

Pore-scale imaging of multiphase flow fluctuations in core-scale samples

Shan Wang¹, Catherine Spurin², and Tom Bultreys¹

¹Ghent University

²Stanford University

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Abstract

Representative elementary volumes (REV) are an important concept in studying subsurface multiphase flow at the continuum scale. However, fluctuations in multiphase flow are currently not represented in continuum scale models, and their impact at the REV-scale is unknown. Previous pore-scale imaging studies on these fluctuations were limited to small samples with mm-scale diameters and volumes on the order of ~ 0.5 cm³. Here, we image steady-state co-injection experiments on a one-inch diameter core plug sample, with nearly two orders of magnitude larger volume (21 cm³), while maintaining a pore-scale resolution with X-ray micro-computed tomography. This was done for three total flow rates in a series of drainage fractional flow steps. Our observations differ markedly from those reported for mm-scale samples in two ways: the macroscopic fluid distribution was less ramified at low capillary numbers (Ca) of 10⁻⁷; and the volume fraction of intermittency initially increased with increasing Ca (similar to mm-scale observations), but then decreased at Ca of 10⁻⁷. Our results suggest that viscous forces may play a role in the cm-scale fluid distribution, even at such low Ca, dampening intermittent pathway flow. A REV study of the fluid saturation showed that this may be missed in smaller-scale samples. Pressure drop measurements suggest that the observed pore-scale fluctuations resulted in non-Darcy like upscaled behavior. Overall, we show the importance of large field-of-view high-resolution imaging to bridge the gap between pore- and continuum-scale multiphase flow studies, in particular of pore-scale fluctuations.

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1 **Pore-scale imaging of multiphase flow fluctuations in core-scale samples**

2 Shan Wang^{1,2}, Catherine Spurin³ and Tom Bultreys^{1,2}

3 ¹Department of Geology, Pore-Scale Processes in Geomaterials Research (PProGRes), Ghent University,
4 Krijgslaan 281/S8, B-9000, Ghent, Belgium

5 ²Centre for X-ray Tomography (UGCT), Ghent University, Proeftuinstraat 86, B-9000, Ghent, Belgium

6 ³Department of Energy Science & Engineering, Stanford University, Palo Alto, CA, USA

7 Corresponding author: Shan Wang (Shan.Wang@UGent.be)

8 **Key Points:**

- 9 • The observations of fluctuations in multiphase flow on cm-scale sample differ
10 markedly from those reported for mm-scale samples
- 11 • Viscous forces may play a role in the cm-scale fluid distribution even at low
12 capillary numbers
- 13 • Pore-scale fluctuations can result in non-Darcy like upscaled behavior

14 **Abstract**

15 Representative elementary volumes (REV) are an important concept in studying subsurface
16 multiphase flow at the continuum scale. However, fluctuations in multiphase flow are
17 currently not represented in continuum scale models, and their impact at the REV-scale is
18 unknown. Previous pore-scale imaging studies on these fluctuations were limited to small
19 samples with mm-scale diameters and volumes on the order of $\sim 0.5 \text{ cm}^3$. Here, we image
20 steady-state co-injection experiments on a one-inch diameter core plug sample, with nearly
21 two orders of magnitude larger volume (21 cm^3), while maintaining a pore-scale resolution
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33 pore-scale fluctuations.

34 **1 Introduction**

35 Understanding multiphase flow in geological porous materials is central to the safe storage
36 of CO_2 underground (Jeddizahed & Rostami, 2016; Streit & Hillis, 2004) and successful
37 containment of contaminants in the subsurface (McCarthy, 2018). Complex flow dynamics
38 arise from fluid-fluid and fluid-solid interactions over multiple length and time scales
39 (Bultreys et al., 2016; Krevor et al., 2015; Pentland et al., 2011). The underlying pore-scale
40 physics are considered to be mainly controlled by the competition between capillary forces
41 and viscous forces (Chen et al., 2018; Panda et al., 2019; Spurin et al., 2019b). The ratio of

these two forces expressed by means of the capillary number ($Ca = \mu v / \sigma$) is commonly used to differentiate between flow regimes. In the majority of subsurface porous medium applications, the fluid flow is very slow, resulting in capillary numbers $< 10^{-7}$ (Bultreys, 2016).

At the Darcy scale, multiphase flow in porous media is described using averaged properties such as capillary pressure and relative permeability (Lin et al., 2018; Parker, 1989; Zahasky et al., 2020), ignoring fluctuations at the pore scale. However, recent observations at the pore-scale have shown that complex interface dynamics occur even during so-called ‘steady-state’ flow, where the average fluid saturation of the system remains constant (Reynolds et al., 2017; Zou et al., 2018). For example, fluid phases can rearrange and periodically disconnect and reconnect in a process called intermittent pathway flow, or intermittency (Gao et al., 2019; Reynolds et al., 2017; Spurin et al., 2019a). This influences the energy dissipation in the system and, therefore, impacts the averaged behavior at larger scales (Rücker et al., 2021). Thus the assumption of static interfaces in quasi-static models or continuum frameworks may not be accurate. These phenomena occur even in capillary dominated flow regimes that are commonly assumed to be quasi-static, especially when the viscosity ratio (i.e. ratio of nonwetting phase viscosity to wetting phase viscosity) of the two fluids is very low, as for liquid-gas flows. Previous studies, in small mm-scale samples found intermittent pathway flow was most common, and important to fluid connectivity, at capillary numbers around 10^{-8} - 10^{-6} , with the percentage of intermittently-occupied pores increasing with capillary number, and heterogeneity of the pore space (Spurin et al., 2019a, 2019b).

However, previous pore-scale observations have been limited to mm-scale samples, as 3D X-ray imaging has a trade-off between sample size and resolution (Cnudde & Boone, 2013). These samples are smaller than the typical representative elementary volume (REV) for multiphase flow, making the upscaling from the pore-scale to the core-scale more difficult (Jackson et al., 2020, Zahasky et al., 2020). It has been hypothesized that intermittency does not average out at the REV-scale based on the analysis of fluctuations in the pressure drop

70 over the sample (Rücker et al., 2021; Spurin et al., 2022), yet pore-scale variations in the
71 fluid distribution have not been observed and characterized directly in REV-scale samples.
72 As such, it is currently unclear how intermittency impacts REV-scale multiphase flow.

73 In this study, we use the “High-Energy μ CT scanner optimized for Research” (HECTOR) at
74 Ghent University’s Center for X-ray Tomography (Masschaele et al., 2013) to study
75 pore-scale intermittent fluid dynamics at the core-scale in a sample that is 25 mm in
76 diameter, with a voxel size of 9.6 μ m. This sample size - corresponding to a 1 inch drill bit -
77 is a standard for many (relative) permeability measurements, and is thus the smallest size at
78 which the REV concept is typically assumed to be valid in practical applications.

79 We conduct a series of steady-state two-phase flow experiments on a Bentheimer sandstone
80 sample. Nitrogen and brine were simultaneously injected into the sample at three different
81 total flow rates, representing capillary numbers from 2.21×10^{-9} to 3.59×10^{-7} . At each total
82 flow rate, the brine fractional flow was decreased while the total flow rate was fixed. The
83 micro-CT images allowed us to identify variations in the pore-scale fluid distribution in a
84 time-averaged sense over the course of the scan time (53 minutes) at each fractional flow
85 step (Gao et al., 2019; Spurin et al., 2021). We first present the observation of fluid
86 distribution based on the micro-CT images in Section 3.1.1, followed by an analysis of the
87 influence of capillary number on intermittent pathway flow (Section 3.1.2). The importance
88 of performing multiphase flow study at core-scale is then illustrated by carrying out the
89 representative elementary volume (REV) analysis in Section 3.2. The investigation of fluid
90 distribution in the 3D pore network is shown in Section 3.3 to further understand the
91 intermittency behavior at the core-scale. Finally, Section 3.4 characterizes the dynamics of
92 the pressure signal, supplementing the imaging data with information at a time resolution at
93 the scale of seconds. Overall, the observations discussed in this paper were markedly
94 different than those previously reported on mm-scale samples. The results provide a link
95 between scales, and will aid future upscaling research.

96 **2 Materials and methods**

97 **2.1 Core flooding experiment**

98 We perform core flooding experiments on a cylindrical Bentheimer sandstone core of
99 diameter 25 mm and length 42 mm, nearly two orders of magnitude larger volume than
100 previous experiments looking at intermittency (Figure 1). It is a well-sorted German
101 sandstone that contains > 90% quartz (Peksa et al., 2015). For Bentheimer sandstones, the
102 REV for porosity has been observed to be between 1 and 60 mm³ (Halisch, 2013; Herring et
103 al., 2013). The absolute permeability of the sample measured with deionized water was 1.71
104 D. The sample was wrapped by a Viton sleeve and placed in an aluminum flow cell (RS
105 Systems, Norway), which has two injection ports and one outflow port. The flow cell and
106 flow lines were firmly attached to the rotation stage of the micro-CT scanner, avoiding
107 effects of the fluid lines tugging or tangling during the imaging. A differential pressure
108 transducer (Keller PD-33X) was used to monitor the differential pressure over the brine
109 inlet and the outlet of the sample.

110 Steady-state co-injection experiments were conducted with nitrogen as the non-wetting
111 phase and brine (25 wt% potassium iodine) as the wetting phase. The confining pressure
112 and the back pressure were set to 4000 kPa and 2000 kPa respectively, and kept constant
113 during the experiment. The sample was first scanned in its dry state to obtain the
114 geometrical information of the pore structure, this is referred to as the dry scan. Then, brine
115 was injected through the sample at the set back pressure, and a second high-quality scan
116 was made to confirm that all the air was displaced out of the sample, this is referred to as
117 the brine saturated scan. After that, the nitrogen and brine were injected simultaneously
118 through the two injection lines into the sample at a fixed total volumetric flow rate, while
119 the fractional flow f_w (i.e. the volumetric flow rate of brine over the total flow rate) was
120 decreased in a series of drainage fractional flow step. At each step, a scan was taken when
121 the pressure drop across the sample measured by the differential pressure transducer became
122 stable. In this study, 3 observations were made at the total flow rate of 4 ml/min (for $f_w = 0.9$,
123 0.7, 0.5); 5 observations at the total flow rate of 1 ml/min (for $f_w = 0.9, 0.7, 0.5, 0.25, 0$);

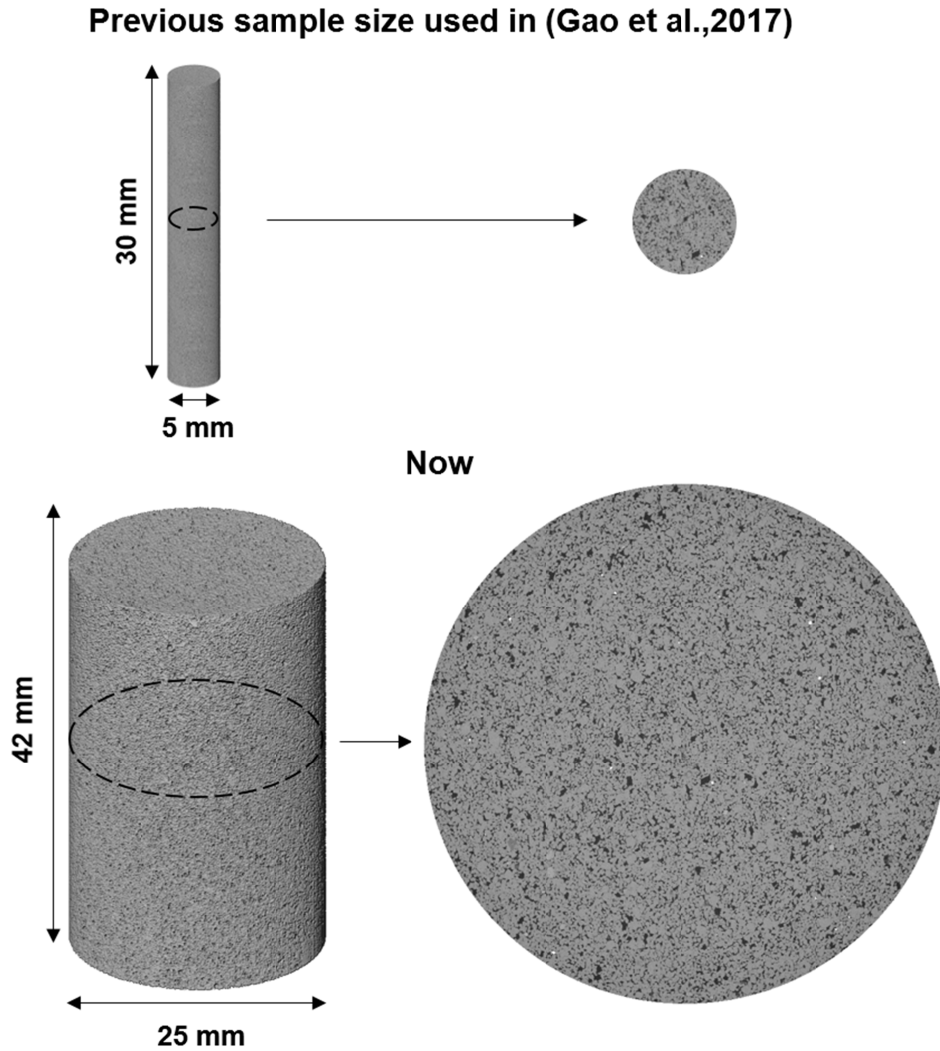
and 5 observations at the total flow rate of 0.2 ml/min (for $f_w = 0.9, 0.7, 0.5, 0.25, 0$). For convenience, we will refer to the three total flow rate experiments 4 ml/min, 1 ml/min and 0.2 ml/min as experiments H, M and L (high, middle and low flow rate) and note the f_w in subscript to describe the fractional flow at each experiment in the following sections. For example, experiment $L_{0.5}$ represents the two-phase flow experiment at $f_w = 0.5$ for the $Q = 0.2$ ml/min experiment.

The capillary number (Ca) describes the relative importance of capillary forces to viscous forces, and is commonly used to categorize flow regimes. Here, we used the following expression (Spurin et al., 2019b) to quantify the Ca at different fractional flows:

$$Ca = \frac{Q_t}{\sigma \left(\frac{f_w}{\mu_w} + \frac{1-f_w}{\mu_{nw}} \right)} \quad (1)$$

where Q_t is the total flow rate, σ is the interfacial tension, μ is the fluid viscosity for the wetting (w) or non-wetting (nw) phase.

The X-ray imaging was performed with the “High Energy micro-CT Optimized for Research” scanner (HECTOR) at the center for X-ray tomography at Ghent University (UGCT). The X-ray energy and the power were 150 kV and 10 W respectively. 3201 projections with 1 s integration time per radiograph were acquired to obtain each image. The voxel size was 9.6 μm for all images, which was the highest resolution the setup could reach to image the full width of the sample. The Octopus software (Tescan-XRE, Belgium) was used to perform the image reconstruction.



143

144 Figure 1. The comparison of sample sizes used in previous experiments (top) and in this study (bottom).

145 2.2 Image processing

146 The reconstructed images were registered using normalized mutual information and
 147 denoised with a non-local means edge-preserving filter (Buades et al., 2008). To quantify
 148 the porosity contributed by macropores (pores clearly resolved at the resolution of the scans)
 149 and sub-resolution pores (pores below image resolution), the differential imaging method
 150 was used (Gao et al., 2017). The dry scan was first subtracted from the brine saturated scan.
 151 Then, the macropores segmented from the filtered dry scan using histogram thresholding
 152 were masked out on the differential image and the rest of the fluid-filled phases on

differential image were identified as sub-resolution pores. If we consider the macropore voxels to be 100% porous, while solid grain is 0% porous, the porosity of voxels with sub-resolution pores can be calculated as $\phi_{sub} = (I_{diff} - CT1)/(CT2 - CT1)$, where I_{diff} is the grey value difference of two images, $CT1$ is the threshold value for solid phase, $CT2$ is the threshold value for macropores. The detailed procedure can be found in our previous study (Wang et al., 2022). Figure 2(c) shows the porosity distribution map. The total porosity of the sample measured from the differential imaging was 19.58%, with 90% of the total porosity assigned as macropores, the remainder were micropores that could not be resolved with the voxel size of 9.6 μm . This agrees with previously-published results on Bentheimer sandstone (Bultreys et al., 2015). As the sub-resolution microporosity occupies a small percentage of the pore space, and is susceptible to partial volume effects, we focus solely on the fluid distribution in macropores.

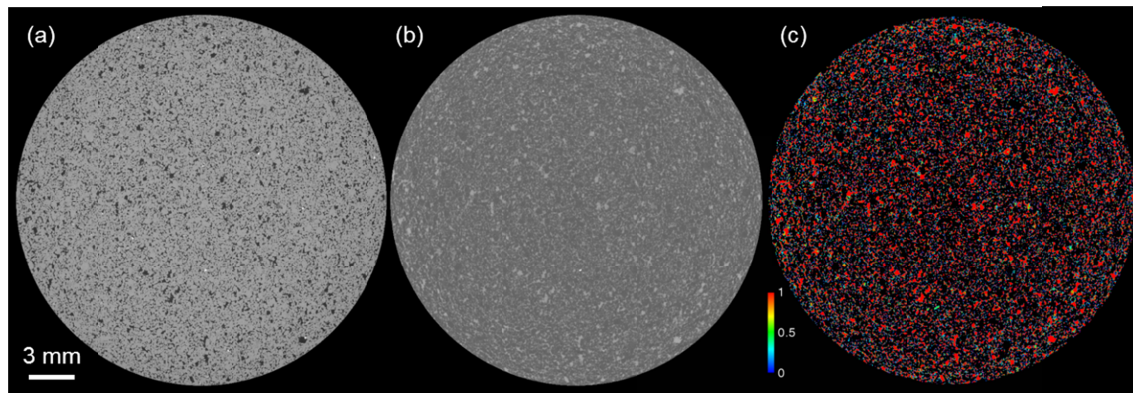


Figure 2. A 2D slice of (a) dry image, (b) brine saturated image and (c) the corresponding porosity distribution map.

As it took approximately 55 minutes to acquire and transfer radiographs for each scan, the fluid distribution in the images reflected time-averaged information. If there was no movement in the sample during the scanning, the pores would be occupied by either nitrogen or brine, presenting as respectively dark or bright gray values in micro-CT images. In case the presence of nitrogen and brine varied periodically in a certain location, this would result in an intermediate gray value, which can be linked to fluid phase intermittency (Spurin et al., 2019a). Similar to the workflow above, the segmentation of nitrogen, brine

and intermittent phases on multiphase scans was also based on the differential imaging method, i.e. the difference image between the brine saturated and the fractional flow scans was used to find the location including both nitrogen and intermittent phases in macropore masked region, then, the nitrogen segmented from the fractional flow scan was subtracted from this image, and the remaining voxels were identified as having intermittent fluid occupancy. To remove partial volume effects that might occur at the fluid-fluid interface, a morphological opening operation (a one-voxel erosion followed by a one-voxel dilation) was performed on the segmented intermittent voxels.

3 Results and discussion

We present the observation of fluid distributions and intermittent pathway flow in the micro-CT images (Section 3.1). The results show that the volume of pore space intermittently occupied by both fluid phases first increases with increasing Ca , and then decreases as Ca increases further. This differs from a continuously positive correlation between Ca number and amount of intermittency observed in mm-scale samples (Spurin et al., 2019b) up to much larger Ca . To understand why, we first show the importance of performing multiphase flow studies on core-scale samples by calculating the deterministic REV (dREV) for the nitrogen saturation in Section 3.2. Then the fluid distribution in the 3D pore network is further analyzed to explain the manifestation of intermittent flow pathways at a REV-scale (Section 3.3). We also investigate the pressure fluctuations and discuss the possible relationship between the pressure signal response and the intermittent flow (Section 3.4).

3.1 Observation of the two-phase flow

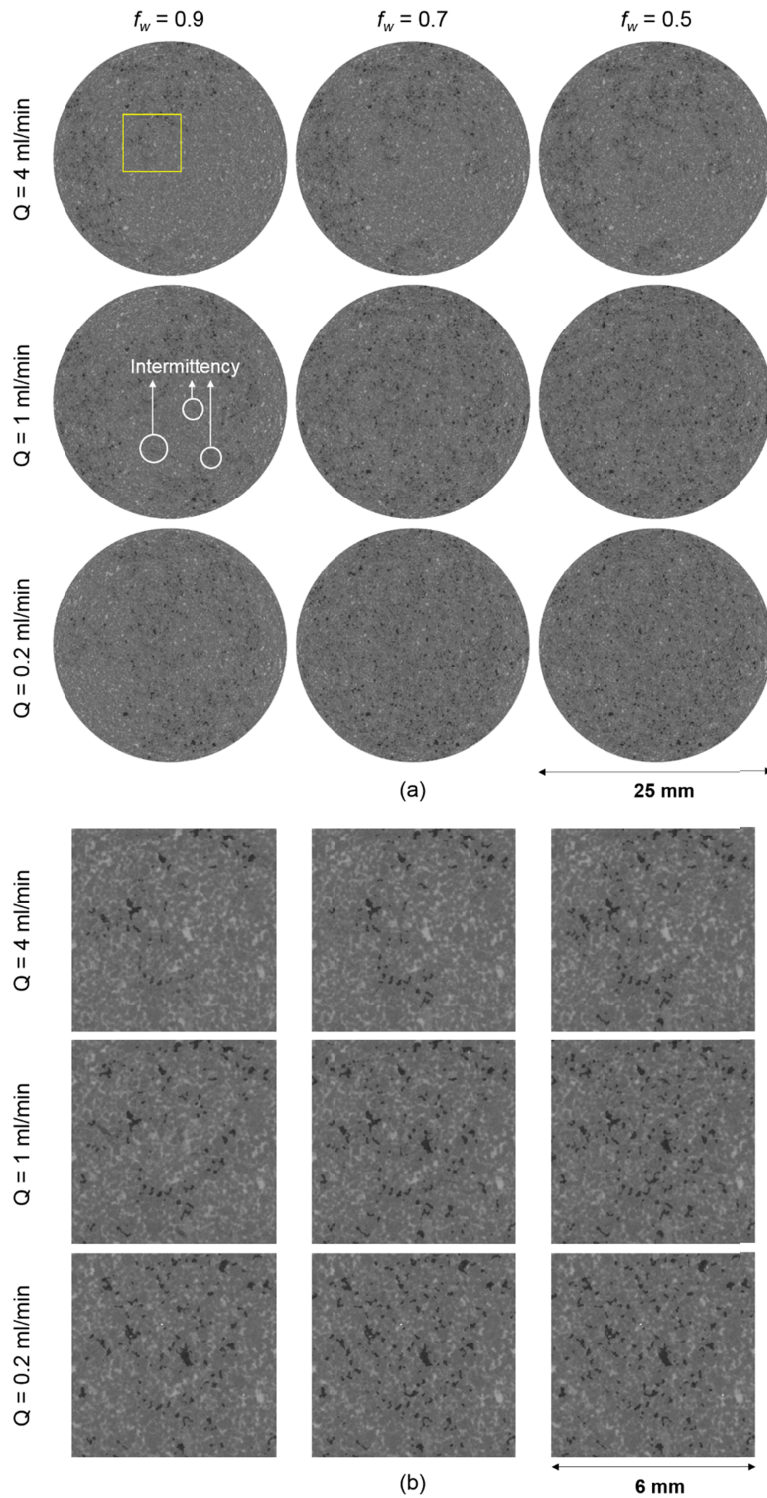
3.1.1 Fluid distribution in micro-CT images

In our fractional flow experiments, the Ca ranges from 2.21×10^{-9} to 3.59×10^{-7} , indicating the system is in the capillary-dominated regime (the threshold of this flow regime is capillary number below $Ca < 10^{-6}$ (Niu et al., 2015)). Our results confirm previous pore-scale studies, which showed the occurrence of intermittency even at capillary numbers

below this threshold.

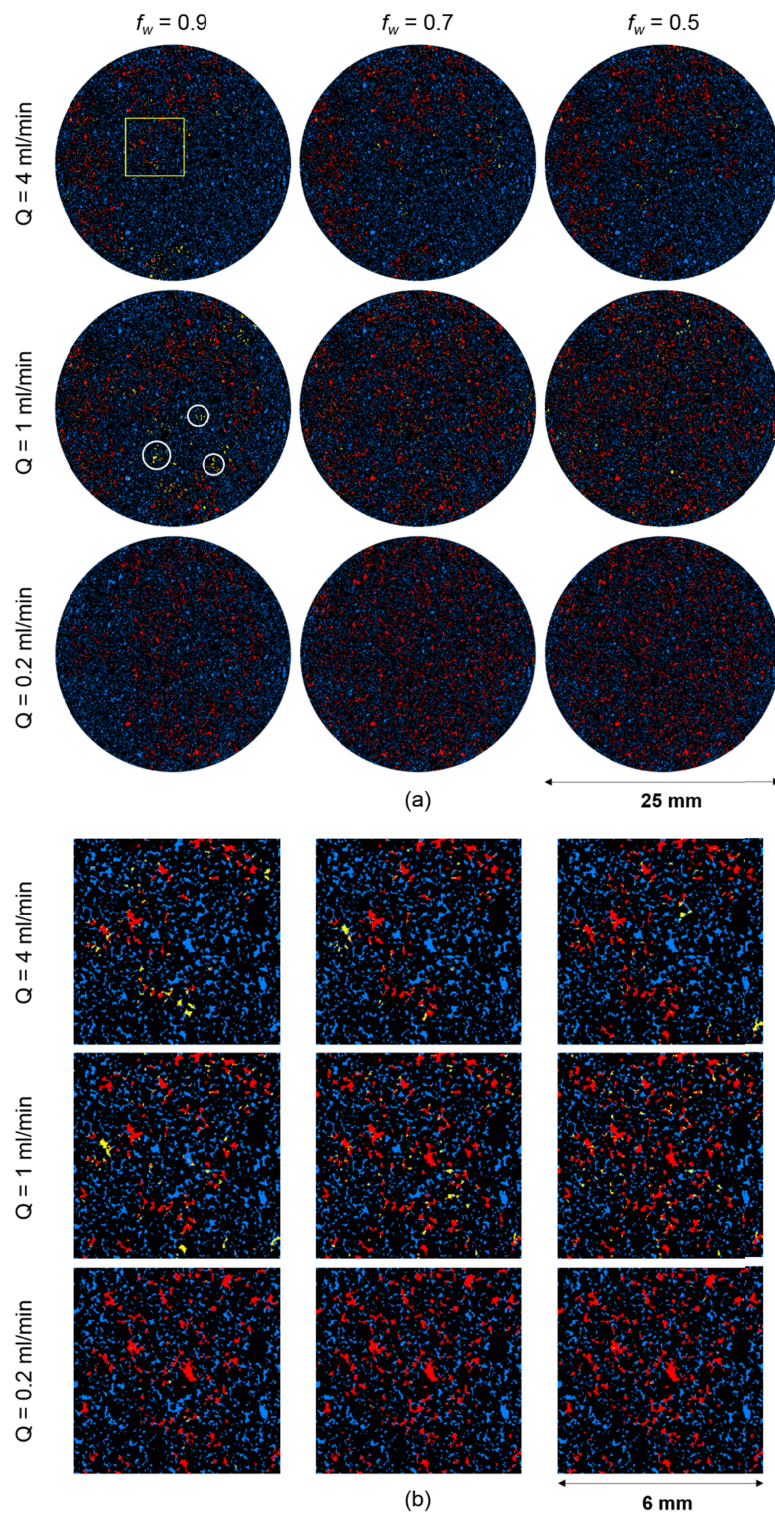
Figure 3 shows the processed greyscale images for the different fractional flows, with the segmented images shown in Figure 4. For the highest total flow rate experiment (experiment H), the nitrogen mainly invaded the left half of the sample in the beginning, and new flow paths in the right part of the sample were gradually built with decreasing fractional flows, shown in the top panel of Figures 3(a) and 4(a). The fluid distribution for experiments M and L was more ramified, as expected for the case of capillary fingering. In co-injection experiments performed on smaller sandstones or carbonate rock samples (5-6 mm in diameter) by Gao et al. (2020), Lin et al. (2018), Spurin et al. (2021) and Zhang et al. (2021), fluid distributions similar to those in our high flow rate experiment were not reported. One possible reason is that our sample is much larger, the viscous forces at $Q = 4$ ml/min on the cm-scale start playing a role in the fluid distribution on this scale. If we zoom in on a small part (Figures 3(b) and 4(b)), the distribution may still look like a capillary finger, but globally these fingers are not distributed homogeneously throughout the cross-section of the whole sample, due to viscous forces (Figure 5(a)). Since the total flow rates were lower in the experiments M and L, the capillary effect was stronger. The nonwetting phase therefore generates a ramified fluid distribution like that depicted in Figure 5(b), dominated by the capillary pressure needed to invade individual pore throats (Blunt et al., 1992).

Another observation is the amount of intermittently occupied pore space. As shown in Figure 3, the periodic invasion of nitrogen and brine in specific pores presented intermediate grayscale values in the micro-CT images. Note that the sub-resolution pores also result in voxels with averaged grey values, due to partial volume effects, but these voxels were masked out by the macropore segmentation (as described in Section 2.2). Our image processing workflow thus avoids the erroneous detection of voxels with partial volume effects as containing intermittency. Figure 4. shows the segmentation results of nitrogen, brine and intermittency at different fractional flows.



229

230 Figure 3. Greyscale two-dimensional slices of three-dimensional X-ray images at different fractional
 231 flows for (a) the whole sample and (b) a zoom in region of the sample for better visibility. The yellow
 232 box in the upper left image shows the location of the zoom in region for all images in (a).



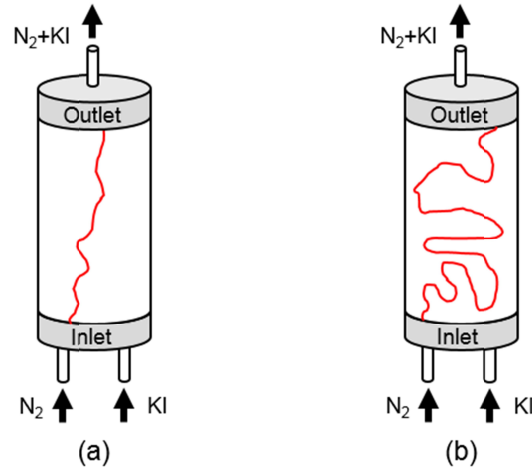
233

234 Figure 4. Segmented images on the same slice as the greyscale images at different fractional flows for (a)

235 the whole sample and (b) a zoom in region of the sample for better visibility. The yellow box in the upper

236 left image shows the location of the zoom in region for all images in (a). The blue, yellow, red and black

237 represent brine, intermittent phase, nitrogen and solid grain, respectively.



238

239 Figure 5. Schematic diagram of typical nitrogen pathways observed in our experiments at (a) high and (b)
240 low flow rate conditions.

241 3.1.2 Impact of Ca on intermittency

242 According to the fractional flow experiments performed by Spurin et al. (2021) and Gao et
243 al. (2020) on rock samples with diameters around 5 mm, the percentage of intermittency has
244 a positive correlation with the Ca when the latter is of the order 10^{-7} to 10^{-5} , reaching a
245 plateau from 10^{-5} to 10^{-4} . However, despite the similarity of the rock type used, our data did
246 not follow the same trend, due to the variability of the macroscopic saturation distribution in
247 these larger samples.

248 As shown in Figure 6(a), little intermittency was observed when the Ca was lower than 10^{-9} .
249 For the experiments M and L, the capillary forces stabilized the fluid distribution. When the
250 Ca increased, the volume fraction of pores being intermittently-occupied at the total flow
251 rate of 1 ml/min was higher than the highest flow rate (4 ml/min) experiment. A possible
252 explanation for the different relationship from mm-scale sample observations is that the
253 brine saturation was relatively high in experiment H (Figure 6(b)), especially in case of $f_w =$
254 0.9 which showed highly channeled flow of nitrogen on the left half side of the sample
255 (Figure 7). Intermittent pathway flow could, therefore, only form in limited regions, where

both nitrogen and brine were present. With decreasing f_w , more nitrogen entered the pore space and developed stable pathways, leading the volume of intermittent phase to reduce at $f_w = 0.7$ and 0.5. In experiment M the brine saturation was lower, and nitrogen was distributed in a more ramified pattern. This causes more opportunity for competition between nitrogen and brine, resulting in more intermittency compared with its highest total flow rate counterpart (Spurin et al., 2021).

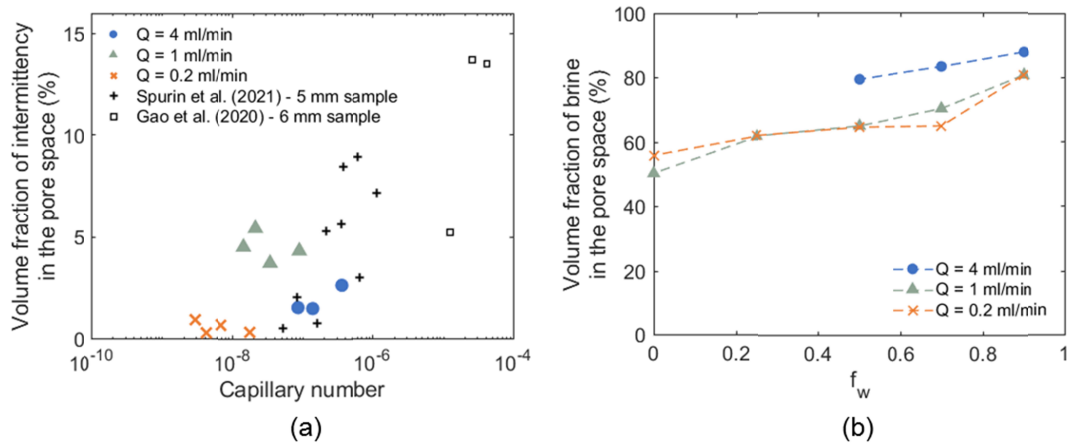


Figure 6. (a) The volume fraction of pores occupied by intermittent phase versus capillary number measured from our 25 mm diameter sample. The results are compared to data obtained on mm-scale experiments (i.e. sample diameter of 5 mm and 6 mm) by Spurin et al. (2021) and Gao et al. (2020). (b) The volume fraction of pores occupied by brine at different fractional flows.

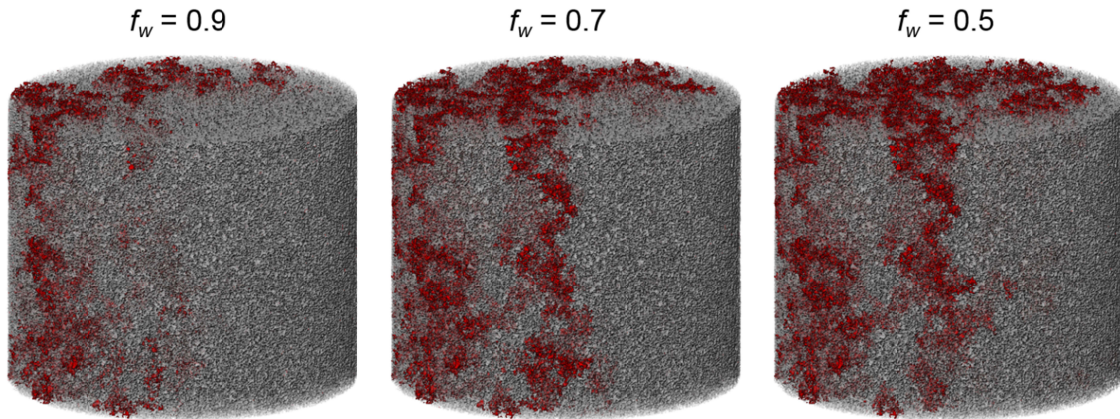


Figure 7. Nitrogen (red) distribution in the 3D pore space (grey) in experiment H. Brine is transparent.

3.2 Representative elementary volume

Linking pore-scale flow behavior to macro-scale or continuum-scale characteristics of porous materials relies on the determination of REV (Singh et al., 2020). A REV is defined as the minimum volume for which the average of a microscopic property first become independent of the averaging volume (Bear, 1972). The size of the REV is not universal and can be different for different properties (e.g. porosity, permeability, saturation, capillary pressure, etc.) of a rock under consideration. In this study, the REV analysis was performed by increasing a cubic domain size from the center of the sample (also called deterministic REV, dREV), calculating the average porosity and nitrogen saturation of the cube calculated at each incremental step. The porosity shows an increasing trend with the cubic volume increasing, and reaches a plateau at around 2 mm linear length (Figure 8(a)). This compares well with the porosity REV size for Bentheimer of >1.75 mm suggested by Halisch (2013) and ≈ 1.25 mm by Jackson et al. (2020). However, the REVs for saturation depend on the flow regime. As seen in Figures 8(b)-8(d), for $Ca < 10^{-7}$ (experiments H_{0.5}, M and L), the nitrogen saturation (S_{nw}) continues to slowly decrease even at the largest scale shown, implying that the values of REV exceed the maximum domain size (18 mm) investigated here. This is because the flow paths have a high degree of channeling: if the volume size is increased past the typical cross-sectional size of these channels (past ~ 5 -7 mm), the global saturation decreases. The effect may thus go unnoticed in experiments on 5 mm diameter samples. Based on the convergence trend, it appears that for the same fractional flow, a smaller Ca results in a larger REV. In the flow regime for $Ca > 10^{-7}$, the S_{nw} shows less variance for subvolumes larger than 10 mm linear dimension in experiment H_{0.7}, indicating that the REV in this regime is approximately 10 mm. This is similar to the observation by Jackson et al. (2020), in which the REV for saturation was larger than the maximum image size (8 mm).

The above analysis indicates that most of the current studies of pore-scale dynamics

(Alhammadi et al., 2020; Gao et al., 2019; Lin et al., 2021; Mascini et al., 2021) on samples with only 5-6 mm diameter are far below the REV requirement for multiphase flow studies. That is why in this study, we use the full image (25 mm diameter) to analyze the fluid performance rather than a cropped region, as this sample size is a standard for many (relative) permeability measurements in the laboratory, and is thus the smallest size at which the REV concept is typically assumed to be valid in real applications.

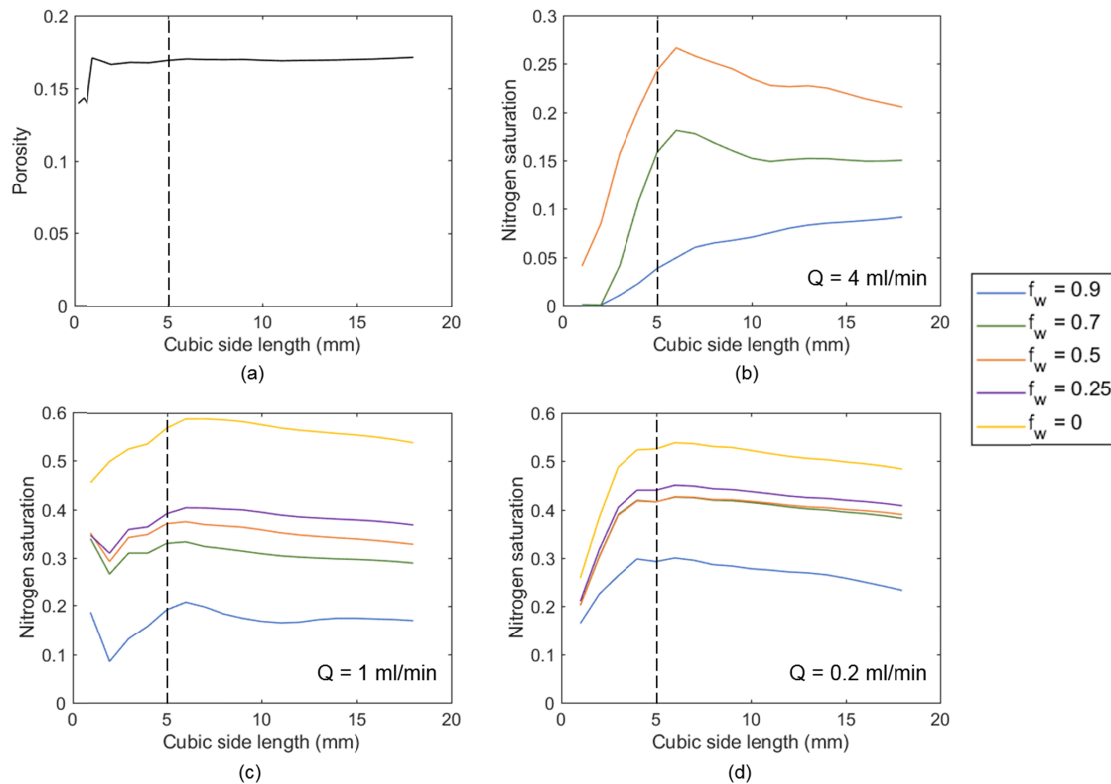


Figure 8. Deterministic REV analysis for (a) porosity and (b)-(d) nitrogen saturation variation in experiments H, M and L. The dotted lines on 5 mm cubic side length show the typical sample size used in previous imaging studies on multiphase flow dynamics in rock samples. This REV study shows that the latter is likely too small to probe the full physical picture.

3.3 Fluid occupancy in the pore network

Intermittent pathway flow provides connections where the non-wetting phase is poorly connected, and could even provide a flow path for otherwise trapped non-wetting phase. This means that it can change the fluid distribution pattern and impact the relative

permeability of fluids. To quantify fluid occupancy in the pore space, a pore network extraction (PNE) algorithm (Raeini et al., 2017) was used to extract and simplify the complex pore morphology into spherical pores (i.e. local dilations in the geometry) connected by throats (i.e. local constrictions in the geometry). The inscribed spheres for the pores were overlaid on the segmented multiphase images to determine which phase (i.e. brine, nitrogen or intermittent fluid) occupied the majority of its voxels. This way, the relationship between pore size and fluid occupancy at each fractional flow step was characterized. As shown in Figure 10, almost all smaller-size pores ($< 20 \mu\text{m}$) were filled with brine and remained uninvaded. The intermittent phase mainly occupied the intermediate-sized pores ($20\text{-}40 \mu\text{m}$), where the wetting and nonwetting fluids showed more competition. For experiment H (Figure 9(a)), the percentage of nitrogen in pores with $25\text{-}45 \mu\text{m}$ radius showed a notably increase with the decrease of f_w , while that in large pores ($>50 \mu\text{m}$) was lower than the percentage of brine in all fractional flows. This is contrary to the expectation of capillary-dominated drainage, where the large pores tend to be invaded by the nonwetting fluid first, followed by the invasion of smaller-sized pores due to their correlation with small throats and high entry pressures. This suggests that the fluid invasion behavior is significantly affected by viscous forces, having the effect of causing less intermittency. For experiments M and L (Figures 9(b) and 9(c)), the nitrogen was mainly distributed in pores with $35\text{-}45 \mu\text{m}$ radius. The fraction of nitrogen in large pores ($>50 \mu\text{m}$) became higher than brine when the f_w was lower than 0.7, indicating that the capillary effect was stronger. This supports our hypothesis that viscous forces are playing an important role in fluid distribution.

Table 1 presents the average coordination numbers (CN) for the pores that remained brine filled, the pores that contained intermittency and the pores that remained nitrogen filled. The coordination measures the number of surrounding pores that are connected via throats to the pore in question. As expected, pores with higher CN are more likely to provide more flow pathways for the invading nitrogen, and are therefore prone to be occupied by nitrogen. Most of the intermittent pores had CN around 4-6 (Figure 10(a)), implying that the

intermittency was favorable in pores with less neighbors. As the brine saturation for experiments $H_{0.5}$, $M_{0.9}$ and $L_{0.9}$ was similar, we compared the CN of intermittent pores and their neighboring pores occupied by different fluids in these three cases (Figure 10(b)). This indicates that the intermittent pores with a large number of CN were likely to be surrounded by brine-filled pores. A possible reason is that if a pore has many neighboring pores and most of them are all filled with nitrogen, they may create a connected flow path directly to perform the displacement. In contrast, if the surrounding pores are brine-filled, they will have more possibilities to reenter the nitrogen-filled pores in a cooperative filling manner, and the intermittent fluid-fluid interface provides the only path for nonwetting fluid to keep the connectivity, which lead to periodic occupancy of both fluids (Spurin et al., 2019a). In addition, Figure 10(b) shows that for the intermittent pores with the same CN, the percentage of nitrogen-occupied neighboring pores in the experiment $M_{0.9}$ case was lower than the other two counterparts, this means that the gas was better connected for the highest and lowest total flow rate cases and there would be fewer potential locations for the water to snap the gas off, which may explain why we observed more intermittency in experiment M.

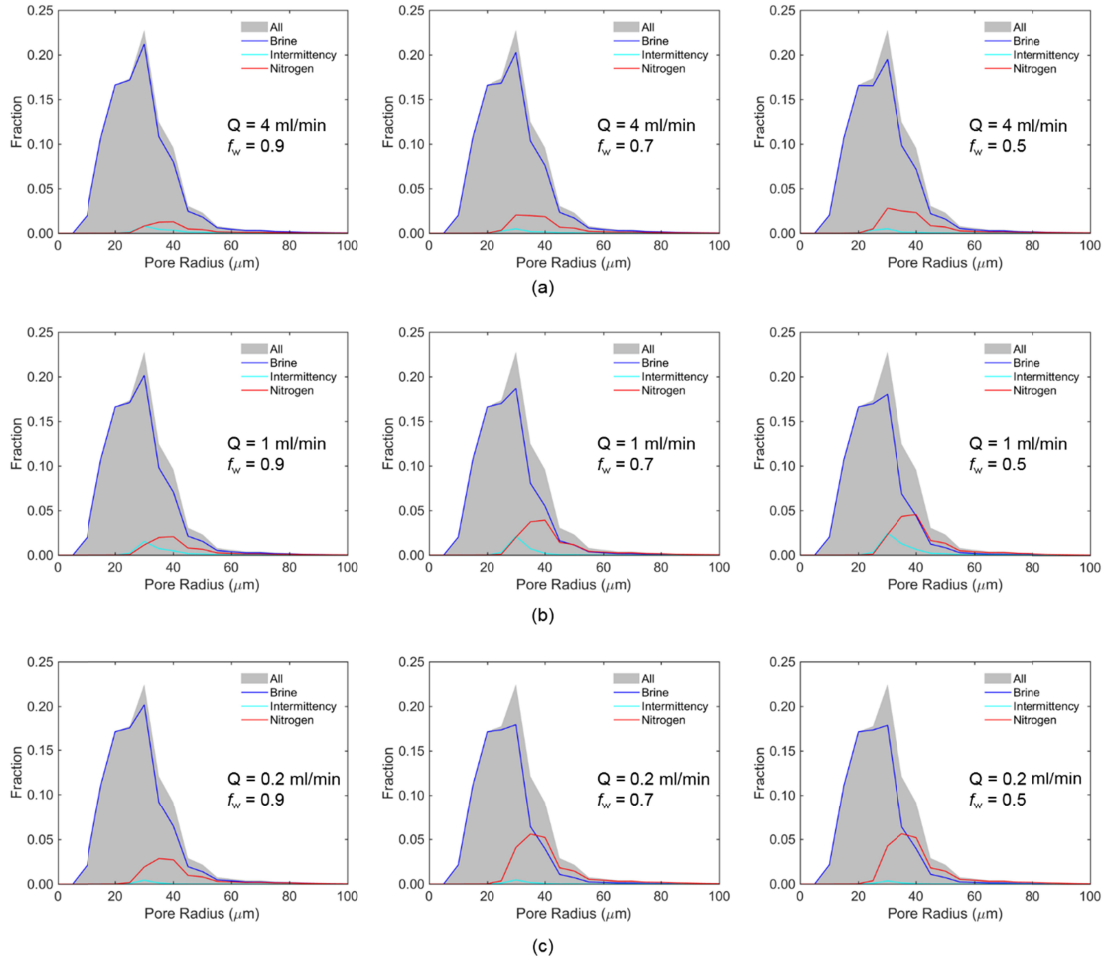


Figure 9. The pore size distribution of different fluid-filling pores in (a) experiment H, (b) experiment M and (c) experiment L. The pore size distribution for all macropores is shown in grey areas, which is obtained from the PNE.

Table 1 Average CN for the brine-filled, intermittency-filled and nitrogen-filled pores during the co-injection process at three total flow rate experiments.

Total flow rate (ml/min)	Brine-filled	Intermittency-filled	Nitrogen-filled
4	3.9	5.6	7.0
1	3.5	5.6	7.3
0.2	3.5	6.0	7.1

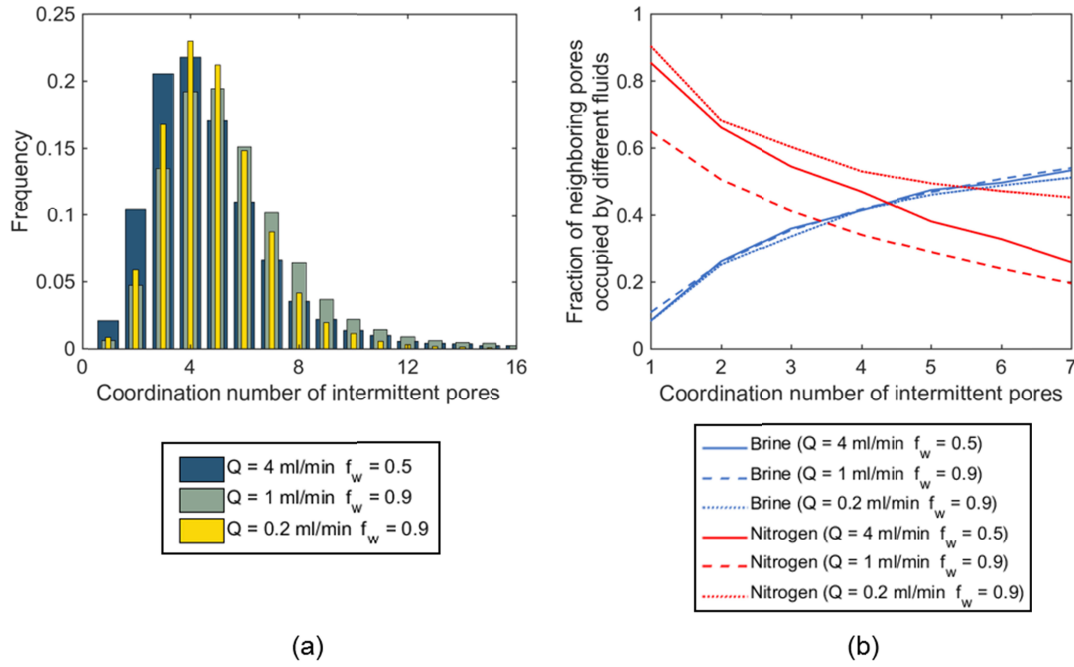


Figure 10. (a) Coordination number distribution of intermittently-occupied pores. (b) The fraction of brine-filled and nitrogen-filled pores surrounding the intermittent pores for different fractional flows. The experiments $H_{0.5}$, $M_{0.9}$ and $L_{0.9}$ are selected because of the similar brine saturation in these three cases.

3.4 Pressure fluctuations in fractional flow experiments

3.4.1 Differential pressure measurements and Darcy's law

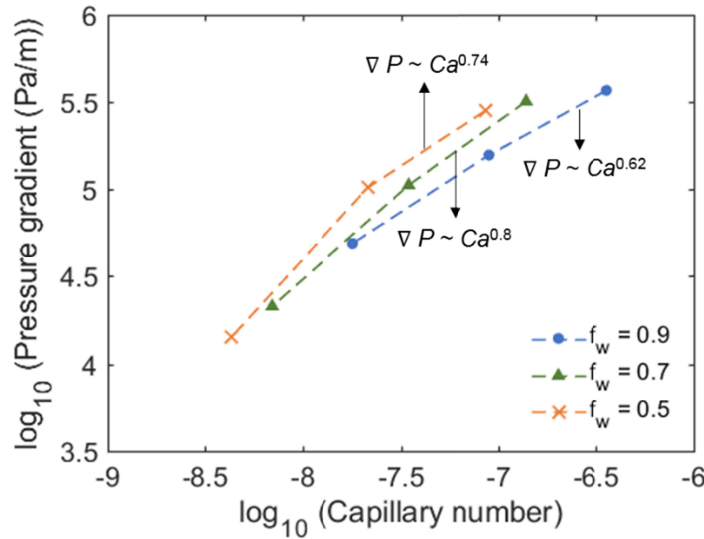
Fractional flow experiments typically aim to achieve a “steady-state” at each fractional flow step, which means both the saturation and pressure drop become time-independent. However, clear pressure fluctuations can be found in many fractional flow experiments (Lin et al., 2018; Menke et al., 2022; Spurin et al., 2022; Zou et al., 2018), and also in the experiments presented here. These fluctuations have been shown to be caused by multiphase fluid dynamics, rather than just representing experimental noise (Rucker et al. 2021, Spurin et al. 2022). In this study, the pressure drop over the sample during the co-injection process was measured by a differential pressure transducer, through which we determined whether the system reached the steady state condition (i.e. a stable pressure difference) before each scan was taken. Figure 11 shows the pressure signal during the final 53 minutes of the scan

for each fractional flow.

We first investigate how the measured time-averaged pressure measurements relate to the imposed Ca , investigating the meaning of our observations for large-scale modeling of multiphase flow. According to Darcy's law, the Ca is proportional to ∇P (i.e. $\nabla P \sim Ca$) in the capillary-dominated regime. This linear relation is known to break down when viscous forces become comparable to capillary forces at a threshold value around $Ca \sim 10^{-3}$ (Blunt, 2017). Recent research has however shown that complex dynamics (e.g. intermittency) that already occur at low Ca induce a transition regime for which a power-law relation has been proposed: $\nabla P \sim Ca^a$ (Zhang et al., 2021). This represents a reduction in the resistance to flow compared to Darcy's law, as the fluid distributions (intermittently) change in a way that reduces viscous dissipation. The exponent a has been found to be in a range of 0.3 to 0.6, both from theoretical arguments as experimental measurements on small samples and simplified systems (e.g. micromodels and bead packs) (Rassi et al., 2014; Sinha et al., 2017; Tallakstad et al., 2009). Figure 12 shows the measured pressure gradients ∇P as a function of Ca for our experiments. While there are only three datapoints for each fractional flow, the curves do appear to show a non-Darcy dependence ($a < 1$), illustrating the relevance of the observed fluctuations towards large-scale simulations. A rough estimate of the exponent a from the limited datapoints available is in the range of 0.62 - 0.8, which is higher than values between 0.42 and 0.6 reported for 6 mm diameter Bentheimer samples (Gao et al., 2020; Zhang et al., 2021). The threshold capillary number (Ca^i) for the onset of intermittency derived from Figure 12 is $\sim 10^{-8}$ for $f_w > 0.5$, compared to $\sim 10^{-5}$ in (Gao et al., 2020; Zhang et al., 2021), indicating that the Ca^i for REV-scale sample might be much lower than that defined at the mm-scale. This provides evidence for theoretical analyses on how the effective rheology during multiphase flow scales with length (Roy et al., 2019). Further research with more data points is needed to investigate the results presented here.

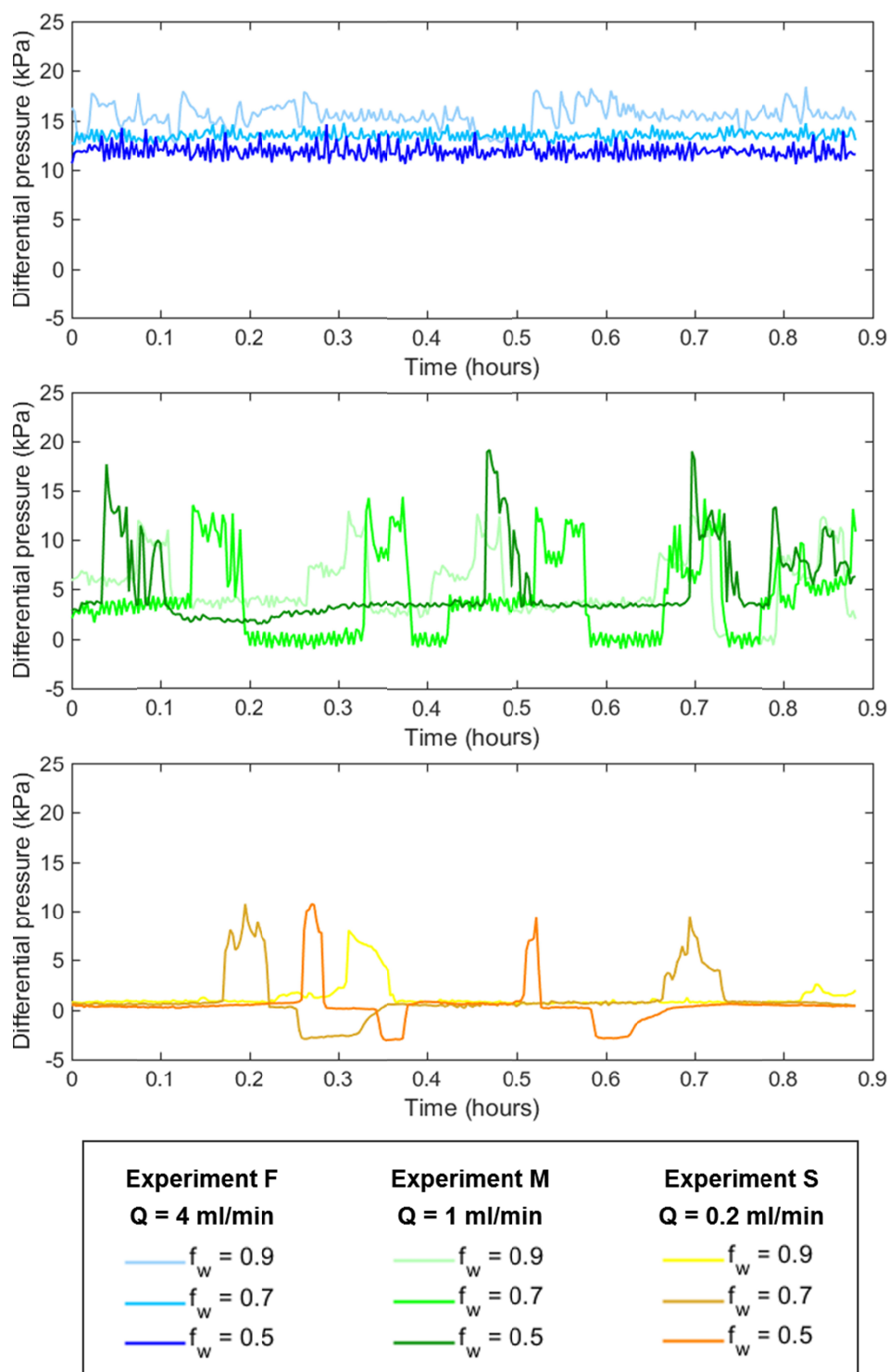
Next, we investigate the fluctuations in the pressure signal. The amplitude of these fluctuations was lower in experiment H than in the other experiments, and fluctuations in experiments M and L showed notable periodicity. To differentiate the pressure fluctuations

403 from noise, the fluctuation histogram is plotted (Figure 13). If the instrumental noise was
 404 the main cause of the large fluctuations, this histogram would generally be expected to
 405 approximate a Gaussian shape (Rücker et al., 2021). However, in all fractional flows of our
 406 experiment, we found non-Gaussian, non-symmetric distributions, implying that the
 407 pressure behavior may be a consequence of pore scale displacement events. This leads to
 408 the hypothesis that the more pronounced fluctuations in experiment M resulted from the
 409 occurrence of more displacement events, confirming the results presented in Figure 6(a): the
 410 highest percentage of intermittency was observed under this condition in the imaging.
 411 Furthermore, the pressure profile at $f_w = 0$ was smooth (see the supporting information)
 412 since there was no fluid rearrangement in this case, providing further proof that pore-scale
 413 fluid rearrangement corresponded to the observed pressure fluctuations. For the lowest total
 414 flow rate (experiment L), the pressures were very low (close to 0 kPa) and were less
 415 periodic. Comparison to the profile at $f_w = 0$ implies that the fluid distributions in S were
 416 more stable than in the other two cases.



417

418 Figure 12. The measured pressure gradients ∇P as a function of Ca at different fractional flows.



419

420 Figure 11. The differential pressure across the sample measured at steady state during the scan for
 421 different fractional flows.

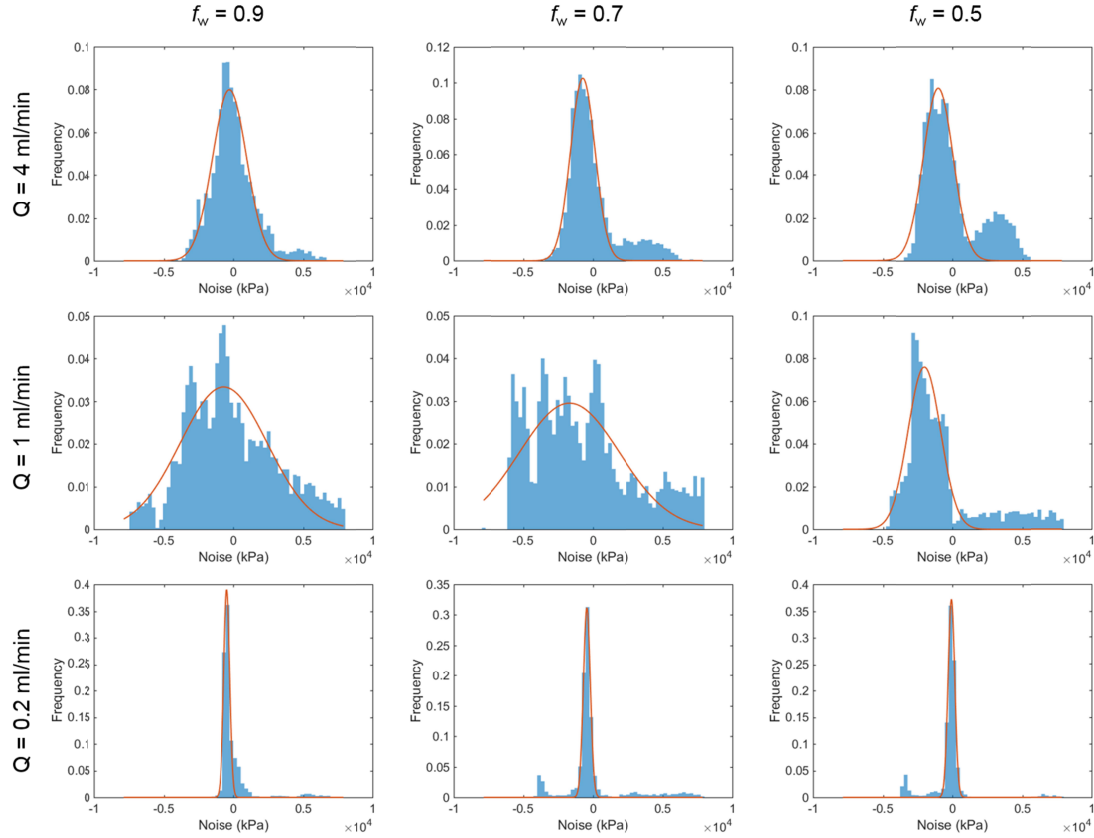


Figure 13. Fluctuation histogram of the pressure signal. A Gaussian fit (orange solid curve) is plotted for comparison with the distribution.

3.4.2 Spectral analysis of pressure data

Here, we analyze the frequency behavior of the pressure fluctuations, thereby supplementing the micro-CT data with higher temporal resolution information. Spurin et al. (2022) observed that fluctuations in differential pressure measurements in a mm-scale carbonate rock sample had the spectral properties of red noise, or $1/f^2$ scaling, by decomposing the pressure data into the frequency domain using a Fourier transformation. This indicates that pressure fluctuations are a stochastic process characterized by self-organized criticality, with no characteristic time or length scale. The scaling relates the power spectral density (S) to the frequency (f):

$$S(f) \sim \frac{1}{f^2} \quad (2)$$

Spurin et al. (2022) asserted that the longest time-scales in this spectrum correspond to repetitive filling of the largest intermittent pores. They showed that the gas connectivity changed for intermittency with a time scale of 8-10 minutes as gas ganglia repeatedly connected and disconnected, while the intermittent gas occupancy with shorter time scales (i.e. 30 s to 2 minutes) were associated with fluctuations without connectivity change, but which may still affect the energy dissipation.

We investigated the spectral properties for our experiments by performing a Fourier transformation on pressure data from the H and M experiments, with the results shown in Figure 14. Experiment L was discounted from this analysis as the pressure drop was small, and close to the resolution of the pressure transducer. As can be seen in Figure 14, the $1/f^2$ scaling (red noise) fitted well for all fractional flow cases in experiment M, where the percentage of intermittently-occupied pores was higher than 3.5%. However, in experiment H, it matched only the $f_w = 0.9$ case, which had an intermittency volume of 2.6%. For $f_w = 0.7$ and 0.5 , with intermittency volumes around 1.5%, the power associated to the longer timescales was significantly below red noise scaling, and thus differed from mm-scale observations by Spurin et al. (2022). Since lower frequencies relate to larger sized fluid redistribution events, this may be further evidence for the need to study multiphase dynamics at the core-scale rather than in smaller samples.

For experiment M, the highest amplitudes were at frequencies that correspond to timescales of 10-20 mins. This is the same for $H_{0.9}$, but for $H_{0.7}$ and $H_{0.5}$ the peak is for timescale of around 20 s. Therefore, we would expect that the intermittently-occupied pores had a large contribution to the non-wetting fluid connectivity in experiment $H_{0.9}$. With the decrease of brine fractional flow, the intermittency may still have played an important role in energy dissipation in experiments $H_{0.7}$ and $H_{0.5}$ – leading to the non-Darcy like behaviour in Figure 12.

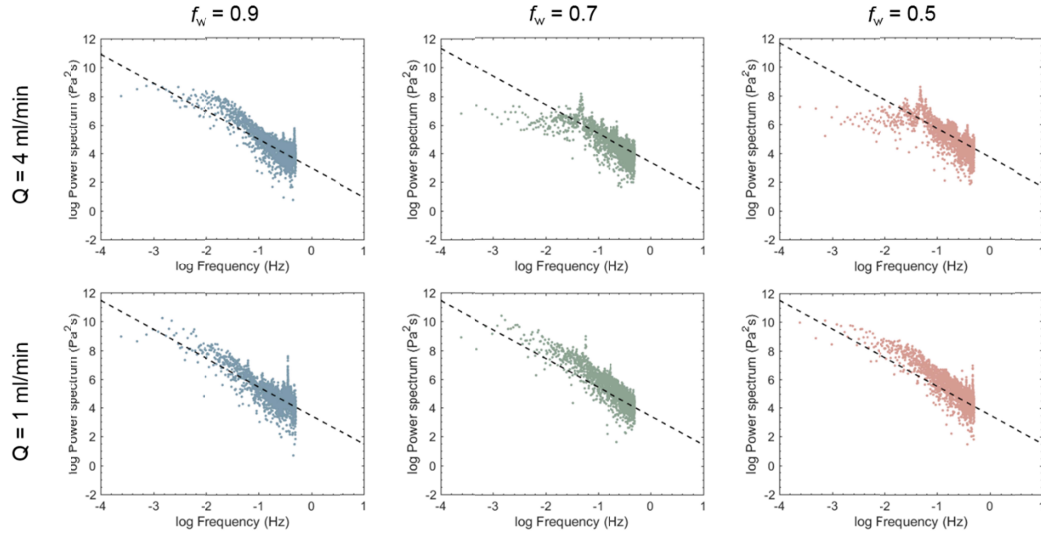


Figure 14. Power spectral density for different fractional flows for $Q = 4$ ml/min and $Q = 1$ ml/min. The black dashed line denotes $1/f^2$ scaling.

4 Conclusions

One of the most important challenges in multiphase flow studies is to upscale the fluid dynamics from the pore-scale to the continuum scale. In this work, we observe pore scale dynamics in a core scale sample, assess the upscaled manifestation of these dynamics in the fluid distribution and fluid connectivity, and ultimately link this to the flow resistance reflected by the pressure drop over the sample. At very low Ca , we observed the same underlying pore scale dynamics as in small samples. However, at Ca on the order of 10^{-7} – traditionally considered to still be well within the capillary-dominated regime – we observed dampening in the amount of intermittent pathway flow. We hypothesize that this is caused by an increased importance of viscous forces, explaining the observation of a less ramified fluid distribution. We show that the latter is difficult to detect on a small sample or a magnified small part of the image. This is reflected in an REV study of the fluid saturation: the saturation varied strongly for averaging volumes with cube sizes up to approximately 10 - 15 mm, after which the variation tailed off but never fully died down to a true constant value reflecting REV.

The analysis of the pressure drop over the sample showed that the observed intermittent

fluid dynamics impact the flow resistance, confirming previous studies that found a non-Darcy-like scaling of the pressure drop with the capillary number, yet finding a larger than expected slope for the $Ca \sim 10^{-7}$ case (i.e. the case with the less ramified distribution). A spectral analysis of the pressure drop showed that the red noise scaling observed in mm-scale samples was only valid for core-scale cases where the percentage of intermittently-occupied pores was relatively high. At higher Ca , the spectral slope in our measurements (i.e. experiments $H_{0.7}$ and $H_{0.5}$) became flatter for timescales > 20 s. We suggest that the intermittency may still play an important role in energy dissipation in these two cases, leading to the non-Darcy like behaviour.

Overall, our research shows the need to study pore-scale dynamics in samples that approach the REV scale – or, from a practical point of view, at least the scale at which continuum properties such as capillary pressure and (relative) permeability curves are typically measured, in case a true REV does not exist. However, the limited time resolution of the laboratory-based micro-CT scanner for such samples did not allow us to further track the fluid dynamics at different time scales. Our findings need to be confirmed by more experiments on cm-scale samples with different fluids, rock types, wettability and pore structures. This may provide us a deeper understanding of fluid flow from small scale to large scale, which could be important for the design of secure subsurface storage of carbon dioxide and energy, as well as for ground-water studies.

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