

Hydrothermal friction experiments on simulated basaltic fault gouge and implications for megathrust earthquakes

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Abstract

Nucleation of earthquake slip at the plate boundary fault (décollement) in subduction zones has been widely linked to the frictional properties of subducting sedimentary facies. However, recent seismological and geological observations suggest that the décollement develops in the subducting oceanic crust in the depth range of the seismogenic zone, at least in some cases. To understand the frictional properties of oceanic crustal material and their influence on seismogenesis, we performed hydrothermal friction experiments on simulated fault gouges of altered basalt, at temperatures of 100-550 °C. The friction coefficient (μ) lies around 0.6 at most temperature conditions but a low μ down to 0.3 was observed at the highest temperature and lowest velocity condition. The velocity dependence of μ , a-b, changes with increasing temperature from positive to negative at 100-200 °C and from negative to positive at 450-500 °C. Compared to gouges derived from sedimentary facies, the altered basalt gouge showed potentially unstable velocity weakening over a wider temperature range. Microstructural observations and microphysical interpretation infer that competition between dilatant granular flow and viscous compaction through pressure-solution creep of albite contributed to the observed transition in a-b. Alteration of oceanic crust during subduction produces fine grains of albite and chlorite through interactions with interstitial water, leading to reduction in its frictional strength and an increase in its seismogenic potential. Therefore, shear deformation possibly localizes within the altered oceanic crust leading to a larger potential for the nucleation of a megathrust earthquake in the depth range of the seismogenic zone.

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Key points:

- Altered basalt shows unstable frictional behavior under a wide range of hydrothermal conditions.

- Production of fine-grained albite during subduction promotes the frictional instability via pressure solution creep.
- Subducting oceanic crust may serve as a source of nucleating megathrust earthquakes in subduction zones.

Abstract

Nucleation of earthquake slip at the plate boundary fault (décollement) in subduction zones has been widely linked to the frictional properties of subducting sedimentary facies. However, recent seismological and geological observations suggest that the décollement develops in the subducting oceanic crust in the depth range of the seismogenic zone, at least in some cases. To understand the frictional properties of oceanic crustal material and their influence on seismogenesis, we performed hydrothermal friction experiments on simulated fault gouges of altered basalt, at temperatures of 100-550 °C. The friction coefficient (μ) lies around 0.6 at most temperature conditions but a low μ down to 0.3 was observed at the highest temperature and lowest velocity condition. The velocity dependence of μ , $a-b$, changes with increasing temperature from positive to negative at 100-200 °C and from negative to positive at 450-500 °C. Compared to gouges derived from sedimentary facies, the altered basalt gouge showed potentially unstable velocity weakening over a wider temperature range. Microstructural observations and microphysical interpretation infer that competition between dilatant granular flow and viscous compaction through pressure-solution creep of albite contributed to the observed transition in $a-b$. Alteration of oceanic crust during subduction produces fine grains of albite and chlorite through interactions with interstitial water, leading to reduction in its frictional strength and an increase in its seismogenic potential. Therefore, shear deformation possibly localizes within the altered oceanic crust leading to a larger potential for the nucleation of a megathrust earthquake in the depth range of the seismogenic zone.

Plain Language Summary

Megathrust earthquakes in subduction zones have long been studied to mitigate damage by ground shakings and tsunamis. Frictional properties of plate boundary fault are fundamental information to understand the slip activities causing megathrust earthquakes. In this study, we focused on altered basalt, which is a rock of subducting oceanic crust and has not been focused on as much as sedimentary rocks. Laboratory friction experiments were performed at a wide temperature range with water pressurized conditions. We found that the altered basalt shows frictionally unstable behavior of the type that is prerequisite for generating an earthquake in the temperature conditions of seismogenic zone. This unstable behavior is likely to be result of alteration of oceanic crust during subduction. Because the altered basalt can be mechanically as weak as sedimentary facies, subducting oceanic crust forms an additional or perhaps even preferred candidate for sourcing megathrust earthquakes in subduction zones.

Introduction

Megathrust earthquakes in subduction zones generally source in the depth range of ~5-25 km corresponding to a temperature (T) range of ~150-350 °C (Hyndman et al., 1997). The extent of this “seismogenic zone” was originally postulated to be related to the smectite-illite dewatering transition as the transition temperature is consistent with the temperature condition at the updip limit of the seismogenic zone (Oleskevich et al., 1999). However, this hypothesis is not fully supported by experiments (e.g. Saffer and Marone, 2003). Instead, recent experimental studies showed that the effect of temperature on the velocity dependence of illite-quartz mixture can explain both up-dip and down-dip limits (den Hartog, Peach, et al., 2012), and that a change in the extent of lithification of sediments during subduction may contribute to making the plate boundary fault (décollement) frictionally unstable (Ikari & Hupers, 2021).

The frictional properties of sediments have long been the focus for understanding the frictional behavior of the décollement. This notion is certainly valid for shallow depths near the trench where sedimentary décollement materials have been successfully drilled from the plate boundary, e.g. in the Japan Trench, NE Japan, in relation to the 2011 Tohoku-oki Earthquake (Chester et al., 2013) or in the Nankai Trough, SW Japan (Sakaguchi et al., 2011). However, at the depth of the updip limit of the seismogenic zone,

interpretation of seismic reflection profiles of the Nankai and Sagami (SE Japan) regions suggests that the decollement develops within the subducting oceanic crust beneath the sedimentary layer. This is called “decollement stepdown”, which produces a duplex structure due to the underplating process (H. Kimura et al., 2010; Park et al., 2002). Although the interpretation of seismic reflection profiles varies among studies, geological structures with underplated basaltic layers that are considered to represent ancient oceanic crust or seamounts have been found in exhumed accretionary complexes all over the world (Figure 1) (G. Kimura & Ludden, 1995; Kusky et al., 2013; Wakita, 2015). In the case of the Shimanto accretionary complex in SW Japan, which is thought to have been located along a plate boundary similar to the current Nankai Trough, cataclasite is observed at the top part of the basaltic layer. This is interpreted to represent the decollement at shallow depth, whereas shear deformation features, developed after the decollement stepdown, are preserved at the bottom part of the basaltic layer (Ikesawa et al., 2005; G. Kimura et al., 2012). In addition, vitrinite reflectance data and fluid inclusion geothermometry indicate that the duplex structures in the Shimanto complex that involve a basaltic layer experienced temperatures of 150-300 (Kameda et al., 2017). This suggests that the decollement is not always located within underthrusting sediments at the updip depth limit of the seismogenic zone (~ 150) but possibly within the subducting oceanic crust. However, experimental studies on basaltic fault rock in subduction zones, and under subduction zone conditions, are limited despite their possible importance for hosting megathrust earthquakes.

It is well established that oceanic crust commonly experiences partial alteration soon after its formation, because of the interaction between mid-ocean ridge (fresh) basalt and interstitial water (Braden & Behr, 2021; Kameda et al., 2017; Phillips et al., 2019; Ujiie et al., 2007). At shallow depths, such as the current seafloor, the volcanic glass component alters into saponite, which is an Mg-rich smectite (Kameda et al., 2011). As the altered oceanic crust later subducts, saponite dehydrates to form chlorite at ~ 150 (Kameda et al., 2011). At a similar temperature, albitization of anorthic plagioclase also occurs (Moore et al., 2007), which also produces chlorite (Rosenbauer et al., 1988). The mineral assemblage present in altered basalt up to ~ 300 is accordingly $\sim 25\%$ saponite or chlorite, $\sim 25\%$ clinopyroxene, and $\sim 50\%$ plagioclase (Kameda et al., 2017). At temperatures > 300 , clinopyroxene decomposes into epidote and quartz (Kameda et al., 2017) or actinolite (and quartz) (Humphris & Thompson, 1978; Takeshita et al., 2015).

In previous room temperature studies (Ikari et al., 2020), unaltered basalt gouge under 25 MPa effective normal stress ($\sigma_v^{\epsilon\varphi\varphi}$) with 5 or 24 MPa pore pressure (P_f) conditions exhibited velocity-neutral to velocity-weakening behavior at slip velocities of 3-300 $\mu\text{m/s}$, whereas altered basalt gouge showed a clear trend toward more frictionally stable behavior with increasing velocity ($> 3 \mu\text{m/s}$). Velocity-weakening behavior was observed only at low velocities ($< 1 \mu\text{m/s}$) in the case of surface sliding of altered basalt with saponite, suggesting that the altered basalt is capable of hosting slow slip events at shallow depths (Ikari et al., 2020). At elevated T conditions, unaltered basalt gouge under ~ 50 MPa $\sigma_v^{\epsilon\varphi\varphi}$ with 100 MPa P_f showed velocity-weakening behavior in the range of $T = 250$ -600 and at shearing velocities of 0.02-1.15 $\mu\text{m/s}$ (Zhang et al., 2017). Altered basalt with chlorite has only been tested under hydrothermal conditions at $T = 150$ with confining pressure of 120 MPa and 43 or 84 MPa P_f , showing velocity-weakening behavior (Phillips et al., 2020). Friction coefficients of unaltered and altered basalt are 0.6-0.7 at $T = 150$, higher than those of illite-rich shale (0.45-0.55) (den Hartog, Niemeijer, et al., 2012; Phillips et al., 2020). Mixed actinolite-chlorite and chlorite gouges also show velocity-weakening behavior at $T = 200$ -400 and 300, respectively (Okamoto et al., 2019, 2020). In addition, a low $\sigma_v^{\epsilon\varphi\varphi}$ (< 50 MPa) is reported to promote velocity-weakening behavior in the case of blueschist gouge sheared at $T = 22$ -400 under $P_f = \sigma_v^{\epsilon\varphi\varphi}$ conditions (Sawai et al., 2016). These studies imply that subducting altered oceanic crustal material has the potential to exhibit unstable frictional behavior, but the dependencies of its frictional stability on T , P_f , and $\sigma_v^{\epsilon\varphi\varphi}$ are not yet fully understood.

In this study, we collected altered basaltic rock from an exhumed *mélange* in SW Japan and conducted friction experiments on a simulated gouge prepared from it at temperatures ranging from 100 to 550. The aim was to investigate the frictional behavior of subducting oceanic crustal material under the conditions of the seismogenic zone. We mostly used an $\sigma_v^{\epsilon\varphi\varphi}$ of 100 MPa and P_f of 100 MPa, and independently tested the effects of increasing P_f and reducing $\sigma_v^{\epsilon\varphi\varphi}$ on frictional behavior.

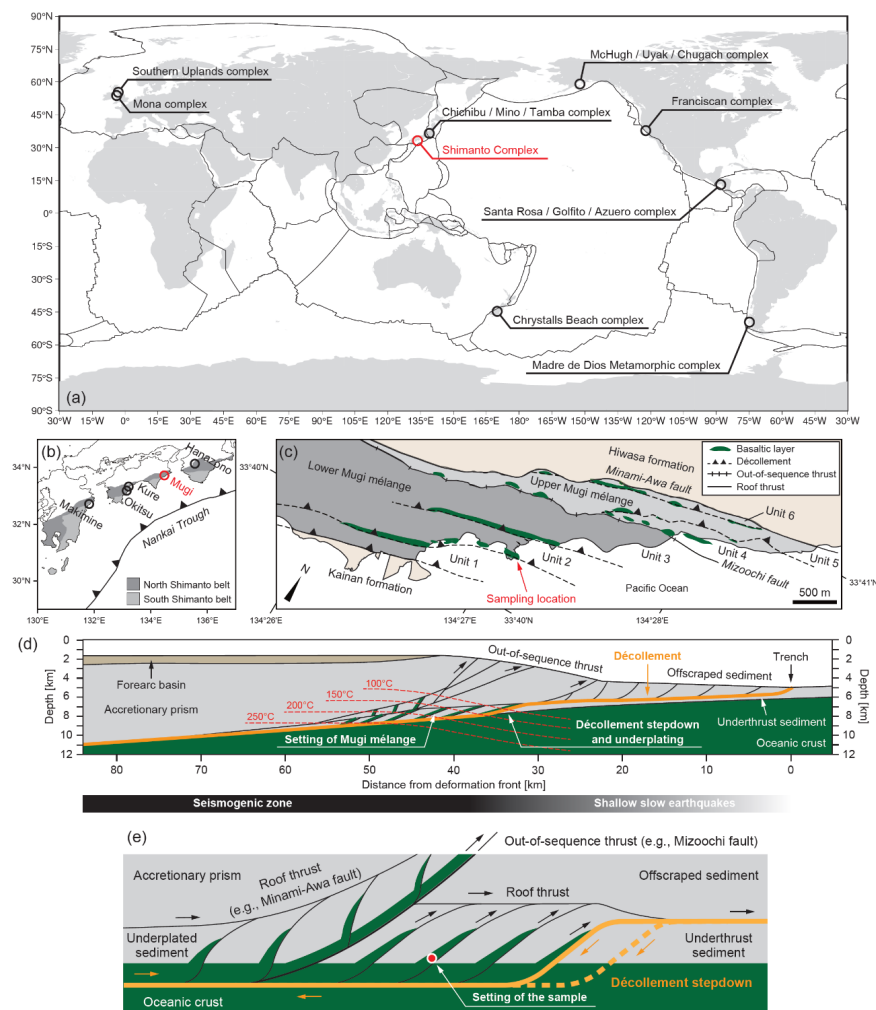


Figure 1. (a) Global map showing examples of accretionary complexes where underplated ocean floor basalt or seamount basalts are found at relatively shallow depths ($T < 300$) (cf., G. Kimura & Ludden (1995); Kusky et al. (2013); Raymond (2019); Wakita (2015)). Shimanto complex in SW Japan (Kameda et al., 2017), Chichibu, Mino, Tamba complex in central Japan (G. Kimura & Ludden, 1995), Franciscan complex in California (Meneghini & Moore, 2007), McHugh, Uyak, Chugach complex in southern Alaska (Braden & Behr, 2021; Kusky & Bradley, 1999), Southern Uplands complex in Scotland (Leggett et al., 1979), Mona complex in Wales (Kawai et al., 2007; Maruyama et al., 2010), Chrystalls Beach complex in New Zealand (Fagereng & Cooper, 2010), Madre de Dios Metamorphic complex in southern Chile (Willner et al., 2009), Santa Rosa, Gofito, Azuero complex in Costa Rica and Panama (Baumgartner & Denyer, 2006; Buchs et al., 2010). (b) Mélanges where underplated basaltic layers are found in the Shimanto complex: Hanazono mélangé (Onishi et al., 2001), Mugi mélangé (Ikasawa et al., 2005; G. Kimura et al., 2012; Kitamura et al., 2005), Kure mélangé (Mukoyoshi et al., 2006), Okitsu mélangé (Ikasawa et al., 2003), Makimine mélangé (Hara & Kimura, 2008). (c) Closeup map view of Mugi mélangé modified after Yamaguchi et al. (2012) showing the sampling location. (d) Schematic cross section of the Nankai Trough and (e) schematic cross section showing the geological structures of Mugi mélangé where the décollement steps down into the oceanic crust (G. Kimura et al., 2012).

Method

Samples

The altered basalt sample was collected from an outcrop of the Mugi mélangé, in the Shimanto accretionary complex, SW Japan (Figure 1). This mélangé formed in the Late Cretaceous and experienced T of 150-200 based on vitrinite reflectance data and P_f of ~ 100 MPa based on fluid inclusion geothermometry (Ikesawa et al., 2005; G. Kimura et al., 2012; Kitamura et al., 2005; Matsumura et al., 2003). The basalt initially formed as mid-ocean ridge basalt, subducted down to the seismogenic zone depth of a former subduction plate boundary that is similar to the current Nankai Trough. It was then incorporated into the accretionary prism by underplating associated with decollement stepdown, and then exhumed (G. Kimura et al., 2012). The altered basalt sample is composed of albitized plagioclase, clinopyroxene, and chlorite (Figure 2). The albitized plagioclase consists of fine grains of albite with a grain size of about $10\ \mu\text{m}$ (Figure 2b). Chlorite is formed within and around albitized plagioclase (Figure 2d). Before experimentation, we crushed and sieved the sample to obtain a simulated gouge material with a grain size of $<100\ \mu\text{m}$. Mineral composition of the sample was estimated by point counting with ~ 1300 grains in a thin section. We obtained $\sim 50\%$ albite, $\sim 27\%$ clinopyroxene, $\sim 15\%$ chlorite, and $\sim 8\%$ opaque minerals, which is generally consistent with previously reported compositions of basaltic rock from the Mugi mélangé (Kameda et al., 2017; Phillips et al., 2020).

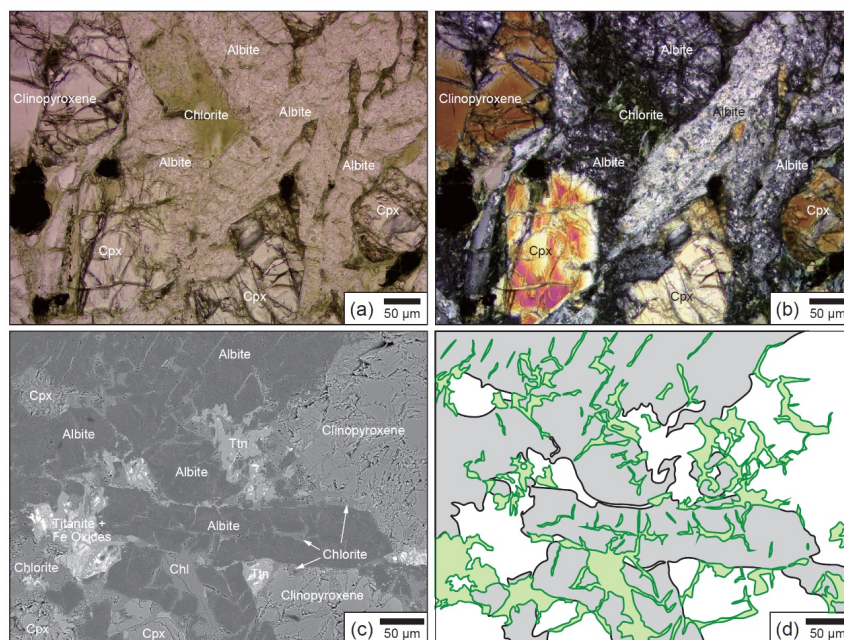


Figure 2. Microstructures of intact altered basalt sample under plane-polarized (a), crossed-polarized (b), and BSE images (c). (d) Albite (gray areas) and chlorite (green areas) distributions based on (c).

Experiments

Laboratory friction experiments were conducted on the simulated gouge material using the hydrothermal ring shear apparatus at Utrecht University (Figure 3). In preparing each experiment, 0.5 g of sample was sandwiched between two René-41 Superalloy pistons, confined laterally between an outer confining ring (diameter=28 mm) and an inner confining ring (diameter=22 mm). The gouge had a thickness of ~ 1.2 mm before imposing the normal load. The piston-sample assembly was subsequently placed inside the hydrothermal pressure vessel in line with the machine's pressure-compensated loading piston, allowing us to control both the $\sigma_v^{\epsilon\varphi\varphi}$ and P_f independently. Distilled water was introduced into the pressure vessel as the pore fluid and heated up by an internal furnace to achieve given T conditions. Because the sample is not sealed by the outer/inner rings, pore fluid can freely go through the sample. See previous studies for details

of the apparatus (den Hartog, Niemeijer, et al., 2012; Niemeijer et al., 2016).

Experiments were performed at an $\sigma_v^{\epsilon\varphi\varphi}$ of 100 MPa, a P_f of 100 MPa, and velocities (V) of 1-3-10-30-100 $\mu\text{m/s}$. Shear displacement was set to be 1.5 mm for 1 to 10 $\mu\text{m/s}$ and 3 mm for 30 and 100 $\mu\text{m/s}$, except for the first shearing at 1 $\mu\text{m/s}$ for which we imposed 5 mm of shear displacement. Various T conditions from 100 to 550 were tested by stepping T by 50 : 100-150-200-250 for u968, 250-300-350-400 for u972, 400-450-500-550 for u992 and u996. We refer to each T condition in one experiment as a “stage” (e.g., stage 1 for u968 was done under $T = 100$; Figure 3d). Changes in V were abruptly imposed, whereas we waited at least 1 hour after a change in T to allow the system to stabilize. To elucidate the effect of shear displacement on frictional behavior, tests with 250 and 400 were performed at different displacement conditions. At $T = 200$ and 500 , the effects of overpressured conditions with respect to the hydrostatic condition ($\sigma_v^{\epsilon\varphi\varphi} [?] P_f$) were tested by varying P_f from 50 MPa to 200 MPa and $\sigma_v^{\epsilon\varphi\varphi}$ from 30 MPa to 100 MPa, independently. An additional experiment with V in the range from 0.003 $\mu\text{m/s}$ to 1 $\mu\text{m/s}$ was performed specifically at $T = 400$ to investigate the frictional behavior at a V close to the plate convergence rate. Several constant V experiments were also performed, which were used for microstructural observations. We also performed one test stepping the temperature from $T = 100$ to 200 under vacuum dry condition to see the effect of the absence vs. presence of fluid (pressure) on frictional behavior. See Tables 1 and S1 for the detailed experimental conditions.

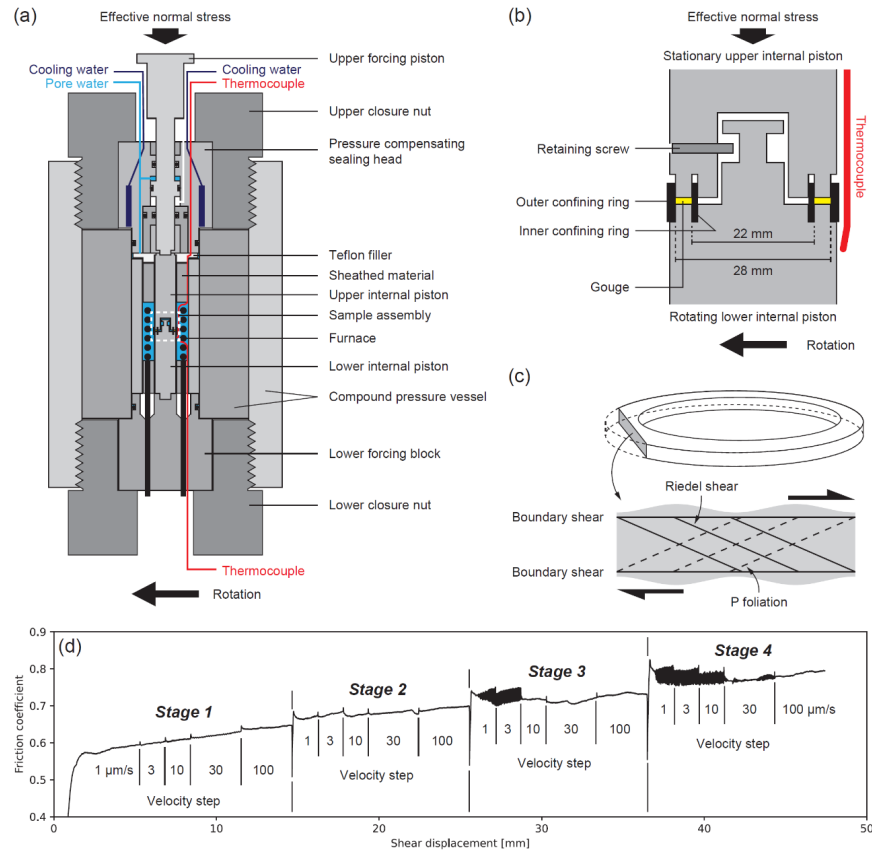


Figure 3. Schematic views of (a) the hydrothermal ring shear apparatus and (b) the close-up view of the sample assembly (Chen et al., 2020; den Hartog, Niemeijer, et al., 2012). After the experiment, the sample was retrieved and microstructure was observed using the cross section shown in (c). (d) Overview of the velocity sequences and stages employed in this study (example of u968).

Data acquisition and processing

During individual experiments, shear displacement, normal displacement, applied normal force, torque, temperature, and pore pressure signals were continuously logged at a sampling rate of 1-100 Hz. The raw data was converted to (effective) normal and shear stresses using the sensor calibrations and sample dimensions (see information in data repository). Friction coefficient μ was obtained from the shear stress normalized by the $\sigma_v^{\epsilon\varphi\varphi}$ without considering cohesion. The V dependence of μ was determined using quasi-instantaneous V steps and quantified using the following equation:

$$a - b = \frac{\Delta\mu_{ss}}{\Delta \ln V}, \# (1)$$

where $\Delta\mu_{ss}$ is the difference between the steady state μ values at V -conditions before and after the V -step, $\Delta \ln V$ is the difference in V in the logarithmic scale, and $a-b$ is the nondimensional value representing the V dependence of μ which is originally formulated with rate- and state-dependent friction constitutive law (Dieterich, 1979; Ruina, 1983). We only focus on $a-b$ because this parameter controls whether a fault has the potential to slip unstably or not: a fault slips stably when $a-b$ is positive (V -strengthening) whereas a fault can slip unstably, thus an earthquake can occur, when $a-b$ is negative (V -weakening). The $\Delta\mu_{ss}$ was obtained by comparing the averaged μ values just before and after the V step after removal of linear slip-dependent trends. Although we sometimes observed a hardening trend which can be modeled with negative b_2 with long d_{c2} (Blanpied et al., 1998), we did not take this hardening into account because such a long displacement for the transition of μ would not much affect the V dependence of μ during the accelerating earthquake nucleation phase. We used the averaged μ values in the case of stick-slips were observed, which led to a large standard deviation of $a-b$ of <0.04 whereas this was <0.006 when stick slips were not observed.

Table 1. List of experiments and corresponding conditions. T = temperature, $\sigma_v^{\epsilon\varphi\varphi}$ = effective normal stress, P_f = pore fluid pressure, V = velocity, and d = shear displacement.

Run	Stage	T [°C]	$\sigma_v^{\epsilon\varphi\varphi}$ [MPa]	P_f [MPa]	V [$\mu\text{m/s}$]	d [mm]
u968	1 2 3 4	100 150 200 250	100	100	1-3-10-30- 100	0-14.6 14.6-25.6 25.6-36.5 36.5-47.4
u972	1 2 3 4	250 300 350 400	100	100	1-3-10-30- 100	0-14.6 14.6-25.6 25.6-36.5 36.5-47.4
u992	1 2 3 4	400 450 500 550	100	100	1-3-10-30- 100	0-14.6 14.6-25.6 25.6-36.5 36.5-47.4
u996	1 2 3 4	400 450 500 550	100	100	1-3-10-30- 100	0-14.6 14.6-25.6 25.6-36.5 36.5-47.4
u991	1 2 3 4	200	100	50 100 150 200	1-3-10-30- 100	0-14.6 14.6-25.6 25.6-36.5 36.5-47.4
u993	1 2 3 4	500	100	50 100 150 200	1-3-10-30- 100	0-14.6 14.6-25.6 25.6-36.5 36.5-47.4

Run	Stage	T [°C]	$\sigma_{\nu}^{\epsilon\varphi\varphi}$ [MPa]	P_f [MPa]	V [μm/s]	d [mm]
u1002	1 2 3 4	200	30 50 100 50	100	1-3-10-30-100	0-14.6 14.6-25.6 25.6-36.5 36.5-47.4
u1006	1 2 3 4	500	30 50 100 50	100	1-3-10-30-100	0-14.6 14.6-25.6 25.6-36.5 36.5-47.4
u1003	1 2 3	100 150 200	100	Vacuum dry	1-3-10-30-100	0-14.6 14.6-25.6 25.6-36.5
u1017	1	400	100	100	1-0.003-0.01-0.03-0.1-0.3-1	0-10.6
u975	1	550	100	100	1-0.01	0-8.7
u980	1	400	100	100	1	0-8.7
u981	1	100	100		100	0-8.7

Microstructural analysis

After three constant V experiments (u975, u980, and u981), the samples were retrieved from the apparatus and impregnated with epoxy after drying for 24 hours at 50 °C. Thin sections were prepared from the impregnated sample by cutting parallel to the shear direction (Figure 3c). Polarized optical microscopy and Scanning Electron microscopy (SEM, Zeiss Evo 15 located at the Electron Microscope center at Utrecht University) were used to observe the microstructure. SEM was conducted using backscattered electron (BSE) mode and employing Energy Dispersive Spectrometer (EDS) for the acquisition of chemical information.

1. **Results**
2. **Mechanical data**
3. **Effects of temperature, velocity and shear displacement**

3.1.1.1. On friction coefficient

The evolution of friction coefficient (μ) with displacement (d) at different T and V conditions and at $\sigma_{\nu}^{\epsilon\varphi\varphi} = P_f = 100$ MPa is shown in Figure 4a. Because we stepped T at larger d , friction data at higher T were influenced by the displacement history. To focus only on V - T effects on frictional behavior, here we describe results per stage.

In stage 1 ($0 < d < 14.6$ mm; $T = 100, 250, 400$), μ showed rapid increase to 0.57-0.58 at the first 1-2 mm of displacement, followed by gradual increases to 0.62-0.65 at the end of stage 1 ($d = 14.6$ mm). We observed V -strengthening behavior only at V -steps from $V = 10$ to 30 μm/s and 30 to 100 μm/s for $T = 100$ (u978). Other V -steps in stage 1 were showing V -weakening and stick-slips were observed at $V = 1$ and 3 μm/s for u996 ($T = 400$).

In stage 2 ($14.6 < d < 25.6$ mm; $T = 150, 300, 450$), μ increased rapidly at the beginning and showed peaks at $d \sim 0.5$ mm. This behavior was also observed for stage 3 and 4. After the peaks, μ once dropped and then showed a little slip-hardening trend. For $T = 150$ (u968), V -strengthening behavior was observed at the step from $V = 30$ to 100 μm/s and other V -steps showed V weakening. All V steps for $T = 300$ (u972) showed V -weakening behavior (stick-slips were observed up to $V = 30$ μm/s). For $T = 450$ (u992 and u996), μ continuously dropped from peak values during $V = 1$ μm/s, whereas μ showed slip-hardening trends at $V > 3$ μm/s. Mostly stick slips were observed for u996 whereas they did not occur but at the last

of $V = 30 \mu\text{m/s}$ for u992. Final μ values of stage 2 were 0.70 for $T = 150$ (u968), 0.66 for 300 (u972), and 0.73 for 450 (u992 and u996).

In stage 3 ($25.6 < d < 36.5 \text{ mm}$; $T = 200, 350, 500$), nearly constant μ values over shear displacements with V -weakening behavior and stick-slips were observed for $T = 200$ (u968) and 350 (u972). The μ values at the end of the stage were 0.74 for $T = 200$ (u968) and 0.69 for $T = 350$ (u972). Frictional behavior for $T = 500$ (u992 and u996) was quite different from lower T conditions. After the peak, μ continuously dropped at $V = 1 \mu\text{m/s}$ and subsequently increased with concave upward curve (thus V -strengthening) at $V = 3$ and $10 \mu\text{m/s}$. In contrast, V -weakening behavior (and stick slips for u996) was observed at $V > 30 \mu\text{m/s}$ with slip hardening trend. The final μ values were 0.83 (u992) and 0.79 (u996).

In stage 4 ($36.5 < d < 47.4 \text{ mm}$; $T = 250, 400, 550$), frictional behavior of $T = 250$ (u968) and 400 (u972) was similar to that at stage 3 showing nearly constant μ values with V -weakening behavior. Stick slips were observed at all V conditions for $T = 400$ (u972) and all but $V = 100 \mu\text{m/s}$ for $T = 250$ (u968). For the tests with $T = 550$ (u992 and u996), μ dropped from the peak values at $V = 1 \mu\text{m/s}$ and subsequently showed concave upward increase at $V = 3, 10$, and at $30 \mu\text{m/s}$. At $V = 100 \mu\text{m/s}$, both u992 and u996 showed minor slip-hardening trends with V -strengthening behavior for u992 and V -weakening behavior for u996 (stick-slips were also observed). The final μ values were 0.79 for 250 (u968), 0.75 for 400 (u972), 0.91 and 0.85 for 550 (u992 and u996, respectively).

Because the higher T and/or higher V conditions were imposed at later stages with larger d , the observed μ at such conditions would be overestimated due to a continuous background strain hardening trend (Figure 4c). Hence, μ values of 0.57-0.58 at yield points at $d \sim 1\text{-}2 \text{ mm}$ in the stage 1 are the μ values for the tested altered basalt that are least affected. To evaluate the effect of strain hardening trend on μ at large d , our experiments were designed to have the same T condition at different d for $T = 250$ (stage 4 for u968 and stage 1 for u972) and 400 (stage 4 for u972 and stage 1 for u992 and u996). Using the data with $V = 10 \mu\text{m/s}$ which had less fluctuation than those with other V conditions, we obtained slip-hardening trends (μ / δ) of 0.005 mm^{-1} for $T = 250$ and 0.003 mm^{-1} for 400. Therefore, we use 0.004 mm^{-1} for a universal slip-hardening trend (gray line in Figure 4a) to obtain the first estimation of μ values without slip-hardening trend and detrended μ values are shown in Figure 4b. The detrended data may include an error in μ of ± 0.05 at most, resulting from using the bounds of 0.003 or 0.005 mm^{-1} for the slip-hardening trend (Figure 4a). In Figures 4d, we show the relationship between detrended μ , T and V , which will be used for the discussion in this study. The representative μ value at each P - T - V condition was determined at the last part of each condition after detrending the universal slip-hardening trend: $\mu \sim 0.6$ at $T < 400 \text{ }^\circ\text{C}$ with $V = 1\text{-}100 \mu\text{m/s}$; μ at low V conditions decreases with T at $T > 400 \text{ }^\circ\text{C}$; μ becomes 0.45 for $V = 1 \mu\text{m/s}$ and 0.7 for $V = 100 \mu\text{m/s}$ at $T = 550 \text{ }^\circ\text{C}$ (Figure 4d).

3.1.1.2. On velocity dependence of friction coefficient (a - b)

The a - b values vary depending on V and T . For example, at $T = 100 \text{ }^\circ\text{C}$, negative a - b values were observed at $V < 10 \mu\text{m/s}$, whereas positive a - b values were observed at $V > 30 \mu\text{m/s}$. At $V = 100 \mu\text{m/s}$, positive a - b values were observed up to $T = 200 \text{ }^\circ\text{C}$, negative a - b values up to $T = 500 \text{ }^\circ\text{C}$, and positive a - b values were again observed at higher T (Figure 4e). In general, a - b values were positive at high- V -low- T and low- V -high- T conditions, whereas a - b values were negative at intermediate- V -intermediate- T conditions. We define three Regimes based on the sign of a - b values in the V - T space as follows: Regime A is the high- V -low- T range where a - b values are positive; Regime B is the intermediate- V -intermediate- T range where a - b values are negative; Regime C is the low- V -high- T range where a - b values are positive (Figure 4e). Both transitions between Regimes at lower T occurred at lower V conditions, e.g., the transition between Regime B and C was at $T = 450 \text{ }^\circ\text{C}$ for $V = 3\text{-}10 \mu\text{m/s}$ whereas $T = 550 \text{ }^\circ\text{C}$ for $V = 30\text{-}100 \mu\text{m/s}$. Results from experiments with $T = 250$ and 400 , run at different d (Figure 4f), suggest that d has little influence on the a - b values, despite the slip hardening and T strengthening observed. A previous study on similar altered basalt showed similar values for the μ (0.60-0.69) and a - b (-0.003 - -0.006) at a T of 150 and V of 0.2-2 $\mu\text{m/s}$ (Phillips et al., 2020).

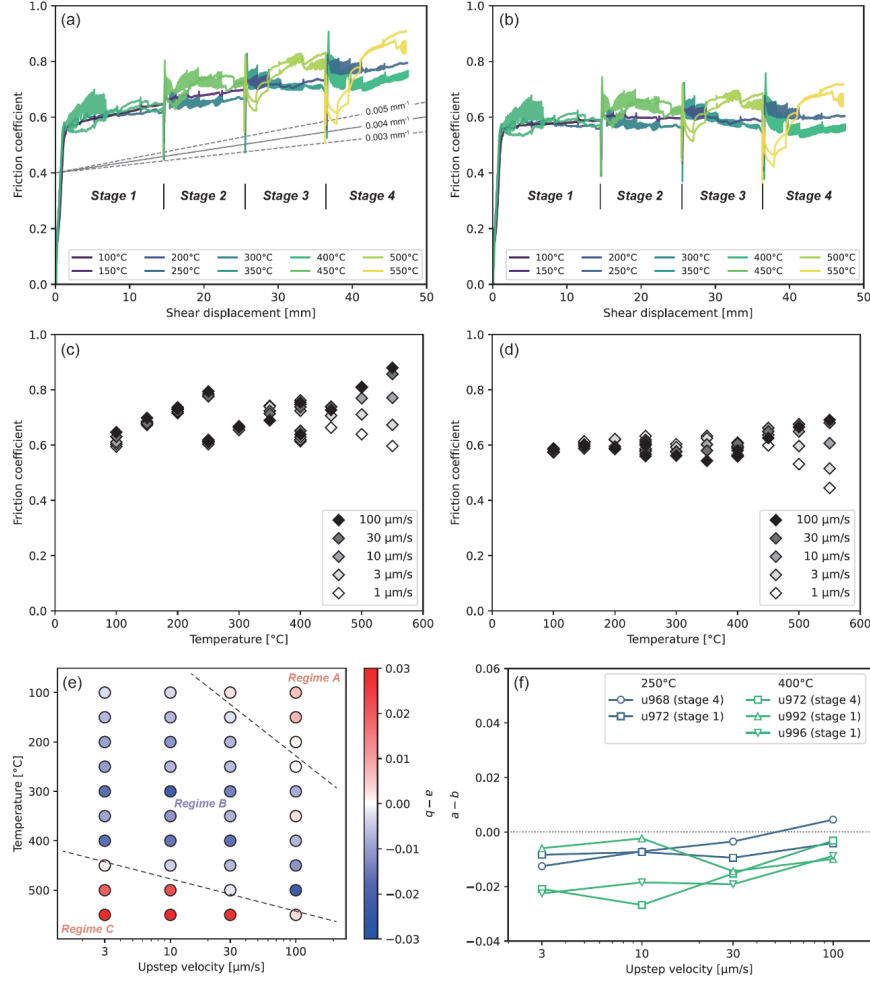


Figure 4. (a) Frictional behavior of altered basalt at $T = 100$ -250 (u968), 250-400 (u972), and 400-550 (u992, u996) with $\sigma_v^{\epsilon\phi\phi} = P_f = 100$ MPa. Trends of μ are also indicated. (b) Frictional behavior after detrending a universal trend of 0.004 mm^{-1} . (c) Variations of μ values (original data) at each V - T condition. (d) Variations of μ values (detrended data) at each V - T condition. (e) Obtained a - b values at each V - T condition. Regime A: V -strengthening regime at high- V -low- T conditions; Regime B: V -weakening regime at wide V - T conditions; Regime C: V -strengthening regime at low- V -high- T conditions. (f) Observed a - b values at 250 and at 400 in different shear displacement. See table 1 for the displacements at which the respective stages were done.

Effect of high pore pressure or low effective normal stress at 200 and 500

At an $\sigma_v^{\epsilon\phi\phi}$ of 100 MPa and P_f of 100 MPa at $T = 200$, the a - b values increase with V and become positive at $100 \text{ } \mu\text{m/s}$ which corresponds to the transition from Regime B to A (open symbols in Figures 5a and b). We did not observe significant variations in the curves of a - b with V when P_f (50-200 MPa) was changed (Figure 5a). Similarly, the effect of $\sigma_v^{\epsilon\phi\phi}$ is minor, but for a - b values a mild increase with $\sigma_v^{\epsilon\phi\phi}$ (Figure 5b) might be inferred. At the $\sigma_v^{\epsilon\phi\phi}$ of 50 MPa, the result of stage 4 shows slightly lower a - b than that of stage 2 (Figure 5b).

At an $\sigma_v^{\epsilon\phi\phi}$ of 100 MPa and aP_f of 100 MPa at $T = 500$, the a - b values decreased with V and became negative at an up-step V of 10 - $30 \text{ } \mu\text{m/s}$ which corresponds to the transition from Regime C to B (open

symbols in Figures 5c and d). The $a-b$ curves shifted towards higher $a-b$ values for higher P_f conditions (Figure 5c). The $a-b$ values increased with $\sigma_v^{\epsilon\phi\phi}$ but only at low V conditions (Figure 5d). Note that only positive values for $a-b$ were observed at high P_f (150 and 200 MPa), whereas negative $a-b$ values were still observed for all other P_f and $\sigma_v^{\epsilon\phi\phi}$ conditions. A larger d caused an increase in $a-b$, particularly at low up-step V (Figure 5d).

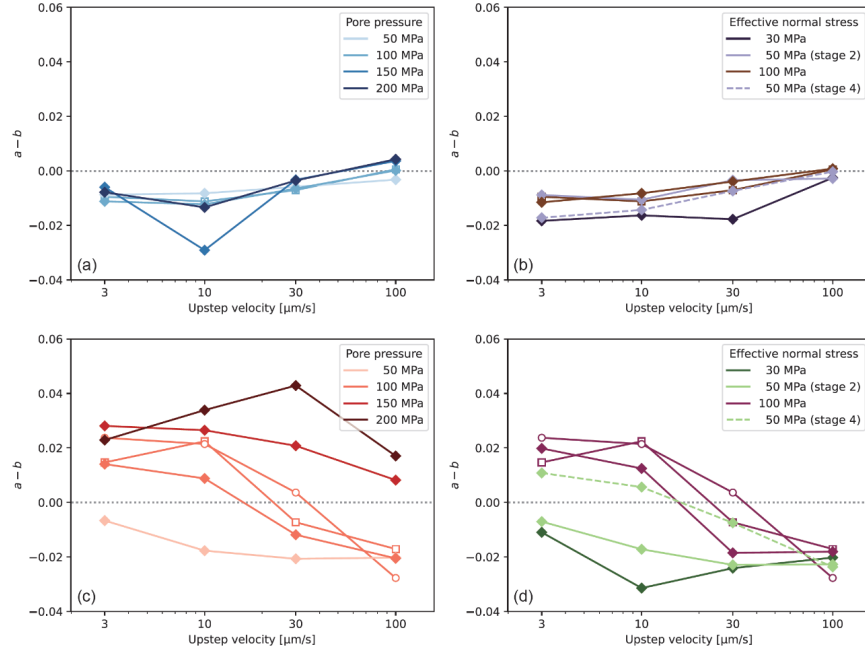


Figure 5. The $a-b$ values for (a) variable P_f conditions with a constant $\sigma_v^{\epsilon\phi\phi}$ of 100 MPa at $T = 200$, (b) variable $\sigma_v^{\epsilon\phi\phi}$ conditions with a constant P_f of 100 MPa at $T = 200$, (c) variable P_f conditions with a constant $\sigma_v^{\epsilon\phi\phi}$ of 100 MPa at $T = 500$, and (d) variable $\sigma_v^{\epsilon\phi\phi}$ conditions with a constant P_f of 100 MPa at $T = 500$. Open symbols represent the “reference” data shown in Figure 3; filled symbols represents the newly obtained data in u991, u993, u1002, and u1006; colors represent different $\sigma_v^{\epsilon\phi\phi}$ or P_f conditions. Dashed lines in (b) and (d) represent the results at the same $\sigma_v^{\epsilon\phi\phi}$ - P_f conditions but different d conditions (stage 2 vs. stage 4). See Table 1 for the displacements which the respective stages were done.

Low velocity conditions at 400 and vacuum dry conditions at 100-200

Detrended μ values obtained for u1017, which was conducted at low V of 0.003-1 $\mu\text{m/s}$, ranged from 0.52 to 0.64, similar to those in other experiments (u972, u992, u996) at $T = 400$ (Figure 6a). The $a-b$ values were negative at all tested V conditions except for the V -step from 0.3 to 1 $\mu\text{m/s}$ (Figure 6b).

Under vacuum dry conditions at $T = 100$ -200, the detrended μ values ranged from 0.59 to 0.67 and the $a-b$ values were close to zero at all V - T conditions. In contrast, wet experiments at the same T and $\sigma_v^{\epsilon\phi\phi}$ conditions (u968) showed slightly lower μ values of 0.57-0.62, and lower $a-b$ values at lower V and/or higher T conditions (Figures 6c-f).

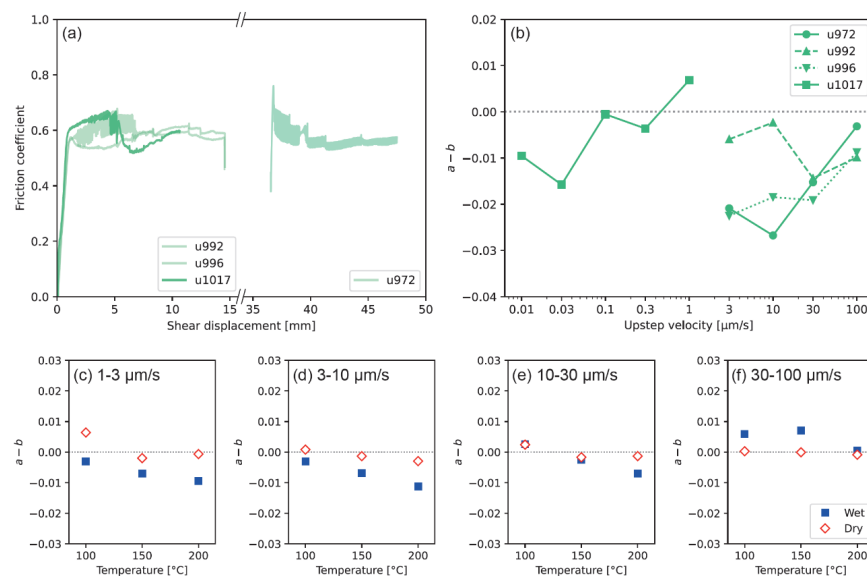


Figure 6. (a-b) Results of detrended μ and $a-b$ for u1017 at low V conditions at $T = 400$ plotted with other experiments at $T = 400$ with $V = 1-100 \mu\text{m/s}$. (c-f) Results of vacuum dry experiments from $T = 100$ to 200 . Blue filled markers are the tests under $100 \text{ MPa } P_f$ (annotated with “wet”) and red open markers are the tests with vacuum dry (annotated with “dry”).

Constant velocity experiments in Regimes A, B, and C

The T and V conditions for the constant V tests were selected on the basis of the three different regimes of V dependence of friction (Figure 7a). The test in Regime A (u981, $T = 100$, $V = 100 \mu\text{m/s}$) showed stable frictional behavior while stick slip behavior was observed in the test in Regime B (u980, $T = 400$, $V = 1 \mu\text{m/s}$). The V -step from 1 to $0.01 \mu\text{m/s}$ in the test in Regime C (u975, $T = 550$, $V = 1-0.01 \mu\text{m/s}$) showed a strong V -strengthening behavior characterized by a gradual decrease to the steady state μ for $V = 0.01 \mu\text{m/s}$, which was about 0.3 at the shear displacement of 8.7 mm (Figure 7b).

Microstructures

After the above constant V experiments, the microstructures of retrieved samples were analyzed to observe the microstructural characteristics of the three Regimes (Figure 7a). In Regime A, the microstructure is characterized by a wide, boundary-parallel cataclastic shear band of $\sim 300-400 \mu\text{m}$ width, and Riedel shears, identified by open fractures (Figure 7c). The shear band is porous and the long axis of larger fragmented grains of both albite and clinopyroxene with grain size less than $\sim 30 \mu\text{m}$ are aligned parallel to the shear direction. Outside the shear band (center part of the gouge), grains are slightly rounded but their sizes are larger (but less than $\sim 50 \mu\text{m}$) than those in the shear band.

In Regime B, the shear band is narrower ($\sim 100 \mu\text{m}$) with a principal slip zone (PSZ) at the center of the shear band (Figure 7d). The PSZ is denser than the shear band in Regime A. Grain size in the PSZ is reduced to sizes $< 1 \mu\text{m}$. At the outside of PSZ but in the shear band, both Riedel shears, characterized by open fractures, and P foliations, characterized by aligned grains which are cataclastically fragmented (grain size $\sim 1-10 \mu\text{m}$), are observed. The long axis of an assemblage of fragmented grains of albite and clinopyroxene are aligned along the P foliation (Figure 8a) but the textures of these grains vary with mineralogy. At the same grain size of around $1 \mu\text{m}$, albite grains are round and interlocking together whereas clinopyroxene grains are angular and do not show interlocking features but form porous aggregates (Figures 8b and c). At the area far from the shear band, grains are angular and their sizes are larger (but less than $100 \mu\text{m}$) than those in the shear band.

In Regime C, the shear band is much narrower ($\sim 50 \mu\text{m}$ in width) and denser than that in Regime B (Figure 7e). Albite grains in the shear band are tightly interlocked and individual grains are difficult to distinguish. Grain size of clinopyroxene is less than $5 \mu\text{m}$ in the shear band (Figure 8d). At the outside of the boundary shear band, grains are angular, and their sizes are $\sim 100 \mu\text{m}$. Variations in textures with mineralogy are also found in Regime C where isolated pores are observed between tightly interlocking albite grains (Figures 8e and f), whereas clinopyroxene grains are angular and occasionally show an indentation into an albite grain at the same scale (Figure 8e). These features suggest that the albite likely underwent dissolution and precipitation processes, such as a pressure solution, whereas clinopyroxene deformed in a mostly brittle manner. Similarly, we observed that large albite grains outside of the shear band tend to have pores inside characterized by unclear grain boundaries (Figure 8f). We also observed limited volumes of very thin ($< 1 \text{ mm}$) chlorite foliation between grains, subparallel to shear deformation (Figure 8f).

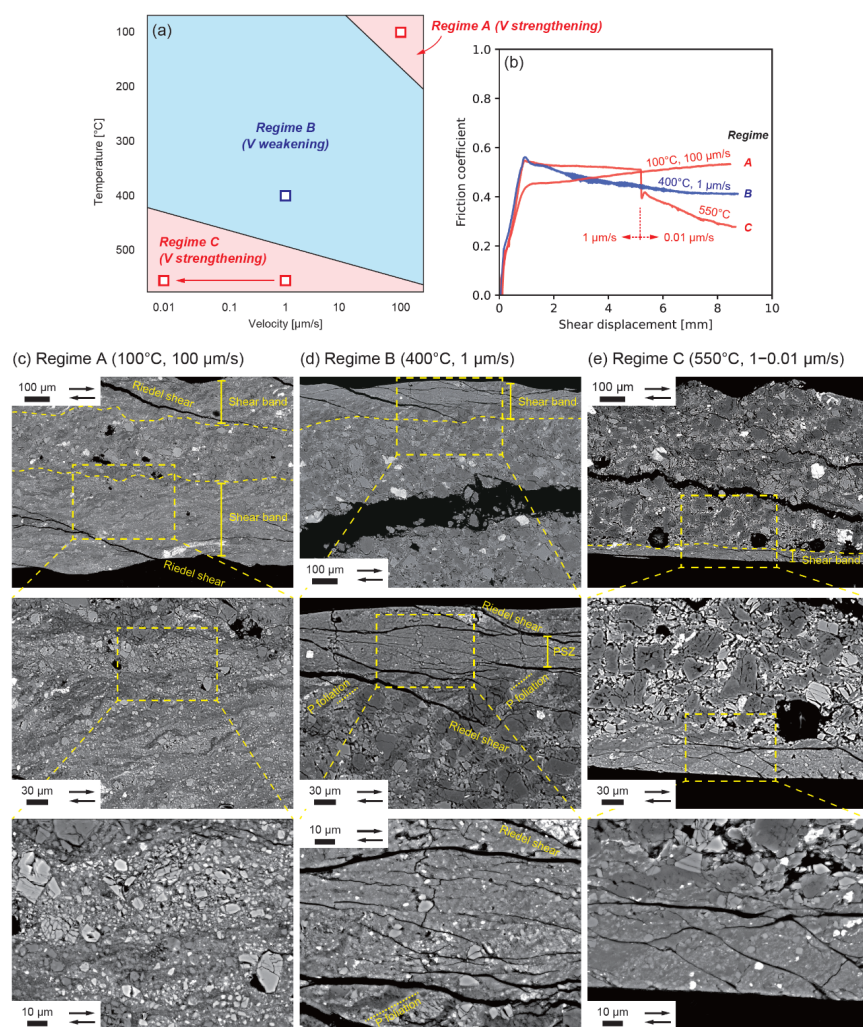


Figure 7. (a) Diagram of three Regimes in V - T space based on Figure 4d. Experimental conditions for three constant V experiments are plotted by square markers. (b) Detrended μ values of three tests for microstructural observation. (c-e) Characteristic microstructures observed in constant V experiment in each regime. The yellow square in each figure is the location of the image in the lower row. PSZ: principal slip zone.

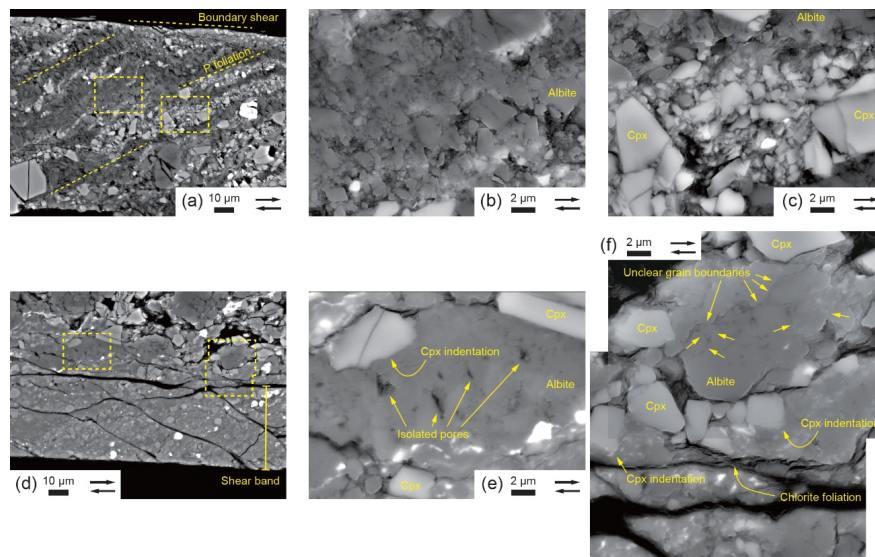


Figure 8. Characteristic microstructures for samples deformed in Regime B (a-c) and Regime C (d-f). The yellow squares in (a) and (d) are the locations of (b, c, e, f).

Discussions

Deformation micromechanisms

In our experiments, we have observed three Regimes of V -dependence of friction: (Regime A) V -strengthening at higher V and/or lower T conditions, characterized by a thick cataclastic and porous shear band at the boundary; (Regime B) V -weakening at intermediate V - T conditions which showed a narrow, relatively dense shear band at the boundary and interlocking clusters of round albite grains along the P foliations; and (Regime C) marked V -strengthening at lower V and/or higher T conditions ($a-b > 0.01$ at $T > 450$) with a dense shear band microstructure featuring limited volume of chlorite foliations and deformation by dissolution and precipitation processes, possibly pressure-solution creep, in albite grains rather than clinopyroxene grains (Figures 7 & 8).

When the system is dry, fluid-assisted processes like pressure-solution creep cannot be active. We observed little dependences of $a-b$ on V - T conditions in the case of dry experiments (conducted at $V = 1-3-10-30-100$ $\mu\text{m/s}$, $T = 100-150-200$, u1003), in contrast to the wet experiments which showed that the transition between Regime A (V -strengthening) and B (V -weakening) occurs around $V = 30-100$ $\mu\text{m/s}$ at $T = 100-200$ (Figure 6). This difference between dry and wet experiments demonstrates that the presence of a fluid (pressure) has a large effect on the V -dependence of friction even at low T conditions. As the shear band microstructures observed in Regime B and C under wet conditions are characterized by interlocking albite grains, and as the fractures in albite grains outside the shear band in Regime C also showed interlocking features (Figure 8), pressure-solution creep of albite may be a possible process involved in controlling mechanical behavior (Rutter & Mainprice, 1979; Spiers et al., 2004).

Results from previous studies on simulated gouges prepared from halite-phyllsilicate mixtures, calcite, illite-rich shale, granite, quartz, and gabbro, under hydrothermal conditions, showed similar transitions in frictional behavior from V strengthening, V weakening, to V strengthening with respect to V or T conditions (Blanpied et al., 1995; Chen et al., 2020; Chester & Higgs, 1992; den Hartog & Spiers, 2013; He et al., 2007; Niemeijer & Spiers, 2007; Verberne et al., 2015). The three-regime behavior can be explained by the microphysical model of Chen-Niemeijer-Spiers (CNS) model which is based on a competition between a time-dependent, thermally activated deformation/compaction mechanism and slip-dependent dilatation resulting from intergranular sliding (granular flow), characterized by mild V -strengthening (Chen & Spiers,

2016; Niemeijer & Spiers, 2007). When V is sufficiently low or T is sufficiently high, compaction by pressure-solution creep of grains occurs efficiently and porosity within the gouge is kept low; the shearing behavior of gouge is then governed by pressure-solution creep and is therefore viscous (Bos & Spiers, 2002; Niemeijer & Spiers, 2005, 2007). This mechanism leads to markedly V -strengthening behavior at high T and/or low V conditions corresponding to Regime C. At even lower V and/or higher T , the shear strength and apparent friction coefficient μ will be controlled by non-dilatant frictional sliding on phyllosilicate (chlorite in this study) coated grain boundaries or foliation planes as the resistance offered by serial operation of pressure solution becomes negligible (Niemeijer & Spiers, 2005). Although we observed a limited volume of chlorite between grains (Figure 8f), the apparent μ of 0.3 observed at $T = 550$ and $V = 0.01 \mu\text{m/s}$ (Figure 7b) is consistent with the value obtained for chlorite gouge by Okamoto et al. (2019), implying that grain boundary sliding along chlorite foliation surfaces may define the asymptote to the low μ seen in Regime C, notably at the highest- T /lowest- V and largest displacement conditions.

When the shear strain rate becomes fast enough for one grain to start to override the next grain, due to the increase in stress needed to drive shear by pressure solution at rapid strain rates, then porosity of the gouge starts to increase and the shear strength originating from dilatant frictional sliding (granular flow) decreases, leading to the V -weakening behavior seen in Regime B. This situation involves a competition between the rate of dilatation due to granular flow and compaction by pressure solution, leading to a balance at steady state that is characterized by a steady state porosity and negative a - b value (Niemeijer & Spiers, 2007). In both Regimes B ($T = 400$) and C ($T = 550$), we observed interlocking features of albite grains inside (and also outside in Regime C) the shear bands (Figures 7 & 8) which suggest the occurrence of compaction by pressure solution creep at the corresponding T conditions. When V is high or T is low enough to render compaction creep unable to compete with dilatation due to granular flow, then critical state granular flow ensues at a fixed (critical state) porosity (Niemeijer & Spiers, 2007). At this point, V -strengthening intergranular friction causes re-emergence of V -strengthening behavior at the sample scale (Chen & Spiers, 2016), causing the observed transition to Regime A. Grains in the shear band formed in the test in the Regime A did not show interlocking features of grains but cataclastically fragmented grains were observed (Figure 7). The model for the regime transitions predicts higher shear band porosity in Regime A and lower porosity in Regimes B and C, which is also clearly observed in our microstructural observations (Figure 7).

The good agreement of the trends seen in our experimental results and microstructures with the trends predicted by the above CNS microphysical model implies that the CNS model can be used to extrapolate the fault slip behavior seen within the altered basalt beyond the lab conditions explored. Although our experiments were mostly done at $V = 1\text{--}100 \mu\text{m/s}$, the V -weakening behavior for $0.01\text{--}1 \mu\text{m/s}$ at $T = 400$ suggests that the tested material will show V -weakening behavior (Regime B) at a wide range of $V < 100 \mu\text{m/s}$ at $T < 400$, except for the conditions of Regime A at $T < 200$ and high V ($>30 \mu\text{m/s}$) conditions, provided that the (localized) thickness of the deforming zone is comparable between experiments and nature. The V -weakening behavior (Regime B) at $0.03 \mu\text{m/s} < V < 100 \mu\text{m/s}$ conditions at $T < 400$ implies a potential to nucleate an earthquake on faults in the subducting oceanic crust at the seismogenic zone depths ($T \sim 150\text{--}350$).

Role of alteration and its influence on the frictional properties of subducting oceanic crust

The CNS model for frictional behavior predicts V -weakening behavior when pressure-solution creep of albite and dilatant frictional shear deformation among grains occur at comparable rates. Both albite and chlorite are originally present in our uncrushed material (Figure 2) which means those minerals are not formed during an experiment – they result from early seafloor alteration processes and subsequent subduction (Braden & Behr, 2021; Ikari et al., 2020; Kameda et al., 2011, 2017; Moore et al., 2007; Phillips et al., 2020; Ujiie et al., 2007). As seen in Figure 2, albitization produces fine albite grains from single anorthite grains and mechanically weak chlorite as well (Ramseyer et al., 1992; Rosenbauer et al., 1988). The low μ of chlorite (0.24–0.36) reduces the bulk strength of gouge if sufficient chlorite is present (Logan & Rauenzahn, 1987; Okamoto et al., 2019, 2020), so that altered subducting oceanic crust will be weaker than fresh oceanic basalt. In addition, finer grains deform more easily via pressure solution than large grains, which promotes

viscous compaction and shear creep leading to Regime B and C at lower T conditions than fresh oceanic basalt. Compared to fresh oceanic basalt (Zhang et al., 2017), the present altered basalt showed a) slightly lower μ (Figure 9a) and potentially unstable frictional behavior (Regime B) at a wider T range, including those expected at seismogenic zone depths, and b) positive $a-b$ (Regime C) at high T conditions (Figure 10a). Our finding of a potential for frictional instability over a wide T range (< 400) is also different from that found for chlorite (Okamoto et al., 2019) and for single mineral phases of pyroxene and plagioclase (He et al., 2013). This suggests that the presence of small grains of albite as an alteration product promotes the V -weakening behavior of altered basalt under conditions that are relevant for nucleating megathrust earthquakes in subduction zones.

According to previous studies that reported mineral compositions of basaltic layers in different mélanges in Shimanto accretionary complexes, albite-clinopyroxene-chlorite assemblages disappear at $T > 300$ (Kameda et al., 2017). Therefore, our experimental results can only be applicable at subduction depth ranges where $T < 300$. At greater depths, clinopyroxene will disappear and epidote-quartz or actinolite(-quartz) will emerge. Note that we did not observe any mineralogical changes in our high T experiments confirmed by microstructural observations and EDS analyses. In the Makimine melange and Nishisonogi metamorphic rocks, SW Japan, deformed oceanic crust materials are exposed and they experienced T of 370 and 500, respectively. Previous studies estimated shear stresses from grain size in quartz veins to be 25-60 MPa at Makimine melange and 10-30 MPa at Nishisonogi metamorphic rocks, which are regarded as the ductile shear strength of the subducting oceanic crust at depths (Tulley et al., 2020). An overpressured condition with respect to the hydrostatic condition in the subducting oceanic crust is expected by a combination of dehydration of saponite around 150 and low permeability of overlying sediment that hampers the fluid escaping from the oceanic crust (Kameda et al., 2011). Assuming the pore pressure ratio λ (pore pressure / lithostatic pressure) = 0.8 (Tulley et al., 2020), the altered oceanic crust have 70-90 MPa of shear stress at the depth of $T = 300-400$ (Figure 9c). Therefore, we expect the depth profile of shear stress of subduction oceanic crust will follow the green line in Figure 9d as a combination of Coulomb stress of altered oceanic crust with $\mu = 0.6$ and ductile shear stress of quartz. However, there is still a small, but important gap of experimental data for albite-epidote-quartz-chlorite or albite-actinolite(-quartz)-chlorite system at $T = 300-400$ which is the inferred T of the intersection of Coulomb strength of altered basalt and ductile shear strength of oceanic crust, corresponding to the brittle-ductile transition of oceanic crust. It has been suggested that the presence of small amounts of quartz (3-5%) can stabilize the frictional behavior of a fault gouge mixture of plagioclase and pyroxene because of the high solubility of quartz which inhibits the growth of contacts of plagioclase and pyroxene by pressure-solution creep due to silica saturation (He et al., 2013). Therefore, further experiments with albite-epidote-quartz-chlorite or albite-actinolite(-quartz)-chlorite system are needed to understand the fault slip behavior around the brittle-ductile transition of subducting oceanic crust and its relation to the downdip limit of seismogenic zone and deep slow earthquakes (Shibazaki & Iio, 2003).

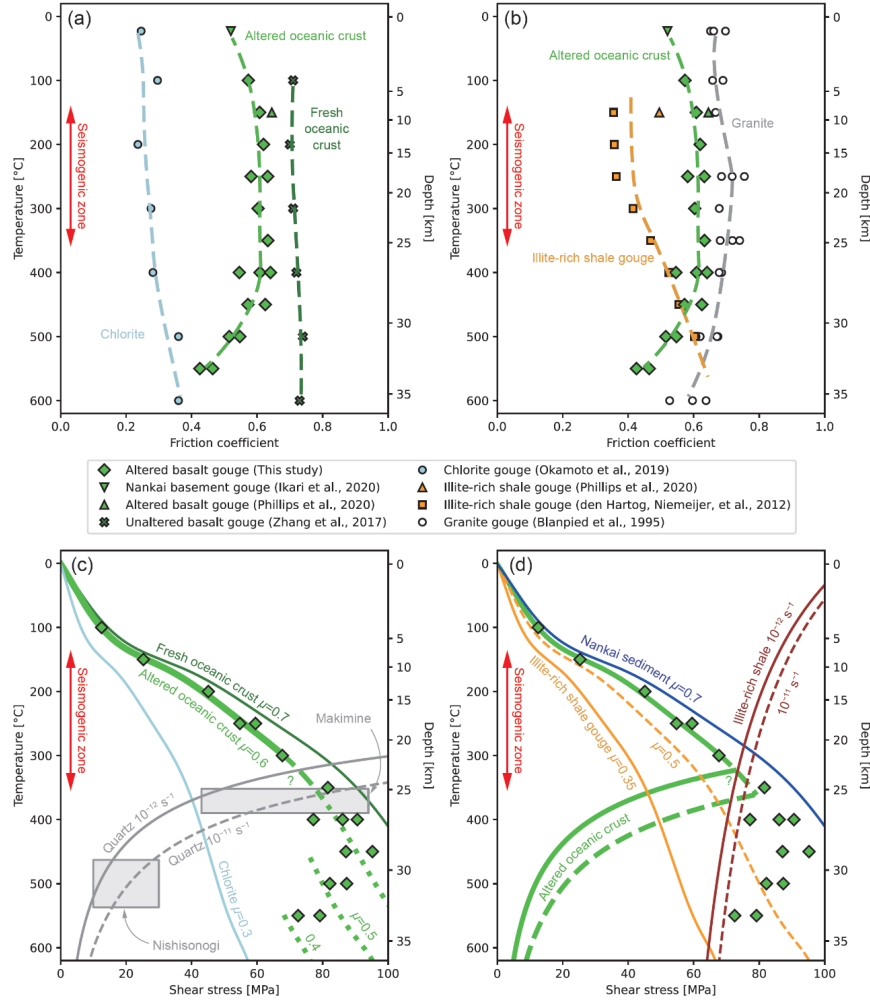


Figure 9. Depth profiles of detrended μ for altered oceanic crust at $V = 1 \mu\text{m/s}$ (a) with altered oceanic crust (Ikari et al., 2020; Phillips et al., 2020), fresh oceanic crust (Zhang et al., 2017), and chlorite gouge (Okamoto et al., 2019); (b) with illite-rich shale (den Hartog, Niemeijer, et al., 2012; Phillips et al., 2020) and granite gouge (Blanpied et al., 1995). Depth profiles of shear stress for altered oceanic crust at $V = 1 \mu\text{m/s}$ (c) with fresh oceanic crust (Zhang et al., 2017), chlorite gouge (Okamoto et al., 2019), estimated shear stresses at the Makimine mélangé and Nishisonogi metamorphic rock (Tulley et al., 2020), and quartz rheology (Hirth et al., 2001; Tulley et al., 2020); (d) with illite-rich shale gouge (den Hartog, Niemeijer, et al., 2012; Phillips et al., 2020), the Nankai sediment (Okuda, Ikari, et al., 2021), and rheology for illite-rich shale (Ibanez & Kronenberg, 1993). Shear stresses were calculated based on μ and an overpressured condition with λ (pore pressure / lithostatic pressure) = 0.8 was assumed. Vertical direction is assumed to be the lithostatic pressure which is calculated by the product of density (2650 kg/m^3), depth, and gravitational acceleration. T -depth relation is from Yoshioka et al. (2013).

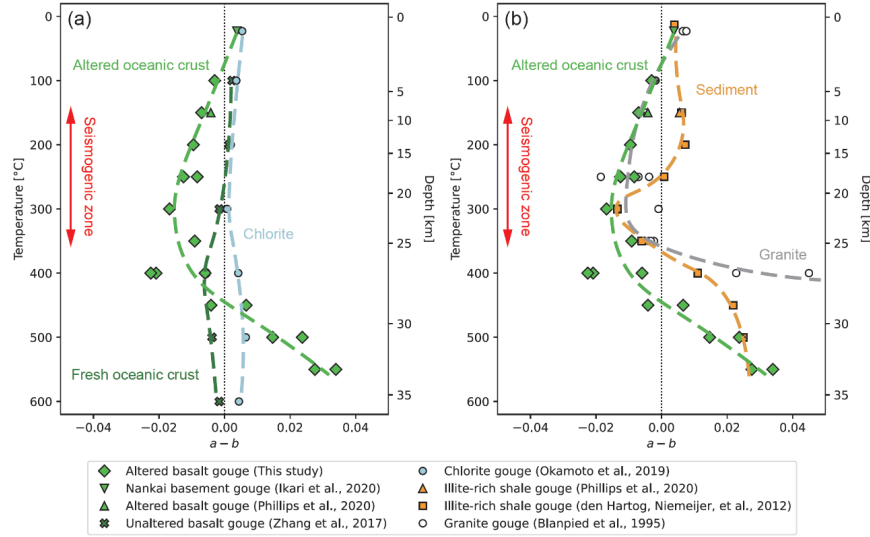


Figure 10. Depth profile of $a-b$ values for altered oceanic crust at the V -step from $V = 1$ to $3 \mu\text{m/s}$ (a) with altered oceanic crust (Ikari et al., 2020; Phillips et al., 2020), fresh oceanic crust (Zhang et al., 2017), and chlorite gouge (Okamoto et al., 2019); (b) with illite-rich shale (den Hartog, Niemeijer, et al., 2012; Phillips et al., 2020) and granite gouge (Blanpied et al., 1995). T -depth relation is from Yoshioka et al. (2013).

Implication for fault slip activities in subduction zones

Regarding $a-b$ values, the altered basalt showed a large potential for unstable frictional behavior at a wider T range than sediment and granitic rocks (Figure 10b). Therefore, the altered basalt may be more likely to nucleate an earthquake than sediment. To achieve unstable frictional slip leading to an earthquake, the shear stiffness K of surrounding rocks should be lower than the critical stiffness K_c defined as (Dieterich, 1979; Ruina, 1983):

$$K_c = -\frac{(a-b)\sigma_n^{\text{eff}}}{d_c}, \# (2)$$

where d_c is a critical slip distance in the V -step although we do not quantify it in this study. Equation 2 shows that the unstable fault slip, i.e., earthquake, is more likely to occur when $a-b$ and/or σ_n^{eff} are large or d_c is small. Therefore, more negative $a-b$ values of altered oceanic crust than other materials lead to a higher possibility to nucleate an earthquake within the altered oceanic crust. In previous sections, we inferred that albite grains as an altered material of oceanic crust promote unstable frictional behavior. Because detrital materials also often contain anorthite that can be altered into albite at the same T condition in shallow depths of subduction zones, further experimental studies on sediments may be needed to fully understand the difference in frictional behavior between sediments and altered oceanic crust. Since illite-rich shale gouge showed lower μ (around 0.35-0.5) than that of altered basalt at seismogenic zone depths (den Hartog, Niemeijer, et al., 2012; Phillips et al., 2020), sediment is the first candidate to be sheared easily (Figure 9b). However, the plate boundary fault in the Nankai Trough, SW Japan, is proposed to have a high μ of ~ 0.7 at a depth of > 5 km according to the inference from Coulomb wedge model combining friction coefficients of sediment inside accretionary wedges, observed pore pressure conditions inside wedges and along the plate boundary, and observed topographical information of wedges (Okuda, Ikari, et al., 2021). Because the altered basalt showed $\mu \sim 0.6$ at the T range of 100-400, the altered oceanic crust may also sustain similar or sometimes lower shear stress to sediment at least in the Nankai Trough, whose tectonic setting is similar to the one which the altered basaltic sample used in this study had experienced (Figure 9d).

Frictional strength of the altered oceanic crust can be lowered substantially when more chlorite is contained and/or when P_f is high enough. Assuming that the μ for sediment is 0.35 or 0.5 (den Hartog, Niemeijer, et al., 2012) and that it is 0.6 for altered oceanic crust, a higher P_f is required in the altered oceanic crust than that in the sedimentary facies to make the frictional strength of the altered oceanic crust lower than that of the sedimentary facies: λ for the altered oceanic crust should be 0.88 or 0.83 to make the apparent frictional strengths of both materials the same when λ for the sediment is 0.8. Necessary pore pressure changes are 17.3 MPa at $T = 150$ and 53.7 MPa at $T = 350$ from $\lambda = 0.8$ to $\lambda = 0.88$, and 6.9 MPa at $T = 150$ and 21.5 MPa at $T = 350$ from $\lambda = 0.8$ to $\lambda = 0.83$. When the frictional strength of the altered oceanic crust is lower than that of sediment by such a pore fluid overpressure, deformation at the plate boundary would be accommodated by the altered oceanic crust rather than by the sediment, and the accumulated stress along the plate boundary starts to be released by earthquake nucleation within the oceanic crust at the seismogenic zone depths (~ 10 -25 km) where we obtained V -weakening of altered basalt (Phillips et al., 2020). Notably, the overpressured conditions with respect to the hydrostatic condition achieved by both a decrease in $\sigma_v^{\epsilon\varphi\varphi}$ and an increase in P_f do not influence the a - b value of altered basalt at $T = 200$ unlike blueschist, actinolite-chlorite mixture, and other materials (Bedford et al., 2021; Okamoto et al., 2020; Okuda, Katayama, et al., 2021; Sawai et al., 2016), which reduces K_c by simply decreasing in $\sigma_v^{\epsilon\varphi\varphi}$ and thus increases the nucleation size and possibly induces a slower slip, although the effects of $\sigma_v^{\epsilon\varphi\varphi}$ and P_f on d_c are unknown. Since sedimentary facies at shallow depths (< 10 km) along décollement are overpressured driven by sediment compaction (Saffer et al., 2008; Tsuji et al., 2014), the coseismic rupture may propagate within the weak sedimentary facies rather than the altered oceanic crust at a depth of < 10 km. Those situations will lead the décollement to “stepup” from the nucleation phase in the oceanic crust at the seismogenic zone (~ 5 -25 km) to the rupture propagation phase in the sedimentary facies at shallower depths which will result in the observation of décollement stepdown.

Conclusion

Seismological and geological studies suggest that the plate boundary fault (décollement) in subduction zones possibly develops within the subducting oceanic crust rather than sedimentary facies in the seismogenic zone depths. To understand the frictional properties of the subducting oceanic crust, we performed hydrothermal friction experiments on altered basalt at temperatures (T) of 100-550 °C, effective normal stresses ($\sigma_v^{\epsilon\varphi\varphi}$) of 30-100 MPa, pore pressure (P_f) of 50-200 MPa, and velocity conditions (V) of 1-100 $\mu\text{m/s}$. Friction coefficient (μ) of the altered basalt was about 0.6 for all V conditions at $T < 400$ °C, and became 0.45 at $T = 550$ °C and $V = 1$ $\mu\text{m/s}$ with V -strengthening behavior to $\mu = 0.7$ at $V = 100$ $\mu\text{m/s}$ considering a slip hardening trend of 0.004 mm^{-1} . Three regimes of V dependence were found: Regime A was at lower T (< 200 °C) and higher V (> 30 $\mu\text{m/s}$) showing V -strengthening behavior; Regime B was at intermediate T (100-450 °C) and almost all the V conditions showing V -weakening behavior; Regime C was at higher T (> 500 °C) and lower V showing V -strengthening behavior. These regimes are well-explained by a microphysical model that considers a balance between compaction creep and dilatant frictional behavior at grain boundaries. Microstructural observations revealed that the pressure-solution processes of albite is the control of creep deformation, which shifts Regime B to higher V conditions at a given T . Alteration of oceanic crust during subduction produces fine grains of albite contributing to the viscous deformation by pressure-solution creep in natural conditions. Because albitization also produces the mechanically weak chlorite, the altered oceanic crust can have a similar frictional strength to the sediment, which is also affected by P_f and thus $\sigma_v^{\epsilon\varphi\varphi}$ conditions. The possible unstable frictional behavior of altered basalt at wide T range suggests that a megathrust earthquake would nucleate within the oceanic crust in the seismogenic zone depths.

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Open Research

Experimental data are freely available from the Yoda data repository: <https://public.yoda.uu.nl/geo/UU01/6DSAJH.html>.

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Hydrothermal friction experiments on simulated basaltic fault gouge and implications for megathrust earthquakes

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Key points:

- Altered basalt shows unstable frictional behavior under a wide range of hydrothermal conditions.
- Production of fine-grained albite during subduction promotes the frictional instability via pressure solution creep.
- Subducting oceanic crust may serve as a source of nucleating megathrust earthquakes in subduction zones.

24 **Abstract**

25 Nucleation of earthquake slip at the plate boundary fault (décollement) in
26 subduction zones has been widely linked to the frictional properties of subducting
27 sedimentary facies. However, recent seismological and geological observations suggest
28 that the décollement develops in the subducting oceanic crust in the depth range of the
29 seismogenic zone, at least in some cases. To understand the frictional properties of
30 oceanic crustal material and their influence on seismogenesis, we performed
31 hydrothermal friction experiments on simulated fault gouges of altered basalt, at
32 temperatures of 100-550 °C. The friction coefficient (μ) lies around 0.6 at most
33 temperature conditions but a low μ down to 0.3 was observed at the highest temperature
34 and lowest velocity condition. The velocity dependence of μ , $a-b$, changes with
35 increasing temperature from positive to negative at 100-200 °C and from negative to
36 positive at 450-500 °C. Compared to gouges derived from sedimentary facies, the
37 altered basalt gouge showed potentially unstable velocity weakening over a wider
38 temperature range. Microstructural observations and microphysical interpretation infer
39 that competition between dilatant granular flow and viscous compaction through
40 pressure-solution creep of albite contributed to the observed transition in $a-b$.
41 Alteration of oceanic crust during subduction produces fine grains of albite and chlorite
42 through interactions with interstitial water, leading to reduction in its frictional strength
43 and an increase in its seismogenic potential. Therefore, shear deformation possibly
44 localizes within the altered oceanic crust leading to a larger potential for the nucleation
45 of a megathrust earthquake in the depth range of the seismogenic zone.

46

47 **Plain Language Summary**

48 Megathrust earthquakes in subduction zones have long been studied to mitigate
49 damage by ground shakings and tsunamis. Frictional properties of plate boundary fault
50 are fundamental information to understand the slip activities causing megathrust
51 earthquakes. In this study, we focused on altered basalt, which is a rock of subducting
52 oceanic crust and has not been focused on as much as sedimentary rocks. Laboratory
53 friction experiments were performed at a wide temperature range with water pressurized
54 conditions. We found that the altered basalt shows frictionally unstable behavior of the
55 type that is prerequisite for generating an earthquake in the temperature conditions of
56 seismogenic zone. This unstable behavior is likely to be result of alteration of oceanic
57 crust during subduction. Because the altered basalt can be mechanically as weak as
58 sedimentary facies, subducting oceanic crust forms an additional or perhaps even
59 preferred candidate for sourcing megathrust earthquakes in subduction zones.

60 **1. Introduction**

61 Megathrust earthquakes in subduction zones generally source in the depth range
62 of ~5-25 km corresponding to a temperature (T) range of ~150-350 °C (Hyndman et al.,
63 1997). The extent of this “seismogenic zone” was originally postulated to be related to
64 the smectite-illite dewatering transition as the transition temperature is consistent with
65 the temperature condition at the updip limit of the seismogenic zone (Oleskevich et al.,
66 1999). However, this hypothesis is not fully supported by experiments (e.g. Saffer and
67 Marone, 2003). Instead, recent experimental studies showed that the effect of
68 temperature on the velocity dependence of illite-quartz mixture can explain both up-dip
69 and down-dip limits (den Hartog, Peach, et al., 2012), and that a change in the extent of
70 lithification of sediments during subduction may contribute to making the plate
71 boundary fault (décollement) frictionally unstable (Ikari & Hüpers, 2021).

72 The frictional properties of sediments have long been the focus for
73 understanding the frictional behavior of the décollement. This notion is certainly valid
74 for shallow depths near the trench where sedimentary décollement materials have been
75 successfully drilled from the plate boundary, e.g. in the Japan Trench, NE Japan, in
76 relation to the 2011 Tohoku-oki Earthquake (Chester et al., 2013) or in the Nankai
77 Trough, SW Japan (Sakaguchi et al., 2011). However, at the depth of the updip limit of
78 the seismogenic zone, interpretation of seismic reflection profiles of the Nankai and
79 Sagami (SE Japan) regions suggests that the décollement develops within the
80 subducting oceanic crust beneath the sedimentary layer. This is called “décollement
81 stepdown”, which produces a duplex structure due to the underplating process (H.
82 Kimura et al., 2010; Park et al., 2002). Although the interpretation of seismic reflection
83 profiles varies among studies, geological structures with underplated basaltic layers that

84 are considered to represent ancient oceanic crust or seamounts have been found in
85 exhumed accretionary complexes all over the world (Figure 1) (G. Kimura & Ludden,
86 1995; Kusky et al., 2013; Wakita, 2015). In the case of the Shimanto accretionary
87 complex in SW Japan, which is thought to have been located along a plate boundary
88 similar to the current Nankai Trough, cataclasite is observed at the top part of the
89 basaltic layer. This is interpreted to represent the décollement at shallow depth, whereas
90 shear deformation features, developed after the décollement stepdown, are preserved at
91 the bottom part of the basaltic layer (Ikesawa et al., 2005; G. Kimura et al., 2012). In
92 addition, vitrinite reflectance data and fluid inclusion geothermometry indicate that the
93 duplex structures in the Shimanto complex that involve a basaltic layer experienced
94 temperatures of 150-300 °C (Kameda et al., 2017). This suggests that the décollement is
95 not always located within underthrusting sediments at the updip depth limit of the
96 seismogenic zone (~150 °C) but possibly within the subducting oceanic crust. However,
97 experimental studies on basaltic fault rock in subduction zones, and under subduction
98 zone conditions, are limited despite their possible importance for hosting megathrust
99 earthquakes.

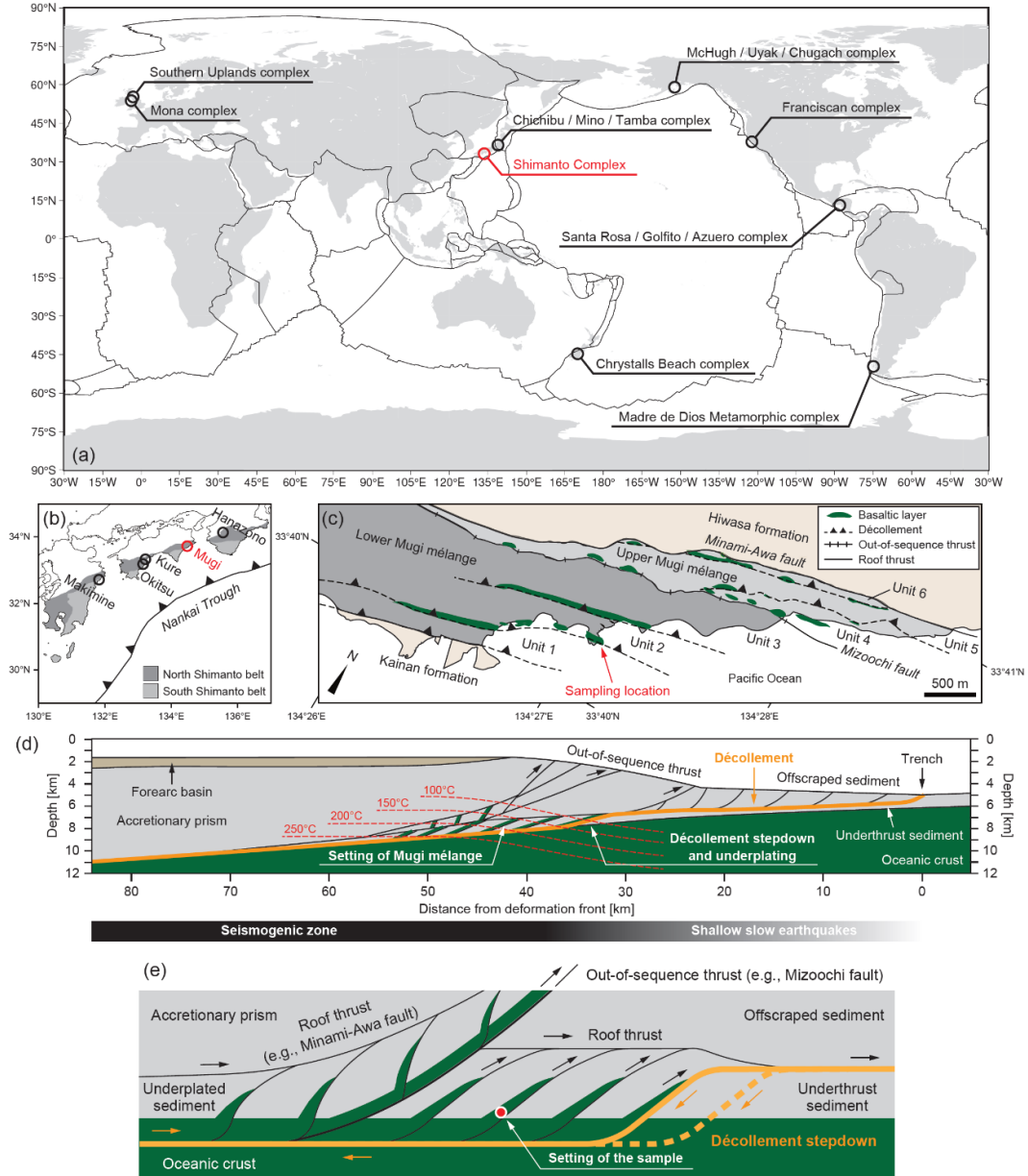
100 It is well established that oceanic crust commonly experiences partial alteration
101 soon after its formation, because of the interaction between mid-ocean ridge (fresh)
102 basalt and interstitial water (Braden & Behr, 2021; Kameda et al., 2017; Phillips et al.,
103 2019; Ujiie et al., 2007). At shallow depths, such as the current seafloor, the volcanic
104 glass component alters into saponite, which is an Mg-rich smectite (Kameda et al.,
105 2011). As the altered oceanic crust later subducts, saponite dehydrates to form chlorite
106 at ~ 150 °C (Kameda et al., 2011). At a similar temperature, albitization of anorthic
107 plagioclase also occurs (Moore et al., 2007), which also produces chlorite (Rosenbauer

108 et al., 1988). The mineral assemblage present in altered basalt up to ~300°C is
 109 accordingly ~25% saponite or chlorite, ~25% clinopyroxene, and ~50% plagioclase
 110 (Kameda et al., 2017). At temperatures > 300 °C, clinopyroxene decomposes into
 111 epidote and quartz (Kameda et al., 2017) or actinolite (and quartz) (Humphris &
 112 Thompson, 1978; Takeshita et al., 2015).

113 In previous room temperature studies (Ikari et al., 2020), unaltered basalt
 114 gouge under 25 MPa effective normal stress (σ_n^{eff}) with 5 or 24 MPa pore pressure (P_f)
 115 conditions exhibited velocity-neutral to velocity-weakening behavior at slip velocities
 116 of 3-300 $\mu\text{m/s}$, whereas altered basalt gouge showed a clear trend toward more
 117 frictionally stable behavior with increasing velocity (> 3 $\mu\text{m/s}$). Velocity-weakening
 118 behavior was observed only at low velocities (< 1 $\mu\text{m/s}$) in the case of surface sliding of
 119 altered basalt with saponite, suggesting that the altered basalt is capable of hosting slow
 120 slip events at shallow depths (Ikari et al., 2020). At elevated T conditions, unaltered
 121 basalt gouge under ~50 MPa σ_n^{eff} with 100 MPa P_f showed velocity-weakening behavior
 122 in the range of $T = 250\text{-}600$ °C and at shearing velocities of 0.02-1.15 $\mu\text{m/s}$ (Zhang et al.,
 123 2017). Altered basalt with chlorite has only been tested under hydrothermal conditions
 124 at $T = 150$ °C with confining pressure of 120 MPa and 43 or 84 MPa P_f , showing
 125 velocity-weakening behavior (Phillips et al., 2020). Friction coefficients of unaltered
 126 and altered basalt are 0.6-0.7 at $T = 150$ °C, higher than those of illite-rich shale
 127 (0.45-0.55) (den Hartog, Niemeijer, et al., 2012; Phillips et al., 2020). Mixed
 128 actinolite-chlorite and chlorite gouges also show velocity-weakening behavior at $T =$
 129 200-400°C and 300°C, respectively (Okamoto et al., 2019, 2020). In addition, a low σ_n^{eff}
 130 (< 50 MPa) is reported to promote velocity-weakening behavior in the case of blueschist
 131 gouge sheared at $T = 22\text{-}400$ °C under $P_f = \sigma_n^{eff}$ conditions (Sawai et al., 2016). These

132 studies imply that subducting altered oceanic crustal material has the potential to exhibit
133 unstable frictional behavior, but the dependencies of its frictional stability on T , P_f , and
134 σ_n^{eff} are not yet fully understood.

135 In this study, we collected altered basaltic rock from an exhumed *mélange* in
136 SW Japan and conducted friction experiments on a simulated gouge prepared from it at
137 temperatures ranging from 100°C to 550 °C. The aim was to investigate the frictional
138 behavior of subducting oceanic crustal material under the conditions of the seismogenic
139 zone. We mostly used an σ_n^{eff} of 100 MPa and P_f of 100 MPa, and independently tested
140 the effects of increasing P_f and reducing σ_n^{eff} on frictional behavior.



141
 142 **Figure 1.** (a) Global map showing examples of accretionary complexes where
 143 underplated ocean floor basalt or seamount basalts are found at relatively shallow
 144 depths ($T < 300^{\circ}\text{C}$) (cf., G. Kimura & Ludden (1995); Kusky et al. (2013); Raymond
 145 (2019); Wakita (2015)). Shimanto complex in SW Japan (Kameda et al., 2017),
 146 Chichibu, Mino, Tamba complex in central Japan (G. Kimura & Ludden, 1995),

147 Franciscan complex in California (Meneghini & Moore, 2007), McHugh, Uyak,
 148 Chugach complex in southern Alaska (Braden & Behr, 2021; Kusky & Bradley, 1999),
 149 Southern Uplands complex in Scotland (Leggett et al., 1979), Mona complex in Wales
 150 (Kawai et al., 2007; Maruyama et al., 2010), Chrystalls Beach complex in New Zealand
 151 (Fagereng & Cooper, 2010), Madre de Dios Metamorphic complex in southern Chile
 152 (Willner et al., 2009), Santa Rosa, Golfito, Azuero complex in Costa Rica and Panama
 153 (Baumgartner & Denyer, 2006; Buchs et al., 2010). (b) Mélanges where underplated
 154 basaltic layers are found in the Shimanto complex: Hanazono mélange (Onishi et al.,
 155 2001), Mugi mélange (Ikesawa et al., 2005; G. Kimura et al., 2012; Kitamura et al.,
 156 2005), Kure mélange (Mukoyoshi et al., 2006), Okitsu mélange (Ikesawa et al., 2003),
 157 Makimine mélange (Hara & Kimura, 2008). (c) Closeup map view of Mugi mélange
 158 modified after Yamaguchi et al. (2012) showing the sampling location. (d) Schematic
 159 cross section of the Nankai Trough and (e) schematic cross section showing the
 160 geological structures of Mugi mélange where the décollement steps down into the
 161 oceanic crust (G. Kimura et al., 2012).

162

163 **2. Method**

164 **2.1. Samples**

165 The altered basalt sample was collected from an outcrop of the Mugi mélange,
 166 in the Shimanto accretionary complex, SW Japan (Figure 1). This mélange formed in
 167 the Late Cretaceous and experienced T of 150-200 °C based on vitrinite reflectance data
 168 and P_f of ~100 MPa based on fluid inclusion geothermometry (Ikesawa et al., 2005; G.
 169 Kimura et al., 2012; Kitamura et al., 2005; Matsumura et al., 2003). The basalt initially
 170 formed as mid-ocean ridge basalt, subducted down to the seismogenic zone depth of a

171 former subduction plate boundary that is similar to the current Nankai Trough. It was
172 then incorporated into the accretionary prism by underplating associated with
173 décollement stepdown, and then exhumed (G. Kimura et al., 2012). The altered basalt
174 sample is composed of albitized plagioclase, clinopyroxene, and chlorite (Figure 2). The
175 albitized plagioclase consists of fine grains of albite with a grain size of about 10 μm
176 (Figure 2b). Chlorite is formed within and around albitized plagioclase (Figure 2d).
177 Before experimentation, we crushed and sieved the sample to obtain a simulated gouge
178 material with a grain size of $<100 \mu\text{m}$. Mineral composition of the sample was
179 estimated by point counting with ~ 1300 grains in a thin section. We obtained $\sim 50\%$
180 albite, $\sim 27\%$ clinopyroxene, $\sim 15\%$ chlorite, and $\sim 8\%$ opaque minerals, which is
181 generally consistent with previously reported compositions of basaltic rock from the
182 Mugi mélange (Kameda et al., 2017; Phillips et al., 2020).
183

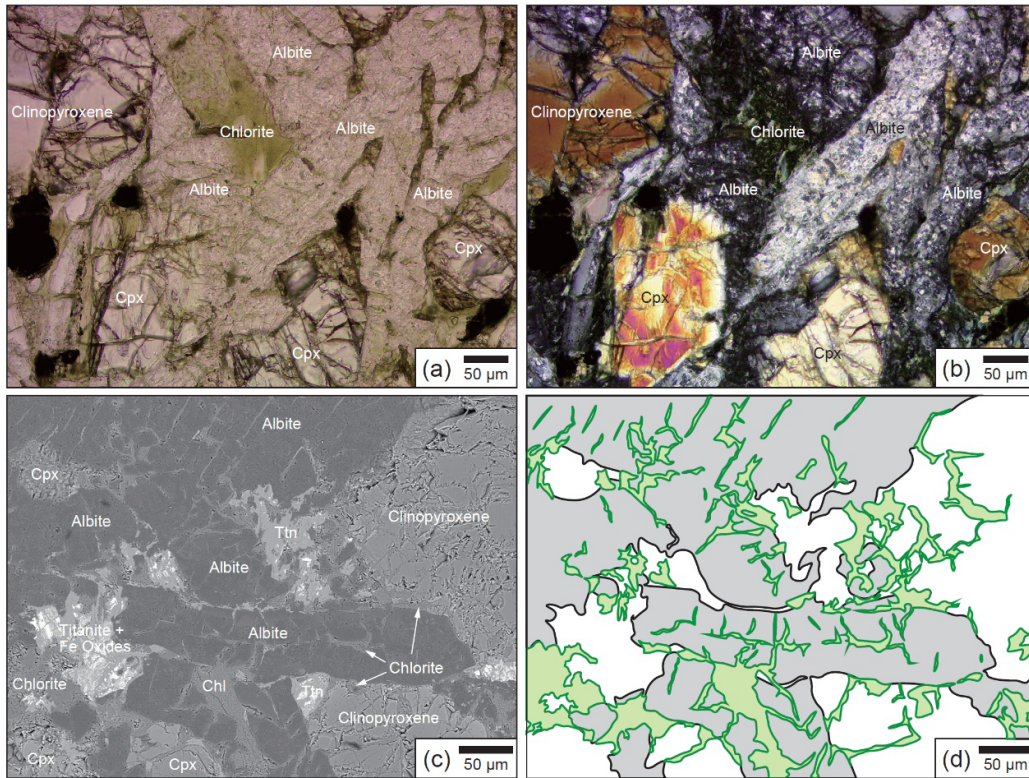


Figure 2. Microstructures of intact altered basalt sample under plane-polarized (a), crossed-polarized (b), and BSE images (c). (d) Albite (gray areas) and chlorite (green areas) distributions based on (c).

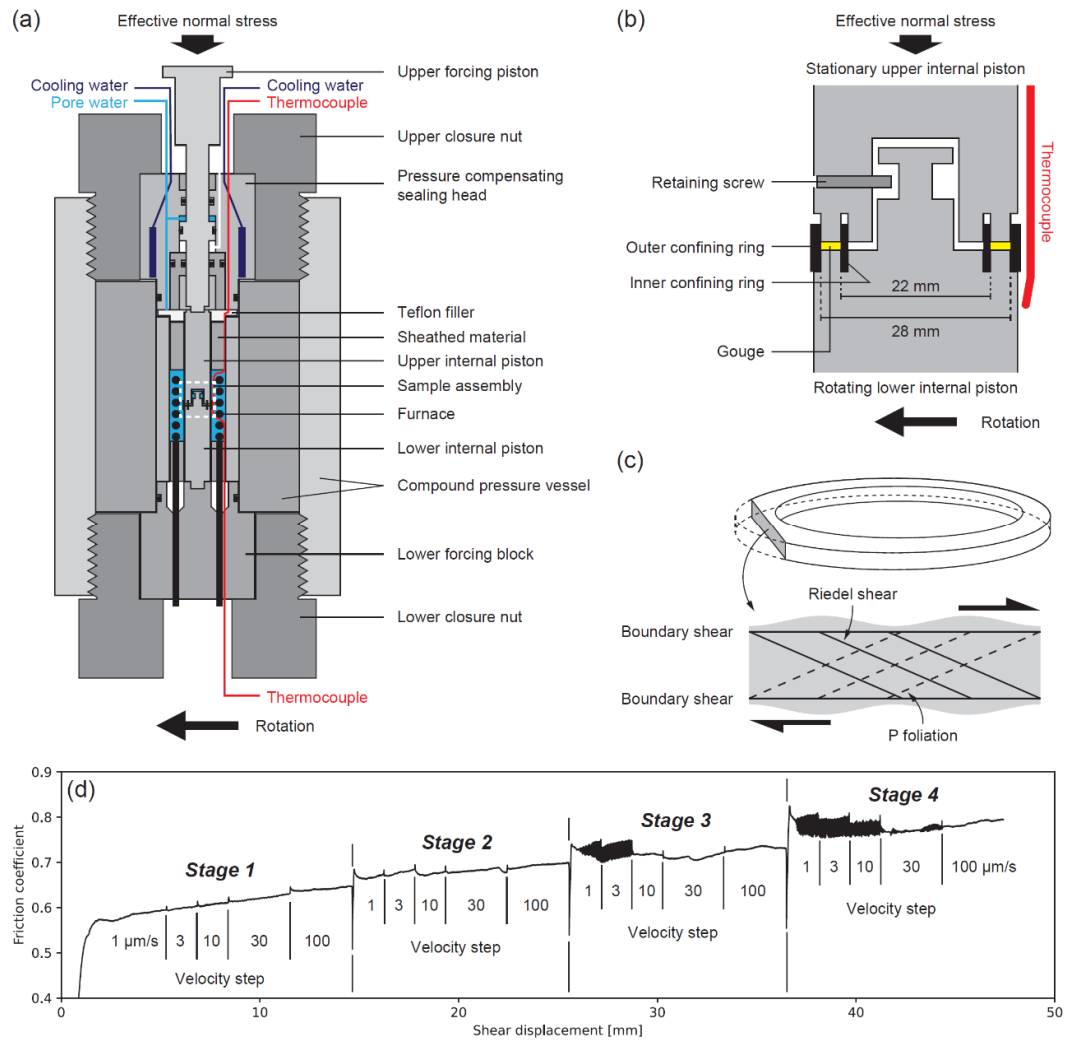
2.2. Experiments

Laboratory friction experiments were conducted on the simulated gouge material using the hydrothermal ring shear apparatus at Utrecht University (Figure 3). In preparing each experiment, 0.5 g of sample was sandwiched between two René-41 Superalloy pistons, confined laterally between an outer confining ring (diameter=28 mm) and an inner confining ring (diameter=22 mm). The gouge had a thickness of ~1.2 mm before imposing the normal load. The piston-sample assembly was subsequently placed inside the hydrothermal pressure vessel in line with the machine's

197 pressure-compensated loading piston, allowing us to control both the σ_n^{eff} and P_f
198 independently. Distilled water was introduced into the pressure vessel as the pore fluid
199 and heated up by an internal furnace to achieve given T conditions. Because the sample
200 is not sealed by the outer/inner rings, pore fluid can freely go through the sample. See
201 previous studies for details of the apparatus (den Hartog, Niemeijer, et al., 2012;
202 Niemeijer et al., 2016).

203 Experiments were performed at an σ_n^{eff} of 100 MPa, a P_f of 100 MPa, and
204 velocities (V) of 1-3-10-30-100 $\mu\text{m/s}$. Shear displacement was set to be 1.5 mm for 1 to
205 10 $\mu\text{m/s}$ and 3 mm for 30 and 100 $\mu\text{m/s}$, except for the first shearing at 1 $\mu\text{m/s}$ for which
206 we imposed 5 mm of shear displacement. Various T conditions from 100 °C to 550 °C
207 were tested by stepping T by 50 °C: 100-150-200-250 °C for u968, 250-300-350-400 °C
208 for u972, 400-450-500-550 °C for u992 and u996. We refer to each T condition in one
209 experiment as a “stage” (e.g., stage 1 for u968 was done under $T = 100$ °C; Figure 3d).
210 Changes in V were abruptly imposed, whereas we waited at least 1 hour after a change
211 in T to allow the system to stabilize. To elucidate the effect of shear displacement on
212 frictional behavior, tests with 250 °C and 400 °C were performed at different
213 displacement conditions. At $T = 200$ °C and 500 °C, the effects of overpressured
214 conditions with respect to the hydrostatic condition ($\sigma_n^{eff} \approx P_f$) were tested by varying P_f
215 from 50 MPa to 200 MPa and σ_n^{eff} from 30 MPa to 100 MPa, independently. An
216 additional experiment with V in the range from 0.003 $\mu\text{m/s}$ to 1 $\mu\text{m/s}$ was performed
217 specifically at $T = 400$ °C to investigate the frictional behavior at a V close to the plate
218 convergence rate. Several constant V experiments were also performed, which were
219 used for microstructural observations. We also performed one test stepping the
220 temperature from $T = 100$ to 200 °C under vacuum dry condition to see the effect of the

221 absence vs. presence of fluid (pressure) on frictional behavior. See Tables 1 and S1 for
 222 the detailed experimental conditions.
 223



224 **Figure 3.** Schematic views of (a) the hydrothermal ring shear apparatus and (b) the
 225 close-up view of the sample assembly (Chen et al., 2020; den Hartog, Niemeijer, et al.,
 226 2012). After the experiment, the sample was retrieved and microstructure was observed
 227 using the cross section shown in (c). (d) Overview of the velocity sequences and stages
 228 employed in this study (example of u968).
 229

230

231 **2.3. Data acquisition and processing**

232 During individual experiments, shear displacement, normal displacement,
233 applied normal force, torque, temperature, and pore pressure signals were continuously
234 logged at a sampling rate of 1-100 Hz. The raw data was converted to (effective) normal
235 and shear stresses using the sensor calibrations and sample dimensions (see information
236 in data repository). Friction coefficient μ was obtained from the shear stress normalized
237 by the σ_n^{eff} without considering cohesion. The V dependence of μ was determined using
238 quasi-instantaneous V steps and quantified using the following equation:

$$a - b = \frac{\Delta\mu_{ss}}{\Delta \ln V}, \#(1)$$

239 where $\Delta\mu_{ss}$ is the difference between the steady state μ values at V -conditions before and
240 after the V -step, $\Delta \ln V$ is the difference in V in the logarithmic scale, and $a-b$ is the
241 nondimensional value representing the V dependence of μ which is originally
242 formulated with rate- and state-dependent friction constitutive law (Dieterich, 1979;
243 Ruina, 1983). We only focus on $a-b$ because this parameter controls whether a fault has
244 the potential to slip unstably or not: a fault slips stably when $a-b$ is positive
245 (V -strengthening) whereas a fault can slip unstably, thus an earthquake can occur, when
246 $a-b$ is negative (V -weakening). The $\Delta\mu_{ss}$ was obtained by comparing the averaged μ
247 values just before and after the V step after removal of linear slip-dependent trends.
248 Although we sometimes observed a hardening trend which can be modeled with
249 negative b_2 with long d_{c2} (Blanpied et al., 1998), we did not take this hardening into
250 account because such a long displacement for the transition of μ would not much affect
251 the V dependence of μ during the accelerating earthquake nucleation phase. We used the
252 averaged μ values in the case of stick-slips were observed, which led to a large standard

253 deviation of $a-b$ of <0.04 whereas this was <0.006 when stick slips were not observed.

254

255 **Table 1.** List of experiments and corresponding conditions. T = temperature, σ_n^{eff} =

256 effective normal stress, P_f = pore fluid pressure, V = velocity, and d = shear

257 displacement.

Run	Stage	T [°C]	σ_n^{eff} [MPa]	P_f [MPa]	V [μm/s]	d [mm]
u968	1	100	100	100	1-3-10-30-100	0-14.6
	2	150				14.6-25.6
	3	200				25.6-36.5
	4	250				36.5-47.4
u972	1	250	100	100	1-3-10-30-100	0-14.6
	2	300				14.6-25.6
	3	350				25.6-36.5
	4	400				36.5-47.4
u992	1	400	100	100	1-3-10-30-100	0-14.6
	2	450				14.6-25.6
	3	500				25.6-36.5
	4	550				36.5-47.4
u996	1	400	100	100	1-3-10-30-100	0-14.6
	2	450				14.6-25.6
	3	500				25.6-36.5
	4	550				36.5-47.4
u991	1	200	100	50	1-3-10-30-100	0-14.6
	2			100		14.6-25.6
	3			150		25.6-36.5
	4			200		36.5-47.4
u993	1	500	100	50	1-3-10-30-100	0-14.6
	2			100		14.6-25.6
	3			150		25.6-36.5
	4			200		36.5-47.4
u1002	1	200	30	100	1-3-10-30-100	0-14.6
	2		50			14.6-25.6

	3		100			25.6-36.5
	4		50			36.5-47.4
	1		30			0-14.6
u1006	2	500	50	100	1-3-10-30-100	14.6-25.6
	3		100			25.6-36.5
	4		50			36.5-47.4
	1	100				0-14.6
u1003	2	150	100	Vacuum dry	1-3-10-30-100	14.6-25.6
	3	200				25.6-36.5
u1017	1	400	100	100	1-0.003-0.01-0.03-0.1-0.3-1	0-10.6
u975	1	550	100	100	1-0.01	0-8.7
u980	1	400	100	100	1	0-8.7
u981	1	100	100	100	100	0-8.7

258

259 **2.4. Microstructural analysis**

260 After three constant V experiments (u975, u980, and u981), the samples were
261 retrieved from the apparatus and impregnated with epoxy after drying for 24 hours at 50
262 °C. Thin sections were prepared from the impregnated sample by cutting parallel to the
263 shear direction (Figure 3c). Polarized optical microscopy and Scanning Electron
264 microscopy (SEM, Zeiss Evo 15 located at the Electron Microscope center at Utrecht
265 University) were used to observe the microstructure. SEM was conducted using
266 backscattered electron (BSE) mode and employing Energy Dispersive Spectrometer
267 (EDS) for the acquisition of chemical information.

268

269 **3. Results**

270 **3.1. Mechanical data**

271 **3.1.1. Effects of temperature, velocity and shear displacement**

272 3.1.1.1. On friction coefficient

273 The evolution of friction coefficient (μ) with displacement (d) at different T
274 and V conditions and at $\sigma_n^{eff} = P_f = 100$ MPa is shown in Figure 4a. Because we stepped
275 T at larger d , friction data at higher T were influenced by the displacement history. To
276 focus only on V - T effects on frictional behavior, here we describe results per stage.

277 In stage 1 ($0 < d < 14.6$ mm; $T = 100, 250, 400$ °C), μ showed rapid increase to
278 0.57-0.58 at the first 1-2 mm of displacement, followed by gradual increases to
279 0.62-0.65 at the end of stage 1 ($d = 14.6$ mm). We observed V -strengthening behavior
280 only at V -steps from $V = 10$ to 30 $\mu\text{m/s}$ and 30 to 100 $\mu\text{m/s}$ for $T = 100$ °C (u978). Other
281 V -steps in stage 1 were showing V -weakening and stick-slips were observed at $V = 1$
282 and 3 $\mu\text{m/s}$ for u996 ($T = 400$ °C).

283 In stage 2 ($14.6 < d < 25.6$ mm; $T = 150, 300, 450$ °C), μ increased rapidly at
284 the beginning and showed peaks at $d \sim 0.5$ mm. This behavior was also observed for
285 stage 3 and 4. After the peaks, μ once dropped and then showed a little slip-hardening
286 trend. For $T = 150$ °C (u968), V -strengthening behavior was observed at the step from V
287 $= 30$ to 100 $\mu\text{m/s}$ and other V -steps showed V weakening. All V steps for $T = 300$ °C
288 (u972) showed V -weakening behavior (stick-slips were observed up to $V = 30$ $\mu\text{m/s}$).
289 For $T = 450$ °C (u992 and u996), μ continuously dropped from peak values during $V = 1$
290 $\mu\text{m/s}$, whereas μ showed slip-hardening trends at $V > 3$ $\mu\text{m/s}$. Mostly stick slips were
291 observed for u996 whereas they did not occur but at the last of $V = 30$ $\mu\text{m/s}$ for u992.
292 Final μ values of stage 2 were 0.70 for $T = 150$ °C (u968), 0.66 for 300 °C (u972), and
293 0.73 for 450 °C (u992 and u996).

294 In stage 3 ($25.6 < d < 36.5$ mm; $T = 200, 350, 500$ °C), nearly constant μ values
295 over shear displacements with V -weakening behavior and stick-slips were observed for

296 $T = 200\text{ }^{\circ}\text{C}$ (u968) and $350\text{ }^{\circ}\text{C}$ (u972). The μ values at the end of the stage were 0.74 for
 297 $T = 200\text{ }^{\circ}\text{C}$ (u968) and 0.69 for $T = 350\text{ }^{\circ}\text{C}$ (u972). Frictional behavior for $T = 500\text{ }^{\circ}\text{C}$
 298 (u992 and u996) was quite different from lower T conditions. After the peak, μ
 299 continuously dropped at $V = 1\text{ }\mu\text{m/s}$ and subsequently increased with concave upward
 300 curve (thus V strengthening) at $V = 3$ and $10\text{ }\mu\text{m/s}$. In contrast, V -weakening behavior
 301 (and stick slips for u996) was observed at $V > 30\text{ }\mu\text{m/s}$ with slip hardening trend. The
 302 final μ values were 0.83 (u992) and 0.79 (u996).

303 In stage 4 ($36.5 < d < 47.4\text{ mm}$; $T = 250, 400, 550\text{ }^{\circ}\text{C}$), frictional behavior of T
 304 $= 250\text{ }^{\circ}\text{C}$ (u968) and $400\text{ }^{\circ}\text{C}$ (u972) was similar to that at stage 3 showing nearly
 305 constant μ values with V -weakening behavior. Stick slips were observed at all V
 306 conditions for $T = 400\text{ }^{\circ}\text{C}$ (u972) and all but $V = 100\text{ }\mu\text{m/s}$ for $T = 250\text{ }^{\circ}\text{C}$ (u968). For
 307 the tests with $T = 550\text{ }^{\circ}\text{C}$ (u992 and u996), μ dropped from the peak values at $V = 1$
 308 $\mu\text{m/s}$ and subsequently showed concave upward increase at $V = 3, 10$, and at $30\text{ }\mu\text{m/s}$.
 309 At $V = 100\text{ }\mu\text{m/s}$, both u992 and u996 showed minor slip-hardening trends with
 310 V -strengthening behavior for u992 and V -weakening behavior for u996 (stick-slips were
 311 also observed). The final μ values were 0.79 for $250\text{ }^{\circ}\text{C}$ (u968), 0.75 for $400\text{ }^{\circ}\text{C}$ (u972),
 312 0.91 and 0.85 for $550\text{ }^{\circ}\text{C}$ (u992 and u996, respectively).

313 Because the higher T and/or higher V conditions were imposed at later stages
 314 with larger d , the observed μ at such conditions would be overestimated due to a
 315 continuous background strain hardening trend (Figure 4c). Hence, μ values of 0.57-0.58
 316 at yield points at $d \sim 1\text{-}2\text{ mm}$ in the stage 1 are the μ values for the tested altered basalt
 317 that are least affected. To evaluate the effect of strain hardening trend on μ at large d ,
 318 our experiments were designed to have the same T condition at different d for $T =$
 319 $250\text{ }^{\circ}\text{C}$ (stage 4 for u968 and stage 1 for u972) and $400\text{ }^{\circ}\text{C}$ (stage 4 for u972 and stage 1

for u992 and u996). Using the data with $V = 10 \mu\text{m/s}$ which had less fluctuation than those with other V conditions, we obtained slip-hardening trends (μ/d) of 0.005 mm^{-1} for $T = 250 \text{ }^\circ\text{C}$ and 0.003 mm^{-1} for $400 \text{ }^\circ\text{C}$. Therefore, we use 0.004 mm^{-1} for a universal slip-hardening trend (gray line in Figure 4a) to obtain the first estimation of μ values without slip-hardening trend and detrended μ values are shown in Figure 4b. The detrended data may include an error in μ of ± 0.05 at most, resulting from using the bounds of 0.003 or 0.005 mm^{-1} for the slip-hardening trend (Figure 4a). In Figures 4d, we show the relationship between detrended μ , T and V , which will be used for the discussion in this study. The representative μ value at each P - T - V condition was determined at the last part of each condition after detrending the universal slip-hardening trend: $\mu = \sim 0.6$ at $T < 400 \text{ }^\circ\text{C}$ with $V = 1\text{-}100 \mu\text{m/s}$; μ at low V conditions decreases with T at $T > 400 \text{ }^\circ\text{C}$; μ becomes 0.45 for $V = 1 \mu\text{m/s}$ and 0.7 for $V = 100 \mu\text{m/s}$ at $T = 550 \text{ }^\circ\text{C}$ (Figure 4d).

333

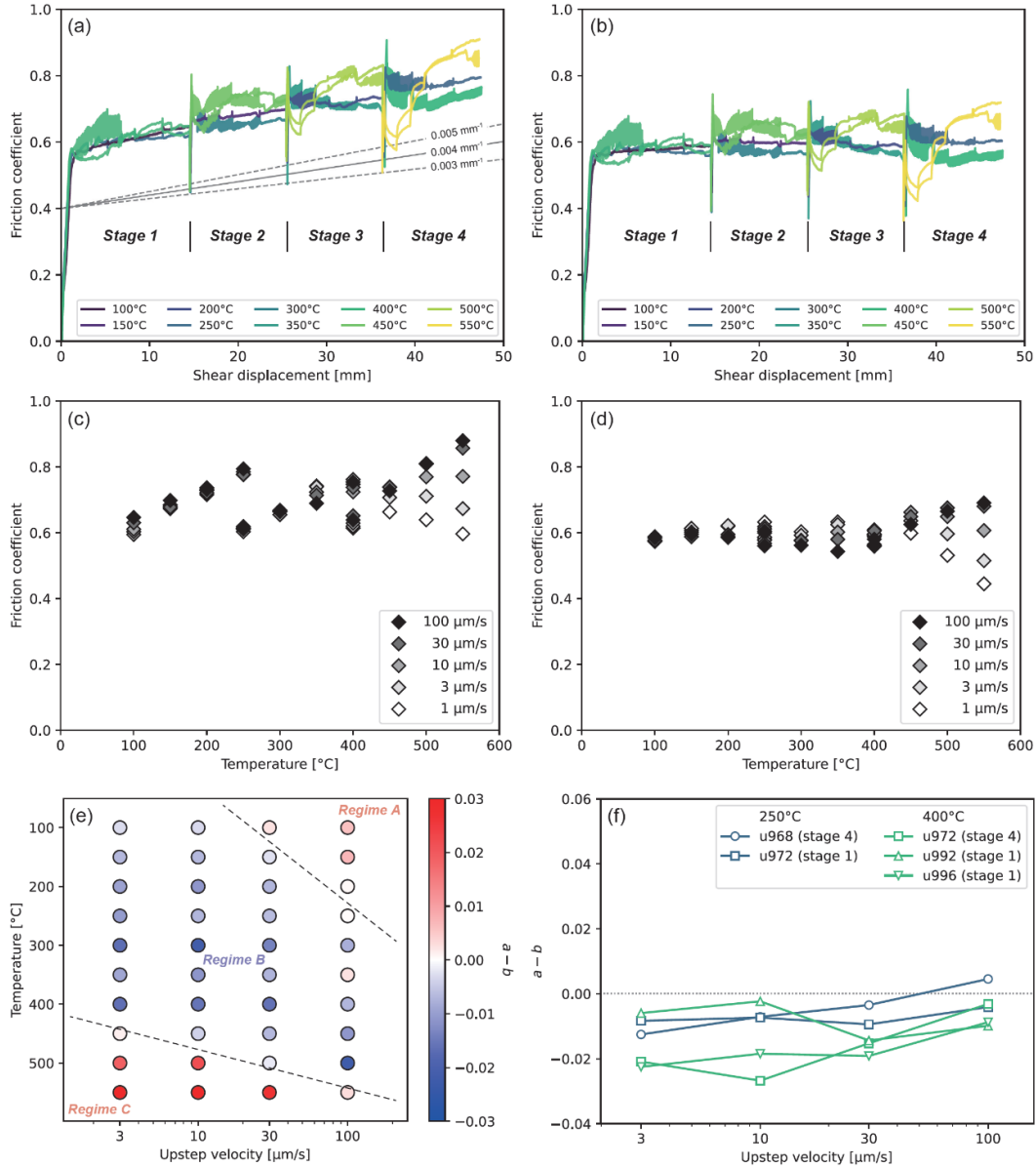
3.1.1.2. On velocity dependence of friction coefficient ($a-b$)

The $a-b$ values vary depending on V and T . For example, at $T = 100 \text{ }^\circ\text{C}$, negative $a-b$ values were observed at $V < 10 \mu\text{m/s}$, whereas positive $a-b$ values were observed at $V > 30 \mu\text{m/s}$. At $V = 100 \mu\text{m/s}$, positive $a-b$ values were observed up to $T = 200 \text{ }^\circ\text{C}$, negative $a-b$ values up to $T = 500 \text{ }^\circ\text{C}$, and positive $a-b$ values were again observed at higher T (Figure 4e). In general, $a-b$ values were positive at high- V -low- T and low- V -high- T conditions, whereas $a-b$ values were negative at intermediate- V -intermediate- T conditions. We define three Regimes based on the sign of $a-b$ values in the V - T space as follows: Regime A is the high- V -low- T range where $a-b$ values are positive; Regime B is the intermediate- V -intermediate- T range where $a-b$

344 values are negative; Regime C is the low- V -high- T range where $a-b$ values are positive
345 (Figure 4e). Both transitions between Regimes at lower T occurred at lower V
346 conditions, e.g., the transition between Regime B and C was at $T = 450$ °C for $V = 3$ -10
347 $\mu\text{m/s}$ whereas $T = 550$ °C for $V = 30$ -100 $\mu\text{m/s}$. Results from experiments with $T = 250$
348 and 400 °C, run at different d (Figure 4f), suggest that d has little influence on the $a-b$
349 values, despite the slip hardening and T strengthening observed. A previous study on
350 similar altered basalt showed similar values for the μ (0.60-0.69) and $a-b$ (-0.003 -
351 -0.006) at a T of 150 °C and V of 0.2-2 $\mu\text{m/s}$ (Phillips et al., 2020).

352

353



354
 355 **Figure 4.** (a) Frictional behavior of altered basalt at $T = 100\text{--}250^\circ\text{C}$ (u968), $250\text{--}400^\circ\text{C}$
 356 (u972), and $400\text{--}550^\circ\text{C}$ (u992, u996) with $\sigma_n^{eff} = P_f = 100\text{ MPa}$. Trends of μ are also
 357 indicated. (b) Frictional behavior after detrending a universal trend of 0.004 mm^{-1} . (c)
 358 Variations of μ values (original data) at each V - T condition. (d) Variations of μ values
 359 (detrended data) at each V - T condition. (e) Obtained $a-b$ values at each V - T condition.
 360 Regime A: V -strengthening regime at high- V -low- T conditions; Regime B: V -weakening

361 regime at wide V - T conditions; Regime C: V -strengthening regime at low- V -high- T
362 conditions. (f) Observed $a-b$ values at 250 °C and at 400 °C in different shear
363 displacement. See table 1 for the displacements at which the respective stages were
364 done.

365

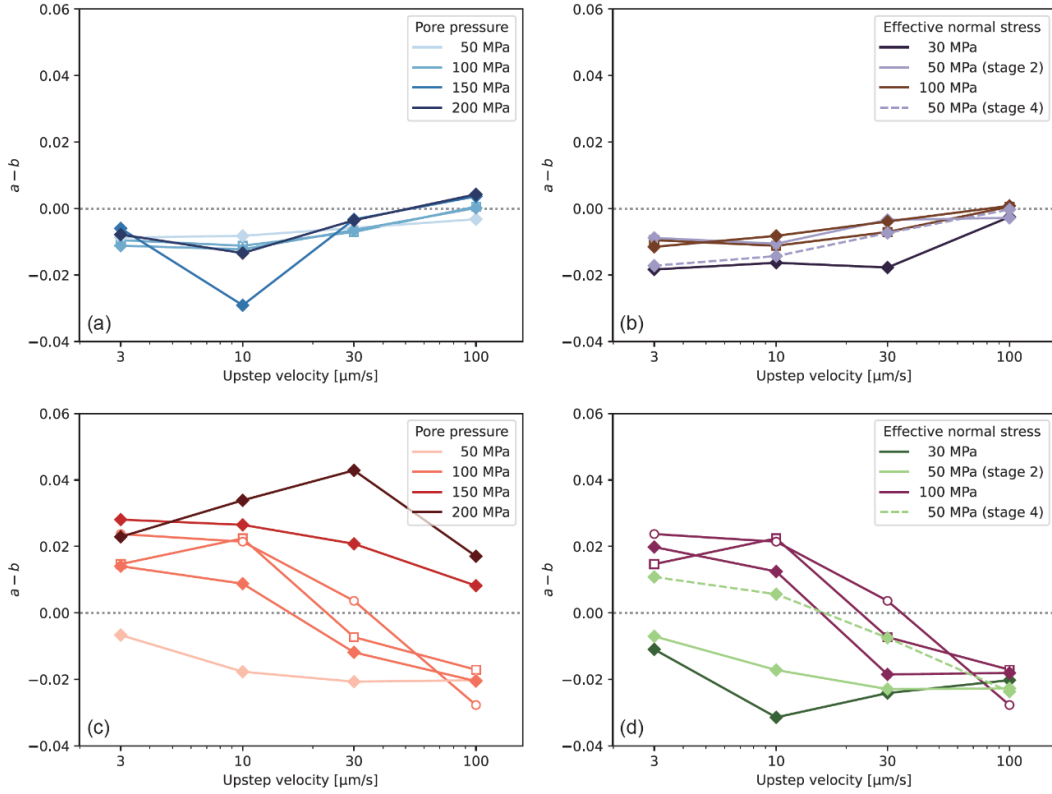
366 **3.1.2. Effect of high pore pressure or low effective normal stress at 200 °C and** 367 **500 °C**

368 At an σ_n^{eff} of 100 MPa and P_f of 100 MPa at $T = 200$ °C, the $a-b$ values
369 increase with V and become positive at 100 $\mu\text{m/s}$ which corresponds to the transition
370 from Regime B to A (open symbols in Figures 5a and b). We did not observe significant
371 variations in the curves of $a-b$ with V when P_f (50-200 MPa) was changed (Figure 5a).
372 Similarly, the effect of σ_n^{eff} is minor, but for $a-b$ values a mild increase with σ_n^{eff}
373 (Figure 5b) might be inferred. At the σ_n^{eff} of 50 MPa, the result of stage 4 shows slightly
374 lower $a-b$ than that of stage 2 (Figure 5b).

375 At an σ_n^{eff} of 100 MPa and a P_f of 100 MPa at $T = 500$ °C, the $a-b$ values
376 decreased with V and became negative at an up-step V of 10-30 $\mu\text{m/s}$ which corresponds
377 to the transition from Regime C to B (open symbols in Figures 5c and d). The $a-b$
378 curves shifted towards higher $a-b$ values for higher P_f conditions (Figure 5c). The $a-b$
379 values increased with σ_n^{eff} but only at low V conditions (Figure 5d). Note that only
380 positive values for $a-b$ were observed at high P_f (150 and 200 MPa), whereas negative
381 $a-b$ values were still observed for all other P_f and σ_n^{eff} conditions. A larger d caused an
382 increase in $a-b$, particularly at low up-step V (Figure 5d).

383

384



385 **Figure 5.** The $a-b$ values for (a) variable P_f conditions with a constant σ_n^{eff} of 100 MPa
 386 at $T = 200^\circ\text{C}$, (b) variable σ_n^{eff} conditions with a constant P_f of 100 MPa at $T = 200^\circ\text{C}$,
 387 (c) variable P_f conditions with a constant σ_n^{eff} of 100 MPa at $T = 500^\circ\text{C}$, and (d) variable
 388 σ_n^{eff} conditions with a constant P_f of 100 MPa at $T = 500^\circ\text{C}$. Open symbols represent the
 389 “reference” data shown in Figure 3; filled symbols represents the newly obtained data in
 390 u991, u993, u1002, and u1006; colors represent different σ_n^{eff} or P_f conditions. Dashed
 391 lines in (b) and (d) represent the results at the same σ_n^{eff} - P_f conditions but different d
 392 conditions (stage 2 vs. stage 4). See Table 1 for the displacements which the respective
 393 stages were done.

394 395 **3.1.3. Low velocity conditions at 400 °C and vacuum dry conditions at 100-200 °C**

396 Detrended μ values obtained for u1017, which was conducted at low V of

0.003-1 $\mu\text{m/s}$, ranged from 0.52 to 0.64, similar to those in other experiments (u972, u992, u996) at $T = 400^\circ\text{C}$ (Figure 6a). The $a-b$ values were negative at all tested V conditions except for the V -step from 0.3 to 1 $\mu\text{m/s}$ (Figure 6b).

Under vacuum dry conditions at $T = 100$ -200 $^\circ\text{C}$, the detrended μ values ranged from 0.59 to 0.67 and the $a-b$ values were close to zero at all V - T conditions. In contrast, wet experiments at the same T and σ_n^{eff} conditions (u968) showed slightly lower μ values of 0.57-0.62, and lower $a-b$ values at lower V and/or higher T conditions (Figures 6c-f).

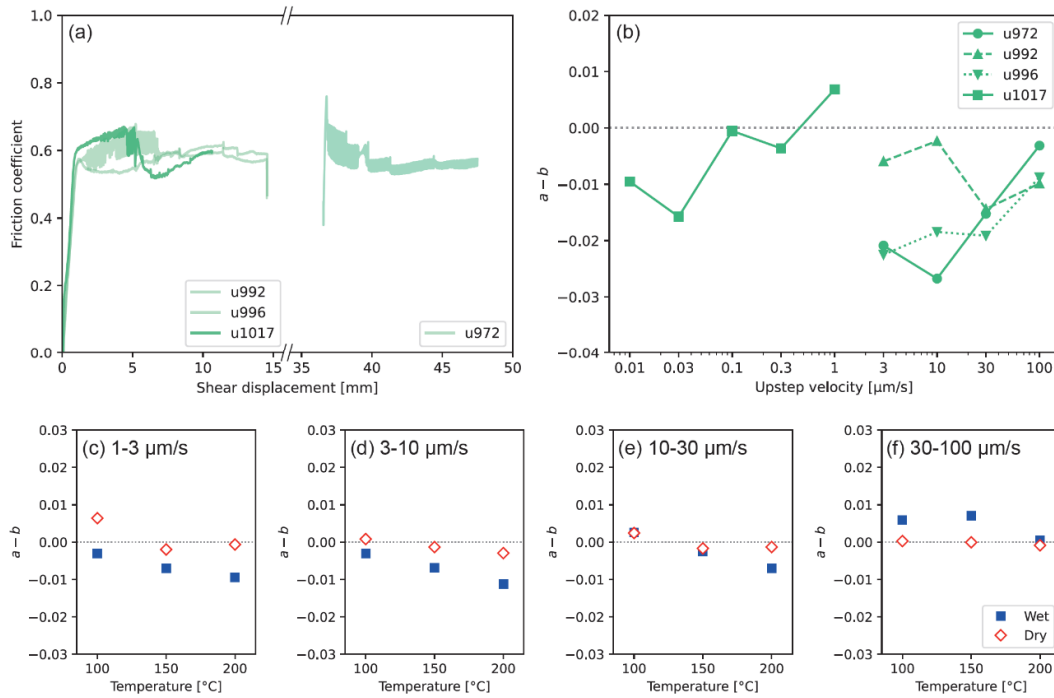


Figure 6. (a-b) Results of detrended μ and $a-b$ for u1017 at low V conditions at $T = 400^\circ\text{C}$ plotted with other experiments at $T = 400^\circ\text{C}$ with $V = 1$ -100 $\mu\text{m/s}$. (c-f) Results of vacuum dry experiments from $T = 100^\circ\text{C}$ to 200°C . Blue filled markers are the tests under 100 MPa P_f (annotated with “wet”) and red open markers are the tests with

411 vacuum dry (annotated with “dry”).

412

413 **3.1.4. Constant velocity experiments in Regimes A, B, and C**

414 The T and V conditions for the constant V tests were selected on the basis of the
415 three different regimes of V dependence of friction (Figure 7a). The test in Regime A
416 (u981, $T = 100\text{ }^{\circ}\text{C}$, $V = 100\text{ }\mu\text{m/s}$) showed stable frictional behavior while stick slip
417 behavior was observed in the test in Regime B (u980, $T = 400\text{ }^{\circ}\text{C}$, $V = 1\text{ }\mu\text{m/s}$). The
418 V -step from 1 to $0.01\text{ }\mu\text{m/s}$ in the test in Regime C (u975, $T = 550\text{ }^{\circ}\text{C}$, $V = 1\text{--}0.01\text{ }\mu\text{m/s}$)
419 showed a strong V -strengthening behavior characterized by a gradual decrease to the
420 steady state μ for $V = 0.01\text{ }\mu\text{m/s}$, which was about 0.3 at the shear displacement of 8.7
421 mm (Figure 7b).

422

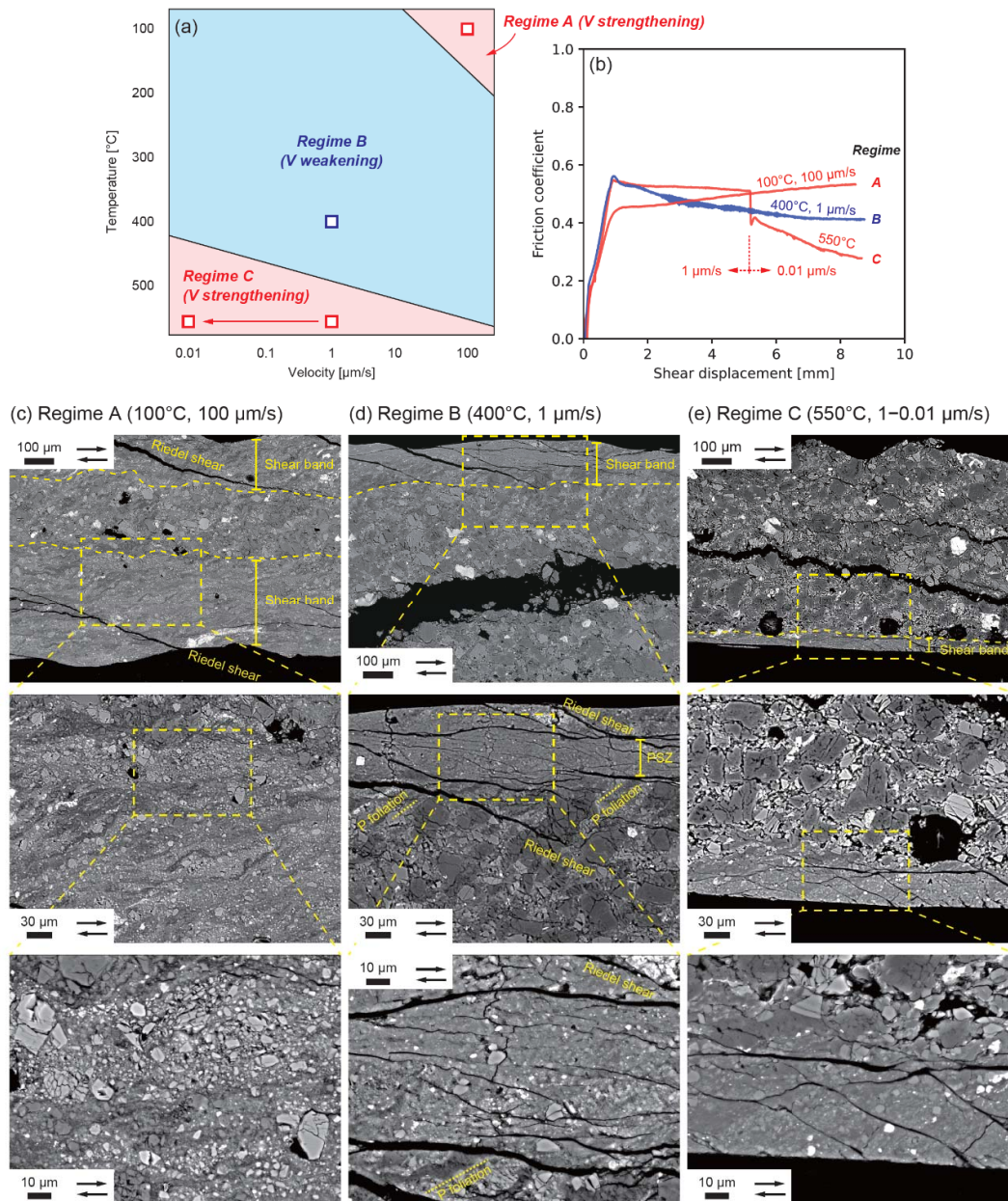
423 **3.2. Microstructures**

424 After the above constant V experiments, the microstructures of retrieved
425 samples were analyzed to observe the microstructural characteristics of the three
426 Regimes (Figure 7a). In Regime A, the microstructure is characterized by a wide,
427 boundary-parallel cataclastic shear band of $\sim 300\text{--}400\text{ }\mu\text{m}$ width, and Riedel shears,
428 identified by open fractures (Figure 7c). The shear band is porous and the long axis of
429 larger fragmented grains of both albite and clinopyroxene with grain size less than ~ 30
430 μm are aligned parallel to the shear direction. Outside the shear band (center part of the
431 gouge), grains are slightly rounded but their sizes are larger (but less than $\sim 50\text{ }\mu\text{m}$) than
432 those in the shear band.

433 In Regime B, the shear band is narrower ($\sim 100\text{ }\mu\text{m}$) with a principal slip zone
434 (PSZ) at the center of the shear band (Figure 7d). The PSZ is denser than the shear band

435 in Regime A. Grain size in the PSZ is reduced to sizes $< 1 \mu\text{m}$. At the outside of PSZ but
436 in the shear band, both Riedel shears, characterized by open fractures, and P foliations,
437 characterized by aligned grains which are cataclastically fragmented (grain size $\sim 1\text{-}10$
438 μm), are observed. The long axis of an assemblage of fragmented grains of albite and
439 clinopyroxene are aligned along the P foliation (Figure 8a) but the textures of these
440 grains vary with mineralogy. At the same grain size of around $1 \mu\text{m}$, albite grains are
441 round and interlocking together whereas clinopyroxene grains are angular and do not
442 show interlocking features but form porous aggregates (Figures 8b and c). At the area
443 far from the shear band, grains are angular and their sizes are larger (but less than 100
444 μm) than those in the shear band.

445 In Regime C, the shear band is much narrower ($\sim 50 \mu\text{m}$ in width) and denser
446 than that in Regime B (Figure 7e). Albite grains in the shear band are tightly interlocked
447 and individual grains are difficult to distinguish. Grain size of clinopyroxene is less than
448 $5 \mu\text{m}$ in the shear band (Figure 8d). At the outside of the boundary shear band, grains
449 are angular, and their sizes are $\sim 100 \mu\text{m}$. Variations in textures with mineralogy are also
450 found in Regime C where isolated pores are observed between tightly interlocking
451 albite grains (Figures 8e and f), whereas clinopyroxene grains are angular and
452 occasionally show an indentation into an albite grain at the same scale (Figure 8e).
453 These features suggest that the albite likely underwent dissolution and precipitation
454 processes, such as a pressure solution, whereas clinopyroxene deformed in a mostly
455 brittle manner. Similarly, we observed that large albite grains outside of the shear band
456 tend to have pores inside characterized by unclear grain boundaries (Figure 8f). We also
457 observed limited volumes of very thin ($< 1 \text{ mm}$) chlorite foliation between grains,
458 subparallel to shear deformation (Figure 8f).



460

461 **Figure 7.** (a) Diagram of three Regimes in V - T space based on Figure 4d. Experimental
 462 conditions for three constant V experiments are plotted by square markers. (b)

463 Detrended μ values of three tests for microstructural observation. (c-e) Characteristic

464 microstructures observed in constant V experiment in each regime. The yellow square in

each figure is the location of the image in the lower row. PSZ: principal slip zone.

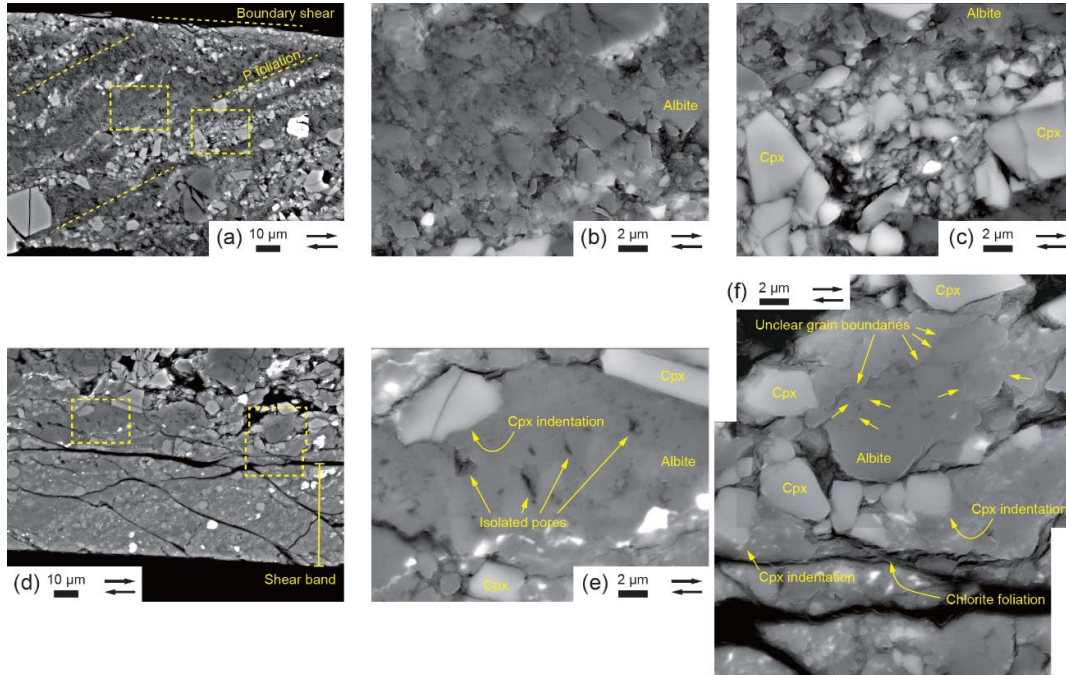


Figure 8. Characteristic microstructures for samples deformed in Regime B (a-c) and Regime C (d-f). The yellow squares in (a) and (d) are the locations of (b, c, e, f).

4. Discussions

4.1. Deformation micromechanisms

In our experiments, we have observed three Regimes of V dependence of friction: (Regime A) V -strengthening at higher V and/or lower T conditions, characterized by a thick cataclastic and porous shear band at the boundary; (Regime B) V -weakening at intermediate V - T conditions which showed a narrow, relatively dense shear band at the boundary and interlocking clusters of round albite grains along the P foliations; and (Regime C) marked V -strengthening at lower V and/or higher T conditions ($a-b > 0.01$ at $T > 450$ °C) with a dense shear band microstructure featuring

480 limited volume of chlorite foliations and deformation by dissolution and precipitation
481 processes, possibly pressure-solution creep, in albite grains rather than clinopyroxene
482 grains (Figures 7 & 8).

483 When the system is dry, fluid-assisted processes like pressure-solution creep
484 cannot be active. We observed little dependences of $a-b$ on V - T conditions in the case
485 of dry experiments (conducted at $V = 1\text{-}3\text{-}10\text{-}30\text{-}100\text{ }\mu\text{m/s}$, $T = 100\text{-}150\text{-}200\text{ }^{\circ}\text{C}$, u1003),
486 in contrast to the wet experiments which showed that the transition between Regime A
487 (V -strengthening) and B (V -weakening) occurs around $V = 30\text{-}100\text{ }\mu\text{m/s}$ at $T =$
488 $100\text{-}200\text{ }^{\circ}\text{C}$ (Figure 6). This difference between dry and wet experiments demonstrates
489 that the presence of a fluid (pressure) has a large effect on the V dependence of friction
490 even at low T conditions. As the shear band microstructures observed in Regime B and
491 C under wet conditions are characterized by interlocking albite grains, and as the
492 fractures in albite grains outside the shear band in Regime C also showed interlocking
493 features (Figure 8), pressure-solution creep of albite may be a possible process involved
494 in controlling mechanical behavior (Rutter & Mainprice, 1979; Spiers et al., 2004).

495 Results from previous studies on simulated gouges prepared from
496 halite-phylosilicate mixtures, calcite, illite-rich shale, granite, quartz, and gabbro, under
497 hydrothermal conditions, showed similar transitions in frictional behavior from V
498 strengthening, V weakening, to V strengthening with respect to V or T conditions
499 (Blanpied et al., 1995; Chen et al., 2020; Chester & Higgs, 1992; den Hartog & Spiers,
500 2013; He et al., 2007; Niemeijer & Spiers, 2007; Verberne et al., 2015). The
501 three-regime behavior can be explained by the microphysical model of
502 Chen-Niemeijer-Spiers (CNS) model which is based on a competition between a
503 time-dependent, thermally activated deformation/compaction mechanism and

504 slip-dependent dilatation resulting from intergranular sliding (granular flow),
505 characterized by mild V -strengthening (Chen & Spiers, 2016; Niemeijer & Spiers, 2007).
506 When V is sufficiently low or T is sufficiently high, compaction by pressure-solution
507 creep of grains occurs efficiently and porosity within the gouge is kept low; the shearing
508 behavior of gouge is then governed by pressure-solution creep and is therefore viscous
509 (Bos & Spiers, 2002; Niemeijer & Spiers, 2005, 2007). This mechanism leads to
510 markedly V -strengthening behavior at high T and/or low V conditions corresponding to
511 Regime C. At even lower V and/or higher T , the shear strength and apparent friction
512 coefficient μ will be controlled by non-dilatant frictional sliding on phyllosilicate
513 (chlorite in this study) coated grain boundaries or foliation planes as the resistance
514 offered by serial operation of pressure solution becomes negligible (Niemeijer & Spiers,
515 2005). Although we observed a limited volume of chlorite between grains (Figure 8f),
516 the apparent μ of 0.3 observed at $T = 550$ °C and $V = 0.01$ $\mu\text{m/s}$ (Figure 7b) is consistent
517 with the value obtained for chlorite gouge by Okamoto et al. (2019), implying that grain
518 boundary sliding along chlorite foliation surfaces may define the asymptote to the low μ
519 seen in Regime C, notably at the highest- T /lowest- V and largest displacement
520 conditions.

521 When the shear strain rate becomes fast enough for one grain to start to
522 override the next grain, due to the increase in stress needed to drive shear by pressure
523 solution at rapid strain rates, then porosity of the gouge starts to increase and the shear
524 strength originating from dilatant frictional sliding (granular flow) decreases, leading to
525 the V -weakening behavior seen in Regime B. This situation involves a competition
526 between the rate of dilatation due to granular flow and compaction by pressure solution,
527 leading to a balance at steady state that is characterized by a steady state porosity and

negative $a-b$ value (Niemeijer & Spiers, 2007). In both Regimes B ($T = 400$ °C) and C ($T = 550$ °C), we observed interlocking features of albite grains inside (and also outside in Regime C) the shear bands (Figures 7 & 8) which suggest the occurrence of compaction by pressure solution creep at the corresponding T conditions. When V is high or T is low enough to render compaction creep unable to compete with dilatation due to granular flow, then critical state granular flow ensues at a fixed (critical state) porosity (Niemeijer & Spiers, 2007). At this point, V -strengthening intergranular friction causes re-emergence of V -strengthening behavior at the sample scale (Chen & Spiers, 2016), causing the observed transition to Regime A. Grains in the shear band formed in the test in the Regime A did not show interlocking features of grains but cataclastically fragmented grains were observed (Figure 7). The model for the regime transitions predicts higher shear band porosity in Regime A and lower porosity in Regimes B and C, which is also clearly observed in our microstructural observations (Figure 7).

The good agreement of the trends seen in our experimental results and microstructures with the trends predicted by the above CNS microphysical model implies that the CNS model can be used to extrapolate the fault slip behavior seen within the altered basalt beyond the lab conditions explored. Although our experiments were mostly done at $V = 1-100$ $\mu\text{m/s}$, the V -weakening behavior for $0.01-1$ $\mu\text{m/s}$ at $T = 400$ °C suggests that the tested material will show V -weakening behavior (Regime B) at a wide range of $V < 100$ $\mu\text{m/s}$ at $T < 400$ °C, except for the conditions of Regime A at $T < 200$ °C and high $V (>30$ $\mu\text{m/s})$ conditions, provided that the (localized) thickness of the deforming zone is comparable between experiments and nature. The V -weakening behavior (Regime B) at 0.03 $\mu\text{m/s} < V < 100$ $\mu\text{m/s}$ conditions at $T < 400$ °C implies a potential to nucleate an earthquake on faults in the subducting oceanic crust at the

552 seismogenic zone depths ($T \sim 150\text{-}350\text{ }^{\circ}\text{C}$).

553

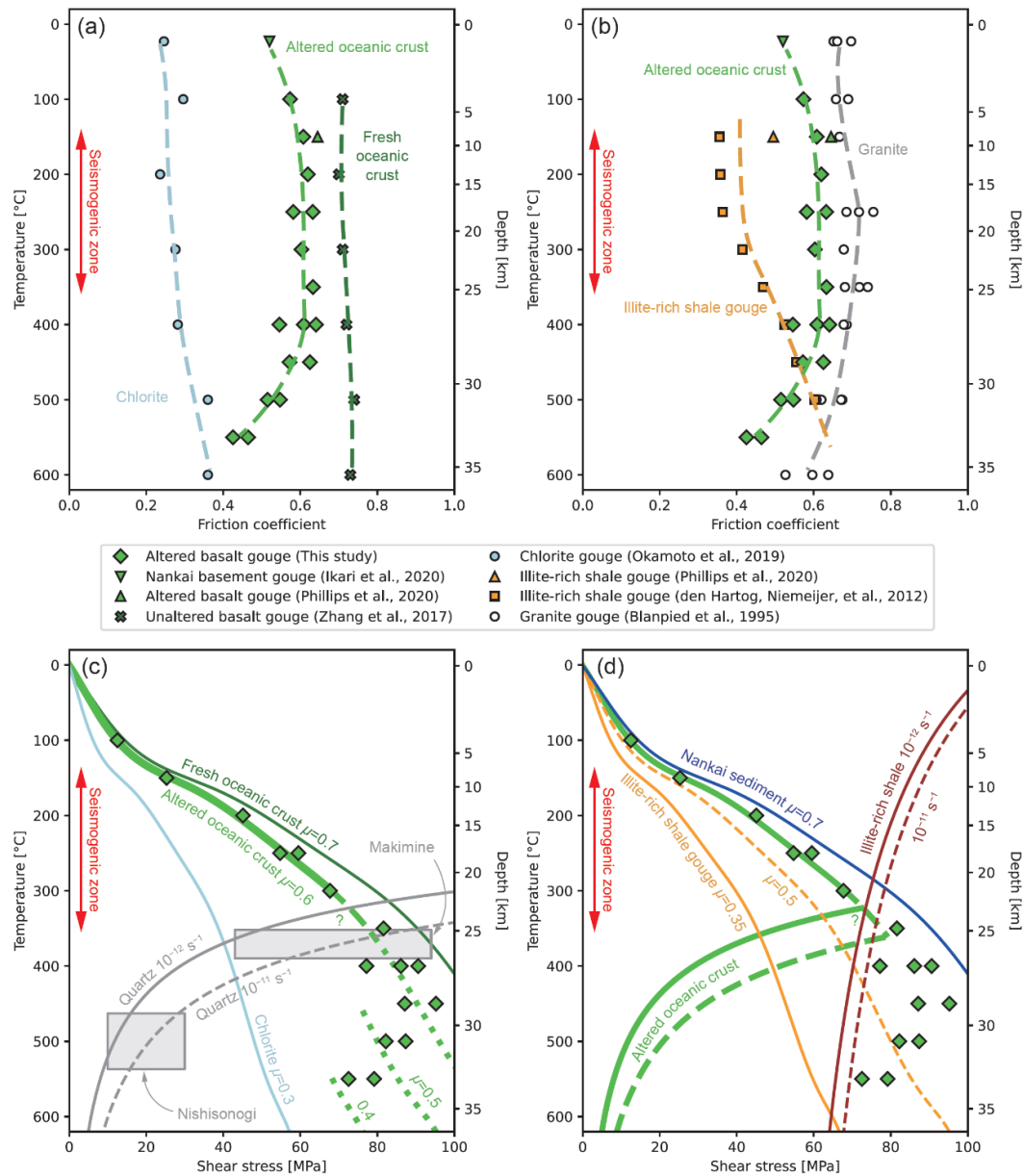
554 **4.2. Role of alteration and its influence on the frictional properties of subducting** 555 **oceanic crust**

556 The CNS model for frictional behavior predicts V -weakening behavior when
557 pressure-solution creep of albite and dilatant frictional shear deformation among grains
558 occur at comparable rates. Both albite and chlorite are originally present in our
559 uncrushed material (Figure 2) which means those minerals are not formed during an
560 experiment – they result from early seafloor alteration processes and subsequent
561 subduction (Braden & Behr, 2021; Ikari et al., 2020; Kameda et al., 2011, 2017; Moore
562 et al., 2007; Phillips et al., 2020; Ujiie et al., 2007). As seen in Figure 2, albitization
563 produces fine albite grains from single anorthite grains and mechanically weak chlorite
564 as well (Ramseyer et al., 1992; Rosenbauer et al., 1988). The low μ of chlorite
565 (0.24-0.36) reduces the bulk strength of gouge if sufficient chlorite is present (Logan &
566 Rauenzahn, 1987; Okamoto et al., 2019, 2020), so that altered subducting oceanic crust
567 will be weaker than fresh oceanic basalt. In addition, finer grains deform more easily via
568 pressure solution than large grains, which promotes viscous compaction and shear creep
569 leading to Regime B and C at lower T conditions than fresh oceanic basalt. Compared to
570 fresh oceanic basalt (Zhang et al., 2017), the present altered basalt showed a) slightly
571 lower μ (Figure 9a) and potentially unstable frictional behavior (Regime B) at a wider T
572 range, including those expected at seismogenic zone depths, and b) positive $a-b$
573 (Regime C) at high T conditions (Figure 10a). Our finding of a potential for frictional
574 instability over a wide T range ($< 400\text{ }^{\circ}\text{C}$) is also different from that found for chlorite
575 (Okamoto et al., 2019) and for single mineral phases of pyroxene and plagioclase (He et

576 al., 2013). This suggests that the presence of small grains of albite as an alteration
577 product promotes the V -weakening behavior of altered basalt under conditions that are
578 relevant for nucleating megathrust earthquakes in subduction zones.

579 According to previous studies that reported mineral compositions of basaltic
580 layers in different mélanges in Shimanto accretionary complexes,
581 albite-clinopyroxene-chlorite assemblages disappear at $T > 300$ °C (Kameda et al., 2017).
582 Therefore, our experimental results can only be applicable at subduction depth ranges
583 where $T < 300$ °C. At greater depths, clinopyroxene will disappear and epidote-quartz or
584 actinolite(-quartz) will emerge. Note that we did not observe any mineralogical changes
585 in our high T experiments confirmed by microstructural observations and EDS analyses.
586 In the Makimine mélange and Nishisonogi metamorphic rocks, SW Japan, deformed
587 oceanic crust materials are exposed and they experienced T of 370°C and 500°C,
588 respectively. Previous studies estimated shear stresses from grain size in quartz veins to
589 be 25-60 MPa at Makimine mélange and 10-30 MPa at Nishisonogi metamorphic rocks,
590 which are regarded as the ductile shear strength of the subducting oceanic crust at
591 depths (Tulley et al., 2020). An overpressured condition with respect to the hydrostatic
592 condition in the subducting oceanic crust is expected by a combination of dehydration
593 of saponite around 150 °C and low permeability of overlying sediment that hampers the
594 fluid escaping from the oceanic crust (Kameda et al., 2011). Assuming the pore pressure
595 ratio λ (pore pressure / lithostatic pressure) = 0.8 (Tulley et al., 2020), the altered
596 oceanic crust have 70-90 MPa of shear stress at the depth of $T = 300$ -400 °C (Figure 9c).
597 Therefore, we expect the depth profile of shear stress of subduction oceanic crust will
598 follow the green line in Figure 9d as a combination of Coulomb stress of altered oceanic
599 crust with $\mu = 0.6$ and ductile shear stress of quartz. However, there is still a small, but

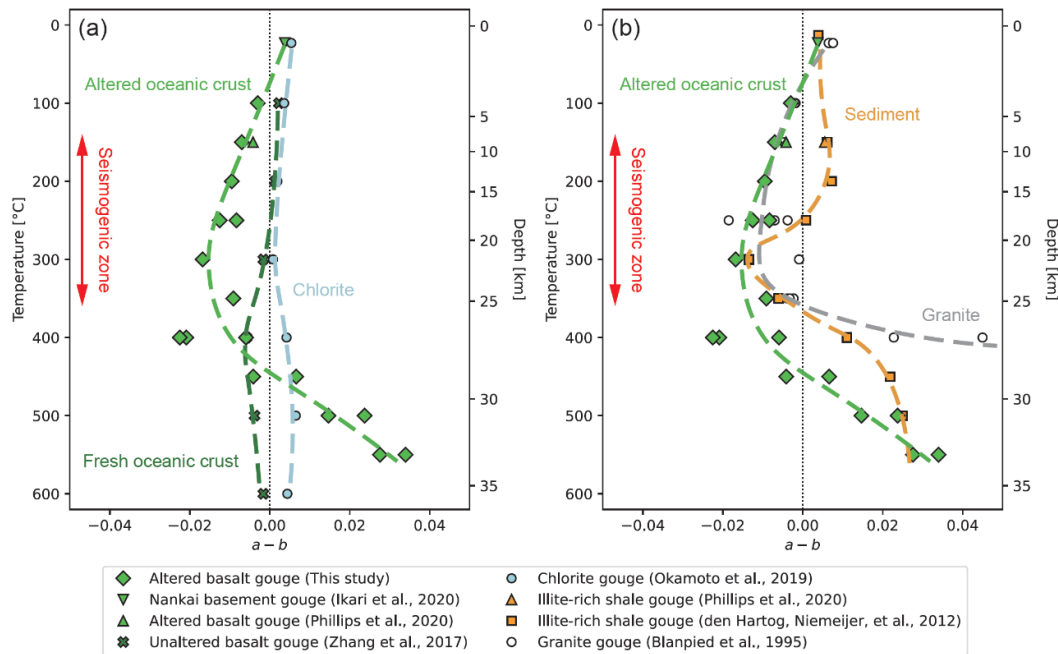
600 important gap of experimental data for albite-epidote-quartz-chlorite or
601 albite-actinolite(-quartz)-chlorite system at $T = 300\text{--}400\text{ }^{\circ}\text{C}$ which is the inferred T of
602 the intersection of Coulomb strength of altered basalt and ductile shear strength of
603 oceanic crust, corresponding to the brittle-ductile transition of oceanic crust. It has been
604 suggested that the presence of small amounts of quartz (3-5%) can stabilize the
605 frictional behavior of a fault gouge mixture of plagioclase and pyroxene because of the
606 high solubility of quartz which inhibits the growth of contacts of plagioclase and
607 pyroxene by pressure-solution creep due to silica saturation (He et al., 2013). Therefore,
608 further experiments with albite-epidote-quartz-chlorite or
609 albite-actinolite(-quartz)-chlorite system are needed to understand the fault slip behavior
610 around the brittle-ductile transition of subducting oceanic crust and its relation to the
611 downdip limit of seismogenic zone and deep slow earthquakes (Shibazaki & Iio, 2003).
612



613

614 **Figure 9.** Depth profiles of detrended μ for altered oceanic crust at $V = 1 \mu\text{m/s}$ (a) with
 615 altered oceanic crust (Ikari et al., 2020; Phillips et al., 2020), fresh oceanic crust (Zhang
 616 et al., 2017), and chlorite gouge (Okamoto et al., 2019); (b) with illite-rich shale (den
 617 Hartog, Niemeijer, et al., 2012; Phillips et al., 2020) and granite gouge (Blanpied et al.,
 618 1995). Depth profiles of shear stress for altered oceanic crust at $V = 1 \mu\text{m/s}$ (c) with

619 fresh oceanic crust (Zhang et al., 2017), chlorite gouge (Okamoto et al., 2019),
 620 estimated shear stresses at the Makimine mélange and Nishisonogi metamorphic rock
 621 (Tulley et al., 2020), and quartz rheology (Hirth et al., 2001; Tulley et al., 2020); (d)
 622 with illite-rich shale gouge (den Hartog, Niemeijer, et al., 2012; Phillips et al., 2020),
 623 the Nankai sediment (Okuda, Ikari, et al., 2021), and rheology for illite-rich shale
 624 (Ibanez & Kronenberg, 1993). Shear stresses were calculated based on μ and an
 625 overpressured condition with λ (pore pressure / lithostatic pressure) = 0.8 was assumed.
 626 Vertical direction is assumed to be the lithostatic pressure which is calculated by the
 627 product of density (2650 kg/m³), depth, and gravitational acceleration. T -depth relation
 628 is from Yoshioka et al. (2013).
 629



630
 631 **Figure 10.** Depth profile of $a-b$ values for altered oceanic crust at the V -step from $V =$
 632 1 to 3 $\mu\text{m/s}$ (a) with altered oceanic crust (Ikari et al., 2020; Phillips et al., 2020), fresh
 633 oceanic crust (Zhang et al., 2017), and chlorite gouge (Okamoto et al., 2019); (b) with

illite-rich shale (den Hartog, Niemeijer, et al., 2012; Phillips et al., 2020) and granite
gouge (Blanpied et al., 1995). T -depth relation is from Yoshioka et al. (2013).

636

637 **4.3. Implication for fault slip activities in subduction zones**

Regarding $a-b$ values, the altered basalt showed a large potential for unstable
frictional behavior at a wider T range than sediment and granitic rocks (Figure 10b).

Therefore, the altered basalt may be more likely to nucleate an earthquake than
sediment. To achieve unstable frictional slip leading to an earthquake, the shear stiffness
 K of surrounding rocks should be lower than the critical stiffness K_c defined as
(Dieterich, 1979; Ruina, 1983):

$$K_c = -\frac{(a-b)\sigma_n^{eff}}{d_c}, \#(2)$$

where d_c is a critical slip distance in the V -step although we do not quantify it in this
study. Equation 2 shows that the unstable fault slip, i.e., earthquake, is more likely to
occur when $a-b$ and/or σ_n^{eff} are large or d_c is small. Therefore, more negative $a-b$
values of altered oceanic crust than other materials lead to a higher possibility to
nucleate an earthquake within the altered oceanic crust. In previous sections, we
inferred that albite grains as an altered material of oceanic crust promote unstable
frictional behavior. Because detrital materials also often contain anorthite that can be
altered into albite at the same T condition in shallow depths of subduction zones, further
experimental studies on sediments may be needed to fully understand the difference in
frictional behavior between sediments and altered oceanic crust. Since illite-rich shale
gouge showed lower μ (around 0.35-0.5) than that of altered basalt at seismogenic zone
depths (den Hartog, Niemeijer, et al., 2012; Phillips et al., 2020), sediment is the first
candidate to be sheared easily (Figure 9b). However, the plate boundary fault in the

657 Nankai Trough, SW Japan, is proposed to have a high μ of ~ 0.7 at a depth of > 5 km
 658 according to the inference from Coulomb wedge model combining friction coefficients
 659 of sediment inside accretionary wedges, observed pore pressure conditions inside
 660 wedges and along the plate boundary, and observed topographical information of
 661 wedges (Okuda, Ikari, et al., 2021). Because the altered basalt showed $\mu \sim 0.6$ at the T
 662 range of 100-400 °C, the altered oceanic crust may also sustain similar or sometimes
 663 lower shear stress to sediment at least in the Nankai Trough, whose tectonic setting is
 664 similar to the one which the altered basaltic sample used in this study had experienced
 665 (Figure 9d). Frictional strength of the altered oceanic crust can be lowered substantially
 666 when more chlorite is contained and/or when P_f is high enough. Assuming that the μ for
 667 sediment is 0.35 or 0.5 (den Hartog, Niemeijer, et al., 2012) and that it is 0.6 for altered
 668 oceanic crust, a higher P_f is required in the altered oceanic crust than that in the
 669 sedimentary facies to make the frictional strength of the altered oceanic crust lower than
 670 that of the sedimentary facies: λ for the altered oceanic crust should be 0.88 or 0.83 to
 671 make the apparent frictional strengths of both materials the same when λ for the
 672 sediment is 0.8. Necessary pore pressure changes are 17.3 MPa at $T = 150$ °C and 53.7
 673 MPa at $T = 350$ °C from $\lambda=0.8$ to $\lambda=0.88$, and 6.9 MPa at $T = 150$ °C and 21.5 MPa at T
 674 $= 350$ °C from $\lambda=0.8$ to $\lambda=0.83$. When the frictional strength of the altered oceanic crust
 675 is lower than that of sediment by such a pore fluid overpressure, deformation at the
 676 plate boundary would be accommodated by the altered oceanic crust rather than by the
 677 sediment, and the accumulated stress along the plate boundary starts to be released by
 678 earthquake nucleation within the oceanic crust at the seismogenic zone depths (~ 10 -25
 679 km) where we obtained V -weakening of altered basalt (Phillips et al., 2020). Notably,
 680 the overpressured conditions with respect to the hydrostatic condition achieved by both

681 a decrease in σ_n^{eff} and an increase in P_f do not influence the $a-b$ value of altered basalt
 682 at $T = 200$ °C unlike blueschist, actinolite-chlorite mixture, and other materials (Bedford
 683 et al., 2021; Okamoto et al., 2020; Okuda, Katayama, et al., 2021; Sawai et al., 2016),
 684 which reduces K_c by simply decreasing in σ_n^{eff} and thus increases the nucleation size and
 685 possibly induces a slower slip, although the effects of σ_n^{eff} and P_f on d_c are unknown.
 686 Since sedimentary facies at shallow depths (<10 km) along décollement are
 687 overpressured driven by sediment compaction (Saffer et al., 2008; Tsuji et al., 2014),
 688 the coseismic rupture may propagate within the weak sedimentary facies rather than the
 689 altered oceanic crust at a depth of <10 km. Those situations will lead the décollement to
 690 “stepup” from the nucleation phase in the oceanic crust at the seismogenic zone (~5-25
 691 km) to the rupture propagation phase in the sedimentary facies at shallower depths
 692 which will result in the observation of décollement stepdown.

694 5. Conclusion

695 Seismological and geological studies suggest that the plate boundary fault
 696 (décollement) in subduction zones possibly develops within the subducting oceanic
 697 crust rather than sedimentary facies in the seismogenic zone depths. To understand the
 698 frictional properties of the subducting oceanic crust, we performed hydrothermal
 699 friction experiments on altered basalt at temperatures (T) of 100-550 °C, effective
 700 normal stresses (σ_n^{eff}) of 30-100 MPa, pore pressure (P_f) of 50-200 MPa, and velocity
 701 conditions (V) of 1-100 $\mu\text{m/s}$. Friction coefficient (μ) of the altered basalt was about 0.6
 702 for all V conditions at $T < 400$ °C, and became 0.45 at $T = 550$ °C and $V = 1$ $\mu\text{m/s}$ with
 703 V -strengthening behavior to $\mu = 0.7$ at $V = 100$ $\mu\text{m/s}$ considering a slip hardening trend
 704 of 0.004 mm^{-1} . Three regimes of V dependence were found: Regime A was at lower T

705 ($< 200\text{ }^{\circ}\text{C}$) and higher V ($> 30\text{ }\mu\text{m/s}$) showing V -strengthening behavior; Regime B was
706 at intermediate T ($100\text{--}450\text{ }^{\circ}\text{C}$) and almost all the V conditions showing V -weakening
707 behavior; Regime C was at higher T ($> 500\text{ }^{\circ}\text{C}$) and lower V showing V -strengthening
708 behavior. These regimes are well-explained by a microphysical model that considers a
709 balance between compaction creep and dilatant frictional behavior at grain boundaries.
710 Microstructural observations revealed that the pressure-solution processes of albite is
711 the control of creep deformation, which shifts Regime B to higher V conditions at a
712 given T . Alteration of oceanic crust during subduction produces fine grains of albite
713 contributing to the viscous deformation by pressure-solution creep in natural conditions.
714 Because albitization also produces the mechanically weak chlorite, the altered oceanic
715 crust can have a similar frictional strength to the sediment, which is also affected by P_f
716 and thus σ_n^{eff} conditions. The possible unstable frictional behavior of altered basalt at
717 wide T range suggests that a megathrust earthquake would nucleate within the oceanic
718 crust in the seismogenic zone depths.

719

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731

732 **Open Research**

733 Experimental data are freely available from the Yoda data repository:

734 <https://public.yoda.uu.nl/geo/UU01/6DSAJH.html>.

735

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Figure 1.

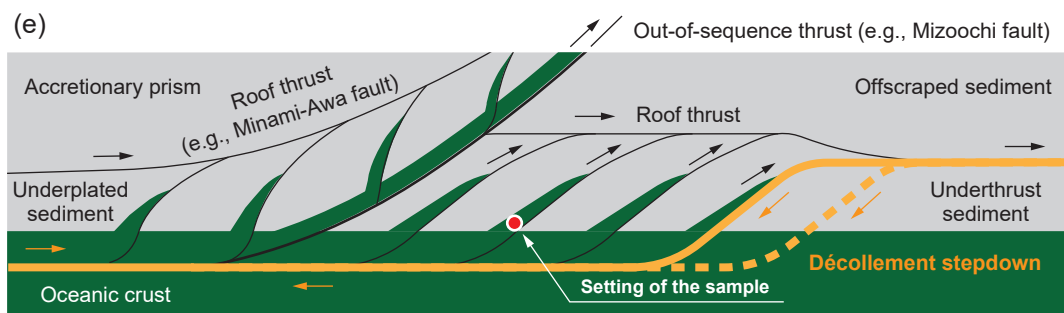
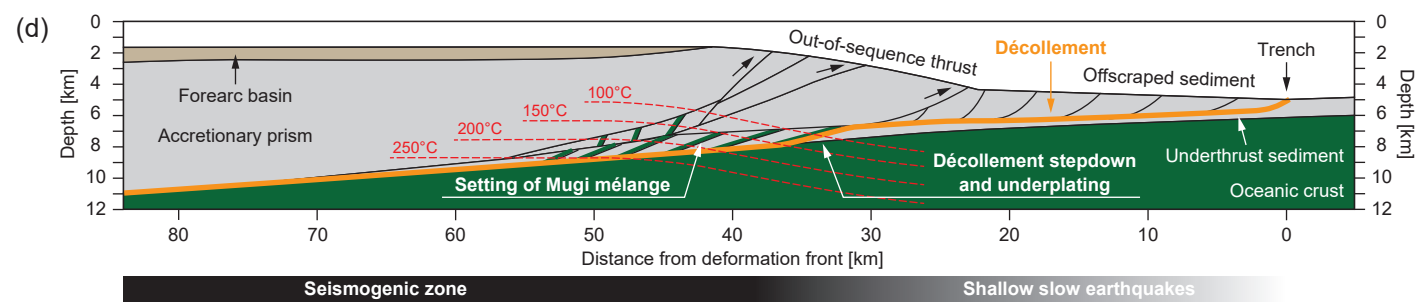
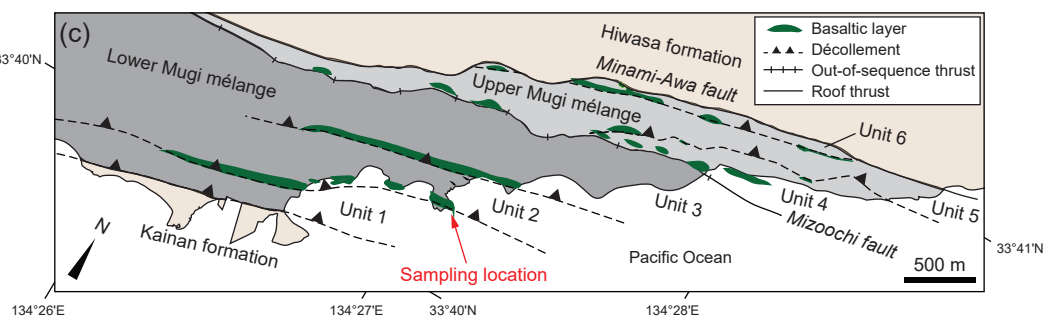
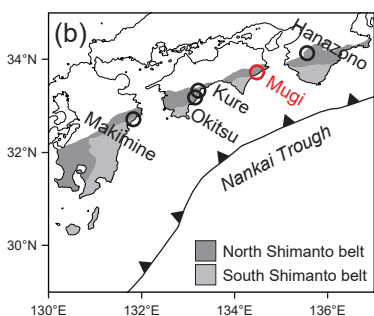
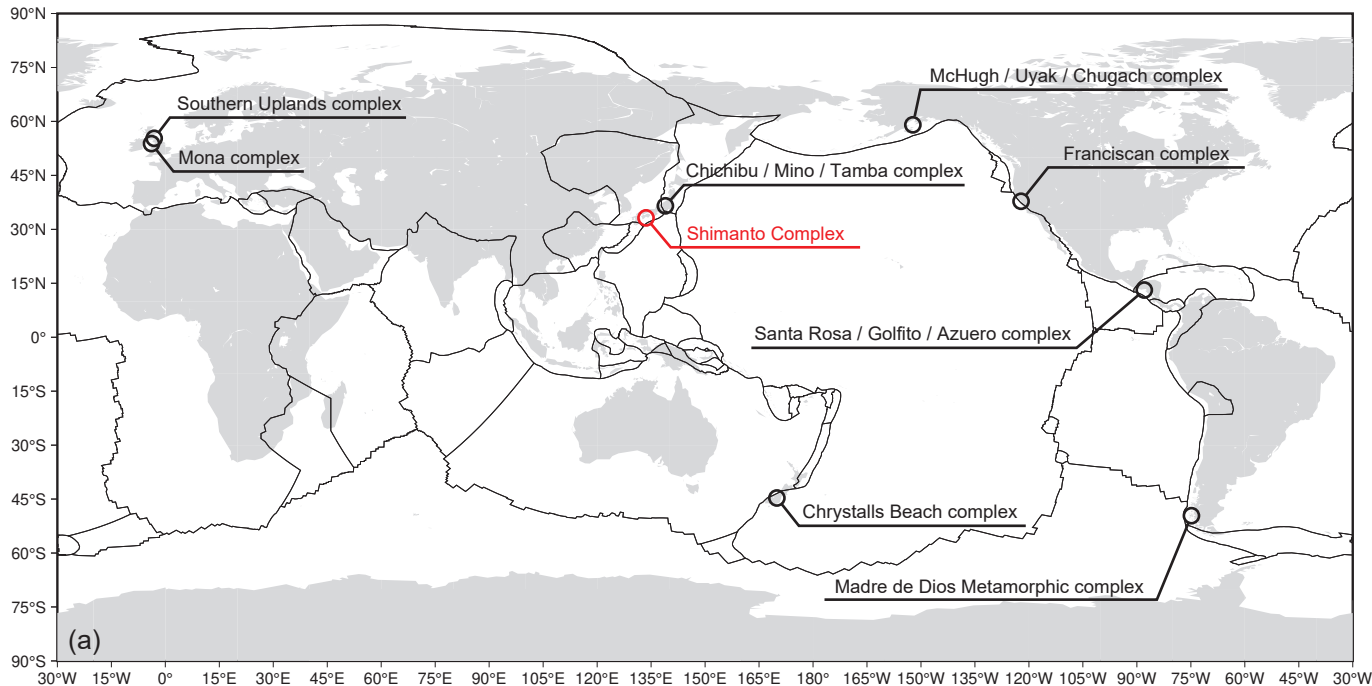


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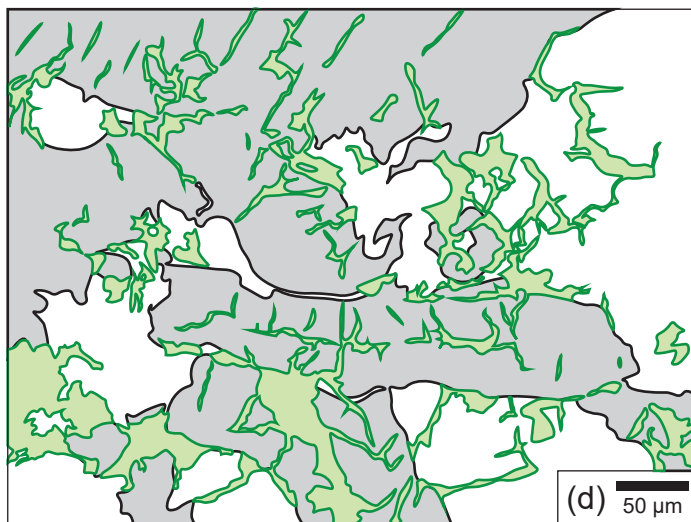
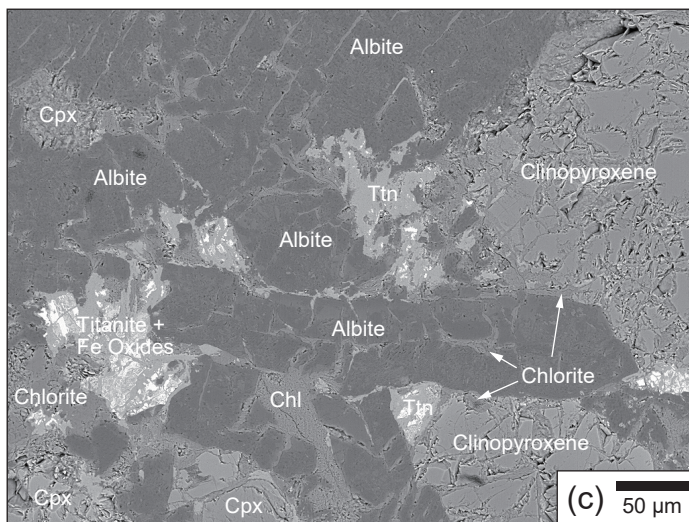
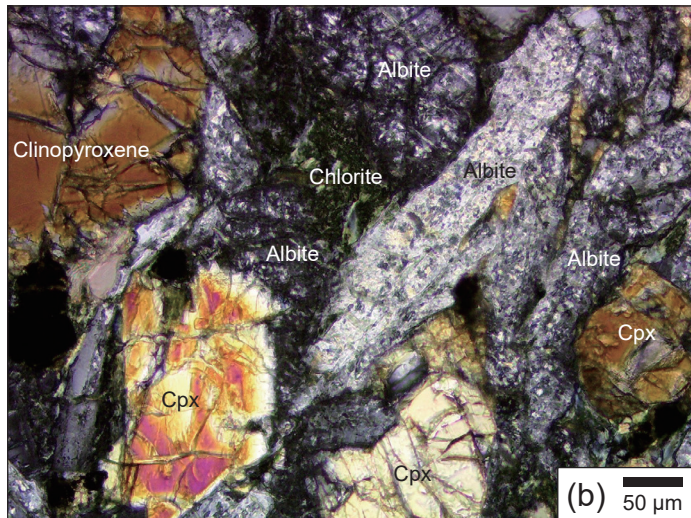
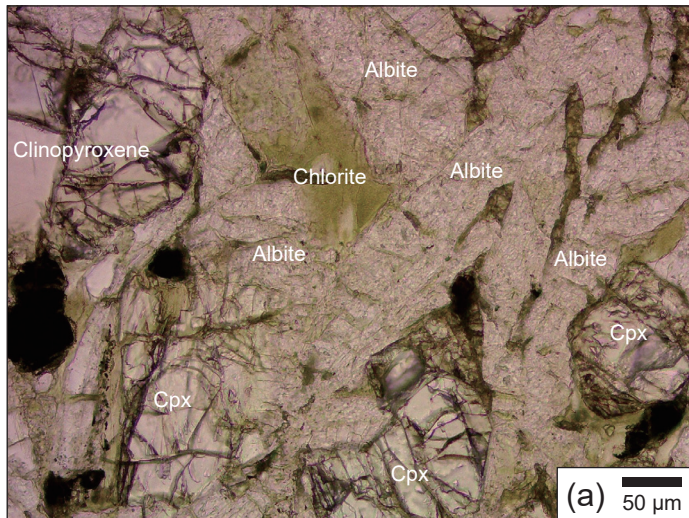


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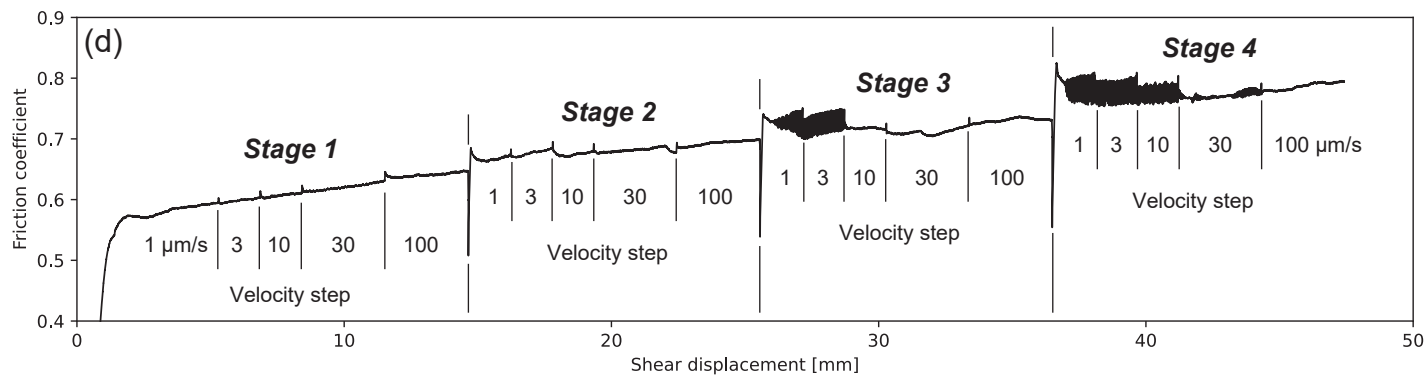
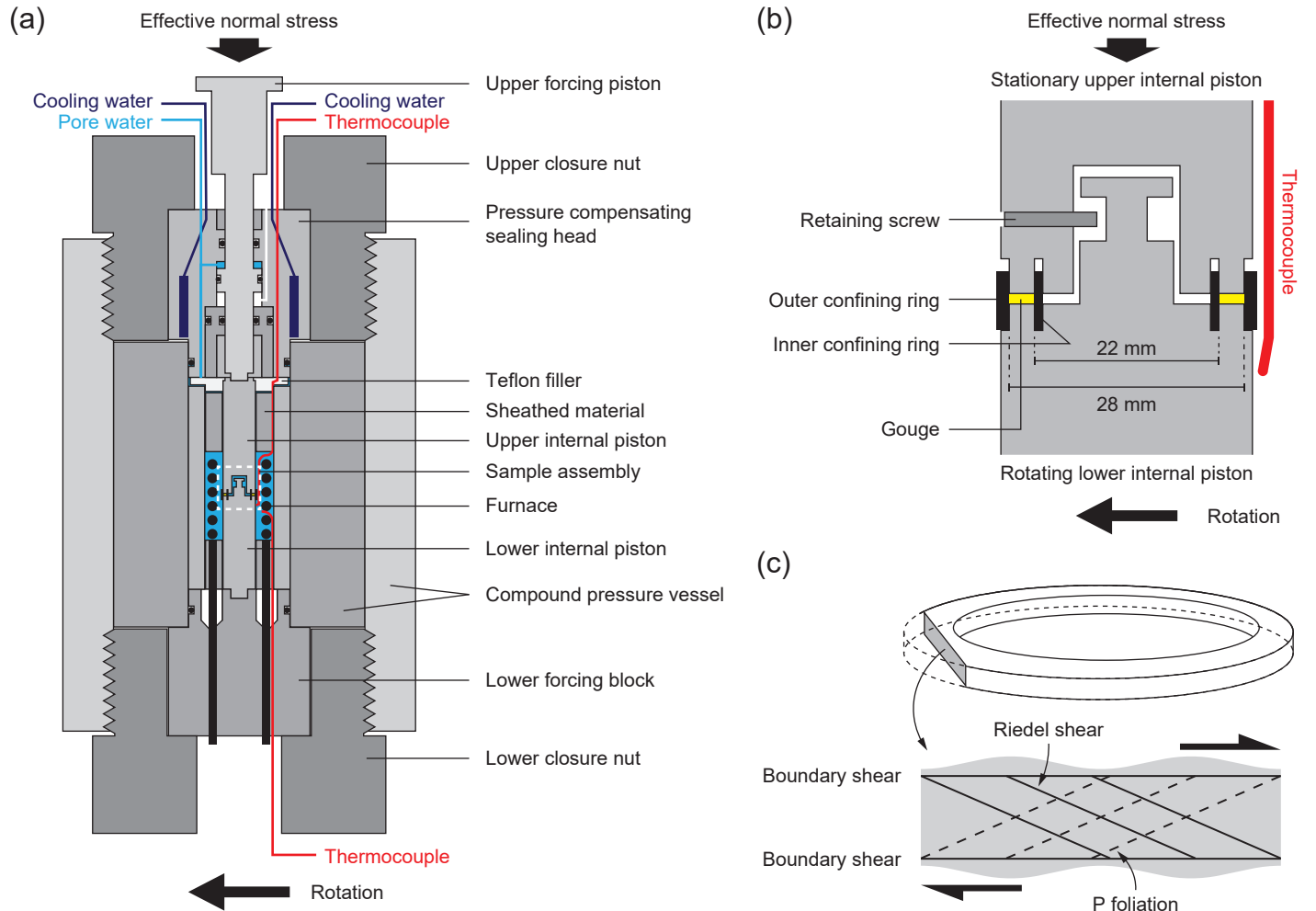


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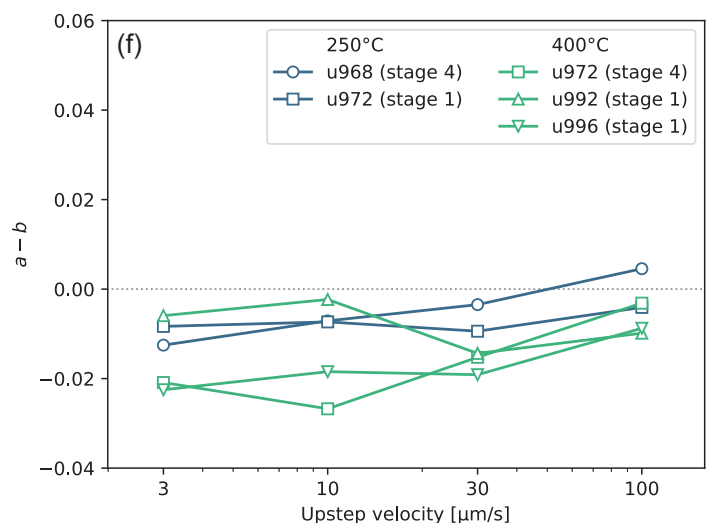
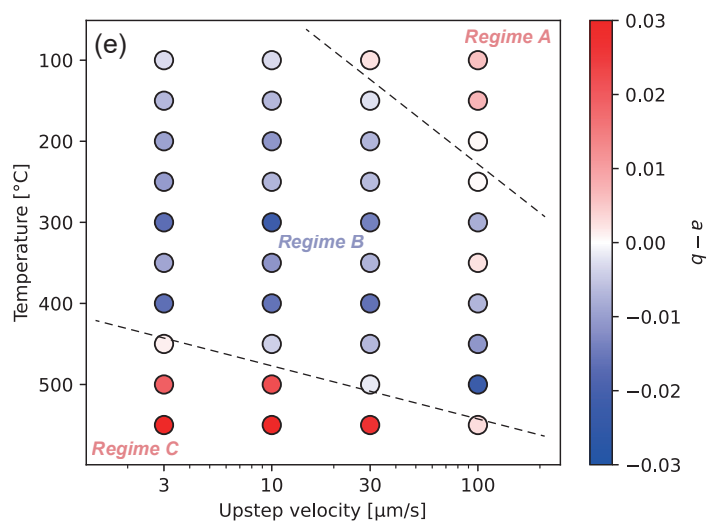
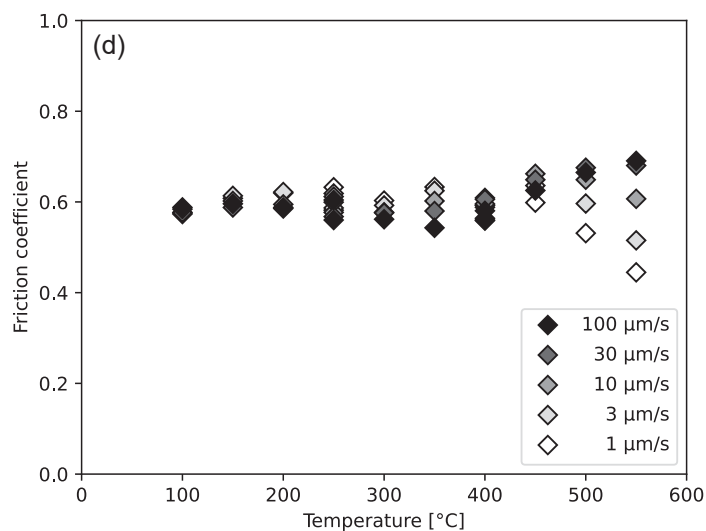
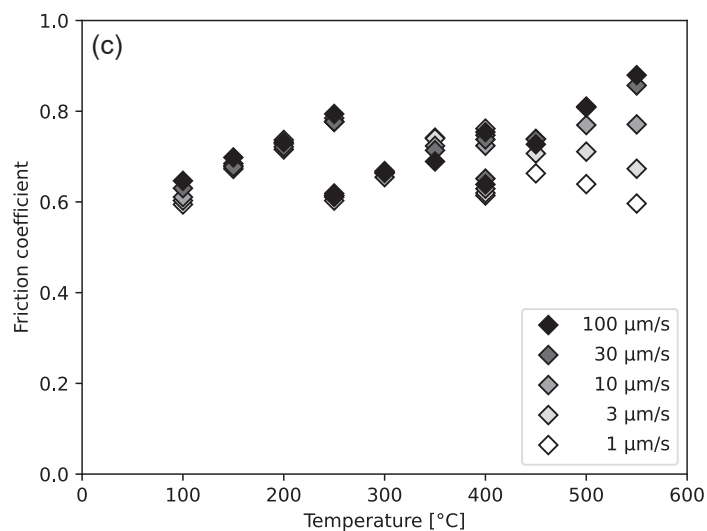
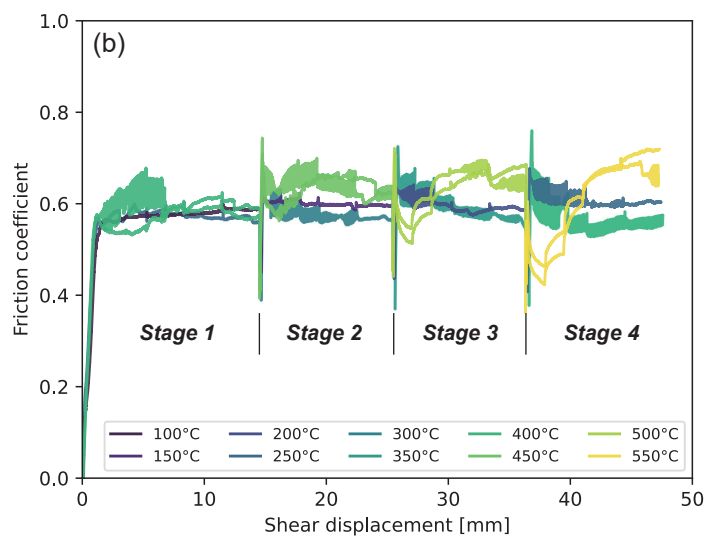
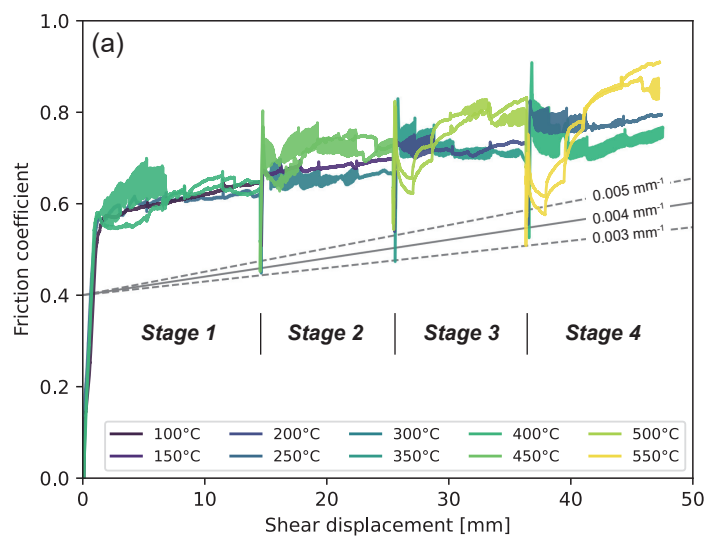


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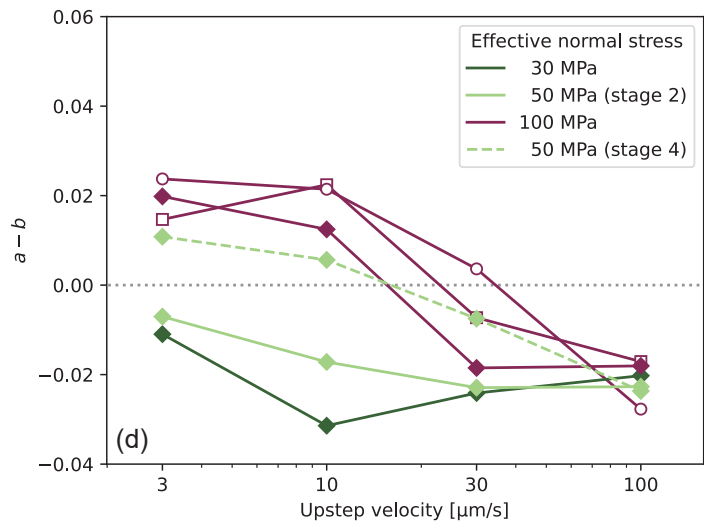
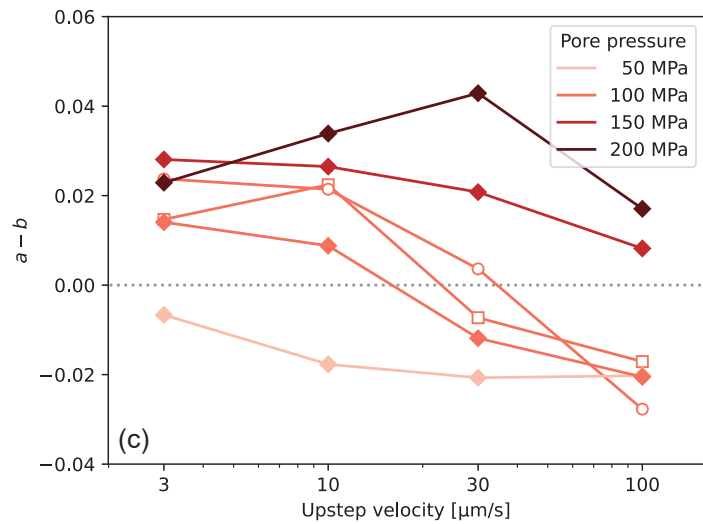
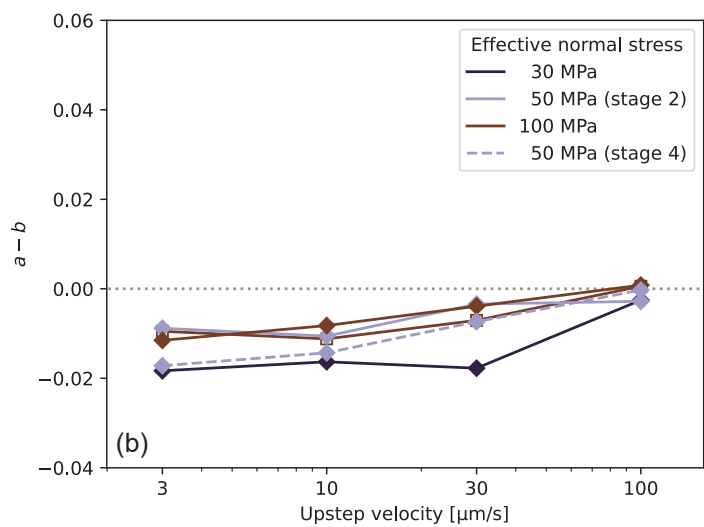
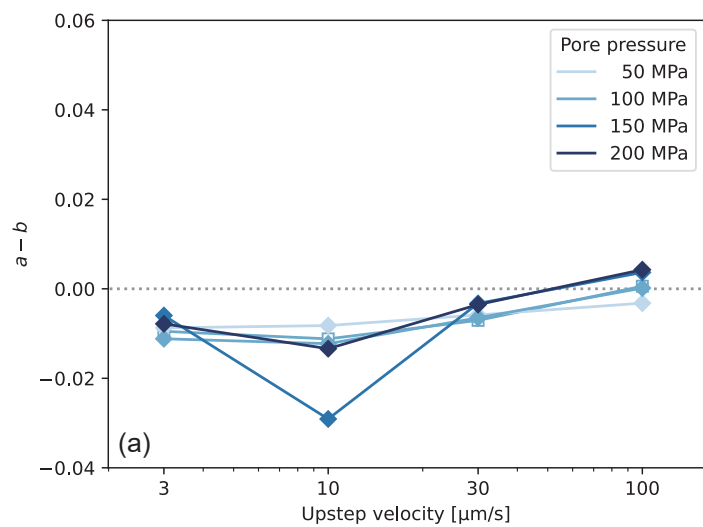


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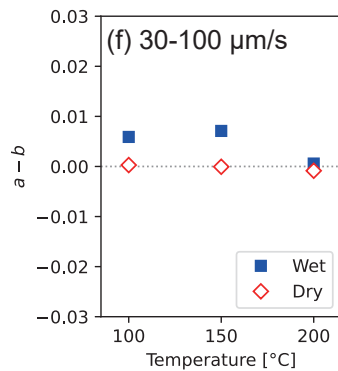
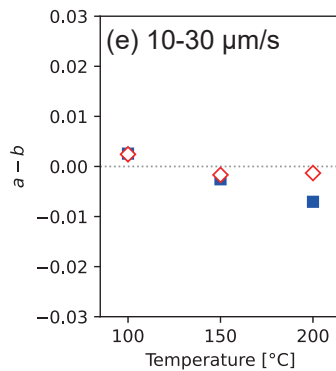
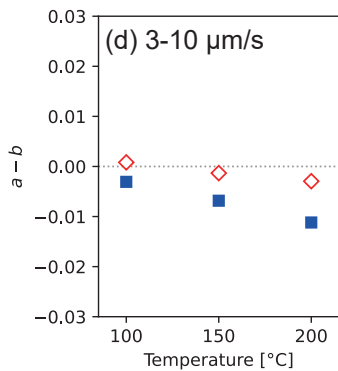
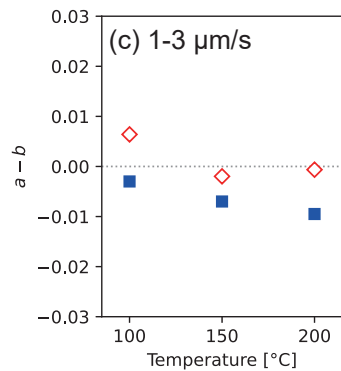
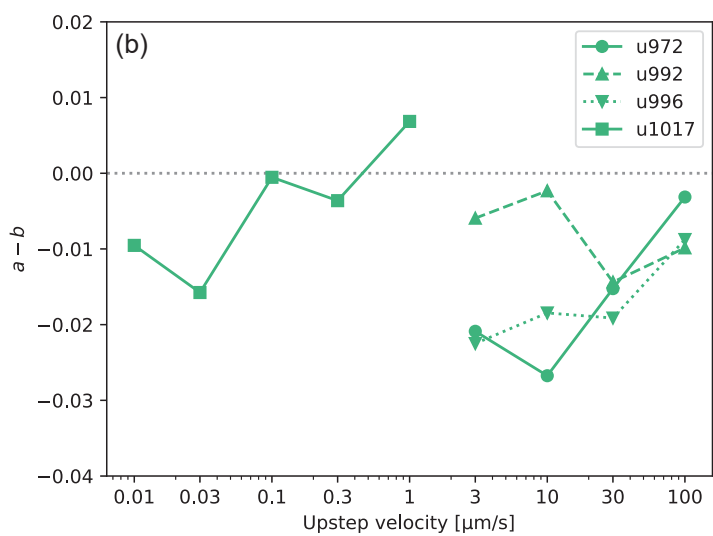
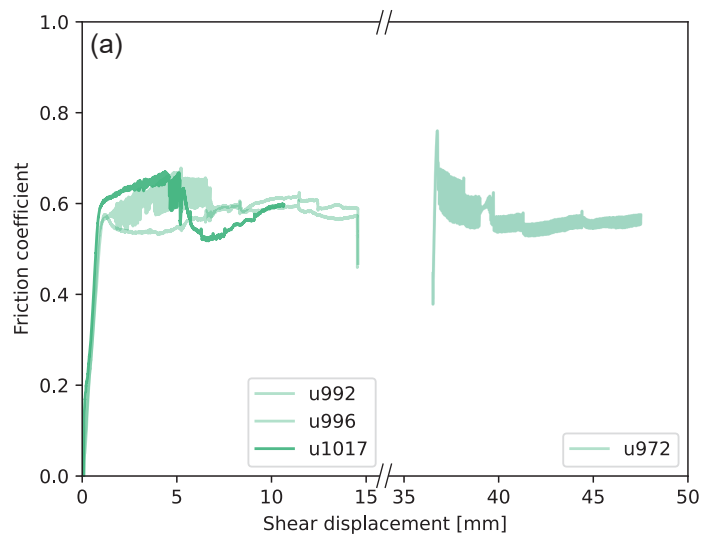
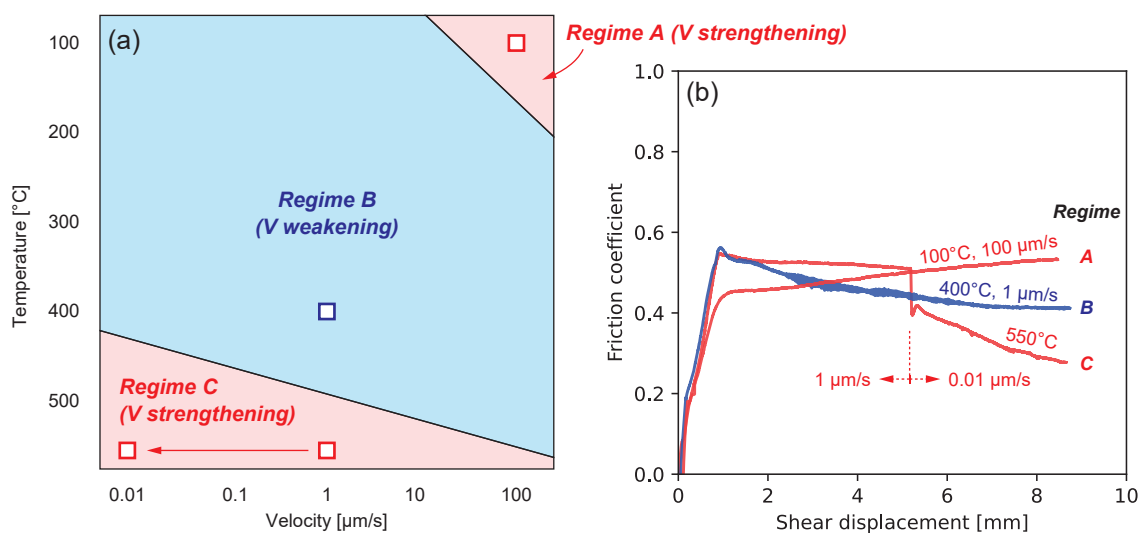
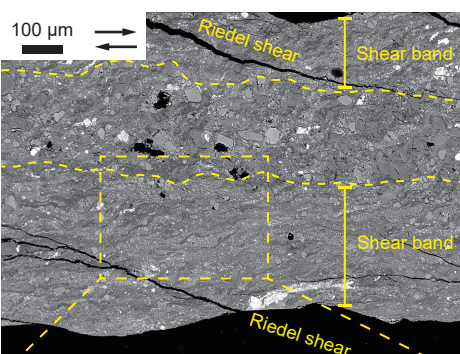


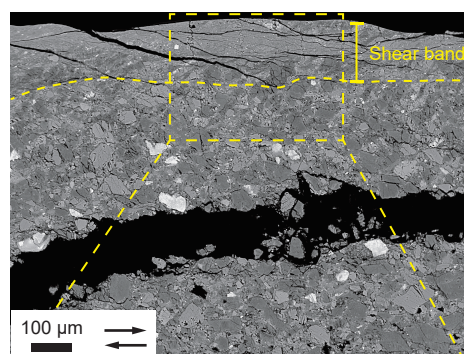
Figure 7.



(c) Regime A (100°C, 100 $\mu\text{m/s}$)



(d) Regime B (400°C, 1 $\mu\text{m/s}$)



(e) Regime C (550°C, 1–0.01 $\mu\text{m/s}$)

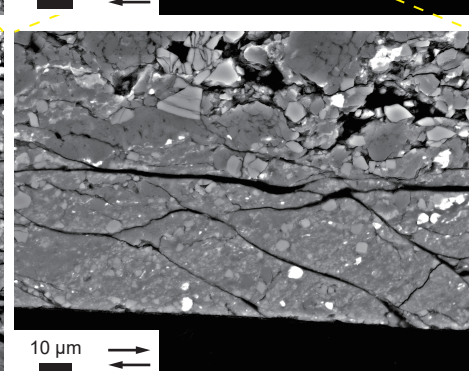
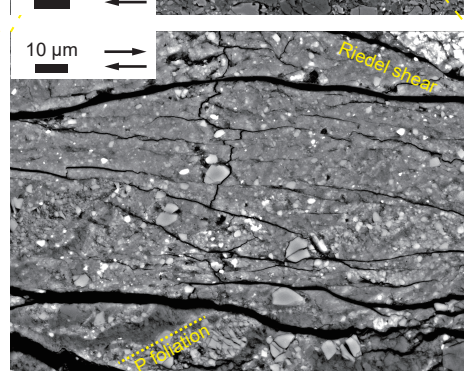
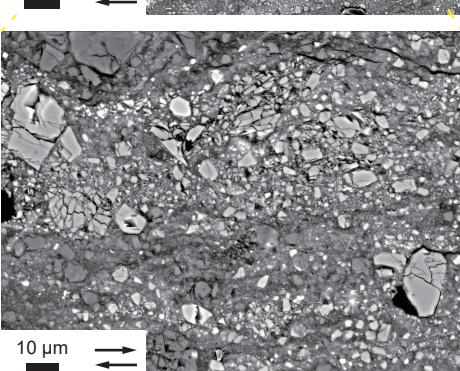
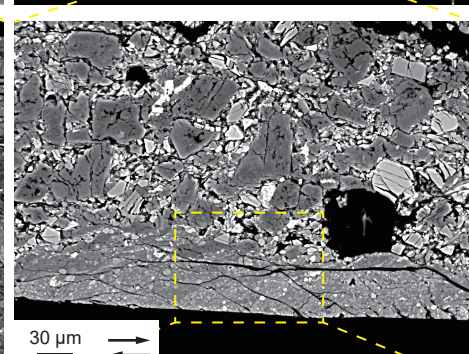
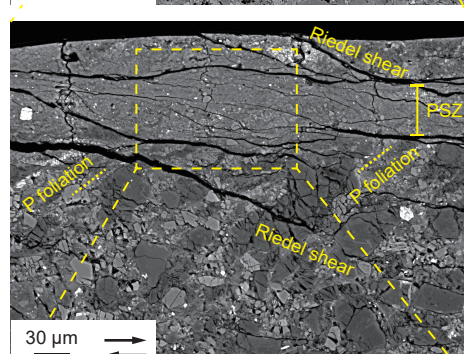
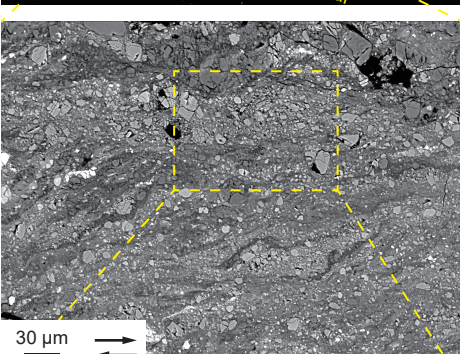
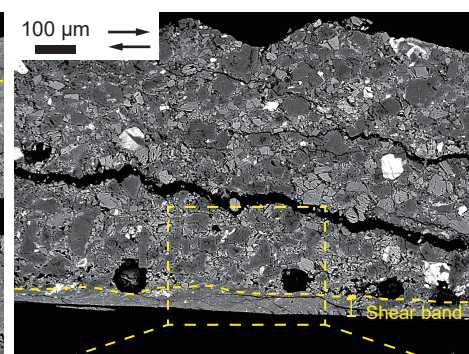


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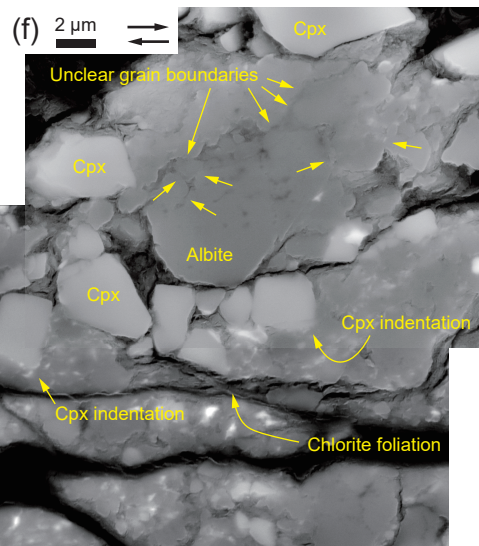
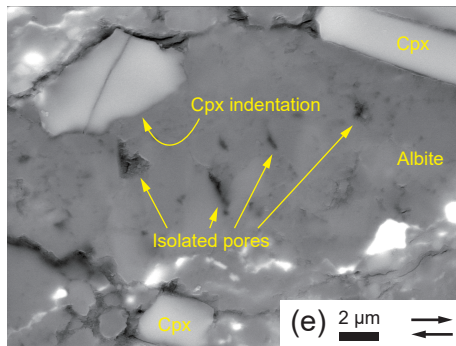
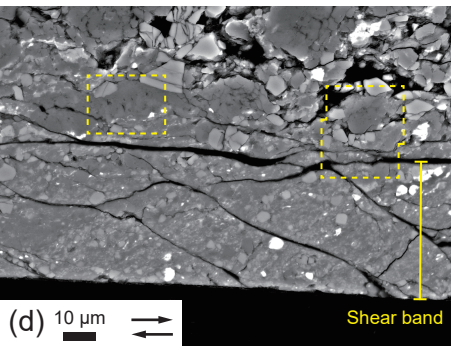
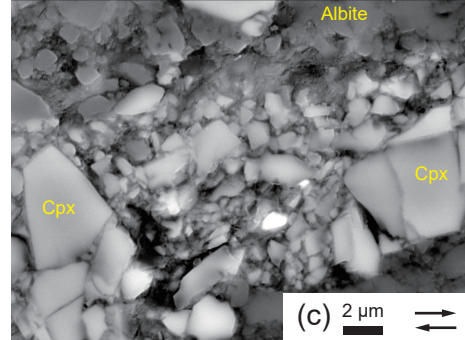
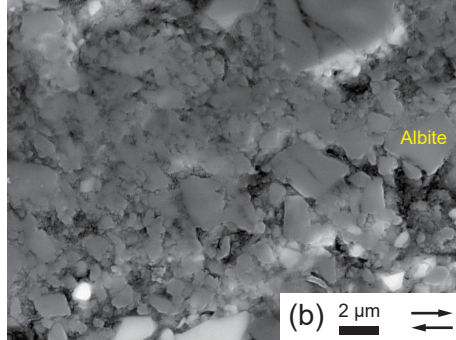
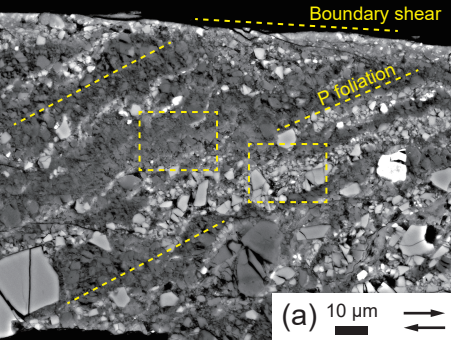


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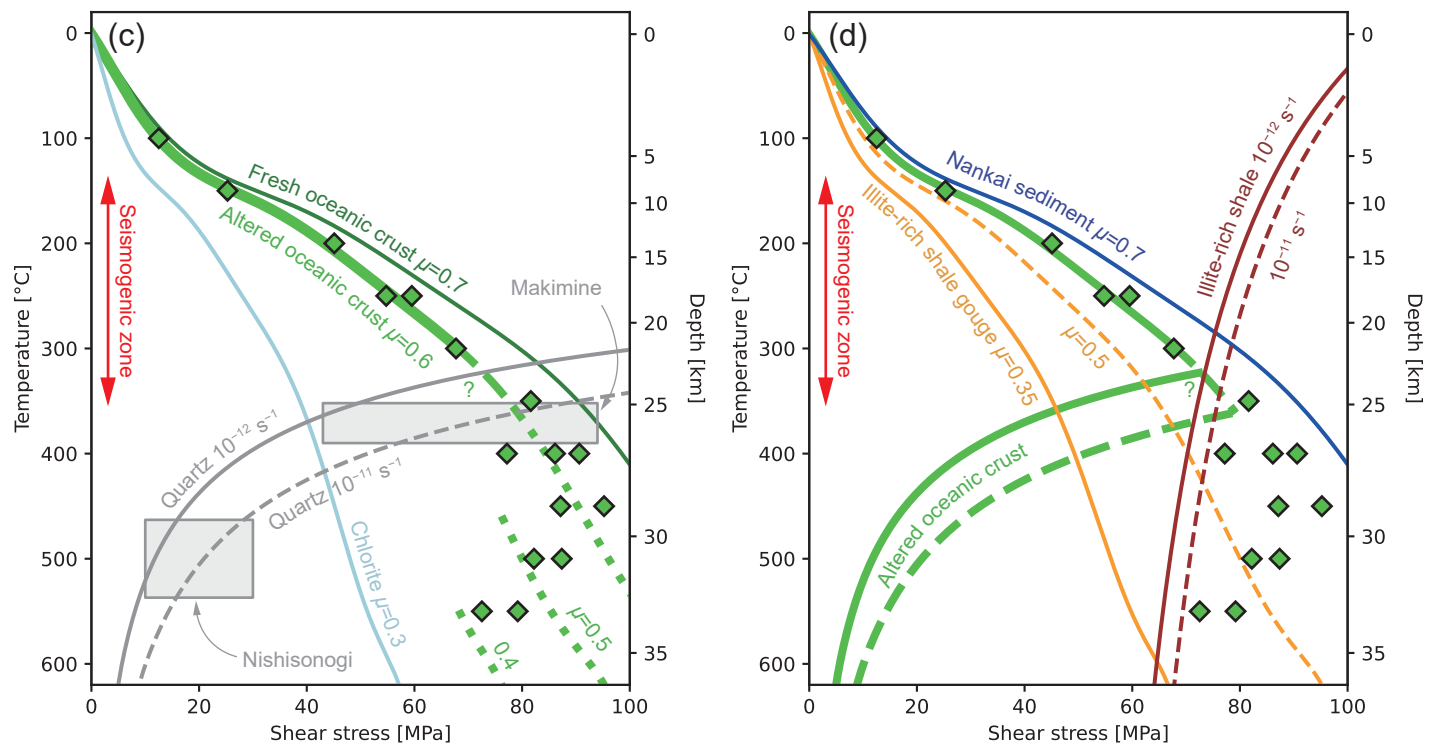
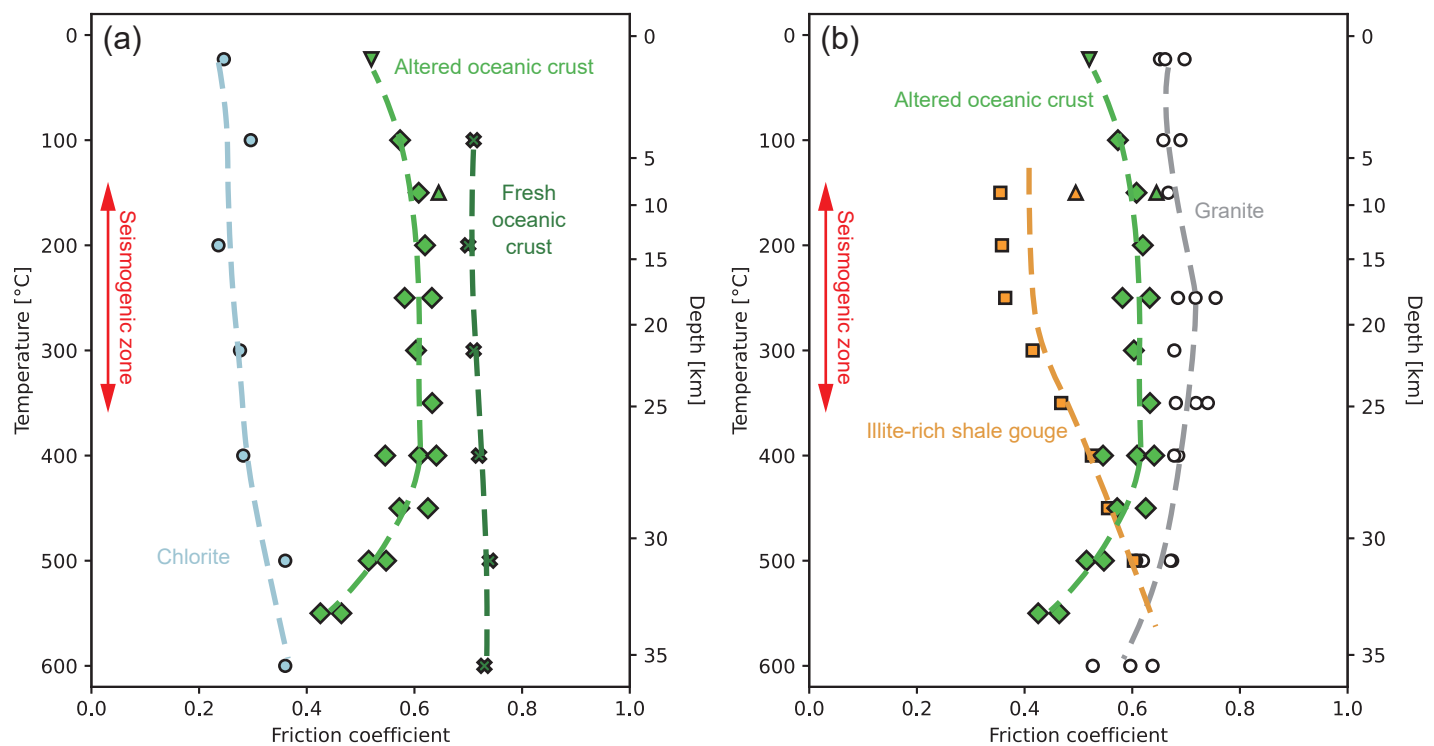
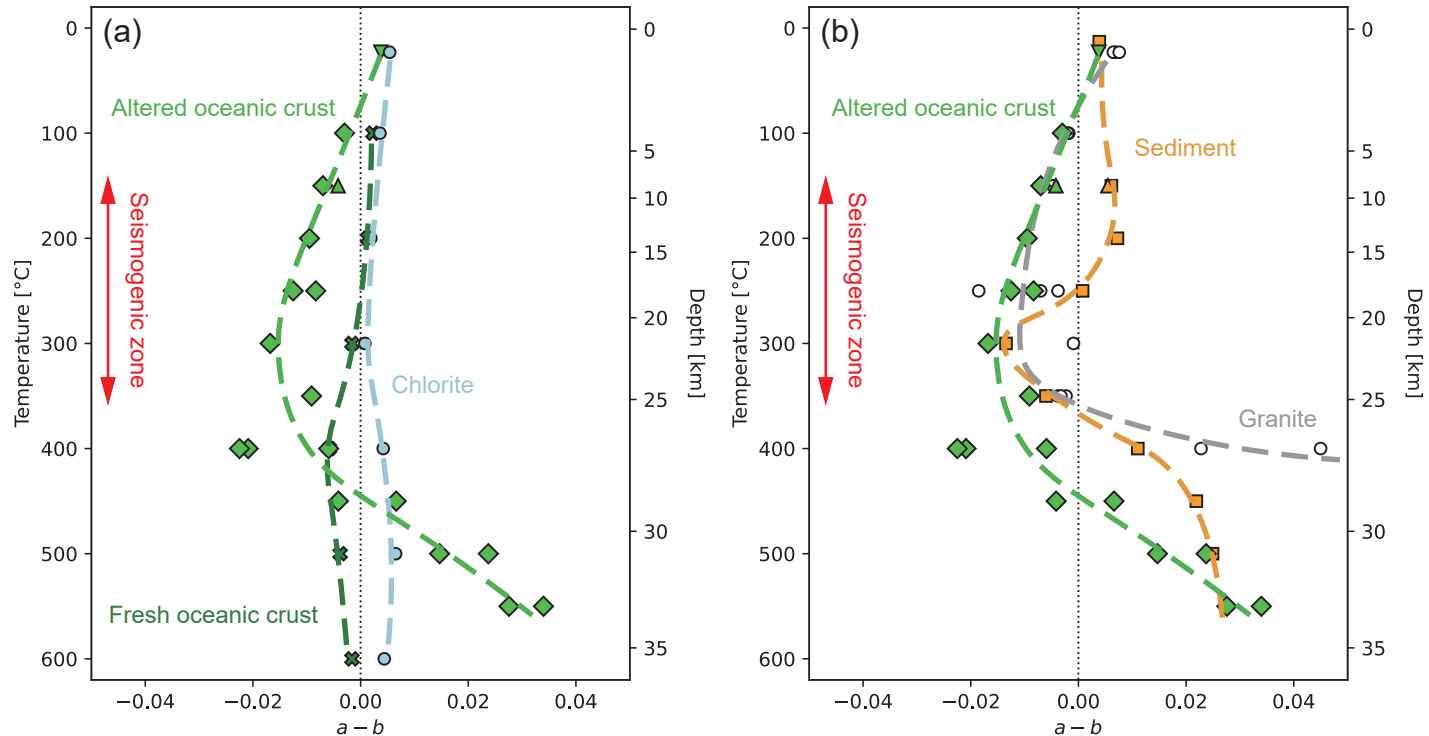


Figure 10.



- | | |
|--|---|
| ◆ Altered basalt gouge (This study) | ● Chlorite gouge (Okamoto et al., 2019) |
| ▼ Nankai basement gouge (Ikari et al., 2020) | ▲ Illite-rich shale gouge (Phillips et al., 2020) |
| ▲ Altered basalt gouge (Phillips et al., 2020) | ■ Illite-rich shale gouge (den Hartog, Niemeijer, et al., 2012) |
| ✱ Unaltered basalt gouge (Zhang et al., 2017) | ○ Granite gouge (Blanpied et al., 1995) |