Fault Zone Imaging with Distributed Acoustic Sensing: Body-to-Surface Wave Scattering

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Abstract

Fault zone structures at many scales largely dictate earthquake ruptures and are controlled by the geologic setting and slip history. Characterizations of these structures at diverse scales inform better understandings of earthquake hazards and earthquake phenomenology. However, characterizing fault zones at sub-kilometer scales has historically been challenging, and these challenges are exacerbated in urban areas, where locating and characterizing faults is critical for hazard assessment. We present a new procedure for characterizing fault zones at sub-kilometer scales using distributed acoustic sensing (DAS). This technique involves the backprojection of the DAS-measured scattered wavefield generated by natural earthquakes. This framework provides a measure of the strength of scattering along a DAS array and thus constrains the positions and properties of local scatterers. The high spatial sampling of DAS arrays makes possible the resolution of these scatterers at the scale of tens of meters over distances of kilometers. We test this methodology using a DAS array in Ridgecrest, CA which recorded much of the 2019 Mw7.1 Ridgecrest earthquake aftershock sequence. We show that peaks in scattering along the DAS array are spatially correlated with mapped faults in the region and that the strength of scattering is frequency-dependent. We present a model of these scatterers as shallow, low-velocity zones that is consistent with how we may expect faults to perturb the local velocity structure. We show that the fault zone geometry can be constrained by comparing our observations with synthetic tests.

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5	Key Points:
6	• We develop a framework for systematically locating fault zones at sub-kilometer
7	scales using the DAS-measured earthquake wavefield.
8	• We present a model for these fault zones and use simulations to show that this
9	model reproduces first-order observations of scattering.
10	• By comparing observations with synthetics, we use this method to constrain lo-
11	cal fault zone geometry.

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12 Abstract

Fault zone structures at many scales largely dictate earthquake ruptures and are con-13 trolled by the geologic setting and slip history. Characterizations of these structures at 14 diverse scales inform better understandings of earthquake hazards and earthquake phe-15 nomenology. However, characterizing fault zones at sub-kilometer scales has historically 16 been challenging, and these challenges are exacerbated in urban areas, where locating 17 and characterizing faults is critical for hazard assessment. We present a new procedure 18 for characterizing fault zones at sub-kilometer scales using distributed acoustic sensing 19 (DAS). This technique involves the backprojection of the DAS-measured scattered wave-20 field generated by natural earthquakes. This framework provides a measure of the strength 21 of scattering along a DAS array and thus constrains the positions and properties of lo-22 cal scatterers. The high spatial sampling of DAS arrays makes possible the resolution 23 of these scatterers at the scale of tens of meters over distances of kilometers. We test this 24 methodology using a DAS array in Ridgecrest, CA which recorded much of the 2019 $M_w 7.1$ 25 Ridgecrest earthquake aftershock sequence. We show that peaks in scattering along the 26 DAS array are spatially correlated with mapped faults in the region and that the strength 27 of scattering is frequency-dependent. We present a model of these scatterers as shallow, 28 low-velocity zones that is consistent with how we may expect faults to perturb the lo-29 cal velocity structure. We show that the fault zone geometry can be constrained by com-30 31 paring our observations with synthetic tests.

32 Plain Language Summary

Fault zones are multi-scale structures that govern where and how earthquakes hap-33 pen. Characterizing fault zones at all scales is thus important for understanding earth-34 quake ruptures and earthquake-related hazards. However, finding and describing fault 35 zones at small scales remains a persistent challenge in earthquake science. We propose 36 a framework for the characterization of fault zones using distributed acoustic sensing (DAS), 37 a recently developed technique that converts fiber optic cables into dense networks of 38 ground motion sensors. Earthquake waves are scattered when they encounter fault zones, 39 and this scattering creates signatures in DAS data that we can use to locate these fault 40 zones. Additionally, the behavior of fault zone scattered waves with frequency may il-41 luminate detailed characteristics of the fault zone. We test this framework using a DAS 42 network in Ridgecrest, CA that recorded aftershocks of the 2019 magnitude 7.1 Ridge-43 crest earthquake. We use these recordings to map fault zone locations near the network. 44 These locations are close to previously mapped faults but are more accurate. By com-45 paring the behavior of observed fault zone scattered waves with frequency with that of 46 simulations, we can constrain shallow fault zone geometry. 47

48 1 Introduction

The Earth's crust is a geologically heterogeneous medium that hosts myriad sharp 49 material contrasts at multiple scales. Among these heterogeneities are fault zones, fea-50 tures consisting of fault cores and surrounding zones of fracture that accommodate strain. 51 Finding new ways to locate and characterize fault zones may potentially serve a variety 52 of societally and scientifically important functions. Proximity to fault zones increases 53 the likelihood of severe damage to infrastructure, both because fault zones host static 54 deformation, and because fault zones may amplify ground motion (Kurzon et al., 2014). 55 56 Additionally, the locations of faults control estimates of fault connectivity, which is an important parameter in some probabilistic hazard estimates (Field et al., 2014). Relat-57 edly, relative fault positioning and fault geometry play a pivotal role in the propogation 58 and termination of earthquakes (Harris & Day, 1993, 1999; Wesnousky, 2008). Fault dam-59 age zone scaling is expected to play an influential role in earthquake nucleation (Ampuero 60 et al., 2002), earthquake potency (Weng et al., 2016), and long-term earthquake sequence 61 behavior (Thakur et al., 2020). Importantly, fault zones are multi-scale structures (Faulkner 62 et al., 2010), and thus developing a more complete picture of fault zone structure at sub-63 kilometer scales contributes to these efforts to evaluate earthquake hazard and geolog-64 ical controls on earthquake phenomenology. 65

Considerable attention is given to major fault zones, those that are large and ac-66 commodate significant strain. But, minor and unmapped fault zones are an important 67 consideration when evaluating the structural deformation and earthquake hazards in a 68 region. Plate deformation is usually not accommodated by a single fault zone, but rather 69 by a broad distribution of fault zones that extend sometimes hundreds of kilometers from 70 the plate boundary, and minor fault zones play a key role in the accommodation of this 71 strain (Scholtz, 2019). In the absence of high deformation rates, minor fault zones can 72 develop a high risk potential if strain accumulates over a long time period, the stress state 73 changes (Freed & Lin, 2001), or the stability of the fault is perturbed (Ellsworth, 2013). 74 Relatedly, many significant earthquakes rupture within minor or unmapped fault zones. 75 For example, the 2019 Ridgecrest earthquake sequence, which included the largest earth-76 quake to take place in California in over two decades, ruptured mostly unmapped faults 77 in the Little Lake and Airport Lake fault zones (Ross et al., 2019), which only accom-78 modated approximately 1 mm/y of slip (Amos et al., 2013). 79

For both major and minor fault zones, shallow fault zone structure is important. 80 The shallowest few hundred meters of fault zones can exhibit sharp and localized veloc-81 ity reductions (e.g. Zigone et al., 2019; Y. Wang et al., 2019; Share et al., 2020) that can 82 amplify ground motion, and shallow crustal faults play an important role in both facil-83 itating and impeding the transport of groundwater and hydrocarbons (Bense et al., 2013). 84 Shallow fault zone structure may also be used to infer the contribution of deep fault struc-85 ture, which is very difficult to constrain, by correcting for shallow structure contribu-86 tions in depth-integrated fault characterization approaches. 87

Previous efforts to locate and describe shallow fault zone structures at sub-kilometer 88 scales have typically relied on geologic mapping, seismic surveying, and satellite imagery. 89 Geologic mapping over decades has produced excellent records of Quaternary faults (e.g. 90 USGS & CGS, 2022), but discerning faults using geologic mapping requires careful field-91 work and evidence of faulting at the surface. Seismic surveying produces detailed im-92 ages of the subsurface, with which fault locations can be inferred (e.g. Liberty et al., 2021; 93 Lay et al., 2021), but surveys are often expensive and logistically challenging, particu-94 larly in urban settings. Satellite imagery is also used to map faults, often by identify-95 96 ing topographic anomalies in images (Joyce et al., 2009). More involved processing, such as producing phase gradient maps from InSAR interferograms (Xu et al., 2020), can also 97 be used to identify fractures. These techniques are powerful, but they require surficial 98 evidence of strain that can be imaged from above. 99

Other studies have used the earthquake wavefield to characterize the structure of 100 major fault zones. For example, some studies have used fault zone head waves, head waves 101 generated by refraction due to a bimaterial contrast across the fault, to image the fault 102 interface and constrain the velocity contrast across the fault (e.g. McGuire & Ben-Zion, 103 2005; Allam et al., 2014; Share & Ben-Zion, 2018; Qin et al., 2020). Additionally, some 104 studies have used travel-time anomalies from regional and teleseismic events to discern 105 properties like the width of the damage zone and the velocity reduction within the dam-106 age zone (e.g. Cochran et al., 2009; H. Yang et al., 2020; Qiu et al., 2021; Share et al., 107 2022). Moreover, low velocity structures can amplify ground motion, and some studies 108 have used S-wave amplification caused by the reduced velocities in fault damage zones 109 to delineate their structure (e.g. Qiu et al., 2021; Song & Yang, 2022). Another approach 110 is to use fault zone trapped waves, waves generated by constructive interference of crit-111 ically reflected waves in the fault damage zone, which can be initiated by sources out-112 side the fault zone (Fohrmann et al., 2004) and have been used to constrain the struc-113 ture of fault damage zones (e.g. Ben-Zion et al., 2003; Catchings et al., 2016; Y. Wang 114 et al., 2019; Qiu et al., 2021). In general, these techniques are highly effective tools for 115 capturing geometric and internal properties of major fault zones. But, fault zones usu-116 ally need to exhibit relatively large and spatially consistent elastic material contrasts for 117 these techniques to be used. Hence, these techniques are typically applied to major fault 118 zones using targeted deployments of dense networks of sensors. These factors make these 119 methods ineffectual for the discovery and characterization of minor fault zones. 120

The weaknesses of these methods motivate the development of complimentary tech-121 niques for identifying and characterizing sub-kilometer scale fractures in the crust. To 122 this end, we suggest an alternative method for identifying and characterizing fractures 123 in the crust using distributed acoustic sensing (DAS) data. DAS is an emergent tech-124 nology that repurposes fiber optic cables as dense arrays of strainmeters. DAS uses a laser 125 interrogator unit to emit pulses of light that probe a fiber optic cable, and natural im-126 perfections in the fiber send echoes back to the interrogator unit. Perturbations of the 127 fiber change the travel times of these echoes, and these changes in travel time are quasi-128 linearly proportional to the strain induced by the perturbations. The high spatial fre-129 quency of DAS data allows for the resolution of high wavenumber phenomena that are 130 incoherent in more sparsely measured data, which is useful for characterizing fault zones 131 at high resolution (Jousset, 2019). One such phenomenon is the scattering of earthquake 132 body waves to surface waves due to small-scale, local heterogeneities in the upper crust. 133 We show an example of this scattering in Figure 1, and we subsequently refer to these 134 features as chevrons, owing to their chevron-like shape in DAS data representations. These 135 chevrons have been observed in other DAS datasets, and the scatterers generating these 136 chevrons have been inferred to be faults (Lindsey et al., 2019; Spica et al., 2020). More-137 over, these scattered surface waves are also visible in empirical Green's functions derived 138 in DAS datasets that can be migrated to infer scatterer locations (Cheng et al., 2021; 139 Y. Yang, Zhan, et al., 2022). 140

Our contributions in this paper are as follows. We suggest a local backprojection framework for the systematic location of the sources of these chevron-like features and find a strong spatial correlation between these locations and mapped faults. We suggest a model of these scatterers as rectangular perturbations in the velocity field, approximating a fault zone, and show that this model reproduces first-order features observed in the data. We then show that we can constrain key geometric features of the fault zone under this backprojection framework.

148 2 Data

In early July 2019, a large earthquake sequence initiated in the Eastern California Shear Zone. This sequence, which included a $M_w 6.4$ foreshock and a $M_w 7.1$ mainshock, produced thousands of aftershocks over the course of a few months. Shortly fol-

lowing the mainshock, a DAS array was deployed in Ridgecrest, CA using an Optasense 152 ODH3 interrogator unit in an effort to record this aftershock sequence (Li et al., 2021). 153 This DAS array began recording on July 10, 2019, and in this study we use recorded af-154 tershocks that took place between the initiation of recording and October 4, 2019. The 155 array is temporally sampled at 250 Hz and is spatially sampled at 8 m intervals over 1250 156 channels, with a total cable length of 10 km. The deployment of this DAS array ensured 157 that numerous Ridgecrest sequence aftershocks were recorded nearby at a high spatial 158 frequency. 159

160 For this study, we choose a subset of well-recorded, low-noise earthquakes on which we perform our subsequent analysis. We choose these earthquakes using straightforward 161 quality control metrics to ensure that scattered surface waves have a high enough signal-162 to-noise ratio to be reliably analyzed and that the scattered surface waves are isolated 163 from any cultural noise that may bias the analysis. As part of this quality control, we 164 select from only events with $M_1 > 2$ or $M_w > 2$ as determined by the Southern Cali-165 fornia Seismic Network catalog. We also restricted our selection to only events that oc-166 curred between 11 pm and 4 am local time, thus only keeping events with a low prob-167 ability of being partially masked by cultural noise. We then manually inspected all of 168 the remaining events and ensured that we only kept events with negligible cultural noise. 169 After performing this processing, we are left with 50 events that meet our quality con-170 trol criteria. These events are plotted in geographic context in Figure 1. These events 171 are reasonably well clustered by distance and azimuth, minimizing variability due to the 172 directional sensitivity of DAS. 173

¹⁷⁴ 3 Mapping faults using local backprojection

To quantify the magnitudes and locations of these scatterers, we employ a simple 175 local backprojection technique to identify the locus points of the scattered waves in the 176 body wave coda. This backprojection is based on the reasonable assumption that these 177 chevron-like waves are surface waves generated by earthquake body waves impinging on 178 a scatterer near the DAS array. We expect this phenomenon to be body-to-surface wave 179 scattering because the scattered waves are dispersive, which we verify subsequently, and 180 the onset of these waves occurs early in the body wave coda. We expect these scatter-181 ers to be local because the scattered waves attenuate rapidly in space, as exemplified by 182 the narrow width of these chevrons shown in Figure 1. A schematic example of the gen-183 eration of these scattered waves is shown in Figure 2. The driving principle of this method-184 ology is the same for standard backprojection techniques used in seismology (Kiser & 185 Ishii, 2017). In particular, for grid points near or above a scatterer, the backscattered 186 energy resultant from the scatterer will align and sum coherently, producing a larger am-187 plitude than that of a grid point far from any scatterers. In this case, we attempt to back-188 project locally scattered surface waves to image the scattering source, illustrated as a 189 fault zone in Figure 2. 190

To accomplish this backprojection, we first bandpass our data to a narrow frequency 191 band; this frequency band can vary depending on the desired dimensional sensitivity. We 192 select frequency bands with 1 Hz widths and center frequencies spanning 2-10 Hz at 0.5193 Hz intervals. For each of these frequency bands, we partition the earthquake wavefield 194 by velocity in the curvelet domain (Atterholt et al., 2021), using a curvelet basis to mute 195 sections of the frequency-wavenumber domain and thus isolate desired wavefield com-196 ponents. This is equivalent to frequency-wavenumber filtering with specialized tapers that 197 minimized velocity filtering artifacts. We use this wavefield-partitioning technique to sep-198 arate the scattered wavefield and the direct waves into two separate windows. We clas-199 sify velocities below 750 m/s to be the scattered wavefield and velocities above 1000 m/s 200 to be the direct wavefield. Of the scattered wavefield, we select only the scattered waves 201 from the early-onset body waves, because these early-onset scattered waves are typically 202 more pronounced relative to the earthquake wavefield and are not convolved with earthquake-203



Figure 1. Top: The geographic setting of the data used in this study. Blue line corresponds to the DAS array. Red dots correspond to the epicenters of the events used in this study. Yellow star corresponds to the epicenter of the event shown below (depth 5.6 km). Green lines correspond to the USGS-mapped Quaternary faults in the area. Bottom: Example of the DAS-measured wavefield of the onset of an event used in this study. Black dotted lines correspond to the locations of the chevron-like features that are mapped in Figure 3.



Figure 2. Schematic illustration of the phenomena observed in the earthquake wavefields used in this study. Top: Record section corresponding to the processes illustrated below. Bottom: Illustration of the phenomena resulting in the generation of the chevron-like features shown in Figure 1. Colors represent the same phenomena in both top and bottom. Green corresponds to incident body wave. Gray features indicate a fault zone. Purple corresponds to the scattered surface waves resulting from the body waves impinging on the fault zone. Orange line and triangles indicate the fiber optic cable and stations, respectively. Blue box represents the DAS interrogator unit.

generated surface waves, which can bias the final result. To isolate the early-onset scat-204 tered waves, we window the scattered wavefield over the time interval between 2 seconds 205 prior to the onset of the P-wave and 5 seconds after the onset of the P-wave. Once we 206 have isolated the scattered waves, we perform a local backprojection of surface wave en-207 ergy according to a local velocity model across the array. For the local velocity model, 208 we use a 1-dimensional velocity model made by taking averages of each period of the ve-209 locity model developed by Y. Yang, Atterholt, et al. (2022). We perform this averaging 210 to avoid biasing of the result due to lateral slopes in the model. We then define a grid 211 of potential scattering sources along the array geometry, and we backproject the surface 212 waves recorded by the surrounding channels, up to a fixed distance, according to their 213 distance from the potential source. Our grid of potential source locations is spaced at 214 8 m along the array, which coincides with the station spacing. In this study, by inspect-215 ing the data, we fix the maximum distance to be 250 m based on the expected distance 216 from the chevron center over which we can expect to get significant constructive inter-217 ference by aligning the waveforms. We then stack the backprojected channels and sum 218 the absolute value of the stack, giving us an amplitude for the grid point. We only de-219 fine the grid at the surface along the array, because linear DAS array geometry poorly 220 constrains backprojection images along orthogonal axes. But, the rapid attenuation of 221 these surface waves suggests that most of the energy in the scattered wavefield is gen-222 erated very close to the array, minimizing the consequence of this poor constraint. Fur-223 thermore, scattered waves from more distant scatterers will have higher apparent veloc-224 ities, minimizing the impact of these scatterers in a backprojection framework that uses 225 true velocity. 226

We can verify that these scattered waves are dispersive under this framework. That is, we apply this backprojection framework to the earthquake wavefield shown in Fig-

ure 1 over a range of velocities for each frequency, rather than using a single velocity model. 229 We can then sum across each resultant profile to get a single value for each frequency 230 and velocity pair. From this we can determine which velocities produce the largest sum 231 at each frequency, which we expect to be correlated with the amount of constructive in-232 terference due to waveform alignment. In this way we can construct a dispersion curve 233 using only the scattered wavefield. This is a similar approach to that taken by Spica et 234 al. (2022), but because we sum across the entire profile, this produces a velocity spec-235 trum that averages the contributions of the scattered waves produced across the array. 236 A plot of this velocity spectrum is shown in Figure S1. This spectrum shows a clear dis-237 persion pattern that is well matched by the dispersive relationship for this setting com-238 puted in Y. Yang, Atterholt, et al. (2022). 239

Since DAS measures longitudinal strain, which is distinct from conventional iner-240 tial seismometers, the sensitivity of DAS to these scattered waves is also distinct. For 241 surface waves generated by scattering from a fault that runs orthogonal to the array, the 242 recorded surface waves will propagate parallel to the fiber. Consequently, a significant 243 component of the particle motion will be parallel to the fiber, motion to which DAS is 244 most sensitive. For a fault that runs oblique to the array, the surface waves will not prop-245 agate exactly parallel to the fiber, and the apparent velocity will increase and the sen-246 sitivity of the DAS array to the waves will decrease. However, since these waves atten-247 uate rapidly in space, the majority of the recorded energy will have been scattered very 248 close to the array, minimizing variability due to obliquity. Additionally, because DAS 249 is more sensitive to lower velocities, surface waves are amplified in DAS data relative to 250 the other components of the earthquake wavefield. This potentially explains why these 251 surface waves are such a common and well-recorded observation in DAS data (e.g. Lind-252 sey et al., 2019; Spica et al., 2020; Ajo-Franklin et al., 2022). These factors suggest that 253 the variability in scattered waves measured across the DAS array is largely due to vari-254 ability in the strength and geometry of the scatterers near the array. Additionally, be-255 cause we're using array seismology, we need to consider apparent velocity when perform-256 ing velocity filtering and backprojecting these waves. But, since the recorded surface waves 257 propagate approximately parallel to the fiber, the apparent velocity of locally scattered 258 surfaces waves is very close to the true velocity. In particular, the apparent velocity fol-259 lows $v_t/\cos(\theta)$; where v_t is the true velocity and θ is the incident angle relative to the 260 array geometry. In the case of surface waves scattered very close to the array, θ is close 261 to zero. 262

We apply this backprojection technique to the 50 high quality events recorded by 263 the DAS array in Ridgecrest, CA described in the preceding section. Backprojecting the 264 scattered wavefields of these earthquakes results in an ensemble of profiles of scattering 265 across the Ridgecrest DAS array. To ensure that the within-array and between-event am-266 plitudes are comparable, we normalize the profile amplitudes by the sum of the abso-267 lute value of the body waves that occupy the same window used for each grid point in 268 each profile. For this normalization, we account for the variability in azimuth and in-269 cident angle according to the directional sensitivity of strainmeters (Benioff, 1935). In 270 particular, noting that the dominant body wave signal we use for this normalization is 271 the P-wave, we divide the direct wavefield by $\cos^2(\theta)$. We smooth these profiles with a 272 Gaussian kernel with a standard deviation of 5 channels to minimize any high-frequency, 273 stochastic variability in these profiles. We show these ensembles of backprojection pro-274 files computed at 4 and 7 Hz center frequencies in Figure 3. These profiles are generally 275 "bumpy," and it can be difficult to determine to which of these peaks to assign signif-276 icance. Additionally, some peaks are of low amplitude, but are noteworthy because they 277 are positioned in areas with low noise floors. To help us determine which peaks are most 278 likely associated with scatterers, we use the metric from mountaineering of topographic 279 prominence, which is a measure of the height of a peak relative to its surroundings. We 280 plot the prominence profiles alongside the backprojection amplitude profiles in Figure 281 3. Additionally, we superimpose these prominence profiles on the DAS array geometry 282



Figure 3. Left: Backprojection profiles made using 50 events recorded by the DAS array in Ridgecrest, CA. Light blue lines correspond to profiles made using a single event. Dark blue lines correspond to the mean profile. Orange lines correspond to the topographic prominence of the mean energy profile. Top and bottom plots correspond to profiles generated with 4 and 7 Hz center frequencies, respectively. Black arrows point to referenced peaks α , β , γ , and ϕ . Right: Prominence profiles to the left, convolved with Gaussian kernel to widen peaks for representation, plotted on the DAS array geometry shown in Figure 1. Color corresponds to prominence amplitude. Green lines correspond to fault locations. Solid lines are moderately or well constrained fault locations, and dotted lines are inferred fault locations. Faults are labeled according to associated peaks indicated in the profiles to the left. Curved black arrows indicate the proposed relocation of the fault associated with peak α .

in Figure 3. Indeed, there is a spatial correlation between peaks in the prominence pro-283 file and the locations of USGS-mapped Quaternary faults near the array. This spatial 284 correlation partially evidences the argument that the nearly ubiquitous chevron-like fea-285 tures in the DAS measured wavefield are fault-zone scattered waves. In Figure 3, we make 286 note of four peaks, which we term peaks α , β , γ , and ϕ . These are the most prominent 287 peaks in both frequency bands, and by visual inspection we can associate these peaks 288 with mapped faults nearby. In particular, peaks α and β are noteworthy in that they 289 are prominent enough that we can analyze their behavior with space and frequency. We 290 use peaks α and β to infer properties of the associated fault zones subsequently. 291

²⁹² 4 Modeling scatterers as fault zones

To further investigate the nature of the sources of scattering evident in DAS data, 293 we present a model for these scatterers as rectangular perturbations in the 2D velocity 294 structure. Although natural faults are neither perfect rectangles nor uniform velocity per-295 turbations, this simple parameterization allows us to capture first order structural prop-296 erties of fault zones without including more complexity than we can feasibly resolve given 297 our data. The few free parameters of this fault model are burial depth, maximum depth, 298 width, and percent change in velocity. For a background velocity model, we use a com-299 bination of the aforementioned shear wave velocity model from Y. Yang, Atterholt, et 300 al. (2022) for the shallowest 150 m and a local 1D velocity profile taken from the SCEC 301 Unified Community Velocity Model (Small et al., 2017) for depths deeper than 150 m; 302 we combine these two models using a linear interpolation. We then create a model fault 303



Figure 4. Left: Example of velocity model modified from (Y. Yang, Atterholt, et al., 2022) and (Small et al., 2017) with two fault zone-approximating velocity perturbations emplaced in the model. Green line corresponds to array of strainmeters. Black arrows point to incident wave direction and fault locations. Note the large vertical exaggeration. Right: Record section generated from scenario illustrated to the left.

zone by multiplying a section of the background model with an assigned rectangular geometry by a constant of proportionality.

We then use this model to perform synthetic tests that we can compare to our ob-306 servations to assess the feasibility of this scatterer model. We generate these synthet-307 ics using Salvus (Afanasiev et al., 2019), a full waveform modeling software that simu-308 lates wave propagation using the spectral element method. We approximate the DAS 309 array at Ridgecrest as a linear, 8 km array of strainmeters at the surface of our Earth 310 model. We emplace a 2D double couple source with a 0.1 s half-duration Gaussian rate 311 source time function 30 km east of the array at 10 km depth, a representative distance 312 and depth for the earthquakes used in this study. We generate an adaptive mesh with 313 which we can compute these synthetics up to 10.5 Hz with at least one element per wave-314 length. We use the same setup to perform tests of the fault geometry that we describe 315 subsequently. We show an example of a simulation for a model with two faults with dif-316 ferent geometries and velocity reductions in Figure 4. The faults in Figure 4 were pa-317 rameterized using models for the faults associated with scatterers α and β that are pro-318 posed in the subsequent section. In particular, the fault on the left is parameterized as 319 a 30% velocity reduction with a width of 20 m and a depth extent of 10 to 60 m. The 320 fault on the right is parameterized as a 10% velocity reduction with a width of 50 m and 321 a depth extent of 0 to 50 m. Both fault parameterizations are vertical. The resultant scat-322 tered waves in the synthetic wavefield match many of the first-order characteristics of 323 the scattered waves in the observations of Figure 1. In particular, we have reproduced 324 the observation of low-velocity scattered surface waves emanating from a narrow source. 325 We can evaluate the similarities in the velocity content of the synthetic data and the ob-326 served data by computing the velocity spectrum of the scatterer component of the syn-327 thetic wavefield, as outlined in the preceding section. We show the velocity spectrum in 328 Figure S2. The dispersion of the scattered wavefield in the synthetic test is a close match 329 to the dispersion for the real data in Figure S1. These simulations thus further confirm 330 that these scatterers may be related to faults. As is clear in Figure 4, variations in the 331 properties of the model fault zones create visually apparent differences in the strength 332 of the scattered wavefield. 333

³³⁴ 5 Constraining fault geometry

Now that we have a method of quantifying the degree of scattering in data and a 335 means of simulating our observations using a reasonable model, we can constrain the prop-336 erties of the sources of scattered waves by comparing features between the data and syn-337 thetics under this backprojection framework. As is evident in Figure 3, the peaks in these 338 backprojection profiles have variant properties in space and frequency, and this variabil-339 ity may inform a better understanding of the faults that generate these peaks. Moreover, 340 since we performed this backprojection for many events, we have an ensemble of profiles 341 342 with which we can evaluate how well constrained the fault-zone properties that control these peak shapes are. 343

To generate our synthetics, we use the velocity model and source described in the 344 preceding section. We also incorporate attenuation into our model. Since we do not have 345 a priori estimates of the attenuation at this site, we parameterize the attenuation using 346 the functional decay of the peaks from our backprojection profiles to obtain a rough es-347 timate of the local attenuation structure. We assume an empirical relationship between 348 shear wave velocity and attenuation structure, a common assumption when building an 349 Earth model with heterogeneous attenuation structure (Graves & Pitarka, 2010), and 350 may be denoted as $Q_{\mu} = cV_s$. To test the attenuation of surface waves away from a lo-351 cal scatterer, we define a fault zone according to the aforementioned simplified fault model 352 with a width of 20 m, a depth extent of 0-100 m, and a 30% velocity reduction. We test 353 several values for c and compare the spatial decay of the resultant synthetic peaks to those 354 of peaks α and β at 4 Hz. We find that the data are best fit by a value of c = 50, a rea-355 sonable value for this relationship (Lin & Jordan, 2018; Lai et al., 2020). These peak com-356 parisons are shown in Figure S3. This empirical relationship between attenuation and 357 velocity is imperfect, as other parameters such as temperature and fluid content also con-358 trol attenuation (Brocher, 2008; Eberhart-Phillips et al., 2014), and other factors such 359 as structural heterogeneity can control surface wave amplitude (Bowden & Tsai, 2017). 360 But, since we are only trying to obtain a reasonable attenuation parameterization for 361 our forward model, this approximation is sufficient for our purposes. 362

To constrain the local fault zone properties, we note that the backprojection pro-363 files shown in Figure 3 are functions of the frequency band in which we filter the data, 364 and that each peak behaves differently with frequency. We investigate this property by 365 evaluating the backprojection profiles for all narrow frequency bands for which we computed profiles in this study, with center frequencies ranging from 2 to 10 Hz. By plot-367 ting the mean profiles at each center frequency together, we can better inform our un-368 derstanding of the behavior of the frequency dependence of individual scattering features 369 along the array. We plot these mean profiles against center frequency and distance as 370 a pseudocolor plot in Figure 5. As is evident in Figure 5, there are peaks that are trace-371 able across a range of center frequencies, and there is a high degree of variability in the 372 behavior of these peaks with frequency. 373

We then focus on the two most prominent peaks in this image, peak α and peak 374 β , both of which are spatially correlated with USGS-mapped faults (USGS & CGS, 2022). 375 By taking cross sections of the center frequency versus distance along array plot, we can 376 determine the frequency dependence of these specific scatterers along this profile. Clearly, 377 these peaks have different frequency dependences, which likely reflects a variability in 378 the depth and geometry of the scattering fault zone. To discern the properties of these 379 faults, we test different fault zone geometries to match these frequency dependent trends. 380 Because the amplitudes of DAS data are not well understood, we only attempt to match 381 382 the shape of the synthetic profile with the shapes of the peak profiles, and we thus normalize the synthetic profile amplitude by the ratio of the integrated amplitude of the mean 383 peak profile to the integrated amplitude of the synthetic peak profile. We attempted to 384 reproduce these frequency-amplitude trends by performing synthetic simulations that 385 included fault zones with varying free parameters. These simulations were too expen-386



Figure 5. A. Pseudocolor plot of mean backprojection amplitude plotted against center frequency and distance along array. Dotted green and dotted blue lines correspond to cross sections of this plot, associated with peaks α and β , respectively. B. Plots of backprojection amplitude versus center frequency for the cross-sections shown in A. Light green and light blue lines are the frequency-amplitude curves determined for a single event for peaks α and β , respectively. Dark green and dark blue lines are the mean frequency amplitude curves for peaks α and β , respectively. Dotted black lines correspond to the frequency-amplitude curves for our preferred fault zone model for each peak. Dotted colored lines are frequency amplitude curves for fault zone models with variant parameters to illustrate the constraints of this methodology. The parameters used for each model are given in Table S1. The asterisk in the legend indicates that, for visualization purposes, the corresponding model is normalized by the maximum height of the data curve rather than the integrated sum.

sive to perform a full grid search over all the fault model parameters, but by identify-387 ing patterns between fault zone parameterizations and subsequent simulated frequency-388 amplitude profiles, we were able to find fault zone models that produced good fits to the 389 profile ensembles for both faults, as shown in Figure 5B. Indeed, reproducing the frequency-390 amplitude curves for the different peaks requires the use of variant fault zone parame-391 terizations. Peak α is best fit by a 30% velocity reduction that is 20 m wide and spans 392 10 to 60 m depths. Peak β is best fit by a 10% velocity reduction that is 50 m wide and 393 spans 0 to 50 m depths. The results for peak α suggest that we may be able to detect 394 and constrain properties of small-scale buried faults. 395

396 6 Discussion

The spatial correlation between the locations of sources of scattering and the mapped 397 faults near the Ridgecrest DAS array shown in Figure 3 suggests that the source of at 398 least some of these scatterers are faults, and thus DAS arrays can detect measurable sig-399 natures of fault zones. An example of the potential utility of this technique is readily avail-400 able in this dataset. In particular, peak α is located near, but is offset from, a mapped 401 fault extending across the array. The Quaternary Fault Catalog (USGS & CGS, 2022) 402 records this fault's location as inferred rather than directly observed; thus, we can use 403 our backprojection profile to refine the location of this fault, treating peak α as a po-404 tential node of the fault trace. This node provides a stronger constraint on this fault's 405 location near the town of Ridgecrest, CA, which has important implications for the lo-406 cation of possible static strain in the event of the activation of the Little Lake Fault Zone. 407 This technique is generalizable to all DAS arrays that record seismicity, and may then 408 be used elsewhere to systematically refine inferred fault locations and suggest the pres-409 ence and locations of previously unmapped faults. 410

The profiles in Figure 3 bear a resemblance to results from distinct fault zone char-411 acterization methodologies, namely S-wave amplification analysis (e.g. Qiu et al., 2021). 412 Both techniques can be used to locate faults at small spatial scales using the peak lo-413 cations, but these techniques otherwise provide complimentary information. For exam-414 ple, the shape of the peaks in S-wave amplification profiles can be interpreted as an es-415 timate of the lateral characteristics of the fault damage zone, while the shape of the peaks 416 in this study are largely reflective of the processing workflow and amplitude attenuation. 417 But, the methodology presented in this study is more sensitive to small variations in the 418 frequency of scattered waves that are reflective of characteristic dimensions of the fault 419 zone, which includes constraints on the depth-dependence of the fault zone. Addition-420 ally, the methodology presented in this study is more readily applicable to DAS, both 421 because DAS amplitudes are not well understood due to variability in coupling of the 422 fiber and because DAS is particularly sensitive to low velocity surface waves. 423

The synthetic simulations in this study provide additional evidence that these chevron-424 like observations in DAS data are well-explained by fault zones. In particular, as shown 425 in Figure 4, an approximation of a fault zone as a rectangular perturbation in velocity 426 reproduces the first order features of these chevron-like observations. Additionally, the 427 complexity in the frequency-amplitude curves shown in Figure 5 evidences a necessary 428 variability in the finite properties of the scattering fault zones (Almuhaidib & Toksöz, 429 2014). But, importantly, this representation is non-unique, and the diversity of geologic 430 heterogeneity in the upper crust suggests that features other than fault zones are likely 431 responsible for at least some of the chevron-like observations we see in DAS data. 432

⁴³³ The geometric constraints we place on the faults in this study illustrate that, us-⁴³⁴ ing DAS recorded earthquakes, we can constrain some aspects of the subsurface geom-⁴³⁵ etry of fault zones on the scale of tens of meters, potentially even for buried faults as is ⁴³⁶ the case for peak α . Although these solutions are non-unique, they provide robust con-⁴³⁷ straints on the approximate scaling of these subsurface structures. As stated prior, we

were able to approach fault models that fit these data by identifying patterns in the re-438 lationship between fault zone geometry and the resultant synthetics. One interesting re-439 lationship, made clear in Figure 5, is related to the observation that peak β has a uni-440 modal frequency-amplitude curve while peak α has a bimodal frequency-amplitude curve. 441 The simulations suggest that two characteristic lengths produce distinct modes in these 442 frequency-amplitude curves: the fault zone width and the fault zone depth extent. In 443 particular, we obtain a unimodal frequency-amplitude curve when these lengths are the 444 same (as with peak β) and a bimodal frequency-amplitude curve when these lengths are 445 distinct (as with peak α), with the smaller characteristic dimension responsible for the 446 highest frequency mode and vice versa. We demonstrate that variant characteristic di-447 mensions can account for each frequency mode of peak α by running separate simula-448 tions for square-shaped buried faults, with velocity perturbations equivalent to the best 449 fitting model for peak α , that extend up to 10 m depth with side lengths of 50 m and 450 20 m, lengths which match the depth extent and width, respectively of the best fitting 451 model for peak α . The amplitude-frequency curves of these simulations are plotted as 452 Models 1 and 2 in Figure 5, respectively. Both of these models well approximate one of 453 the individual modes of the bimodal data curve for peak α . Finally, although we nor-454 malize by amplitude, the magnitude of the velocity perturbation subtly changes the shape 455 of the synthetic curves in our simulations in Figure 5; however, this is a weakly constrained 456 parameter in this methodology. 457

Although this is not the first study to attempt to map fault zones using scattered 458 waves in DAS data, a key contribution of this study is that it provides a framework to 459 systematically locate the origins and discern the dimensions of these scatterers using the 460 earthquake wavefield. Importantly, when using the earthquake wavefield, we are mostly 461 looking at body-to-surface scattered waves, which have a different depth sensitivity than 462 surface-to-surface scattered waves. In particular, body-to-surface wave scattering has a 463 deeper depth sensitivity than surface-to-surface wave scattering because body waves can 464 propagate at depth while surface waves have a frequency-limited depth extent (Barajas 465 et al., 2022). But, body-to-surface wave scattering at a given frequency is still only sen-466 sitive to depths at which a scattering source can excite surface waves. Differences in sen-467 sitivity are important to consider when comparing this methodology to other scatterer 468 characterization methods that use surface-to-surface wave scattering. Since we can only 469 feasibly apply this technique between 2-10 Hz, this depth sensitivity constraint suggests 470 that this methodology is only sensitive to the top few hundred meters. But, we suggest 471 that the depth extents determined in this study are well-constrained by the data. To il-472 lustrate this, we perform a simulation for a fault with the same parameters as the best 473 fitting model for peak β , but change the depth extent from 0-50 m to 0-100 m. The frequency-474 amplitude curve for this simulation is plotted as Model 4 in Figure 5. This curve shows 475 that for a deeper fault, we would expect to observe a frequency-amplitude curve more 476 477 depleted in higher frequencies and enriched in lower frequencies.

In Y. Yang, Zhan, et al. (2022), the authors discern properties of the fault zone as-478 sociated with peak α in this study as a 30% velocity reduction that is 35 m wide and 479 spans 0 to 90 m depths. While this geometry is very close to our result and provides a 480 useful verification of our technique, the differences that arise are likely due to the dif-481 ferent sensitivities of the measurements and the different frequencies used to fit the fault 482 model. Namely, the geometry of the faults discerned in this study were partially con-483 strained by measurements over 6 Hz, which were not used to constrain the geometry in 484 Y. Yang, Zhan, et al. (2022). The higher frequency content used in this study likely ex-485 plains why the characteristic dimensions discerned in this study are both smaller than 486 those found in Y. Yang, Zhan, et al. (2022). The higher frequency content may account 487 for our ability to resolve a shallow burial depth. This fault burial depth is largely con-488 strained by subtle variations in the peak shape. To illustrate this, we generate synthet-489 ics for a fault model with the same parameters as the best fitting model for peak α , but 490 use a depth extent of 0-50 m instead of 10-60 m. The frequency-amplitude curve for this 491

⁴⁹² synthetic test is plotted as Model 3 in Figure 5. This result shows, that for an unburied ⁴⁹³ fault, we achieve a slightly different shape that does not capture any separation of the ⁴⁹⁴ high and low frequency modes of the data curve for peak α .

Finally we note that, although this study focused on relatively minor faults, this 495 methodology can be readily extended to major fault zones, and requires only an across-496 fault DAS array and earthquake observations. Indeed, since the interrogation length for 497 DAS units is increasing, and since many in situ fibers cross major faults, we can expect 498 the number of DAS arrays sensing structure over major fault zones to increase rapidly 499 500 over time. The technique presented in this paper presents an opportunity to leverage these DAS arrays to measure the fracture density and characteristics within major fault zones. 501 Moreover, this study only covers one method with which DAS can be used to charac-502 terize major fault zones. Many of the aforementioned techniques which have previously 503 used densely deployed conventional seismometers can be performed with DAS. The key 504 challenges in applying these techniques, however, are that DAS provides a different ob-505 servation than traditional seismometers, single component strain, and that DAS ampli-506 tudes are not well understood due to variability in coupling. These differences make some 507 traditional fault characterization techniques, such as detecting fault zone head waves us-508 ing particle motion analysis or measuring S-wave amplification, more difficult to apply 509 using only DAS data. But, including some conventional inertial seismometers along a 510 DAS array has the potential to diminish some of the challenges of DAS data (e.g. H. F. Wang 511 et al., 2018; Lindsey et al., 2020; Muir & Zhan, 2021; Y. Yang, Atterholt, et al., 2022). 512 For the fault zone characterization case, including collocated 3-component seismic sen-513 sors allows for amplitude calibration of DAS data and provides local particle motion ob-514 servations. In this way, we can leverage the high station density and extensive deploy-515 ments of DAS data while minimizing its limitations. 516

517 7 Conclusions

In this study we present a framework for the systematic location and character-518 ization of fault zones using the DAS measured earthquake wavefield. This framework, 519 which relies on the simple backprojection of the scattered wavefield following an earth-520 quake, yields profiles of the scattered wave energy across the array. We apply this frame-521 work to 50 earthquake record sections recorded by a DAS array in Ridgecrest, CA, yield-522 ing an ensemble of profiles of scattered wave energy across the array. With these pro-523 files, we identify numerous scattering peaks that are spatially well-correlated with mapped 524 faults in the area, suggesting that these observed scattered waves are faults. Using these 525 backprojection profiles, we suggest a correction to the location of one of the mapped faults 526 in the area. Moreover, we present a model for these scattering sources as rectangular per-527 turbations in the velocity structure, which is a simple approximation of a fault zone, and 528 through simulations we show that this model reproduces first order observations of the 529 observed scattered waves. Using this backprojection technique and these simulations, 530 we establish a framework for using the locally scattered wavefield to evaluate shallow at-531 tenuation structure and infer characteristic dimensions of fault zones. We then apply this 532 framework to the profiles computed for the Ridgecrest DAS array and consequently make 533 claims about the fault zone structure near the array. We use the frequency decay of the 534 profile peaks and synthetic simulations to image local faults at the scale of tens of me-535 ters, and with these images we distinguish between a fault that is surface-breaching and 536 a fault that is buried. 537

538 Open Research

The data used in this study are available online (https://doi.org/10.22002/D1.20038) as 30-second record sections that include the initial onset of the earthquake wavefield for the 50 high signal-to-noise ratio aftershocks recorded by the distributed acoustic sensing (DAS) array in Ridgecrest, CA referenced in this study. The simulations performed for this study were done using the software Salvus, (Afanasiev et al., 2019), available at https://mondaic.com/. Figure 1 was made using The Generic Mapping Tools (GMT),

version 6 (Wessel et al., 2019), available at https://www.generic-mapping-tools.org/.

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Supporting Information for

Fault Zone Imaging with Distributed Acoustic sensing: Body-to-Surface Wave Scattering

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Figures S1 to S3 (Pages 2-3)

Table S1 (Page 4)

Introduction

This file includes three figures and a table that supplement the main text. Figure S1 is a dispersion curve generated using a grid search of backprojected images computed at different velocities, the methodology of which is described in the main text, for the scattered wavefield of the earthquake shown in Figure 1. This figure served as partial verification that the scattered waves in this study are surface waves. Figure S2 is a dispersion curve generated using the same methodology as that of Figure S1, but using the sythetic wavefield shown in Figure 4. This figure helped us ensure there was a first order match between the synthetic wavefield and the observed wavefield. Figure S3 is a fit to the spatial decay of the ensemble of peaks associated with peaks α and β in the study. These fits use the relationship $Q_{\mu} = cV_s$ where we vary c. This plot was used in determining the attenuation relationship for the synthetics used in this study. Table S1 shows all the model parameters for the fault zone models used to make Figure 5. These models were important for evaluating the constraints and sensitivity of the model fits presented in this study.

Figures



Figure S1. Dispersion curve generated using the backprojection framework to perform a grid search at velocities in narrow frequency bands on the earthquake wavefield shown in Figure 1. Black dotted line is the 1D average of the velocity model from Yang et al. (2022)



Figure S2. Dispersion curve generated using the backprojection framework to perform a grid search at velocities in narrow frequency bands on a synthetic shot gather with an emplaced fault model. Black dotted line is the 1D average of the velocity model from Yang et al. (2022)



Figure S3. Peak decay functions of peaks α and β for ensemble of profiles shown in Figure 3. Light green and light blue lines are decay functions of individual profiles for peaks α and β , respectively. Dark green and dark blue lines are mean peak decay functions for peaks α and β , respectively. Dotted lines are peak decay functions for synthetics generated using different attenuation regimes defined using constant of proportionality *c*.

Model Parameters							
Model $\#$	Burial Depth (m)	Maximum Depth (m)	Width (m)	Velocity Reduction (%)			
Model 1	10	60	50	30			
Model 2	10	30	20	30			
Model 3	0	50	50	30			
Model 4	0	100	50	10			
Model α	10	60	20	30			
Model β	0	50	50	10			

Table S1. Model parameters for each of the models shown in Figure 5. Fault model is rectangular, where the burial depth is the depth of the top of the rectangle, the maximum depth is the depth of the bottom of the rectangle, the width is the lateral extent of the rectangle, and the velocity reduction is the applied velocity perturbation. All fault models are vertical.

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