A secondary zone of uplift measured after megathrust earthquakes: caused by early downdip afterslip?

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Abstract

A secondary zone of surface uplift (SZU), located ~300 kilometers from the trench, has been measured after several megathrust earthquakes. The SZU reached a few centimeters hours after the 2011 Mw 9.1 Tohoku (Japan) earthquake. Less than a day after the 2010 Mw 8.8 Maule (Chile) earthquake, it peaked at 12 cm. Published coseismic finite-fault models for these events do not reproduce the measured SZU.

One interpretation is that this SZU is universal, driven by volume deformation around the slab interface (van Dinther et al. 2019). In contrast, with synthetic tests and an investigation of the Maule event, we demonstrate the SZU may instead result from slip on the slab interface. Further, we suggest that slip occurs as rapid postseismic afterslip. We can reproduce the SZU with fault slip if elastic heterogeneities associated with the subducting slab are accounted for, as opposed to assuming homogeneous or layered elastic lithospheric structures.

A secondary zone of uplift measured after megathrust earthquakes: caused by early downdip afterslip?

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Key Points:

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6	•	After large subduction earthquakes, a secondary zone of uplift (SZU) is mea-
7		sured in the forearc several hundred kilometers from the trench
8	•	The SZU is not reproduced by coseismic finite-fault models that neglect 3D
9		elastic heterogeneities in lithospheric structure
10	•	The SZU is reproduced using plausible models of 3D elastic heterogeneities, and

is likely due to slip down-dip of the main coseismic patch

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12 Abstract

A secondary zone of surface uplift (SZU), located ~ 300 kilometers from the trench, 13 has been measured after several megathrust earthquakes. The SZU reached a few 14 centimeters hours after the 2011 M_w 9.1 Tohoku (Japan) earthquake. Less than a 15 day after the 2010 M_w 8.8 Maule (Chile) earthquake, it peaked at 12 cm. Published 16 coseismic finite-fault models for these events do not reproduce the measured SZU. 17 One interpretation is that this SZU is universal, driven by volume deformation around 18 the slab interface (van Dinther et al. 2019). In contrast, with synthetic tests and an 19 investigation of the Maule event, we demonstrate the SZU may instead result from 20 slip on the slab interface. Further, we suggest that slip occurs as rapid postseismic 21 afterslip. We can reproduce the SZU with fault slip if elastic heterogeneities associated 22 with the subducting slab are accounted for, as opposed to assuming homogeneous or 23 layered elastic lithospheric structures. 24

25 Plain Language Summary

Large earthquakes in subduction zones induce displacement of the ground surface, 26 which usually include large amplitude uplift close to the shore, and a mild region 27 of subsidence further inland. After the largest instrumented earthquakes, such as 28 the 2011 M_w 9.1 Tohoku (Japan), the 1960 M_w 9.5 Valdivia (Chile) and 1964 M_w 29 9.2 Alaska earthquakes, a secondary zone of uplift (SZU) is detectable even further 30 31 inland. The origin of this SZU remains enigmatic, but one interpretation is that it derives from deformation of the volume around the subducting fault (van Dinther et 32 al. 2019). In this study, we investigate potential interpretations of its origin, including 33 simple afterslip models. A simple slip model with realistic variations in crustal elastic 34 properties allows one to reproduce the secondary zone of uplift. We then focus on 35 the 2010 M_w 8.8 Maule (Chile) event, for which secondary uplift peaked at 12 cm. 36 Unlike previously published studies, we can reproduce the SZU with aseismic on-fault 37 displacement, located significantly deeper than the region of estimated coseismic slip. 38 This deeper slip likely occurred in the hours to days after the earthquake. 39

40 **1 Introduction**

Models of subduction zone thrust earthquakes based on a dip-slip dislocation 41 embedded in an elastic half space produce a large surface uplift in near field, and a 42 zone of small amplitude subsidence that slowly tapers to zero in the far field (Fig. 1a, 43 primary slip patch, e.g., Savage, 1983). Vertical displacements measured after most 44 subduction earthquakes follow a similar pattern. However, far field geodetic measure-45 ments of megathrusts earthquakes $(M_w > 8)$ detect a secondary zone of uplift (refer 46 to as SZU in the text) a few hundred kilometers from the trench (for a summary, see 47 van Dinther et al., 2019). In the years following the 1960 M_w 9.5 Valdivia and 1964 48 M_w 9.2 Alaska earthquakes (e.g., Plafker & Savage, 1970; Kanamori, 1970), uplift of 49 more than 1 m and 30 cm in amplitude, respectively, were measured in this secondary 50 zone. The 2010 M_w 8.8 Maule and 2011 M_w 9.0 Tohoku earthquakes each produced a 51 few centimeters of secondary uplift in the few hours to days following the mainshock 52 (Figs 1c, S1, as measured by GNSS, Vigny et al., 2011; Ozawa et al., 2011). Whether 53 this uplift is coseismic or rapid postseismic is unknown at this time. 54

The origin and consistency of the SZU remains ambiguous. None of the published coseismic slip models of the 2010 Maule event reproduce the horizontal deformation, the near-field vertical displacements and the SZU (Fig. 1c and enclosed references, Vigny et al., 2011). Similarly, none of the published coseismic slip models for the 2011 Tohoku earthquake explain the observed SZU, whose amplitude is less than a twentieth of the near-field vertical displacement. Note that, for these two events, longterm postseismic SZU can be modeled with afterslip or viscoelastic processes (e.g.,



Figure 1. Synthetic and observed trench perpendicular profiles of vertical surface displacements. (a) Vertical surface displacement induced by a ~40-km-deep primary slip patch, by a secondary down-dip patch (~ 90-km-depth), and the sum of the two. The zoomed inset (c) shows that the sum of these two patches induces a ~10 cm secondary zone of uplift ~250 km from the trench. (b) Cross section of the synthetic subduction zone, with the location of the primary and down-dip slip patches. (c) Measured and predicted vertical surface displacements for the 2010 M_w 8.8 Maule earthquake for profile A (location in Figs S1 and 5). The zoomed inset shows the inability of published finite fault slip models to explain the secondary zone of uplift. Slip models from Delouis et al. (2010); Luttrell et al. (2011); Pollitz et al. (2011); Lin et al. (2013); Hayes (2017); Langer et al. (2020) have been retrieved from the SRCMOD database (Mai & Thingbaijam, 2014); note that these models were derived using different datasets (not necessarily the data shown here). Location of the profile, data and other trench-perpendicular profiles shown in Fig. S1. Vertical bars indicate measurement errors when available.

Klein et al., 2016; Ichimura et al., 2016; Li et al., 2017; Agata et al., 2019; Peña et al.,
2020). But classic elastic or viscoelastic rebound models fail to predict any coseismic
SZU (van Dinther et al., 2019). van Dinther et al. (2019) propose that the SZU is
universal, coseismic, and that is is the result of an elastic rebound of the lithosphere
and an upward elastic flow in the mantle wedge.

⁶⁷ While a single patch of fault slip cannot produce a SZU at the surface, an addi⁶⁸ tional down-dip patch potentially can (Fig. 1a). We should expect that a finite-fault
⁶⁹ model could infer a down-dip slip patch to explain any observed SZU. However, existing
⁷⁰ published slip models do not.

In the following, we investigate under which assumptions this secondary zone of 71 uplift can, or cannot, be predicted with fault slip. We focus on the Maule event, where 72 SZU could not be reproduced (Fig 1c) even with added complexity in crustal prop-73 erties: curved and deeper slab geometries, topography, heterogeneous crustal elastic 74 properties, etc (Lin et al., 2013; Moreno et al., 2012; Langer et al., 2020); but where 75 the particular effect of a stiffer subducting slab, and more compliant forearc, has not 76 been included. While we do not discard the possibility that the secondary zone of 77 uplift might be affected by deformation of the volume around the slab interface, we 78 show it may simply be the result of slip on this interface. We first investigate the effect 79 of 3D elastic heterogeneities for a synthetic case and apply this model to an analysis 80 of the Maule earthquake. We conclude with a discussion of the timing of the SZU 81 relative to the mainshock. 82

⁸³ 2 A synthetic example: secondary zone of uplift caused by down-dip ⁸⁴ slip

We begin by designing a synthetic subduction zone, where the lithosphere is 85 divided in domains of different elastic properties, generic trench-perpendicular topo-86 graphic variations and a curved slab interface whose architecture varies slightly along 87 strike (Fig. 2f). This subduction zone is characterized by a stiff plunging slab over-88 lain by a compliant oceanic crust; the continental domain consists of a 35-km-thick 89 crust, more compliant than the underlying mantle whose density increases with depth 90 (domain properties detailed in Suppl. Mat. Text S2, Tab. S1, Figs S2, S3). We apply 91 slip on a limited region of the slab interface (Fig. 1b). Because of the inhomogeneous 92 elastic structure, we rely on a finite element approach (Pylith, Aagaard et al., 2013) 93 to calculate surface displacements. 94

We first compare the strain produced by a \sim 40-km-deep slip patch on the as-95 sumed fault, embedded either in a 3D lithosphere or in a layered crust (Fig. 2). The 96 layered crust replicates the continental domain of its 3D counterpart and does not 97 incorporate variations in topography (Fig. 2g). Relative to the layered elastic models, 98 the 3D-heterogeneous models produce a primary zone of subsidence (150-200 km from 99 the trench) that is smaller in amplitude and tapers to zero closer to the trench. In the 100 region of primary subsidence, the impact of elastic heterogeneity is ~ 5 times larger 101 for vertical displacements than for horizontal ones (Figs 2, S4, 25% of peak amplitude 102 versus 5% respectively). 103

We then assume two slip patches, the primary patch peaks at 17 m of slip while 104 the secondary down-dip patch has 3.5 m of slip (Fig. 1b). With the heterogeneous elas-105 tic model, we calculate the induced displacement at 50 locations randomly distributed 106 at the surface, along with two additional E-W profiles; these locations imitate the 107 spatial distribution of the GNSS data of the Maule event (Fig S1, Vigny et al., 2011). 108 Induced displacements reproduce the ~ 15 -cm-uplift measured 250-300 km away from 109 the trench after the Maule earthquake (Figs 1a and d, S1). We add white and spatially 110 correlated noise to these synthetic data, and try to recover the target slip patches as-111



Profile: surface displacements produced by the primary slip patch

Figure 2. Displacements produced by a ~40-km-deep slip patch on a slab embedded in a 3D lithosphere or a layered crust. (a) Trench-perpendicular profiles of surface displacements. (b,d) and (c,e) Trench-perpendicular cross-sections of upward and eastward displacements for the elastic properties shown in (f) and (g), respectively.



Figure 3. Synthetic example: (a) Target slip and surface displacements. (b,c) Inferred slip and surface displacement assuming incorrect lithospheric structure, either with a layered crust (b) or with 3D-varying elastic properties, shown in (d). Gray shading is the standard deviation of the inferred slip. In (b) and (c), the assumed fault replicates the true geometry shown in (a), but extends to greater depths. In (c), uncertainties in elastic properties are accounted for: Note the difference in the spatial distribution of posterior uncertainties. (d) Assumed 3D elastic properties, $\mu_0=52$ GPa, which differ from the properties used to calculate synthetic observations (displayed in Fig. 2f). (e) Trench perpendicular profile of the target synthetic data and predicted vertical displacements (at 0-km-along-strike). Vertical error bars indicate the posterior uncertainty. Predictions in light red are for the model shown in Fig. S8.

suming the correct fault geometry (with larger subfaults) and a layered elastic structure
(layered as in Fig. 2g, or inexact material properties with 3D variations, Fig. 3d). We
use a Bayesian sampling approach to infer fault slip from the synthetic displacement
(detailed in Suppl. Mat. section S1, Minson et al., 2013).

When the crust is assumed layered (or homogeneous), the secondary uplift cannot 116 be fit (and is not within posterior uncertainty, Fig. 3a,c, Fig. S5, respectively). Relative 117 to the model with heterogeneous elastic properties, a layered crust produces wider 118 and larger primary zone of subsidence, while the horizontal displacements are only 119 slightly impacted (Fig. 2). The amount of slip required to explain the horizontal 120 displacements is incompatible with the slip required to explain the vertical ones. Most 121 inversions typically favor fitting the horizontal measurements, since they are larger 122 and usually more certain. Some down-dip slip is imaged, as required by the horizontal 123 displacements, if the fault is deep enough. Assuming a fault model that is too shallow, 124 and/or subject to unphysical spatial smoothing, can prevent resolution of the down-125 dip patch (Fig. S6). The SZU can be produced with incorrect inferred slip, and to the 126 detriment of the fit to the horizontal displacements, if assuming very low measurement 127 errors for the vertical displacements only (1 mm, i.e. very strongly favoring their fit) 128 and a fault geometry that extends to great depths (Fig. S7). 129

In contrast, adopting a relatively realistic crustal structure (e.g., with 3D het-130 erogeneities in elastic properties for a typical subduction zone, even if the properties 131 are imperfectly known, detailed in Tab. S2), allows one to reproduce the SZU, and 132 to recover the down-dip slip patch (Fig. 3b,c). Accounting for uncertainties in elastic 133 properties (following the methodology presented in Ragon & Simons, 2021, Fig. 3c,d) 134 improves the fit to the data. The main annoyance in assuming heterogeneous crustal 135 elastic properties for slip inference is the computational burden. With this simple 136 synthetic example, we show that a SZU can be produced by down-dip slip on the slab 137 interface by accounting for 3D variations in elastic properties. 138

¹³⁹ 3 The 2010 M_w 8.8 Maule earthquake: Ockham's Razor for secondary uplift

The results of our synthetic example suggest that assuming a realistic crustal 141 structure when imaging the coseismic slip of the Maule event may allow one to re-142 produce the measured SZU. To this end, we build a realistic crustal model for the 143 calculation of the Green's functions (Figs S9, S10, slab geometry from Slab2, elastic 144 properties from LITHO1.0, topography from ETOPO1, Hayes et al., 2018; Pasyanos et 145 al., 2014; NCEI, 2008). While more detailed models might be available, our goal is to 146 explore the secondary uplift, not to image the slip in detail. We also account for poten-147 tial uncertainties in the assumed fault geometry and elastic properties (following the 148 methodology presented in Ragon & Simons, 2021). We solve for the slip distribution 149 and amplitude using the GNSS data from Lin et al. (2013). 150

The inferred slip model reproduces the SZU (Fig. 4). We image a primary zone of 151 fault slip below the coastal region, with a relatively large uncertainty due to the limited 152 amount of data considered here. Down-dip of this primary region of slip, we infer a 153 well-constrained slip zone with an amplitude of 2.5-3 m, equivalent to $M_w=7.2$, which 154 is responsible for the secondary uplift. Models assuming a layered or homogeneous 155 crust do not image this down-dip slip and do not reproduce the SZU (Fig. 1c and 156 enclosed references, Figs S11, S12, S13). Models assuming an inexact heterogeneous 157 elastic structure, but neglecting related epistemic uncertainties, are able to reproduce 158 the SZU albeit not as well as when epistemic uncertainties are accounted for (Figs S12, 159 S13). 160



Figure 4. The 2010 M_w 8.8 Maule earthquake: (a) inferred coseismic slip model as well as observed and predicted surface displacements, assuming a 3D crustal structure and accounting for related epistemic uncertainties. Grey shading indicates the standard deviation of the inferred slip. (b) Trench perpendicular profile (profile A) of measured and predicted vertical displacements, for the slip model shown in (a), and a slip model inferred assuming an homogeneous crustal structure (Fig. S10). Vertical error bars indicate the posterior uncertainty and data errors. (d) Same as (b) for eastward surface displacements. (c) and (e) Zoomed inset on the SZU region.

Our results suggest that previously published models for the Maule earthquake 161 were not able to reproduce the SZU (Fig. 1c) because most of them were inferred 162 assuming a layered crust. While Moreno et al. (2012) assumed 3D heterogeneous 163 elastic properties, the shallow fault geometry they used and the impact of spatial 164 regularization likely prevented a down-dip patch to be imaged. Note that some authors 165 infer a down-dip patch, as required by horizontal displacements, that could not be 166 associated with the SZU for the same reasons (as shown in our synthetic example, 167 Fig. 3a, Vigny et al., 2011; Bedford et al., 2013). The combined effect of strong 168 assumptions on the crustal elastic structure and fault geometry, and the common use of 169 unphysical regularization (e.g., Ortega-Culaciati et al., 2021), probably prevented most 170 published models from producing the mild secondary uplift of the Tohoku earthquake. 171

That we image down-dip slip does not mean slip is uniquely the cause of the 172 SZU. What we know is that the responsible mechanism should occur very early after 173 the mainshock, at most a few hours to days (as measured by GNSS). Hence, the 174 model proposed by Luo and Wang (2021), which requires a \sim 5-years-long postseismic 175 visco-elastic relaxation to produce the SZU, is too slow to explain these observations. 176 Similarly, challenges in modeling highly disparate time-scales (from seconds to years) 177 prevent van Dinther et al. (2019) from confirming the universal process they invoke 178 is coseismic, rather than lasting several weeks after the mainshock. In contrast, while 179 the potential influence of volume deformation cannot be ruled out, the hypothesis that 180 down-dip slip caused the SZU seems straightforward. 181

¹⁸² 4 Is the secondary zone of uplift induced by down-dip rapid afterslip?

For the Maule earthquake, we infer down-dip slip at \sim 90-km-depth, where only 183 a few aftershocks occurred, none with $M_w > 6$ (Rietbrock et al., 2012; Lange et al., 184 2012). Such depths are generally believed to be relatively aseismic (Lay et al., 2012; 185 Obara & Kato, 2016). Moreover, in south-central Chile intermediate-depth seismicity 186 is relatively sparse (Fig. 5 Ruiz & Madariaga, 2018) We conclude that the down-dip slip 187 we image (equivalent $M_w=7.2$) is likely aseismic in nature, and therefore postseismic. 188 To confirm this hypothesis, we estimate the postseismic deformation that affected the 189 slab interface in the days to months following the mainshock, using similar modeling 190 assumptions to the coseismic case and GNSS observations. Again, our goal here is not 191 to accurately model the postseismic slip. Rather, we wish to verify if afterslip at the 192 location of the down-dip patch we image could be consistent with measured postseismic 193 surface displacements. Due to the limited number of postseismic observations, many 194 slip models are plausible and our stochastic results are poorly informative. We thus 195 rely on a two-steps approach. We first verify if deep slip is within the estimated 196 range of plausible parameters (i.e., within the posterior marginal probability density 197 functions). Then, we specifically check if deep afterslip is coherent with available 198 measurements. To do so, we build a synthetic afterslip model that consists of the 199 previously estimated mean afterslip at depths shallower than 70 km, with additional 200 synthetic slip at \sim 90-km-depth, and compare produced surface displacements with 201 available data. 202

We first model the first 12 days of afterslip: only 3 GNSS stations are located 203 above the fault (data from Vigny et al., 2011, the vertical component is too noisy to be 204 used). Larger westward displacements above the deepest portion of the fault suggest 205 deep afterslip occurred, even if its location is not constrained. Synthetic afterslip at 206 the location of the down-dip patch, added to the estimated 12-days-afterslip model, 207 is coherent with the few available measurements (Figs 5, S14). We also model the 208 postseismic slip in the year following the mainshock (few vertical measurements are 209 available, data spanning 488 days after the rupture, from Lin et al., 2013). While slip at 210 the exact location of the down-dip patch does not appear in the posterior mean model 211 (Fig. S15a), it is within plausible values (Fig. S15c). A synthetic \sim 1-m-amplitude 212



Figure 5. Early afterslip (12 days) following the 2010 M_w 8.8 Maule earthquake, inferred from available GNSS horizontal displacements (published data σ of less than 4 mm Vigny et al., 2011) and with additional synthetic downdip afterslip. Overlayed is the recent seismicity, including aftershocks of the Maule event, that have occurred between 70 and 130-km-depth, from the USGS ANSS Comprehensive Earthquake Catalog (ComCat, events since 1928, $M_w > 3$). Earthquakes with $M_w > 6$ are indicated as large points with a white edge. Slab-depth contours in light gray are from Slab2; they are not in perfect agreement with seismicity depth.

down-dip slip patch is consistent with distal observations (Fig. S15b). Further, the vertical component of distal data requires deep slip (Fig. S15) but is not sensitive to its exact location.

Other authors infer similar deep postseismic slip (60- to 90-km-depth, Vigny 216 et al., 2011; Lin et al., 2013; Bedford et al., 2013). However, we note that at such 217 timescales, more than 1 year after the mainshock, viscoelastic relaxation also could 218 reproduce the measured displacements (as demonstrated by Klein et al., 2016; Peña 219 et al., 2020, 2021), and that we cannot discriminate between postseismic slip or vis-220 221 coelastic relaxation. The down-dip slip we image is therefore consistent with surface displacements measured 12-days and >1 year after the coseismic rupture, further sug-222 gesting the SZU has possibly been caused by very rapid afterslip, which then could 223 have slipped continuously in the days to months following the coseismic rupture. 224

²²⁵ 5 Discussion and conclusion

A secondary zone of uplift (SZU) has been observed after several megathrust 226 earthquakes. The SZU reached more than 12 cm following the 2010 M_w 8.8 Maule 227 (southern Chile) earthquake. In this study, we investigate if (and which) assumptions 228 in the foward and/or inverse approach could prevent the SZU to be reproduced with 229 slip on the slab interface. We show that neglecting variations in elastic properties 230 due to the plunging slab induces an incompatibility in the amount of slip required to 231 explain the measured horizontal, or vertical, displacements, preventing models from re-232 producing the SZU. In contrast, we demonstrate that assuming realistic heterogeneous 233 elastic properties, a sufficiently deep fault geometry, and discarding any non-physical 234 regularization of the inverse problem, we infer the SZU as caused by slip down-dip of 235 the main coseismic rupture. 236

Our synthetic tests suggest that assuming plausible, but inexact, 3D-heterogeneous 237 elastic properties is sufficient to recover the SZU. Accounting for potential uncertainties 238 in these properties (Ragon & Simons, 2021) allows us to improve the fit to the observa-239 tions, and to decrease posterior uncertainty on slip amplitude and surface displacement 240 predictions. Accounting for epistemic uncertainties usually produce opposite effects, 241 increasing posterior uncertainties and residuals (Ragon et al., 2018, 2019). In this 242 particular case, we believe introducing uncertainties in the elastic structure promotes 243 the exploration of a narrow region of the solution space that is otherwise not within 244 reach. 245

For the Maule earthquake, we show that slip down-dip of the coseismic rupture 246 $(\sim 90\text{-km-depth})$ produces a SZU, and that this slip is likely postseismic in nature. 247 Deep afterslip or slow slip events have been observed along the Peru-Chile trench, 248 in northern Chile (M_w 6.9, 50-km-depth, Klein et al., 2018) or Ecuador (before and 249 after the 2016 M_w 7.8 Pedernales earthquake, ~60-km-depth, Rolandone et al., 2018; 250 Tsang et al., 2019). However, the slab geometry and seismicity distribution in the 251 Maule region clearly differ from northern South-America (Fig. 5), preventing further 252 comparisons. In particular, the down-dip slip would have occurred at the transition 253 between the flat slab of central Chile to a more moderately dipping slab in south Chile, 254 as indicated by recent seismicity (Fig. 5, Pesicek et al., 2012). 255

Klein et al. (2018) report an inconsistency in the amount of slow slip needed to fit horizontal versus vertical observations a few hundreds of km from the trench. Both postseismic slip models of the Maule event (Lin et al., 2013), and synthetic tests performed for an infinitely long megathrust (Hsu et al., 2006), report similar inconsistencies in the fit to vertical versus horizontal measurements. It is common practice to discard or down-weight vertical data because of such inconsistencies and larger measurement errors. We show that by accounting for heterogeneities in elastic
 structure, we can reconcile vertical and horizontal observations.

The SZU observed after megathrust earthquakes other than the Maule event is 264 located 300 km from the trench in Chile, 350 km in Japan, and 400 km in Alaska 265 (van Dinther et al., 2019). Assuming that the SZU finds its origin in slip down-266 dip of the coseismic rupture, because of the various slab geometries, the down-dip slip 267 would have consistently occurred at \sim 80-90-km-depth. Due to the lack of observations 268 (in Japan, a potential down-dip slip would be observed mostly offshore), we cannot 269 270 discriminate whether the secondary zone uplift is systematically caused by fault slip or other processes. 271

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Data availability statement. Materials presented in this paper are archived and 275 available in Ragon (2022). The Bayesian simulations were performed with the Al-276 Tar2 package (AlTar, A Bayesian Framework for Inverse Problems, 2022). The Clas-277 sic Slip Inversion (CSI) Python library (Jolivet et al., 2014) developed by Romain 278 Jolivet was used to build inputs for the Bayesian algorithm. The mesh for the FEM 279 simulations was built using Coreform Cubit (Coreform Cubit, 2022). We used the 280 finite-element code Pylith (Aagaard et al., 2013) to perform the simulations. GNSS 281 data have been published in Vigny et al. (2011) and Lin et al. (2013). Slab geometry, 282 topography and crustal elastic properties from Slab2, LITHO1.0, and ETOPO1 mod-283 els are available in Hayes et al. (2018); Pasyanos et al. (2014); NCEI (2008). 3D data 284 were visualized using the open-source parallel visualization software ParaView/VTK 285 (Ahrens et al., 2005). Figures were generated with the Matplotlib (Hunter, 2007) and 286 Seaborn (Waskom, 2021) Python3 libraries. 287

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Supplementary Material for

A secondary zone of uplift measured after megathrust earthquakes: caused by early downdip afterslip?

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Figure S1 Observed surface displacements in map view and trench-perpendicular profiles of vertical displacements. Vertical bars indicate measurement errors when available.

S1 Bayesian Sampling of the inverse problem

S1.1 AlTar

The sampling is performed with a Bayesian approach implemented in the AlTar2 package, originally formulated by Minson et al. (2013). AlTar combines the Metropolis algorithm with a tempering process to iteratively sample the solution space. A large number of samples are tested in parallel at each transitional step, which is followed by a resampling step, allowing us to select only the most probable models. The probability of each sample to be selected depends on its ability to fit the observations d_{obs} within the uncertainties $C_{\chi} = C_d + C_p$, where C_d represents the observational errors and C_p the epistemic uncertainties introduced by approximations of the forward model (e.g. Minson et al., 2013; Duputel et al., 2014; Ragon et al., 2018, 2019).

The solution space is evaluated through repeated updates of the probability density function (PDF) of each sampled parameter

$$p(\mathbf{m}, \beta_i) \propto p(\mathbf{m}) \cdot exp[-\beta_i \cdot \chi(\mathbf{m})],$$
 (1)

where **m** is the sampled model, $p(\mathbf{m})$ the prior information on this sample, *i* corresponds to each iteration and β evolves dynamically from 0 to 1 to optimize the parameter space exploration Minson et al. (2013). $\chi(\mathbf{m})$ is the misfit function which quantifies the discrepancies between observations and predictions within uncertainties described by the covariance matrix \mathbf{C}_{χ} (Tarantola, 2005; Minson et al., 2013, 2014; Duputel et al., 2014)

$$\chi(\mathbf{m}) = \frac{1}{2} [\mathbf{d}_{obs} - \mathbf{G}(\mathbf{m})]^T \cdot \mathbf{C}_{\chi}^{-1} \cdot [\mathbf{d}_{obs} - \mathbf{G}(\mathbf{m})].$$
(2)

S1.2 Priors and outputs

We solve for both slip amplitude and rake, within the assumed prior distributions specified below. For the subduction toy model:

- Positive uniform prior p(m) = U(0 m, 50 m) for the dip-slip parameters, p(m) = N(0 m, 1 m) for the strike-slip parameters.
- Slip is solved at each fault node
- Assumed subfault dimension: 25 km side

For the Maule earthquake:

- Positive uniform prior $p(\mathbf{m}) = \mathcal{U}(0 \text{ m}, 50 \text{ m})$ for the dip-slip parameters, $p(\mathbf{m}) = \mathcal{N}(0 \text{ m}, 2 \text{ m})$ for the strike-slip parameters.
- Slip is solved at each fault node
- Assumed triangular subfault dimension: \sim 37 km side.

The final output consists in a series of models sampled from among the most plausible models of the full solution space. To explore the results, we consider probabilistic variables, such as a combination of the mean of the sampled models and the associated posterior uncertainty (standard deviation).

S2 Details for the synthetic case

S2.1 Mesh properties



Figure S2 Mesh used to compute the true forward model

- Mesh dimensions: 1250 km x 1000 km x 600 km height
- topography ranges from 6 km at the trench to 2 km in the volcanic arc
- Elements are tetrahedrons
- Element size increases from 2 km near the fault to 50 km near the edges
- Fault is 500 km long and 200 km wide
- subfaults are triangular

S2.2 True 3D crustal structure, used to calculate the synthetic data

- fault architecture varies along strike
- subfaults dimensions: 5 km side
- Spatially correlated noise is added to synthetic data: 15 km wavelength, 1.5 cm amplitude

Table 1True 3D elastic properties

Domain	Dimension	Density (kg/m ³)	Vs (m/s)	Vp (m/s)	μ (GPa)	μ/μ_0
oceanic crust	8-km-thick	2800 to 3000	3.5	5.5	34.3 to 50	0.65
wedge	25-km-wide	1900	3.0	5.3	17.0	0.32
slab	12-km-thick	3200	4.5	8	64.8	1.24
continental crust	35-km-thick	2500	4.0	7.0	40	0.76
mantle	-	3000 to 3350	4.2	7.5	52 (μ_0) to 60	1 to 1.15

S2.3 Assumed crustal structures, used for inversion

- Fault architecture is similar to the one adopted for calculating synthetic data, except if indicated otherwise (if planar, the assumed plane is the best fitting one)
- Subfaults dimensions: 25-km-side

 Table 2
 Layered crust: Assumed elastic properties

Domain	Dimension	Density (kg/m ³)	Vs (m/s)	Vp (m/s)	μ (GPa)	μ/μ_0
oceanic crust	8-km-thick	2800	3.5	5.5	34.3	0.65
mantle	-	3000	4.2	7.5	52 (μ_0)	1.00

Domain	Dimension	Density (kg/m ³)	Vs (m/s)	Vp (m/s)	μ (GPa)	μ/μ_0
oceanic crust	6-km-thick	3000	3.5	5.5	36.75	0.63
wedge	15-km-wide	2400	3.5	6.2	29.4	0.50
slab	16-km-thick	3300	4.5	8.0	66.8	1.15
continental crust	26-km-thick	2700	4.0	7.0	43.2	0.74
mantle	-	3300	4.2	7.5	58 (μ_0)	1

Table 3 Assumed (incorrect) 3D crust: elastic properties



Figure S3 Trench-perpendicular profiles showing the geometries and elastic domains of the crustal structures adopted for calculating synthetic observations (top, true) or for imaging slip (bottom, assumed). Elastic properties for each domain are detailed in Tables 1, 2 and 3.

S2.4 Additional results



Figure S4 Difference in surface displacements produced by the main slip patch if assuming 3D or layered elastic properties. In (b), the small length-scale rougness is an artefact due to varying spacing of the mesh at this location: it does not impact the results of the inversions as there are no synthetic data in this location. Note that in the far-field (in the primary zone of subsidence, 150-200 km from the trench), the difference in vertical displacement is more than 5 times larger than the difference in horizontal displacement.



Figure S5 Inferred slip model and predictions assuming the correct fault geometry, an homogeneous crust, and using a simple generalized positive least square approach with very mild spatial smoothing for simplicity. We use the model covariance matrix introduced by Radiguet et al. (2011): $C_m(i,j) = \frac{\sigma \lambda_0}{\lambda}^2 e^{-\frac{||i,j||_2}{\lambda}}$, with σ the amplitude of the correlation, λ the characteristic length scale, and λ_0 a normalizing distance: $\sigma = 2$, $\lambda = 5$ and $\lambda_0 = 5$.



Figure S6 Inferred slip model and predictions assuming a fault extending to a shallower depths, a layered crust, and using a simple generalized positive least square approach with spatial smoothing. We use the model covariance matrix introduced by Radiguet et al. (2011): $C_m(i,j) = \frac{\sigma \lambda_0^2}{\lambda} e^{-\frac{||i,j||_2}{\lambda}}$, with σ the amplitude of the correlation, λ the characteristic length scale, and λ_0 a normalizing distance: $\sigma = 1$, $\lambda = 8$ and $\lambda_0 = 5$.

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(d) Eastward displacement

Figure S12 Trench perpendicular profile along **profile A** (see Fig. 4) of measured and predicted surface displacements, for the slip models inferred assuming homogeneous or 3D crustal structures, with and without accounting for epistemic uncertainties. Vertical error bars show the posterior uncertainty or data errors.



(d) Eastward displacement

Figure S13 Trench perpendicular profile along **profile B** (see Fig. 4) of measured and predicted surface displacements, for the slip models inferred assuming homogeneous or 3D crustal structures, with and without accounting for epistemic uncertainties. Vertical error bars show the posterior uncertainty or data errors. Same colors as in Fig. S12.



(a) Inferred slip model

(b) Synthetic slip model with down-dip slip patch

Figure S14 Plausible **12-days afterslip** models for the Maule earthquake. The model in (a) has been inferred with the same assumptions as for the coseismic model. In (b), we modified the slip below 90 km so that it replicates the down-dip slip patch we inferred: this model is also compatible with the data.



(c) Posterior distribution of potential slip values inferred for model (a) at some locations (black stars, from south to north) within the down-dip patch added in (b)

Figure S15 Plausible >**1-year -post-seismic slip** models for the Maule rarthquake. The model in (a) has been inferred with the same assumptions as for the coseismic model. In (b), we modified the slip below 90 km so that it replicates the down-dip slip patch we inferred: this model is also compatible with the data. In (c), the posterior probability density functions of model (a) tell us that the synthetic ~1 m slip of model (b) falls within inferred potential slip values of model (a).



Figure S16 Post-seismic slip model with deep slip removed: deep slip is required to explain the vertical displacement of the distal data.

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