; Bowman et al., 1998; Gulia et al., 2016; Acosta et al., 2018; 690 Bentz et al., 2019; Picozzi and Iaccarino, 2021; Shreedharan et al., 2021). However, very few if any 691 datasets on the field scale have enough resolution to allow tracking evolution of the parameters 692 discussed in our study during the preparatory phase for large events. This gap may be reduced using 693 modern AI techniques that allow enhancing seismic catalogs (e.g. Mousavi and Beroza, 2022; 694 Trugman and Ross, 2023). This will provide new information on processes preceding large 695 earthquakes via, e.g., additional informative foreshocks (Mignan, 2014). Meanwhile, at the 696 laboratory scale, parameters calculated from continuous waveform data or event catalogs have 697 been used already to successfully forecast the evolution of shear stress, friction, or time-to-failure 698 (see e.g. Lubbers et al., 2018; McBeck et al., 2020, Johnson et al., 2021, and references therein). It is 699 important to note that the seismo-mechanical behavior of smooth laboratory faults differs from that 700 observed for rough faults. The former tends to display a simpler and repetitive behavior, which is 701 attributed to the homogeneity of the fault gouge layer (e.g. Lubbers et al., 2018; Johnson et al., 702 2021) or structural simplicity of the fault surface (e.g. Kwiatek et al., 2014; Goebel et al., 2017). 703 Smooth faults also display clearly identifiable transitions from quasi stable deformation towards 704 rapid acceleration resulting in seismic slip. This is associated with a non-linear accelerating seismic 705 response, and considerably simplifies the training of ML algorithms. Even for such repetitive stick-706 slip experiments on saw-cuts, it was found that fault gouge layers evolve during the experiments 707 reducing the time-to-failure forecasting quality (see discussion in Johnson et al., 2021).

708 Comparisons of past laboratory tests on saw-cut faults and rough faults including results 709 from this study highlight the crucial impact of fault structural heterogeneity or fault roughness, 710 related stress field heterogeneity, stress transfer, and their temporal, spatial and length-scale 711 evolution on our capability of forecasting large failure events. Faults evolve with progressive loading 712 over geological timescales, displaying a qualitatively comparable evolution of many parameters (e.g. 713 localization, b-value) regardless of their structural and mechanical complexity (Tchalenko, 1970; Ben-714 Zion and Sammis, 2003). However, it is feasible to observe very different precursory signatures, 715 depending on fault structure (roughness, complexity) and other conditions (Ellsworth and Bulut, 716 2018; Huang et al., 2020; Kato and Ben-Zion, 2021; Kwiatek et al., 2023). For rough faults, our study 717 suggests that a combination of physics-based parameters, reinforced with ML techniques, can 718 indicate when the system is entering a critical stage. However, identifying the final stage 719 immediately preceding system-size earthquakes may not be possible in the intermittent criticality 720 framework and ultimately conditioned by the finite spatio-temporal resolution of the monitoring 721 capabilities. Additional parameters yet to be developed may allow a closer identification of the final 722 triggering of large events. In any case, the ability to forecast large natural earthquakes will benefit 723 from dense instrumentation around hazardous faults that provide higher resolution data (e.g., Ben-724 Zion et al., 2022).

725 Based on our experimental observations, Karimpouli et al. (2023a) found that the derived 726 parameter pool characterizing different aspects of AE event organization in space and time, damage, 727 stress and roughness evolution, enabled developing and constraining multi-parameter models of 728 time-to-failure forecasting for complex rough laboratory faults. This may be done even with a 729 considerably lower amount of input data compared to the saw-cut faults. In addition, Karimpouli et 730 al. (2023a) emphasize the importance of the new features characterizing local stress evolution derived from seismic moment tensors and stress tensor inversion of AEs in time-to-failure 731 732 forecasting. Interestingly, their analysis highlights that the parameters are collectively important for 733 the accuracy of time-to-failure prediction, but need not necessarily be correlated individually with 734 time to failure. In other words, the developed neural networks benefit from utilization of seemingly 735 unimportant, yet novel details supplied by some parameters to improve the ultimate prediction. 736 Using unsupervised K-means clustering of the seismo-mechanical and statistical parameters 737 developed here, Karimpouli et al. (2023b) showed that it is possible to automatically identify a 738 transition from stable deformation to an intermittent criticality state, with the most significant 739 parameters being clustering properties using the decomposition of Zaliapin and Ben-Zion (2013a, b) 740 as well as seismicity rates. They observed that the developed unsupervised scheme is able to 741 recognize even finer transient processes related to the activation of smaller asperities, and depicted 742 with scaled-down versions of CSDs composed of even shorter and spatially more confined clusters of 743 AEs. These machine-learning enhanced findings are important in the context of the intermittent 744 criticality model of Ben-Zion et al. (2003) shown here to provide a framework that can help to 745 explain our results. As the final large slip may be triggered by a very small stress perturbation at the 746 right location, this would suggest that improving the forecasting of large events requires zooming-in 747 further into the clustering processes of CSDs and searching for potential deviation from their 748 behavior ahead of the main rupture.

749 Conclusions

We studied the preparatory processes preceding laboratory earthquakes on rough faults using an ensemble of 10 seismo-mechanical and statistical features. These physics-based parameters describe damage and stress evolution in the fault zone, localization processes, local micromechanics and earthquake interactions, as well as local stress field evolution and stress field heterogeneity.

The selected features enable understanding a diversity of processes occurring at different spatial and temporal scales during the preparatory phase preceding system-size laboratory earthquakes, these features can help constraining the input for multi-parameter Al-aided models of earthquake forecasting.

The developed set of precursory parameters highlights localization processes preparing system-size earthquakes. However, the parameters are sensitive to length scales of fault surface roughness and associated roughness of the stress field, both rapidly evolving in the course of an experiment. The spatio-temporal evolution of fault surface and stress roughness poses limitations on our ability to monitor and forecast the run-up to large laboratory earthquakes.

We identify a transition from stable deformation to an intermittent criticality state allowing the 763 764 occurrence of large events. This stage is characterized by abundant AE activity highlighting persistent 765 heterogeneity of the stress field at the sub-mm grain-scale. Spatio-temporal AE activity bursts 766 indicate small confined slips in the sample marking a progressive breakdown of asperities. These 767 confined slips superimpose and interact, collectively preparing the fault surface for a system-size slip 768 by progressive smoothing the short- (mm-to-cm) scale stress field. Ultimately, the development of 769 large-scale correlation of elevated stresses enables the propagation of a large slip event over the 770 smoothed portion of the fault, triggered even by a minor stress perturbation.

A system-size earthquake occurring at a state of intermittent criticality is a statistical event that cannot be predicted deterministically. However, using a combination of the parameters described in this study allows identifying the onset time when a fault enters a critical stage. This may be improved with AI classification techniques using cross-scale, physics-based parameters to detect the critical state of a fault system.

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784 Open Research

Seismic catalogs, moment tensor catalogs, raw waveform data, geomechanical data and associated
information related to stick-slip experiments analyzed in this study are available at GFZ Data Services
via separate data publication (CC-BY 4.0 license): Kwiatek and Goebel (2023).

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1118

1119 Figure Captions

- 1120 Figure 1. Overview of mechanical data, AE activity and stick-slip processes at different temporal
- scales occurring during the experiment. (a,b): AE magnitudes (black dots, left axis) and axial load (red
- solid curve, right axis). Onsets of large (LSD), small (SSD), and confined slips events (CSD, see section
- 1123 2.2 for details), the latter not reflected in geomechanical data, are marked with vertical azure lines;
- (b): zoom-in of the time period between 3400 s and 5000 s covering the preparatory processes
- ahead of the LSD1; (c,d,e): zoom-in of the time window framing the representative confined slip
- event CSD (c,f), small slip event SSD (d,g) and large slip event LSD (e,h) with AE magnitudes color-
- 1127 coded with time; (f,g,h): Corresponding top-view of the AE activity with red stars marking the
- location of the AE event initiating the slip. Gray area in (e) denotes short-lasting saturation of the
- 1129 recording system with low-frequency noise from the slip event limiting the detection of individual AE
- events (see text for details) following the occurrence of LSDE. Remaining time windows framing slip
- events are shown in Supplementary Figure S1.
- Figure 2. Temporal evolution of (b) AE event rates, (c) GR *b*-value, and (d) fractal dimension (*d*-value)
 from a boxcounting method calculated using different moving time windows *W* [*s*]. For reference,
 the evolution of AE magnitudes and axial stress is shown in (a).
- Figure 3. Temporal evolution of (a) stress and AE activity for reference, (b) Median event proximity $\hat{\eta}$ (lower $\hat{\eta}$ indicates clustering of events) and (c) proportion between AE background events (i.e. *mainshocks* and *singles*), *foreshocks* and *aftershocks* in the catalog (cf. Fig. 1) as derived from clustering analysis.
- Figure 4. Temporal evolution of the (b) local fault plane variability $\widehat{\psi}_{f}(t)$, (c) plunge of the local maximum stress, $\delta_{\sigma 1}(t)$ (filled circles) and local stress tensor variability $\sigma_{Sij}(t)$ (dots). For reference, the evolution of AE magnitudes and axial stress is shown in (a) (cf. Fig. 1). The visible data gaps during later phases originate from the limited amount of AE-derived MTs.
- 1143 Figure 5. Surface distribution of AE activity following three slip events from the phase P1 of loading 1144 (cf. Fig. 1a-b): (a): CSD T=3414 s (cf. Fig. 1c, f), (b): CSD T=3673 s, (c): SSD T=3963 s (cf. Fig. 1f, h). In 1145 (a, b, c) filled circles show AE activity within a 10-second window starting ~12 seconds following the 1146 nucleation of a slip event (star). The contour plot marks the density of events between the start of 1147 the slip event and the end of the selected time window, aggregating the damage accumulation 1148 during slip. First, two confined slips (a, b) activate small distinct patches representing cm-lengthscale asperities (magenta and green regions in all subfigures). The patches mostly do not overlap 1149 suggesting a shift in activity with subsequent slips. This suggests that failing short-scale asperities 1150

become inactive and 'smooth' at the cm-scales. The smoothed-out region expands ultimately to > 2 cm diameter (c) giving rise to a first SSD that activates a significant part of the fault surface with AE activity accumulating in a narrow diagonal region (blue region in c). The animations presenting the damage evolution framing the occurrence of three slip events are shown in Supplementary Movies S2-S4.

1156

1157 Table Captions

- 1158 Table 1: Parameters characterizing the temporal evolution of damage and stress in the sample.
- 1159 Column 'dimension sensitivity' generalizes whether the particular parameter is sensitive to senses
- 1160 changes in time, space, magnitude, or their combination.

1161

Figure 1.

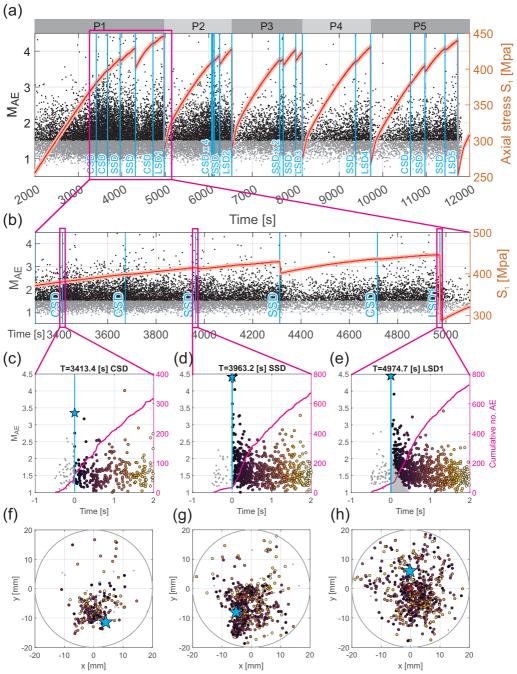


Figure 2.

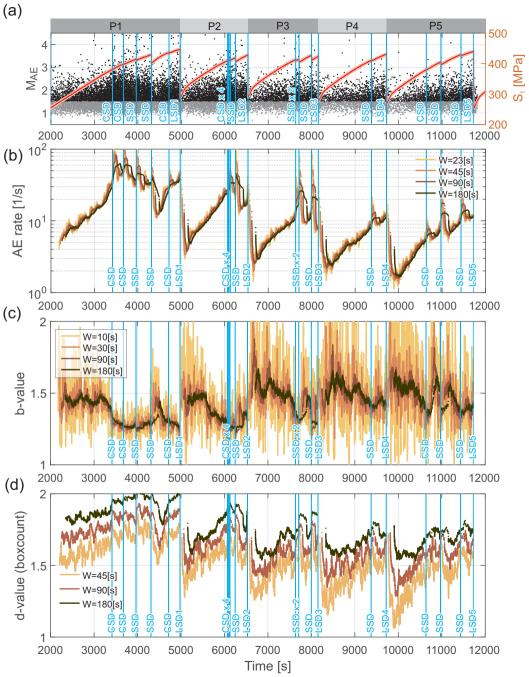


Figure 3.

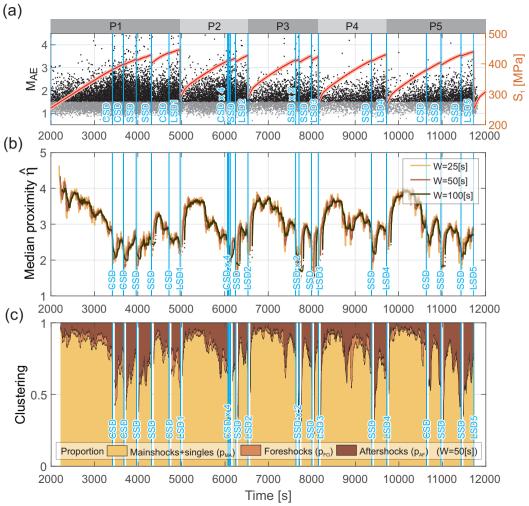


Figure 4.

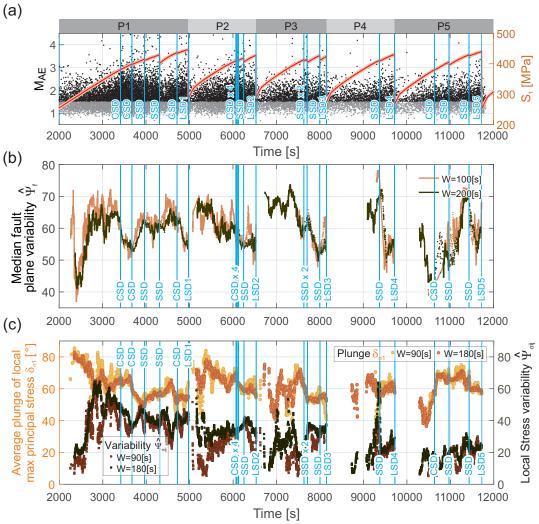
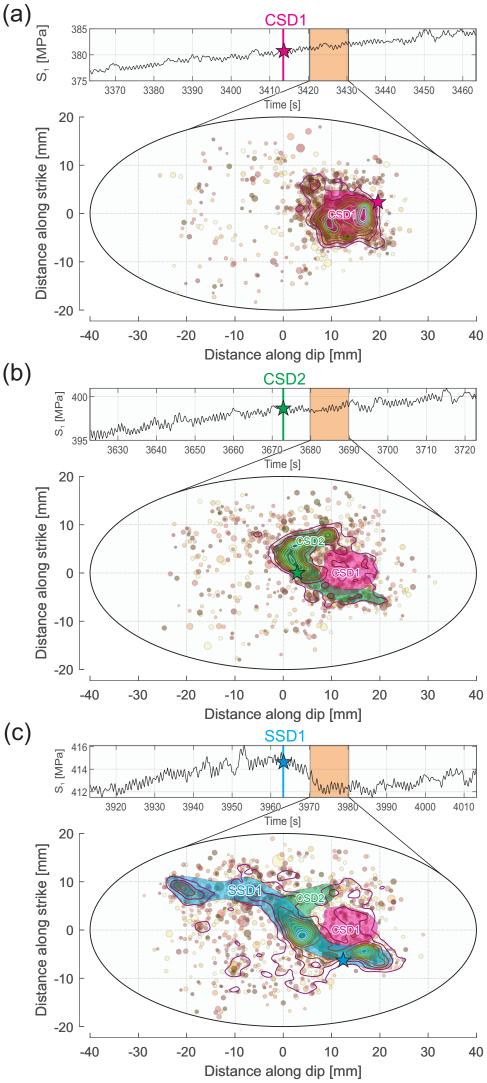


Figure 5.



No.	Parameter	Symbol	Time windows [s]	Dimension sensitivity	Source/method
1	AE event rate	Ņ	23.5, 45, 90, 180	time	AE catalog
2	b-value (maximum likelihood)	b	10, 30, 90, 180	time-magnitude	
3	d-value (boxcounting)	d	45, 90, 180	space-time	
4	Median proximity	$\hat{\eta}$	25, 50, 100	space-time- magnitude	Clustering analysis
5	Proportion of foreshocks	$p_{ m FO}$			
6	Proportion of aftershocks	p_{AF}			
7	Proportion of mainshocks and singles	p_{MA}			
8	Median fault plane variability	$\widehat{\Psi_f}$	100, 200	space-time	Focal mechanisms
9	Plunge of local maximum principal stress	$\delta_{\sigma 1}$	90, 180	space-time	Stress tensor inversion
10	Local stress variability	$\widehat{\Psi_{\sigma_{ij}}}$			