# The influence of I30 on erosivity-J

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# 1 An I<sub>30</sub> focused approach to estimating event erosivity in

# 2 Australia

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### 8 Abstract

9 Storm erosivity in the Universal Soil Loss Equation is given by the product storm kinetic energy 10 and the maximum intensity measured using a 30-minute window. In some locations short term 11 rainfall data are not available to determine these two parameters well. Here it is shown that the 12 estimated energy per unit quantity of rain for the rain that falls during the time the maximum 30-13 min rainfall amount is measured can be used to predict event erosivity at many locations in 14 Australia. There may be merit in using this approach elsewhere where a lack of short-term rainfall 15 data prevent event erosivity from being predicted accurately.

17 Keywords: soil erosion; soil loss prediction; Universal Soil Loss Equation; storm erosion

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## 19 **1. Introduction**

The Universal Soil Loss Equation (USLE (Wischmeier and Smith, 1965; Wischmeier and Smith, 1978) ) is an empirical model (Alewell et al., 2019) that was originally designed to predict long term average annual soil losses (mass/area/time) from field sized areas. It was later revised (Revised Universal Soil Loss (RUSLE (Renard et al., 1997)) to take advantage of new knowledge gained after the USLE was developed in the 1960s and 1970s. Later RUSLE2 (USDA, 2008) was developed to enable USLE technology to apply to complex land management systems that are beyond the capacity of the USLE and the RUSLE. USLE based models operate mathematically in two steps. In the first step, the average annual soil loss on the "unit" plot  $(A_1)$  is predicted by the product of the rainfall runoff factor (R)and the soil "erodibility" factor (K)

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$$A_1 = R K \tag{1}$$

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The unit plot is defined as a 22.1 m long bare fallow area on a 9 % slope with cultivation up and down the slope. In the second step,  $A_1$  is multiplied by factors related to slope length (*L*), slope gradient (S), crops and crop management (*C*) and soil conservation practice (*P*) to predict the soil loss for an area which differs from the unit plot situation (*A*),

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$$A = A_1 L S C P \tag{2}$$

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38 *R* is defined at the average annual sum of the product of storm kinetic energy ( $E_s$ ) and the 39 maximum 30-minute intensity observed during the rainstorm ( $I_{30}$ ).

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$$R = Y^{-1} \sum_{n=1}^{N_s} (E_s \, I_{30})_n \tag{3}$$

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42 where  $N_s$  is the number of effective rainstorms in *Y* years. In the USLE, rain showers of less than 43 12.5 mm (0.5 in) were omitted in the calculation of *R* unless at least 6.25 mm (0.25 in) of rain fell in 44 15 min. A period of 6 hours with less than 1.27 mm (0.05 in) was used as a storm separator. This 45 rule is applied in RUSLE2 but all events were considered in the RUSLE.

46 When *R* is determined using Eq. 3,  $I_{30}$  (mm h<sup>-1</sup>) is usually a measured value and is given by 47 twice the maximum amount of rain that falls in a 30-minute window.  $E_s$  (MJ ha<sup>-1</sup>) is seldom 48 determined directly but is calculated from the relationship between kinetic energy per unit quantity 49 of rain ( $\varepsilon$ ) and rainfall intensity (*I*). The equation adopted in RUSLE2 is

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$$\varepsilon_k = 0.29 \left( 1 - 0.72 \exp\left( -0.082 I_k \right) \right)$$
 (4)

52 where  $\varepsilon$  has units of MJ mm<sup>-1</sup> ha<sup>-1</sup> and *I* has units of mm hr<sup>-1</sup> and *k* is a period of time during the 53 rain storm. Storm energy is then computed using

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$$E_s = \sum_{k=1}^{N_t} \varepsilon_k \, V_k \tag{5}$$

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where  $N_t$  is the total number of periods in the rainstorm and  $V_k$  is the amount (mm) of rainfall in the *kth* period. Other equations have been observed to exist in many geographic locations but Eq. 4 has been used outside the USA including Australia. Rainfall data collected over short time intervals ensure the accurate determinations of  $E_s$  (Tu et al., 2023; Zhu et al., 2019). Rainfall data collected over a 6 min time interval at many locations in Australia are considered suitable. Once  $E_s$  has been determined,  $EI_{30}$  for a rainfall event can be calculated by

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$$EI_{30} = E_s I_{30} \tag{6}$$

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64 The procedure for determining  $EI_{30}$  for a rainfall event using Eqs 3 to 6 requires high 65 resolution rainfall data in order to predict  $EI_{30}$  and *R* values with high precision. In many locations 66 in the world, appropriate data is not available to do this. In this technical note, an approach to 67 estimating event erosivity in Australia focussing on  $I_{30}$  is considered as a means of estimating 68 spatial variations in *R* in Australia when only data on storm rainfall amount and  $I_{30}$  exists.

#### 69 **2.** Theory

It follows from Eq. 6 that a linear relationship exists between  $EI_{30}$  and  $I_{30}$  if  $E_s$  is constant at a location. However,  $E_s$  is known to vary in space and time. Even so, it has been observed (Lal, 1976; Mannaerts and Gabriels, 2000) that, at some locations,  $E_s$  varies directly with event rainfall amount ( $V_s$ , mm). When this occurs,  $EI_{30}$  can be predicted at a location by

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$$EI_{30} = b_1 V_s I_{30} \tag{7}$$

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where  $b_1$  is an empirical coefficient that varies between locations because of geographic differences in the synoptic conditions that dominate the production of rain. Figure 1 shows how Eq. 7 can predict *EI*<sub>30</sub> values at two widely spaced locations in Australia. The data presented in Figure 1 was 79 obtained using historic 6-minute rainfall data collected by Australian Bureau of Meteorology. It is

80 clear from the fact that  $b_1$  for Darwin is 1.22 times the  $b_1$  for Adelaide, that  $b_1$  is influenced by

81 climate. Adelaide has a Mediterranean Climate while Darwin is in the Tropics.

82



Figure 1: Relationships between *EI<sub>30</sub>* and *V<sub>s</sub>I<sub>30</sub>* at Adelaide and Darwin obtained from 6minute rainfall data collected by Australian Bureau Meteorology from 1967-2004 at Adelaide
and 1953-1995 at Darwin.

Although  $b_1$  can be considered to be a regression coefficient, using regression analysis to determine  $b_1$  does not guarantee to predict the same average annual *R* value as observed at a location.  $b_1$  can be calibrated to predict the same average annual *R* value as observed at a location by

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$$b_1 = \frac{\sum_{n=1}^{N_{em}} (V_s \, I_{30s} \, \varepsilon_s)_n}{\sum_{n=1}^{N_{em}} (V_s \, I_{30s} \,)_n} \tag{8}$$

where  $N_{em}$  is the number of erosive storms where  $V_s > 12.6$  mm. Figure 2 illustrates how  $b_1$ determined using Eq.8 varied for 42 Australian locations where the Australian Bureau of Meteorology has collected 6-miute rainfall data for over 70 years up to 2010. The locations are listed by latitude so that the most northern location is first and the most southern location is last. As to be expected from the influence of high intensity rainfall, the highest values of  $b_1$  occur in the tropics. The ratio for the highest  $b_1$  to the lowest  $b_1$  is 1.42.





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120 Figure 3. Relationships between storm rainfall energy per unit quantity of rain and  $I_{30}$  for

121 rains producing more than 12.5 mm at Adelaide and Darwin

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Figure 4. Relationships between storm rainfall energy per unit quantity of rain and rainfall
energy per unit quantity of rain when *I*<sub>30</sub> is recorded for rains producing more than 12.5 mm
at Adelaide and Darwin.

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The total amount of rainfall kinetic for a storm energy includes the amount of rainfall kinetic energy that occurs during the 30 minutes when the maximum amount of rain in 30 mins occurs. Consequently, it is possible that  $\varepsilon_3$  is directly related to the kinetic energy per unit quantity of the rain that falls during the period when  $I_{30}$  is measured ( $\varepsilon_{I30}$ ) at some locations when  $\varepsilon_{I30}$  is calculated using the equation

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$$\varepsilon_{I30} = 0.29 \left( 1 - 0.72 \exp(-0.082 I_{30}) \right) \tag{11}$$

135 Figure 4 show that this is the case at both Adelaide and Darwin. Regression analysis confirmed this

136 finding at all the 42 locations considered here. It follows from this, that

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$$EI_{30} = \beta V_s I_{30} [0.29 - 0.72 \exp(-0.082 I_{30})] \qquad V_s = > 12.6 mm \quad (12)$$

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139 Regression analysis was undertaken to determine  $\beta$  values for all the 42 locations considered here

#### 140 **3 Results**

141 Although  $\beta$  can be considered to be a regression coefficient, like  $b_1$ , using regression analysis to 142 determine  $\beta$  does not guarantee to predict the same average annual *R* value as observed at a 143 location.  $\beta$  can be calibrated to predict the same average annual *R* value as observed at a location by

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$$\beta = \frac{\sum_{n=1}^{N_{em}} (V_s \, I_{30s} \, \varepsilon_s)_n}{\sum_{n=1}^{N_{em}} (V_s \, I_{30s} \, \varepsilon_{I30})_n} \tag{13}$$

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146 where  $N_{em}$  is the number of erosive storms where  $V_s > 12.6$  mm. Fig. 5 illustrates how  $\beta$  determined 147 using Eq.13 varied for the 42 Australian locations being considered. The spatial variation in  $\beta$  is 148 much smaller than that for  $b_1$ . Consequently,  $\beta$  is much less influenced by the climate variations in 149 Australia than  $b_1$ . The spatial variation is small enough for the average value of  $\beta$  to be used to 150 estimate  $EI_{30}$  values at most of the locations considered. Consequently, using a single value of  $\beta$  in 151 Eq. 12 may have a place in predicting spatial variations in R in Australia when only data on  $I_{30}$  and 152 storm rainfall amount exists.

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155 Figure 5. Values of the ratio of  $\beta$  to its average at a number of locations in Australia where 6-156 min rainfall data is recorded by the Australian Bureau of Meteorology

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## 158 **4. Discussion**

159 Spatial variations in R are important when USLE based technology is applied at a country or 160 regional scale. It is common to use R values obtained at a number of different locations to map 161 spatial variations in R at a country or regional scale using GIS techniques. One technique used 162 involves a power relationship between daily  $EI_{30}$  ( $EI_{30d}$ ) and daily rainfall (Yu and Rosewell, 1996),

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$$EI_{30d} = \alpha \left[ 1 + \eta \cos(2\pi j - \varpi) \right] V_d^{b2}$$
(14)

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165 where  $V_d$  is daily rainfall,  $\alpha$ , b2,  $\eta$  and  $\omega$  are model parameters. The primary parameters for a 166 location are  $\alpha$  and b2 and they are inversely related to each other. The term with the squared 167 brackets deals with seasonal changes in erosivity on a monthly basis assuming it follows a 168 sinusoidal form. *j* represents the month as a number from 1 (Jan) to 12 (Dec).  $\omega$  is a number 169 between 1 and 12 divided by 12 and is set to determine the month when EI<sub>30d</sub> is most affected by a 170 value of daily rainfall.  $\alpha$  and b2 can be spatially mapped (Yang and Yu, 2015). It follows from 171 Eq.12 and the data presented in Figure 5 that, if data on both  $V_s$  and  $I_{30}$  are available, reasonably 172 good estimates of  $EI_{30}$  for erosive events can be obtained assuming that the average value of  $\beta$  (0. 173 833) observed for the locations examined is applied at all locations in Australia. Not only can R be 174 predicted for a location using Eq 12 to obtain the storm *EI*<sub>30</sub> values, Eq. 12 can also be used to 175 predict seasonal variations in erosivity required for accounting for the interaction with cropping and 176 crop management on the C factor in Eq. 2. Short term values of R in the RUSLE and RUSLE2 177 involve disaggregation of monthly R values. In this respect, Figure 6 shows monthly values of 178 erosivity  $(R_m)$  for erosive events predicted using Eq. 12 with  $\beta = 0.833$  in comparison with the 179 observed values at 4 widely separated locations in Australia. These 4 locations have different 180 climates. Perth in western Australia and Adelaide in southern Australia have a Mediterranean 181 climate. Perth receives considerably more rain than Adelaide. Darwin in northern Australia has a 182 tropical climate while Sydney in eastern Australia has a humid subtropical climate.



Figure 6. Relationships between monthly R values ( $R_m$ ) and observed monthly R values obtained using Eq.12 with  $\beta = 0.833$  at 4 widely spaced locations in Australia.

186 Obviously, where the temporal resolution of rainfall data at a sub 30-minute level exists, 187 storm  $EI_{30}$  values can be determined with  $E_s$  values calculated using Eqs. 4 and 5. However, there 188 are situations where data on rainfall amount and  $I_{30}$  are available without sub 30-minute data 189 (Panagos et al., 2015) where determining  $EI_{30}$  values using Eq.12 may be practical. Also, rainfall 190 data can be produced using climate generators. For example, Yu (2002) developed a method for 191 predicting both  $I_{30}$  and storm energy for CLIGEN generated rainfalls. CLIGEN is able to reproduce 192 daily rainfall and related storm patterns representing monthly statistics of historical records (Baffaut 193 et al., 1996). The algorithms used by Yu over predicted R values in the USA by a relatively constant 194 factor so that  $EI_{30}$  values predicted by those algorithms could, in general, be multiplied by 0.576 to 195 predict R at locations in the USA. Arguably, Eq. 12 can be used as an alternative to the approach 196 adopted by Yu. Assuming that  $\beta = 0.833$  can be used as a first approximation in the USA,

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$$EI_{30} = b_3 \beta V_{s.CG} I_{30.Yu} [0.29 (1.0.72 \exp(-0.082 I_{30.Yu})] , V_{s.CG} > 12.6 mm$$
(15)

199 where  $V_{s.CG}$  is event rainfall amount predicted by CLIGEN,  $I_{30,Yu}$  is  $I_{30}$  for the event generated by

- 200 Yu method, and  $b_3$  is an empirical coefficient used to match R to the value of R allocated for
- 201 RUSLE2. With values of b<sub>3</sub> varying from 0.601 to 0.788 (Table 1), applying Eq. 15 at 9 locations in
- 202 the USA where Kinnell (2019) applied CLIGEN as a weather generator for RUSLE2 indicated that

- $I_{30}$  values predicted by the Yu method were too high.  $b_3$  tends to increase slightly with the value of
- *R* allocated for RUSLE2 (Figure 7A) with Presque Isle appearing to be an exception to the rule.
- Figure 7B shows the relationship between  $EI_{30}$  values predicted using the algorithms for  $E_s$  and  $I_{30}$
- presented by Yu (2002) and the values of  $EI_{30}$  predicted using Eq. 15 at Holly Springs where  $b_3 =$
- 0.689 and *EI*<sub>30</sub> values predicted by the Yu method when adjusted by a factor of 0.600 rather than
- 208 0.576 as suggested by Yu.
- **Table 1**

location	state	county	R (MJ mm/(ha hr))	b₃
Bethany	MO	Brooke	3330	0.655
Castana	IA	Monona	2650	0.635
Geneva	NY	Ontario	1380	0.601
Guthrie	ОК	Logan	3800	0.656
Holly Springs	MS	Marshall	6360	0.689
Madison	SD	Lake	1330	0.601
Presque Isle	ME	Aroostook	1230	0.738
Tifton	GA	Tilt	7110	0.788
Watkinsville	GA	Oconee	5050	0.684
Average				0.672



Figure 7: (A) The relationship between b<sub>2</sub> values obtained for the 9 locations in the USA and

*R* factor values allocated by RUSLE2. (B) The relationship between  $EI_{3\theta}$  values predicted at

Holly Springs by Eq.15 using  $b_3 = 0.689$  and  $EI_{30}$  value predicted by the Yu method using an

adjustment factor of 0.600 as opposed to 0.576 suggested by Yu.

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217 The data presented here using Eq. 15 with CLIGEN is qualitative because  $\beta = 0.833$  has not 218 been verified for the USA. An analysis for the values of  $\beta$  in the USA is not possible using the 219 rainfall data in the USLE database because the *EI*<sub>30</sub> values given in the USLE database were 220 calculated using

$$\varepsilon_k = 0.119 + 0.0873 \log 10 (i_k)$$
 ,  $i_k < 76 \, mm/hr^{-1}$  (16a)

222

$$\varepsilon_k = 0.288$$
 ,  $i_k \ge 76 \, mm \, hr^{-1}$  (16b)

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not Eq.4. The original rainfall data used to determine  $EI_{30}$  values using Eq. 16 in the USLE database are not available.

226

227 Concerns have been raised about that validity of using  $I_{30}$  as an independent variable in 228 determining erosivity in USLE based models for storms across a wide geographical and climatic 229 range, where rainfall events may last from less than an hour to more than a day (Dunkerley, pers 230 comm, Sept 2022). While the relative duration of the rain in the 30 minutes when  $I_{30}$  is determined 231 may be small for large duration storms and large for short duration storms, the amount of rain 232 kinetic energy when the maximum amount of rain in 30 minutes is recorded relative to amount rain 233 kinetic energy for the storm is the factor being considered in the development of Eq.12. Eq.12 234 works well in Australia because there is a strong correlation between the amount of rain kinetic 235 energy when the maximum amount of rain in 30 minutes is recorded relative to amount rain kinetic 236 energy for the storm in rainstorms at locations in Australia. It is probably that a strong correlation 237 between the amount of rain kinetic energy when the maximum amount of rain in 30 minutes is 238 recorded relative to amount rain kinetic energy for the storm in rainstorms exists at locations in 239 other parts of the world.

#### 240 **1. Conclusion**

241 Generally, in order to predict  $EI_{30}$  values well, values of storm rainfall amount,  $I_{30}$  and the 242 storm energy per unit quantity of rain need to be known (Eq.8). There can be situations where storm rainfall and  $I_{30}$  data are available but not data to determine storm kinetic energies. However, it has been shown here that when  $I_{30}$  is known, the storm energy per unit of rainfall that occurs when  $I_{30}$  is measured can be estimated using Eq.10. This enables variations in the storm energy per unit quantity of rain at a location to be estimated using the equation

$$EI_{30} = \beta V_s I_{30} [0.29 - 0.72 \exp(-0.082 I_{30})] \qquad V_s > 12.6mm \qquad (12)$$

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249 where  $\beta$  is an empirical factor that is determined by

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$$\beta = \frac{\sum_{n=1}^{N_{em}} (V_s \, I_{30s} \, \varepsilon_s)_n}{\sum_{n=1}^{N_{em}} (V_s \, I_{30s} \, \varepsilon_{I30})_n} \tag{13}$$

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252 Although  $\beta$  varies between locations, the spatial variation in Australia is not great so that the  $\beta$  = 253 0.833 enables monthly values of R to be predicted reasonably well in many places in Australia. Eq. 254 12 works well in Australia because there is a strong correlation between the amount of rain kinetic 255 energy when the maximum amount of rain in 30 minutes is recorded and the amount of rain kinetic 256 energy for the storm in rainstorms at locations in Australia. It is probably that a strong correlation 257 between the amount of rain kinetic energy when the maximum amount of rain in 30 minutes is 258 recorded and the amount of rain kinetic energy for the storm in rainstorms exists at locations in 259 other parts of the world. There may be merit in using the approach elsewhere where there is a lack 260 of short-term rainfall data to determine  $EI_{30}$  values more accurately. How useful Eq.12 might be in 261 determining the effects temporal variations in climate at a given location is a matter for future 262 study.

#### 263 **References**

- 264
- Alewell, C., Borrelli, P., Meusburger, K., Panagos, P., 2019. Using the USLE: Chances, challenges
   and limitations of soil erosion modelling. International soil and water conservation research,
   7, 203-225.
- Baffaut, C., Nearing, M.A., Nicks, A.D., 1996. Impact of CLIGEN parameters on WEPP-predicted
   average annual soil loss. Transactions of the ASAE, 39, 447-457.
- 270 Kinnell, P.I.A., 2019. CLIGEN as a weather generator for RUSLE2. Catena, 172, 877-880.
- Lal, R., 1976. Soil erosion on Alfisols in Western Nigeria: III. Effects of rainfall characteristics.
   Geoderma, 16, 389-401.
- Mannaerts, C., Gabriels, D., 2000. Rainfall erosivity in Cape Verde. Soil and Tillage Research, 55,
   207-212.

- Panagos, P. et al., 2015. Rainfall erosivity in Europe. Science of the Total Environment, 511, 801 814.
- Renard, K., Foster, G., Weesies, G., McCool, D., Yoder, D., 1997. Predicting soil erosion by water:
  a guide to conservation planning with the revised universal soil loss equation (RUSLE).U.S.
  Department of Agriculture Agricultural Handbook. No. 703. US Department of Agriculture,
  Washington, DC.
- Tu, A., Xie, S., Li, Y., Liu, Z., Shen, F., 2023. Effect of fixed time interval of rainfall data on
   calculation of rainfall erosivity in the humid area of south China. CATENA, 220, 106714.
- USDA, 2008. Draft User's Reference Guide Revised Universal Soil Loss Equation Version 2.
   USDA-Agricultural Research Service, Washington, DC.
- Wischmeier, W., Smith, D., 1965. Rainfall-erosion losses from cropland east of the Rocky
   Mountains, guide for selection of practices for soil and water conservation. Agriculture
   Handbook, 282.
- Wischmeier, W.H., Smith, D.D., 1978. Predicting rainfall erosion losses-a guide to conservation
   planning. USDA Agricultural Handbook, 537.
- Yang, X., Yu, B., 2015. Modelling and mapping rainfall erosivity in New South Wales, Australia.
  Soil Research, 53, 178-189.
- Yu, B., 2002. Using CLIGEN to generate RUSLE climate inputs. Transactions of the ASAE, 45,
   993.
- Yu, B., Rosewell, C., 1996. An assessment of a daily rainfall erosivity model for New South Wales.
   Soil Research, 34, 139-152.
- Zhu, Q. et al., 2019. Estimation of event-based rainfall erosivity from radar after wildfire. Land
   degradation & development, 30, 33-48.