

Uncertainty decomposition to understand the influence of water systems model error in climate vulnerability assessments

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November 22, 2022

Abstract

Climate vulnerability assessments rely on water infrastructure system models that imperfectly predict performance metrics under ensembles of future scenarios. There is a benefit to reduced complexity system representations to support these assessments, especially when large ensembles are used to better characterize future uncertainties. An important question is whether the total uncertainty in the output metrics is primarily attributable to the climate ensemble or to the systems model itself. Here we develop a method to address this question by combining time series error models of performance metrics with time-varying Sobol sensitivity analysis. The method is applied to a reduced complexity multi-reservoir systems model of the Sacramento-San Joaquin River Basin in California to demonstrate the decomposition of flood risk and water supply uncertainties under an ensemble of climate change scenarios. The results show that the contribution of systems model error to total uncertainty is small (~5-15%) relative to climate based uncertainties. This indicates that the reduced complexity systems model is sufficiently accurate for use in the context of the vulnerability assessment. We also observe that climate uncertainty is dominated by the choice of GCM and its interactive effects with the representative concentration pathway (RCP), rather than the RCP alone. This observation has implications for how climate vulnerabilities should be interpreted.

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2 **climate vulnerability assessments**

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23 **Abstract**

24 Climate vulnerability assessments rely on water infrastructure system models that imperfectly
25 predict performance metrics under ensembles of future scenarios. There is a benefit to reduced
26 complexity system representations to support these assessments, especially when large ensembles
27 are used to better characterize future uncertainties. An important question is whether the total
28 uncertainty in the output metrics is primarily attributable to the climate ensemble or to the systems
29 model itself. Here we develop a method to address this question by combining time series error
30 models of performance metrics with time-varying Sobol sensitivity analysis. The method is applied
31 to a reduced complexity multi-reservoir systems model of the Sacramento-San Joaquin River
32 Basin in California to demonstrate the decomposition of flood risk and water supply uncertainties
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34 model error to total uncertainty is small (~5-15%) relative to climate based uncertainties. This
35 indicates that the reduced complexity systems model is sufficiently accurate for use in the context
36 of the vulnerability assessment. We also observe that climate uncertainty is dominated by the
37 choice of GCM and its interactive effects with the representative concentration pathway (RCP),
38 rather than the RCP alone. This observation has implications for how climate vulnerabilities should
39 be interpreted.

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45 **1. Introduction**

46 Climate vulnerability assessments have become a common feature of water resources systems
47 planning studies (Arnell, 2011; Plummer et al., 2012; US Bureau of Reclamation, 2012; Weaver
48 et al., 2013). These assessments generally require ensemble simulations of future climate scenarios
49 that are passed through a combination of hydrologic models and water resources systems models
50 to measure the vulnerability of the water system to properties of future climate. Once these
51 vulnerabilities are identified, additional simulation or optimization experiments are used to
52 determine how well different adaptation actions mitigate these vulnerabilities (Herman et al., 2015;
53 Herman et al., 2020).

54

55 The literature on the uncertainties that underlie future climate scenarios (Knutti et al., 2008;
56 Northrop and Chandler, 2014; Lehner et al 2020), associated hydrologic responses (Wilby and
57 Harris, 2006; Steinschneider et al., 2015a; Mendoza et al., 2016; Kundzewicz et al., 2018), and
58 water system vulnerability under climate change (Steinschneider et al., 2015b,c) is extensive.
59 However, water resources systems model uncertainties are usually neglected in these climate
60 impact assessments, presumably under the assumption that they are negligible in comparison to
61 other uncertainties. This assumption is likely valid for systems models underpinned by years to
62 decades of development. However, many of these high-fidelity models are computationally
63 expensive and ill-suited for ensemble experiments required by climate vulnerability and adaptation
64 assessments. More parsimonious system models and emulators of complex systems models have
65 become a popular means of reducing the computational cost of systems model simulation in
66 ensemble experiments (Haasnoot et al., 2014; Gijbers et al., 2017; Basco-Carrera and Mendoza
67 2017; Voinov et al., 2018; Badham et al. 2019; Helgeson et al., 2021). These models provide faster

68 runtimes at the expense of some accuracy in system representation. Their use raises the question
69 of whether such reduced complexity models are suitable for use in climate vulnerability
70 assessments and how this should be assessed.

71

72 Past work has considered the question of whether a systems model is fit-for-purpose (Haasnoot et
73 al. 2014; Hamilton et al., 2022). For example, Haasnoot et al. (2014) emphasize the ability of the
74 model to produce “credible outcomes with sufficient accuracy for the screening and ranking of
75 promising actions and pathways in order to support... strategic adaptive planning decisions.” They
76 describe a simplified systems model as fit-for-purpose if it produces decisions that are consistent
77 with a more complex model. In the context of climate vulnerability assessments, we investigate a
78 related concept: whether prediction errors arising from the systems model are negligible compared
79 to the uncertainty in forcing, particularly around key output metrics that are most relevant to
80 decision-making. This emphasizes the relative accuracy of the systems model against the
81 background of other exogenous uncertainties, and thus contributes a complementary viewpoint by
82 assessing if the model is fit-for-purpose in the context of planning under uncertain future
83 conditions. This viewpoint is consistent with recent recommendations to ensure greater
84 transparency and more robustness in climate change impact assessments (Wagener, 2022).

85

86 This technical note advances variance decomposition as an approach to assess the suitability of
87 water systems models in climate vulnerability studies. Uncertainty decomposition is widely used
88 to assess sources of uncertainty in climate models and their influence on key variables of interest
89 (Hawkins and Sutton 2009, Lehner et al 2020). It is also used to identify factors that drive
90 uncertainty in water systems performance metrics (Schlef et al. 2018; Greve et al 2018) and the

91 broader human-Earth system (Lamontagne et al., 2019). In this study we extend this technique to
92 assess whether a water systems model is sufficiently accurate for its intended purpose in a climate
93 vulnerability assessment, providing a diagnostic method to propagate and decompose systems
94 model error in the context of an ensemble of climate scenarios.

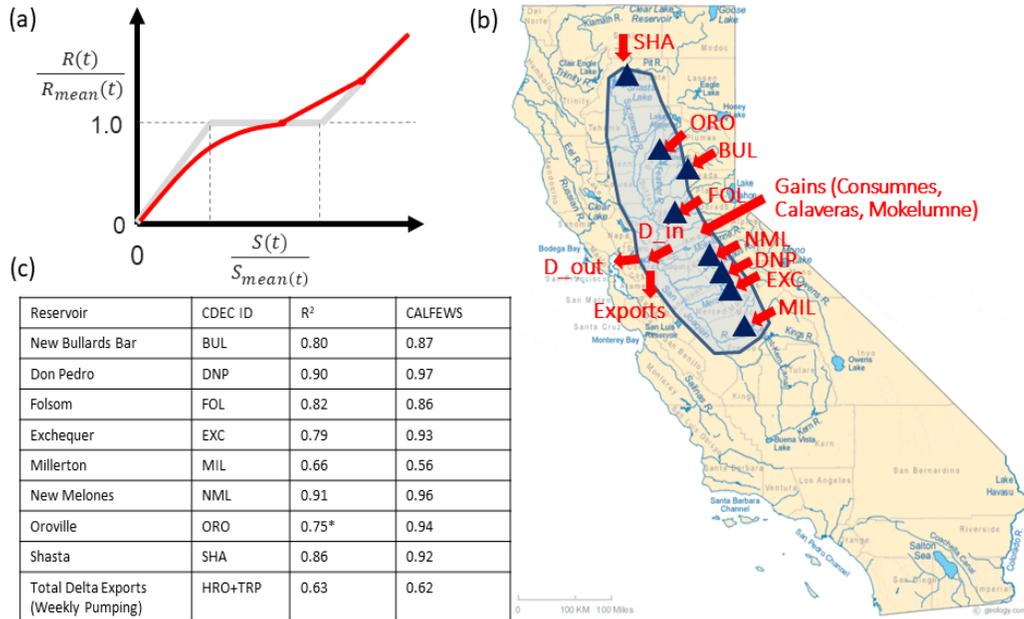
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96 **2. Data and Methods**

97 **2.1 Case Study & Simulation Model**

98 The proposed method is demonstrated using a new, daily time step simulation model of the eight
99 largest reservoirs in the Sacramento-San Joaquin River Basin (SSJRB), California, and the water
100 supply pumping operations near the system outlet in the Sacramento-San Joaquin Delta (Figure
101 1). The model structure and data requirements were simplified from recently developed simulation
102 models of this system (ORCA - Cohen et al. 2020, 2021; CALFEWS - Zeff et al. 2021) for the
103 purpose of efficiently estimating water supply and flooding metrics in the Delta in large ensemble
104 climate vulnerability assessments.

105



106

107 **Figure 1. Overview of the Sacramento-San Joaquin River Basin (SSJRB) simulation model.**
 108 **(a) Reservoir operating policy relating releases R to storage S ; (b) inflow and pumping**
 109 **locations; (c) model accuracy (R^2) for storage at the 8 reservoirs in the system and total delta**
 110 **exports compared to the CALFEWS systems model (Zeff et al., 2021). The time periods for**
 111 **the comparison are Oct 1997-Sept 2021 (SSJRB) and Oct 1996-Sept 2016 (CALFEWS). *The**
 112 **Oroville result for the SSJRB model is impacted by the operational response to the Feb 2017**
 113 **spillway failure over the subsequent year.**

114

115 The SSJRB reduced complexity systems model (referenced hereafter as the SSJRB model) consists
 116 of three components: reservoir release policies, gains, and Delta pumping. The model contains 43
 117 parameters, including: five release policy parameters for each of the eight reservoirs, two
 118 parameters for gains, and one parameter for Delta pumping. The model uses the historical observed
 119 median operating pattern (storage and release for each day of the water year) over the period 1997-
 120 2021, and adjusts this pattern based on current hydrologic conditions. Initially, reservoir operations
 121 are described by 5-parameter (x_0, \dots, x_4) exponential water supply and linear flood hedging rules
 122 (Figure 1a). The water supply rule is given by:

123

$$\frac{R_i(t)}{R_{i,m}(t)} = \left(\frac{S_i(t)}{S_{i,m}(t)} \right)^{x_0} \quad (1)$$

124 where $R_i(t)$ is the release for the i^{th} reservoir, $S_i(t)$ is the storage, and $R_{i,m}(t)$ and $S_{i,m}(t)$ are the
 125 median release and storage for that day of the water year, respectively. The water supply release
 126 determined from Eq. 1 is then increased to model flood control operations. Specifically, if the day
 127 of the water year falls between $[x_1, x_2]$ and $S_i(t) > x_4 S_{i,m}(t)$, then $R_i(t)$ is increased by the
 128 amount $x_3(S_i(t) - x_4 S_{i,m}(t))$.

129
 130 Next, the hydrologic gains into the Delta, $G(t)$, are defined as the Delta inflow $D_{in}(t)$ minus the
 131 sum of reservoir outflows. This term represents the tributaries for which reservoirs are not modeled
 132 (see Figure 1b) as well as additional inflows downstream of the reservoirs. Gains can be either
 133 positive or negative. Positive gains represent winter inflows, while negative gains represent
 134 consumptive withdrawals in the summer. These gains are estimated from historical patterns using
 135 two parameters (x_5, x_6):

$$136 \quad G(t) = G_m(t) \left(\sum_i \frac{S_i(t)}{K_i} \right)^{x_5} + x_6 \sum_i Q_i(t) \quad (2)$$

137 where $G_m(t)$ are the median gains for that day of the water year, K_i is the storage capacity of
 138 reservoir $i \in [1,8]$, and $Q_i(t)$ is the inflow into reservoir i . The first term in (2) covers the broader
 139 seasonal patterns of withdrawals, while the second term represents additional Delta inflows that
 140 are assumed to be correlated with reservoir inflows included in the model.

141
 142 The Delta pumping policy is represented by the following equation with one parameter, x_7 :

$$143 \quad P(t) = D_{in}(t) p_m(t) \left(\sum_i \frac{S_i(t)}{K_i} \right)^{x_7} \quad (3)$$

144 where $P(t)$ is the total pumping volume, $p_m(t)$ is the median pumping for that day of the water
 145 year (percent of inflow), and the storage fraction term is the same as in Eq. 2. We impose an upper

146 bound on pumping to approximate a combination of the infrastructure capacity and environmental
147 guidelines, though this amount can be exceeded if needed.

148

149 The parameters for all of the model components are fit with differential evolution (Storn and Price,
150 1997). The historical data used to find the median daily patterns and to fit the parameters are taken
151 from the California Data Exchange Center (CDEC; cdec.water.ca.gov). These operating rules are
152 empirical simplifications based on the observed data, and do not exactly match those published in
153 water control manuals. However, they ensure that all reservoirs follow the same model structure,
154 and that the model is parsimonious enough to calibrate and modify. Figure 1c shows the ability of
155 the systems model to replicate historical storage for each of the eight reservoirs. Overall, the
156 systems model adequately represents the operations of these facilities, with R^2 values for daily
157 simulated and observed storage ranging between 0.66 and 0.91, with an average of 0.81. This
158 performance is slightly worse than that of a recently published, more detailed, state-of-the-art
159 simulation model of the California water system (CALFEWS; Zeff et al., 2021), which has an
160 average storage R^2 of 0.88 for the same reservoirs, and also contains a more detailed system
161 representation south of the Delta to describe deliveries to irrigation districts. However, the SSJRB
162 model is significantly faster (3-4 orders of magnitude) due to a combination of simplified structure
163 and Numba just-in-time compilation (Lam et al., 2015). In the analysis that follows, we investigate
164 whether the decrease in accuracy significantly influences our understanding of system
165 performance in the context of broader climate uncertainties.

166

167 **2.2 Error Models for Key System Model Outputs**

168 Two output variables from the SSJRB systems model are of interest in this study: a water supply
169 metric - delta pumping exports, $P(t)$ - and a flood control metric - delta outflows, $D_{out}(t) =$
170 $D_{in}(t) - P(t)$. We develop error models for these two metrics using the historical simulation from
171 the SSJRB systems model, which enables stochastic simulation of these errors under a wide range
172 of future scenarios at a daily time step.

173

174 We follow the general approach in McInerney et al. (2017) and define a residual term, ϵ_t , equal to
175 the difference between the daily observations and simulations after transformation:

$$176 \quad \epsilon_t = f(O_t|\lambda) - f(M_t|\lambda) \quad (4)$$

177 Here, O_t is the observed data associated with the decision-relevant variable of interest (e.g., delta
178 outflows or delta pumping exports), M_t is the systems model simulation of that variable, t is a time
179 step (daily in this case) within the historical record of length T , and $f(\cdot|\lambda)$ is a transformation with
180 parameter λ . The transformation is used to simplify the probabilistic behavior of the observed and
181 simulated time series before calculating the residuals. Here, we employ the Box-Cox
182 transformation (Box and Cox, 1964), which becomes the identity transformation for $\lambda=1$ and
183 approaches a logarithmic transformation as λ approaches 0. However, other transformations (e.g.,
184 log-sinh) could also be applied.

185

186 To remove any systematic bias between the simulations and observations, the residuals are
187 regressed against the transformed simulation:

$$188 \quad \epsilon_t = \beta_0 + \beta_1 f(M_t|\lambda) + \epsilon_t \quad (5)$$

189 Two assumptions are made: 1) systems model bias is correlated with the magnitude of the
190 simulated response, e.g., the systems model tends to underestimate the observations when it

191 predicts large flows and overestimate the observations when it predicts low flows; 2) this bias is a
 192 linear function of the magnitude of the simulation itself. The bias correction in Eq. 5 could be
 193 made more general using a non-linear function (e.g., a local weighted regression or generalized
 194 additive model), but initial analysis (not shown) suggested this was unnecessary for the case study
 195 used in this work.

196

197 The bias corrected residuals ϵ_t are then decorrelated in time using an autoregressive (AR) model:

198

$$199 \quad \epsilon_t = \theta_0 + \theta_1 \epsilon_{t-1} + \xi_t \quad (6)$$

200 An AR(1) model was found to be sufficient to remove autocorrelation in the delta outflow and
 201 export residual time series. However, any higher-order autoregressive moving average (ARMA)
 202 model can be selected based on the behavior of the residual series ϵ_t .

203

204 Once the model above is fit to the historical series of data, stochastic traces $\widetilde{O}_{1:T^*}$ are simulated for
 205 new periods of interest ($t^* = 1, \dots, T^*$, e.g., future decades under climate change). These
 206 simulations are produced with the following steps:

- 207 1) Bootstrap a value of ξ_t from the historical record.
- 208 2) For a new time t^* , estimate $\widetilde{\epsilon}_{t^*}$ using Eq. 6, the resampled value of ξ_t , and the previous
 209 value $\widetilde{\epsilon}_{t^*-1}$.
- 210 3) Estimate $\widetilde{\epsilon}_{t^*}$ using Eq. 5, the value $\widetilde{\epsilon}_{t^*}$, and the systems model simulation \widetilde{M}_{t^*} .
- 211 4) Estimate $\widetilde{O}_{t^*} = f(\widetilde{\epsilon}_{t^*} + f(\widetilde{M}_{t^*}|\lambda)|\lambda)^{-1}$

212 Steps 1-4 are then repeated for all time steps $t^* = 1, \dots, T^*$. $\widetilde{\epsilon}_0$ is initialized as 0.

213

214 **2.3 Climate Scenarios**

215 In this study, we assess whether the SSJRB systems model error in key variables of interest (e.g.,
216 delta outflows and exports) is sufficiently small in the broader context of climate uncertainty. This
217 is tested by forcing the systems model with an ensemble of projected flows between 2020-2099
218 for each of the 8 reservoir inflow points of the system (see Figure 1). The ensemble, developed in
219 Brekke et al. (2014), is derived from CMIP5 general circulation model (GCM) simulations (Taylor
220 et al., 2012), downscaled to a daily timescale and $1/8^\circ$ spatial resolution using the updated Bias-
221 Correction and Spatial Disaggregation (BCSD) technique (NCAR, 2014) followed by daily
222 disaggregation (Wood et al., 2004). The ensemble is composed of four different representative
223 concentration pathways (RCPs; 2.6, 4.5, 6.0, 8.5) and 31 different GCMs, with 97 scenarios
224 altogether (not every RCP is used with every GCM). The downscaled, daily climate data force the
225 Variable Infiltration Capacity (VIC) hydrologic model, previously calibrated for watersheds across
226 the US West (see Brekke et al. 2014).

227

228 To generate a balanced ensemble, we filter the full ensemble described above to include only those
229 GCMs with simulations under the RCP 4.5 and 8.5 emission scenarios (i.e., the most common
230 emission scenarios across all GCMs). This leads to 29 GCMs under these two RCPs, for a total of
231 58 scenarios. For each scenario and its associated trace of simulated daily delta outflows and delta
232 exports from the SSJRB systems model, we develop a stochastic ensemble of 100 traces of delta
233 outflow and exports using the error modeling procedure in Section 2.2. This results in a total of
234 5,800 80-year traces of daily delta outflows and exports, which are then analyzed using sensitivity
235 analysis (described next) to partition variance among the various uncertainty sources: GCMs,
236 RCPs, and systems model error. We also consider whether the variance partitioning changes

237 considerably if a smaller set of GCMs is used, for instance based on their ability to capture aspects
238 of regional climate (Gershunov et al., 2017; Pierce et al., 2018).

239

240 **2.4 Sensitivity Analysis**

241 We use Sobol sensitivity analysis to attribute variance within the ensemble of 5,800 traces of delta
242 outflows and exports to the GCMs, the RCPs, systems model error, and interactive effects between
243 these different sources of uncertainty. These three inputs are sampled as integer factors in the
244 sensitivity analysis (i.e., the choice of GCM, RCP, and systems model error realization).
245 Ultimately, the model is classified as fit-for-purpose for large ensemble experiments in a climate
246 vulnerability assessment if the variance attributed to the systems model uncertainty and its
247 interactive effects is small compared to the other sources of uncertainty.

248

249 Sobol sensitivity analysis is described in detail elsewhere (Sobol, 2001; Saltelli et al., 2010; Pianosi
250 et al., 2016; Herman and Usher, 2017) and therefore only briefly reviewed here. Let Y_k be the
251 output metric of interest from the SSJRB systems model, which we define separately for each year
252 of simulation ($k=2020, \dots, 2100$). For delta outflows, we define Y_k as the annual maximum outflow
253 in year k ; for delta exports, Y_k is defined as the annual sum of exports. While other metrics could
254 be chosen, these metrics are representative of annual flood and drought risk in the Sacramento-
255 San Joaquin system. The Sobol method is used to attribute variance in Y_k to individual uncertainty
256 factors and their interactions, and can be written as follows:

$$257 \quad D(Y_k) = \sum_i D_i + \sum_{i < j} D_{ij} + D_{12\dots h} \quad (7)$$

258 Here, $D(Y_k)$ represents the total variance in Y_k , D_i is the first-order variance contribution of the i^{th}
259 factor, D_{ij} is the second-order variance contribution of the interaction between the i^{th} and j^{th} factors,

260 and $D_{12\dots h}$ represents the variance contribution of all higher-order interactions greater than second-
261 order. Sensitivity indices are then defined as the fraction of individual variance contribution terms
262 to the total variance (e.g., $\frac{D_i}{D}$ and $\frac{D_{ij}}{D}$ represent the first-order sensitivity index for factor i and
263 second-order sensitivity index for factors i and j , respectively). Similarly, the total-order sensitivity
264 for a given factor $(1 - \frac{D_{\sim i}}{D})$ uses the variance associated with all factors besides factor i ($D_{\sim i}$) to
265 define the variance attributed to all first-order and higher-order interactions associated with factor
266 i . See Saltelli (2002) for additional detail on the numerical estimation of terms ($D_i, D_{ij}, D_{\sim i}$).

267
268 When making a determination of whether the systems model is sufficiently accurate for use in a
269 climate impact analysis, we avoid setting a distinct threshold for the variance attributed to the
270 systems model. This is ultimately a subjective choice based on user preference, and we believe
271 that forwarding an (arbitrary) threshold here would discourage critical evaluation and collaborative
272 decision-making on a case-by-case basis that is central to effective water resources planning.
273 Similar logic supports recent efforts in the statistical literature to discourage the use of arbitrary p-
274 values when assessing the statistical significance of relationships (Wasserstein and Lazar, 2016).

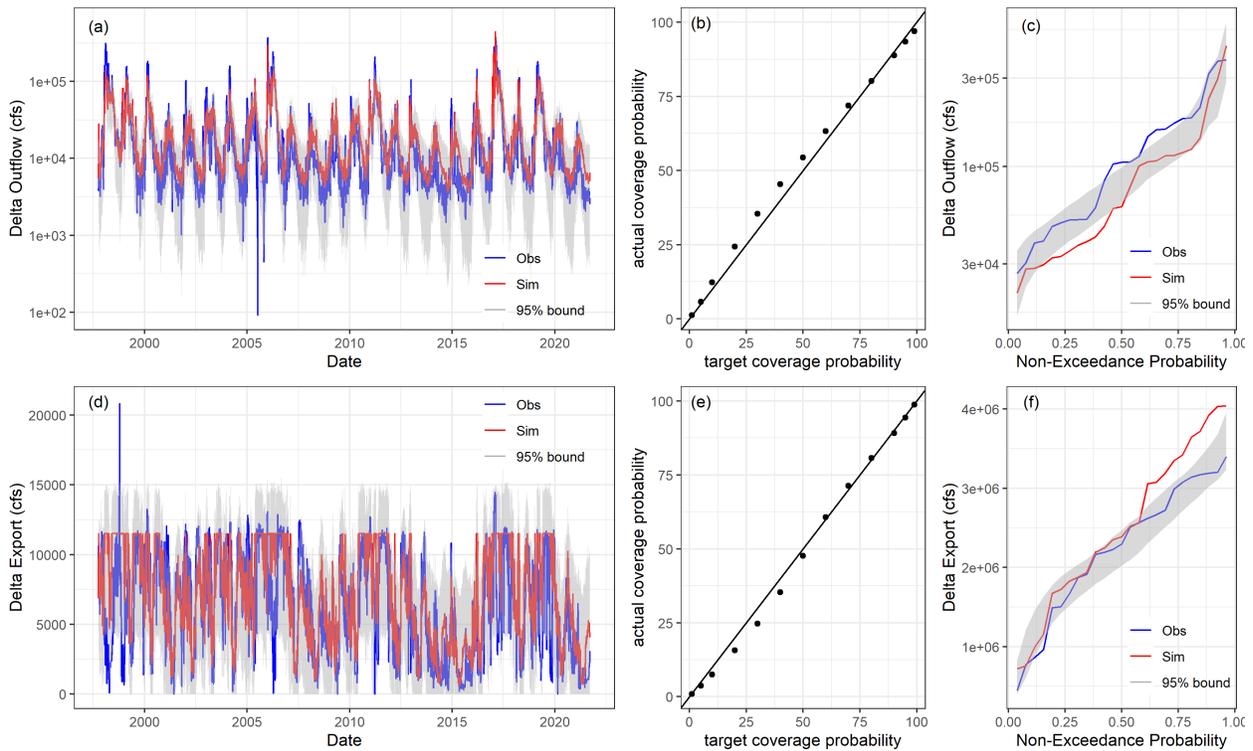
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276 **3. Results and Discussion**

277 **3.1 Systems Error Models**

278 Error accumulates throughout the system to influence the key metrics of interest: delta outflows
279 and exports. Figures 2a and 2d show the observed and simulated time series of daily delta outflows
280 and exports, respectively. The systems model captures the observed outflows well, with a Nash-
281 Sutcliffe efficiency (NSE) over the entire period of 0.74 and a percent bias of 3.2%. Simulations
282 of daily exports are less skillful, with an NSE of 0.32 and percent bias of 12.1%, although when

283 aggregating to a weekly time step the simulations are better (NSE of 0.63). Notably, the systems
 284 model tends to underestimate the largest delta outflows, albeit with one exception in 2017. The
 285 SSJRB systems model imposes a cap on delta exports, but observed exports occasionally exceed
 286 this limit. The systems model also overestimates the smallest delta outflows (Figure 2a),
 287 particularly during dry years, and exhibits fewer and less extreme declines in daily exports (Figure
 288 2d).



289

290 **Figure 2. a) Observed (blue) and simulated (red) daily delta outflows. The grey area shows**
 291 **95% bounds of the stochastic delta outflow simulations. b) Target versus actual coverage**
 292 **probabilities (i.e., the probability that observations fall within the p percent bounds of the**
 293 **simulated ensemble), with p varied from 1% to 99%. c) The CDF of observed (blue) and**
 294 **simulated (red) annual maximum delta outflows, as well as the 95% bounds for the CDF of**
 295 **annual maxima from the stochastic traces. d-e) Same as (a-b) but for daily delta exports. f)**
 296 **Same as (c) but for the annual sum of delta exports.**
 297

298 We fit error models for both the delta outflow and export series in order to generate stochastic
 299 traces of these variables. A Box-Cox transformation with $\lambda=0.3$ is applied to the delta outflows,

300 while the delta exports are not transformed (i.e., $\lambda=1$). Also, delta outflow residuals ε_t did not vary
301 significantly with model simulations, so $\beta_1 = 0$ in Eq. 5. Figures 2a and 2d show 95% bounds
302 generated using the stochastic ensemble. These uncertainty bounds are developed by simulating
303 delta outflow and export residuals and adding them to the SSJRB simulation. Several important
304 features emerge from the ensemble. The delta outflows ensemble clearly captures some of the
305 lowest outflow values, but also captures several of the peak outflow events. Similarly, the
306 stochastic delta exports ensemble better captures many of the lowest observed exports and
307 observed exports that extend above the cap imposed in the SSJRB model.

308

309 This is clear in Figures 2b and 2e, which show coverage probabilities for the stochastic ensemble.

310 Coverage probabilities quantify how often the observations fall between the $\frac{\alpha}{2}$ and $\left(1 - \frac{\alpha}{2}\right)$
311 percentiles of the stochastic ensemble, with α ranging from 0.01 to 0.99 in Figures 2b,e. The target
312 coverage probabilities (i.e., $\alpha \times 100\%$) are compared against the observed coverage probabilities to
313 assess the reliability of the stochastic ensemble. The results show that the ensemble is very reliable,
314 with the largest deviations between target and observed coverage probabilities only reaching
315 $\sim 5.5\%$.

316

317 The assessments above focus on daily data, but we are often interested in specific aggregated
318 metrics of model output. Figures 2c and 2f show the distribution of observed and simulated annual
319 maximum delta outflows and annual total delta exports, respectively. These are the focus of the
320 uncertainty decomposition shown in Section 3.2 below. Also shown in Figure 2c,f are the same
321 distributions from the stochastic traces. For delta outflows, the simulated distribution tends to
322 underestimate that of the observed, except for the very largest annual maxima. However, the

323 stochastic ensemble captures the observed distribution reasonably well, albeit with an
324 underestimation between the 40th and 75th percentiles of the distribution. The opposite issue is
325 apparent in the delta exports data, as the SSJRB model tends to overestimate the observed annual
326 totals. The stochastic ensemble corrects these discrepancies and adequately captures the observed
327 distribution.

328

329 **3.2 Sensitivity Analysis**

330 The SSJRB model was used to generate a 5,800-member ensemble of future simulations across 2
331 RCPs, 29 GCMs, and with 100 stochastic traces of model error (as described above). The Sobol
332 analysis resamples from these discrete factors to decompose the variance in the two output metrics
333 across the entire ensemble for each year, as shown in Figures 3a and 3b. Here we show the first-
334 order sensitivity indices for RCP, GCM, and systems model error, as well as second-order
335 sensitivity indices that quantify the variance associated with interactive effects. Higher order
336 sensitivity is not shown, and so the cumulative variance shown in Figure 3 is always slightly less
337 than 100% of the total variance. All sensitivity indices are smoothed with a 10-year rolling average.

338

339 Several insights emerge from Figures 3a,b. First, the largest source of uncertainty in both metrics
340 stems from the first-order effects of the GCMs. Averaged across all years, first-order GCM
341 uncertainty accounts for 49% and 46% of the total variance in delta outflows and exports,
342 respectively. This result demonstrates that the GCM used to simulate system inflows has the single
343 largest impact on the variance in decision-relevant metrics of interest, regardless of emission
344 scenario or other factors. We speculate that climate model uncertainty dominates the total

345 uncertainty due to the range of regional precipitation responses (from both internal variability and
346 change) across the GCMs (Schlef et al., 2018), but we do not verify that here.

347
348 The second largest source of uncertainty stems from the interactive effect of GCMs with RCPs.
349 The magnitude of this uncertainty rivals that of the first-order GCM effect, and when averaged
350 across years, accounts for 41% and 35% of the variance in delta outflows and exports, respectively.
351 In contrast, the first-order effect of the RCPs is small, on average less than 2%. This result
352 highlights that neither annual maximum delta outflow nor annual total delta exports are explained
353 by consistent differences that emerge across emission scenarios. This is true even by the end of
354 the century when temperature differences between RCP 4.5 and RCP 8.5 are greatest. Instead, it
355 is the variable response of the GCMs to a given RCP that explains a large portion of variance in
356 the delta outflows and exports. That is, if one GCM projects drier conditions as emissions rise, but
357 another projects wetter conditions with greater emissions, only the combination of both the
358 emissions scenario *and* the specific GCM can explain the response of the water system.

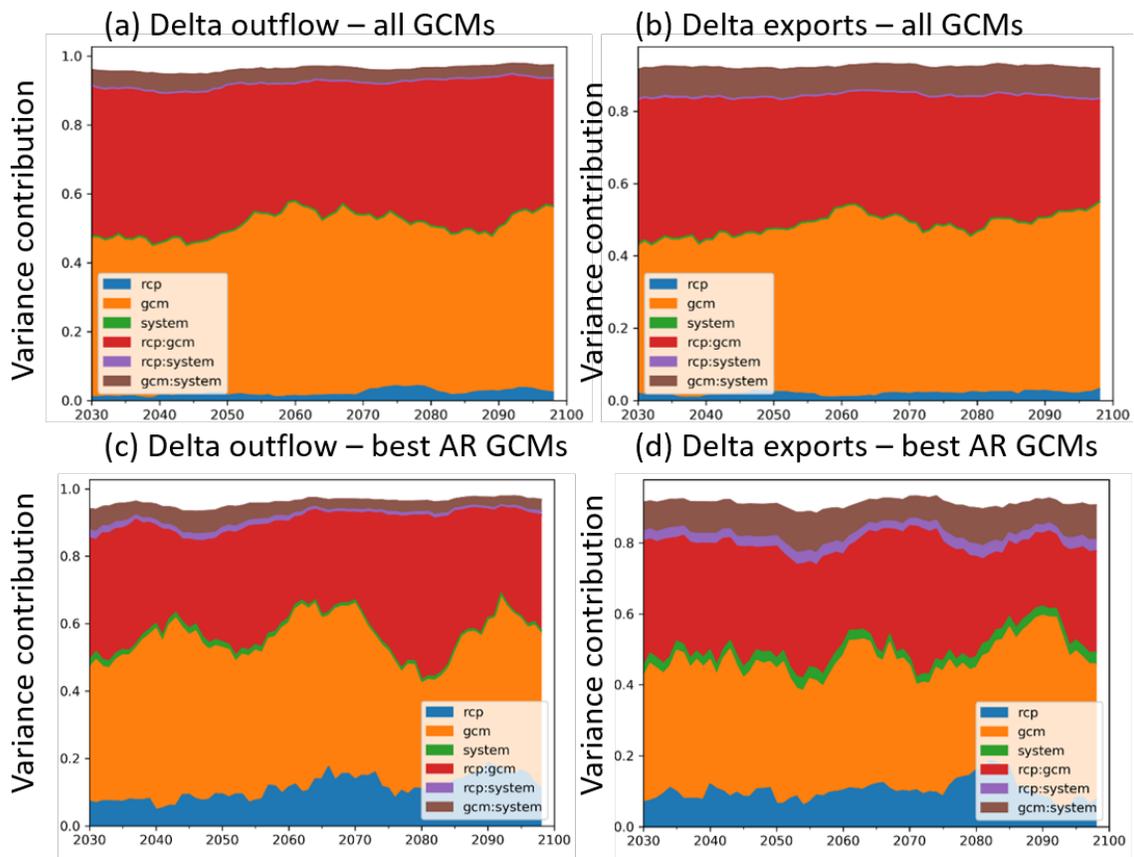
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360 Finally, we consider the variance explained by factors related to the systems model uncertainty.
361 Figures 3a,b show that for both delta outflows and delta pumping, uncertainties related to the
362 system model are small in comparison to the other sources. The uncertainty attributed to the first-
363 order systems model effect is under 1% across time, as is the interactive effect between the system
364 model error and RCP. The interactive effect between systems model error and GCM is larger, with
365 time-averaged values of 4% for delta outflows and 7.9% for delta exports. However, the
366 cumulative uncertainty for all first and higher-order terms related to systems model error (i.e.,
367 total-order sensitivity, not shown in Figure 3) is 8.2% for delta outflows and 16.5% for delta

368 exports, far below the uncertainties related to the GCMs and their interactive effects with emission
369 scenarios. From this perspective, we deem the systems model sufficiently accurate to support
370 climate change vulnerability studies of the system, given the set of 29 GCMs considered in the
371 ensemble.

372
373 It is reasonable to question if this result is consistent when a smaller set of GCMs with less
374 variability and a more consistent representation of the climate system is selected for analysis. To
375 answer this question, Figures 3c,d show the same results as in Figures 3a,b but based on a subset
376 of the original ensemble composed of simulations from the two RCPs and only four GCMs
377 (access1-0, canesm2, cnrm-cm5, gfdl-cm3). These GCMs have been shown to capture atmospheric
378 river dynamics along the US West Coast that are important to water supply and flood risk in the
379 SSJRB system (Gershunov et al., 2017). Note that access1-3 is also highlighted as skillful in
380 Gershunov et al., 2017 but is not available in the ensemble of VIC simulations (see Section 2.3).

381
382 In the restricted set of GCMs, the uncertainty attributable to the first-order effect from the GCMs
383 declines, though it is still substantial. A similar result is seen for the interactive effect between the
384 GCMs and RCPs. Importantly, we only observe a small increase in the variance attributed to the
385 systems model. Instead, the variance contribution associated with the first-order effect of the RCPs
386 increases the most, from less than 2% in the full ensemble to 11% and 10% in the limited ensemble
387 for delta outflows and exports, respectively. This is consistent with the expectation that the effects
388 of emission scenario on hydrologic response are more apparent in GCMs which provide a more
389 consistent representation of regional climate. Still, the main result from the full ensemble persists:
390 systems model uncertainty is small compared to other uncertainties, therefore the reduced

391 complexity model is suitable for climate vulnerability analysis. We note that we repeated this same
 392 experiment with 4 different GCMs that were shown to produce realistic simulations of
 393 precipitation and temperature in California (Pierce et al., 2018), with very similar results (not
 394 shown).
 395



396
 397 **Figure 3. Variance contribution of GCMs, RCPs, and system model uncertainty to the total**
 398 **variance of (a,c) annual maximum delta outflows and (b,d) annual total delta exports, shown**
 399 **by year and for first-order effects and second-order interactions. Results are smoothed using**
 400 **a lagged 10-year rolling average and shown when using (a,b) all GCMs and (c,d) only four**
 401 **GCMs selected for their accurate representation of atmospheric rivers (ARs).**
 402

403 4. Conclusions

404 This technical note contributes a novel approach to determine whether a water resources systems
 405 model is sufficiently accurate for ensemble experiments in climate vulnerability assessments. The

406 approach decomposes the variance in decision-relevant metrics (delta outflows and exports) to
407 compare systems model error to other uncertainty sources (e.g., future climate scenarios). Model
408 error in the output metrics is represented by a time series error model. To our knowledge, this is
409 the first time error models and variance decomposition have been used to assess model suitability
410 for climate impact experiments.

411
412 This technique is demonstrated with a new, computationally efficient, daily systems model of
413 reservoirs within the Sacramento – San Joaquin River Basin California. The analysis shows that
414 uncertainties from the systems model are small in comparison to those associated with future
415 climate scenarios, especially in the key metric of annual maximum delta outflow. Systems model
416 uncertainty contributes more to the total variance in delta exports, although the future climate
417 scenarios continue to dominate variance in the delta export metric. GCMs and their interactive
418 effects with RCPs contribute the most uncertainty in future delta outflows and exports. In
419 comparison, the first-order contributions from the RCPs themselves are small. The conclusions
420 above hold even if smaller ensembles of GCMs are selected based on their ability to represent
421 regional climate, although with a somewhat larger direct contribution from emission scenario.

422
423 The approach presented here is widely applicable and can be extended to consider other uncertainty
424 sources not accounted for in this experiment. For instance, the effects of climate model error and
425 natural climate variability, which were combined in the experiment presented here, could be
426 separated using single-model initial condition large ensembles (Lehner et al., 2020). Similarly,
427 hydrologic model uncertainty can significantly affect water resource impact assessments (Malek
428 et al., 2022) and could be accounted for by using multiple model structures and behavioral

429 parameter sets. As the ensemble size grows, the computational costs of the approach (in particular
430 the Sobol method) may become infeasible. Therefore, future work is needed to consider alternative
431 methods for sensitivity analysis that are more efficient, such as ANOVA or the method of Morris
432 (Morris 1991; Herman et al., 2013). Further consideration of the tradeoff between model accuracy
433 and parsimony is also warranted.

434

435 A few caveats of the approach deserve mention. The systems model uncertainty is quantified based
436 on historical errors between observed and modeled outcomes, but this approach will not capture
437 any nonstationarity in the error distribution that emerges under new boundary conditions.
438 Similarly, the current approach does not capture structural uncertainties related to changes in the
439 system, e.g., infrastructure adaptation or land-use change in response to exogenous forcing.
440 Despite these caveats, the combined use of time series error models and sensitivity analysis
441 provides an effective and straightforward screening method to assess the suitability of a systems
442 model in large ensemble climate vulnerability assessments.

443

444 **Acknowledgement**

445 This work was supported by the United States Army Corps of Engineers, Institute for Water
446 Resources. Jon Herman also received partial support from NSF grant EnvSus-2041826. We further
447 acknowledge the World Climate Research Program's Working Group on Coupled Modeling and
448 the climate modeling groups for producing and making available their model output.

449

450

451 **Data and Software Availability**

452 The code, inputs, and final outputs for all analyses conducted in this study are available at

453 <https://github.com/JohnRushKucharski/systemuncertainty> and

454 <https://zenodo.org/record/6331306#.Yin8uBDMLOQ>.

455

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