

# Separation of Spacecraft Noise from Geomagnetic Field Observations through Density-Based Cluster Analysis and Compressive Sensing

Alex Paul Hoffmann<sup>1</sup> and Mark B. Moldwin<sup>2</sup>

<sup>1</sup>University of Michigan

<sup>2</sup>University of Michigan-Ann Arbor

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## Abstract

Spacecraft equipped with magnetometers provide useful magnetic field data for a variety of applications such as monitoring the Earth's magnetic field. However, spacecraft electrical systems generate magnetic noise that interfere with geomagnetic field data captured by magnetometers. Traditional solutions to this problem utilize mechanical booms to extend magnetometers away from noise sources. This solution can increase design complexity, cost, and introduce boom deployment risk. If a spacecraft is equipped with multiple magnetometers, signal processing algorithms can be used to compare magnetometer measurements and remove stray magnetic noise signals. We propose the use of density-based cluster analysis to identify spacecraft noise signals and compressive sensing to separate spacecraft noise from geomagnetic field data. This method assumes no prior knowledge of the number, location, or amplitude of noise signals, but assumes that they are independent and have minimal overlapping spectral properties. We demonstrate the validity of this algorithm by separating high latitude magnetic perturbations recorded by SWARM from noise signals in simulation and in a laboratory experiment using a mock CubeSat apparatus. In the case of more noise sources than magnetometers, this problem is an instance of Underdetermined Blind Source Separation (UBSS). This work presents a UBSS signal processing algorithm to remove spacecraft noise and eliminate the need for a mechanical boom.

1     **Separation of Spacecraft Noise from Geomagnetic Field**  
2     **Observations through Density-Based Cluster Analysis**  
3     **and Compressive Sensing**

4             **Alex Paul Hoffmann<sup>1</sup>, Mark B. Moldwin<sup>1</sup>**

5             <sup>1</sup>Climate and Space Sciences and Engineering, University of Michigan, Ann Arbor, Michigan

6     **Key Points:**

- 7     • We present the first use of compressive sensing with cluster analysis to separate  
8     spacecraft noise from geomagnetic field data.  
9     • We demonstrate the separation of phase-delayed signals in simulation as well as  
10    in a laboratory experiment using SWARM residual geomagnetic field data.  
11    • The method enables high fidelity magnetic field measurements from resource con-  
12    strained and magnetically noisy spacecraft such as boomless CubeSats.

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Corresponding author: Alex Paul Hoffmann, [aphoff@umich.edu](mailto:aphoff@umich.edu)

**Abstract**

Spacecraft equipped with magnetometers provide useful magnetic field data for a variety of applications such as monitoring the Earth’s magnetic field. However, spacecraft electrical systems generate magnetic noise that interfere with geomagnetic field data captured by magnetometers. Traditional solutions to this problem utilize mechanical booms to extend magnetometers away from noise sources. This solution can increase design complexity, cost, and introduce boom deployment risk. If a spacecraft is equipped with multiple magnetometers, signal processing algorithms can be used to compare magnetometer measurements and remove stray magnetic noise signals. We propose the use of density-based cluster analysis to identify spacecraft noise signals and compressive sensing to separate spacecraft noise from geomagnetic field data. This method assumes no prior knowledge of the number, location, or amplitude of noise signals, but assumes that they are independent and have minimal overlapping spectral properties. We demonstrate the validity of this algorithm by separating high latitude magnetic perturbations recorded by SWARM from noise signals in simulation and in a laboratory experiment using a mock CubeSat apparatus. In the case of more noise sources than magnetometers, this problem is an instance of Underdetermined Blind Source Separation (UBSS). This work presents a UBSS signal processing algorithm to remove spacecraft noise and eliminate the need for a mechanical boom.

**Plain Language Summary**

Magnetometers are instruments designed to measure magnetic fields. They are used for a variety of purposes such as monitoring the magnetic field of the Earth from spacecraft. Spacecraft systems such as solar panels and reaction wheels generate magnetic noise that interferes with magnetometer readings. If the spacecraft has multiple magnetometers, each noise source will have a different magnitude at each magnetometer depending on the location of the noise source. The system which describes the magnitude of each noise source at each magnetometer is called a mixing matrix. We propose the use of unsupervised machine learning to estimate the mixing matrix. Once the mixing matrix is estimated, the Earth’s magnetic field can be separated from spacecraft magnetic noise using a method called Compressive Sensing.

**1 Introduction**

Spacecraft equipped with magnetometers can be used to capture in situ measurements of magnetic phenomena in the geospace environment. These measurements are necessary to answer key questions about the nature of the Earth’s magnetosphere and its interaction with interplanetary magnetic fields. Understanding how the heliosphere directs the flow of energy, mass, and momentum between the Sun and Earth is critical for a number of applications such as space weather modeling, space exploration, and climate science. A number of missions use spacecraft equipped with magnetometers to measure magnetic fields. For example, The European Space Agency’s SWARM mission uses a constellation of three satellites to provide high fidelity magnetic field measurements used to model the Earth’s magnetic field and study the Earth’s dynamo (Fratter et al., 2016). Magnetometers provide invaluable data for space science research, however, the quality of the data is often limited by magnetic noise generated by the spacecraft. Electrical systems onboard a spacecraft generate stray magnetic fields that interfere with magnetic field measurements germane to scientific investigation. The presence of these stray magnetic fields is a significant obstacle for missions which utilize magnetic field data (Russell, 2004; Ludlam et al., 2009).

60 On satellites, stray magnetic fields can be generated by subsystems such as solar  
 61 panels, reaction wheels, battery currents, and magnetorquers. Satellite magnetometers  
 62 are typically fixed at the end of a mechanical boom to reduce the magnitude of noise gen-  
 63 erated by the spacecraft. For example, the mission SWARM uses two magnetometers  
 64 mounted on a 4.3 meter boom (McMahon et al., 2013). However, the use of a boom is  
 65 not always possible in designs such as rovers and CubeSats where gravity and cost are  
 66 limiting factors. Booms are also problematic on non-magnetic spacecraft such as DMSP,  
 67 which are equipped with a tri-axial fluxgate magnetometer on the end of a telescoping  
 68 boom, but still faces issues with spacecraft noise (Kilcommons et al., 2017).

69 The use of a single magnetometer on a spacecraft requires characterization of the  
 70 spacecraft’s magnetic signature in order to remove stray magnetic fields. In the case of  
 71 the spacecraft Cassiope, a software update changed the behavior of the spacecraft’s flux-  
 72 gate magnetometer (MGF). Special spacecraft maneuvers to decrease the spacecraft’s  
 73 noise signature were required in order to recalibrate the MGF (Miles et al., 2019). Al-  
 74 gorithms to autonomously identify spacecraft noise would allow Cassiope to do in situ  
 75 MGF calibration without special spacecraft maneuvers.

76 In spacecraft with multiple magnetometers, the traditional way to cancel stray mag-  
 77 netic field noise is to perform gradiometry. Gradiometry is a technique which compares  
 78 magnetometer signals and calculates the gradient of between them (Ness et al., 1971; Ream  
 79 et al., 2021). The calculated gradient is used to identify and suppress noise signals. This  
 80 method requires spatial knowledge of the magnetometers and assumes that the magnetic  
 81 noise sources are dipole structured. More recently, Imajo et al. (2021) proposed the use  
 82 of Independent Component Analysis (ICA) to separate geomagnetic field data, captured  
 83 by the satellite Michibiki-1, from stray magnetic field noise. Imajo et al. (2021) apply  
 84 ICA by assuming that there are  $M-1$  noise signals recorded by  $M$  magnetometers. The  
 85 satellite, Michibiki-1, has one magnetometer mounted on the end of a short boom, and  
 86 another mounted at the base of the boom on the spacecraft. Because there are two mag-  
 87 netometers, Imajo et al. (2021) assume a single geomagnetic field and noise signal for  
 88 each cartesian axis. This algorithm separates signals based on statistical independence,  
 89 and works well when the number of noise sources is not more than the number of mag-  
 90 netometers (Naik & Kumar, 2009). Spacecraft typically have an abundance of noise gen-  
 91 erating electrical equipment, so this condition is rarely met. Sheinker and Moldwin (2016)  
 92 proposed an analytical method which uses a pair of magnetometers to adaptively cancel  
 93 magnetic interference without prior knowledge of the noise signal. This method is  
 94 designed for the case in which a single noise source is present, and does not account for  
 95 the presence of multiple noise sources. Although, the method may be applied to remove  
 96 multiple noise sources by adding more magnetometers. Other methods employ state es-  
 97 timation of the magnetic fields generated by spacecraft subsystems by examining space-  
 98 craft housekeeping data. Deshmukh et al. (2020) uses a supervised machine learning al-  
 99 gorithm in order to estimate the transfer function of housekeeping currents to stray mag-  
 100 netic fields. Total knowledge of a spacecraft’s magnetic signature would allow for per-  
 101 fect interference cancellation, however, housekeeping telemetry provides an incomplete  
 102 image of a spacecraft’s current distribution. For low cost applications with a large num-  
 103 ber of spacecraft, such as CubeSat constellations, it is advantageous to use an algorithm  
 104 that does not rely on prior knowledge of the spacecraft’s magnetic signature or requires  
 105 human analysis.

106 In this work, we present the application of the unsupervised machine learning al-  
 107 gorithm, Density Based Spatial Clustering of Applications with Noise (DBSCAN), and  
 108 compressive sensing to separate the geomagnetic field signal from stray magnetic field  
 109 noise. The separation of geomagnetic signals from stray magnetic fields is an instance  
 110 of Underdetermined Blind Source Separation (UBSS). UBSS is a class of problems in which  
 111 there are  $m$  listeners,  $B(k) \in \mathbb{C}^m$ , and  $n$  noises sources,  $S(k) \in \mathbb{C}^n$ , such that  $m <$   
 112  $n$ . The source signals combine in an unknown mixing matrix  $\mathbf{K} \in \mathbb{C}^{m \times n}$ . UBSS is a

113 topic that has been thoroughly researched in other fields such as acoustics and radar sig-  
 114 nal processing. The system used to model UBSS is defined by the following relationship.

$$\mathbf{B}(\mathbf{k}) = \mathbf{K}\mathbf{S}(\mathbf{k}) \quad (1)$$

115 In the field of acoustics, this problem is famously referred to as the cocktail party  
 116 problem. In the cocktail party problem, there is a room full of people each having con-  
 117 versations. An array of microphones is placed in the room to record the concurrent con-  
 118 versations. The microphone recordings are then used to separate each individual voice.  
 119 Guo et al. (2017) demonstrate the separation of four human voices using three micro-  
 120 phones. He et al. (2021) also demonstrate the separation of six flutes recorded by three  
 121 microphones using the DBSCAN algorithm.

122 Due to the spatial structure of magnetic fields, the same algorithms developed to  
 123 solve the cocktail party problem can not be directly applied to magnetic noise cancel-  
 124 lation. A magnetic noise signal,  $s(t)$ , will appear to have a different phase and magni-  
 125 tude at each magnetometer depending on the radial distance and magnetic latitude of  
 126 the magnetometer with respect to the noise source. This structure will change depend-  
 127 ing on the geometry of the noise source. In magnetic underdetermined blind source sep-  
 128 aration, the mixing matrix,  $\mathbf{K}$ , represents the gain and phase of each signal at each mag-  
 129 netometer. DBSCAN is used to estimate the mixing matrix,  $\mathbf{K}$ . Once  $\mathbf{K}$  is known, com-  
 130 pressive sensing is used to restore the geomagnetic field signal from the noisy magnetome-  
 131 ter data.

132 We present two experiments to validate this algorithm. The first experiment sep-  
 133 arates four computer-simulated noise signals from an ambient magnetic field signal. The  
 134 second experiment separates the same ambient magnetic field signal using real magnetic  
 135 field data recorded using an experimental CubeSat apparatus with copper coil generated  
 136 signals and three PNI RM3100 magnetometers (Regoli et al., 2018). The aim of this work  
 137 is to develop a robust signal processing algorithm to remove spacecraft noise and elim-  
 138 inate the need for a mechanical boom. This work focuses on developing a noise cancel-  
 139 lation algorithm for geomagnetic field data, but can also be applied to remove noise in  
 140 measurements of planetary magnetospheres and interplanetary magnetic fields.

## 141 2 Methodology

142 We apply an iterative approach to identifying spacecraft noise and reconstructing  
 143 the geomagnetic field signal. Noise signals may be present at different orders of magni-  
 144 tude or frequency spectra. In order to increase the discoverability of a noise signal, we  
 145 iteratively look at limited frequency bands by using a bandpass filter on the input sig-  
 146 nals to analyze the signals over a smaller frequency space. Noise signals are identified  
 147 by transforming the magnetometer data into a sparse domain and clustering the trans-  
 148 formed data. After the noise signals are identified, we use compressive sensing to recon-  
 149 struct the geomagnetic field with the noise signals removed.

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## 2.1 Signal Preprocessing

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The separation of magnetic field signals from stray magnetic fields is analogous to a problem thoroughly researched in other fields such as acoustics and is called Under-determined Blind Source Separation (UBSS). This problem has been heavily investigated for microphone and radar arrays, but the unique structure of a magnetic dipole introduces new complications which have not been well-researched. The placement of magnetometers at different magnetic latitudes makes the magnetic noise signal appear to be phase-delayed, despite mixing instantaneously. As a result, time-frequency domain mixing model,  $B(t,k) = KS(t,k)$ , can be represented as the following system:

$$\begin{bmatrix} B_1(t,k) \\ B_2(t,k) \\ \vdots \\ B_m(t,k) \end{bmatrix} = \begin{bmatrix} 1 & k_{12}\angle\phi_{12} & k_{13}\angle\phi_{13} & \dots & k_{1n}\angle\phi_{1n} \\ 1 & k_{22}\angle\phi_{22} & k_{23}\angle\phi_{23} & \dots & k_{2n}\angle\phi_{2n} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 1 & k_{m2}\angle\phi_{m2} & k_{m3}\angle\phi_{m3} & \dots & k_{mn}\angle\phi_{mn} \end{bmatrix} \begin{bmatrix} S_1(t,k) \\ S_2(t,k) \\ \vdots \\ S_n(t,k) \end{bmatrix} \quad (2)$$

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In this mixing system, the geomagnetic source signal we seek to recover,  $S_1(t,k)$ , is assumed to be identical at each magnetometer a priori. In the geospace environment, this allows us to observe phenomena such as ULF waves which have frequencies less than 5 Hz (Jacobs et al. 1964). The phases,  $\phi_{ij}$ , in the mixing matrix,  $K$ , account for the difference of a signal seen by magnetometers at different magnetic latitudes.

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Once the magnetometer signals,  $b(t)$ , have been filtered through a bandpass, they are transformed into the Time-Frequency (TF) domain using a Fourier transform in order to increase signal sparsity. Sparsity is a precondition of both mixing matrix estimation and compressive sensing, however, spacecraft noise signals are not often sparse in the time domain. Typically, the Short-Time Fourier Transform (STFT) is used because signals that are present in multiple time windows will provide more data points to be clustered. In this work, we use the Non-Stationary Gabor Transform (NSGT) to transform magnetometer signals into the Time-Frequency domain. NSGT has advantages over the STFT because it allows the user to evolve the window size with respect to frequency (Jaillet et al., n.d.). As a result, high and low frequencies are not limited to the same Window size, and frequency resolution is greatly increased. NSGT also improves the representation of transient signals with respect to traditional transforms. We perform the Non-Stationary Gabor Transform to obtain the UBSS model  $B(t,k) = KS(t,k)$ . The mixing system of a sparse time-frequency bin where only the signal,  $S_j(t,k)$ , is present can be defined by a single mixing vector:

$$\begin{bmatrix} \|B_1(t,k)\| \\ \|B_2(t,k)\| \\ \vdots \\ \|B_m(t,k)\| \end{bmatrix} = \begin{bmatrix} k_{1j} \\ k_{2j} \\ \vdots \\ k_{mj} \end{bmatrix} \|S_j(t,k)\| \quad (3)$$

Equation (3) can be rewritten element-wise as:

$$\|S_j(t,k)\| = \frac{\|B_1(t,k)\|}{k_{1j}} = \frac{\|B_2(t,k)\|}{k_{2j}} = \dots = \frac{\|B_m(t,k)\|}{k_{mj}} \quad (4)$$

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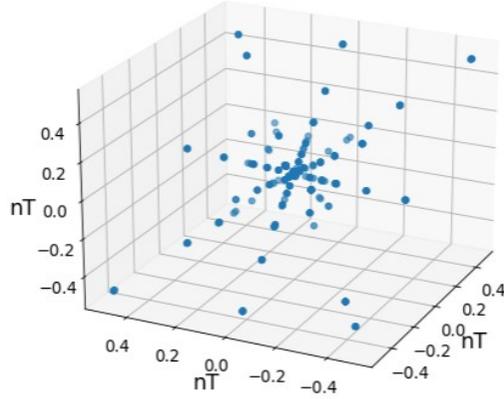
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Equation (4) is equivalent to the symmetric form of a line with slope defined by the mixing vector of the noise signal. In order to exploit this relationship, we define a time-frequency space  $\mathbf{H} \in \mathbb{R}^{2m}$  in which each phase and magnitude of the  $m$  magnetometer signals are an axis. Sparse TF points will draw straight lines through the origin in the  $\mathbf{H}$ -domain with a slope proportional to the signal's mixing vector.



**Figure 1.** Six computer generated signals plotted against each other in the frequency domain.

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## 2.2 Mixing Matrix Estimation

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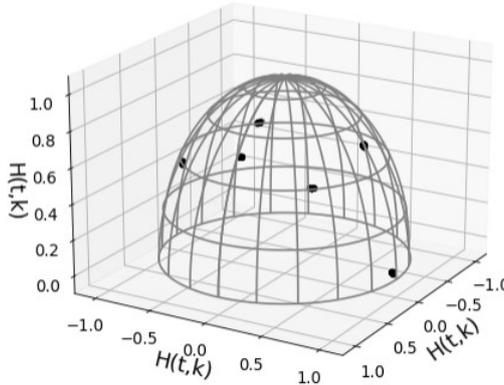
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The slope of the lines drawn through the  $\mathbf{H}$ -domain are not easily clusterable in their current form as a collection of scattered data points. We transform the scattered data points in  $\mathbf{H}$ -domain into a clusterable form by projecting the magnitude subspace onto a unit hypersphere. Figure 2 shows the projected data points of the scattered data in Figure 1.



**Figure 2.** Six computer-generated signals projected onto a half-unit hypersphere in the  $\mathbf{H}$ -Domain.

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The  $\mathbf{H}$ -domain magnitude subspace is projected onto a half-unit hypersphere using the following equation.

$$B^*(t, k) = \frac{|B(t, k)|}{\|B(t, k)\|} \quad (5)$$

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The majority of the frequency space is filled with negligible energy points that will project randomly onto the unit hypersphere (Sun et al., 2016). We attempt to cleanse the data of these points using a magnitude filter with  $\lambda \in (0, 1)$ :

$$|B(t, k)| > \lambda \cdot \max(|B(t, k)|) \quad (6)$$

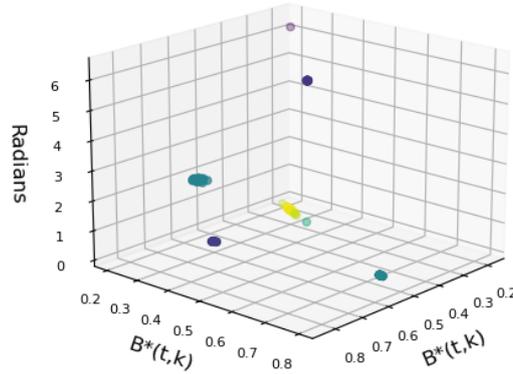
196 The projected data points form tightly clustered groups on the unit hypersphere  
 197 that allow us to discover the relative gain between noise signals at different magnetome-  
 198 ters. However, we need to find the relative phases between noise signals at magnetome-  
 199 ters of different magnetic latitudes. To account for this we join each projected time-frequency  
 200 point to its relative argument. The relative argument is defined by the following trans-  
 201 formation:

$$\arg B(t, k) = \{ \arg B_j(t, k) - \arg (B_0(t, k)) \mid j \in [0, m] \} \quad (7)$$

202 Using the result of Equation 7, we define a new data format  $H(t,k)$  by concatenat-  
 203 ing the projected magnitude data with the argument of the time-frequency data.

$$H(t, k) = (B^*(t, k), \arg (B(t, k))) \quad (8)$$

204 The magnetometer data,  $H(t,k)$ , are now in a format that can be clustered to discover  
 205 the gain and phase of each signal described in the mixing matrix,  $K$ . Figure 3 shows an  
 206 example of signal clusters in a two magnetometer system.



**Figure 3.** Five simulated signals recorded by two magnetometers in the H-Space. The horizontal axes are the magnitudes projected onto a unit hypersphere. The vertical axis is the relative phase found by Equation 7.

207 Now that the projected magnitude and relative phases are joined, a variety of clus-  
 208 tering algorithms can be applied to find the mixing matrix,  $K$ . In this work, we use the  
 209 Density Based Spatial Clustering for Applications with Noise (DBSCAN) algorithm be-  
 210 cause it does not require user input to discern the number of clusters present, and it will  
 211 ignore noise points (Ester et al. 1996). DBSCAN has two essential parameters, *eps* and  
 212 *minPts*, that allow this functionality. The maximum distance for two points to become  
 213 neighbors is the value, *eps*. If a point has *minPts* number of neighbors, it is called a  
 214 core point. Core points are used to define each cluster. If a point is more than *eps*  
 215 distance away from any point in a cluster, it is labeled as noise. We use DBSCAN to  
 216 cluster  $H(t,k)$  and use each cluster's centroid as the noise signal's mixing vector.

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### 2.3 Signal Reconstruction

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Compressive sensing is a method used to reconstruct sparse signals with a sampling rate below two times a signal's bandwidth (Baraniuk, 2007). Reconstructing a signal of length  $N$  from a sampled signal of length  $M$ , where  $M < N$ , is an analogous problem to Underdetermined Blind Source Separation. Ordinarily, the system  $b = Ks$ , where  $K$  is a wide matrix, has infinitely many solutions because if  $b = Ks$  is a solution,  $b = K(s+s')$  is also a solution for any vector  $s'$  in the null space of  $K$ . Compressive sensing can exactly recover sparse signals and approximate near-sparse signals through minimizing the L1 norm of  $S$  with respect to  $b - Ks < \varepsilon$ . The algorithm works with  $O(N^3)$  complexity.

We use CVXPY, A Python-Embedded Modeling Language for Convex Optimization (Diamond & Boyd, n.d.), to reconstruct the signals with the estimated mixing matrix,  $K$ . The constraint used to recover the signal,  $s$ , from  $b$  is:

$$\begin{aligned} \text{Minimize} \quad & \|s\|_1 \\ \text{Subject to} \quad & Ks = b \end{aligned} \tag{9}$$

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This system is solved using the convex optimization algorithm, Embedded Conic Solver (Domahidi et al., 2013).

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## 3 Experimental Data and Results

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We test the proposed method of signal and noise separation through two experiments. The first experiment demonstrates the separation of SWARM magnetic field data from computer simulated signals using virtual magnetometers. The second experiment demonstrates the separation of SWARM magnetic field data from real magnetic noise signals generated with copper coils. The coil-generated magnetic fields were measured using the PNI RM3100 magnetometer and a mock CubeSat described by Deshmukh et al. (2020).

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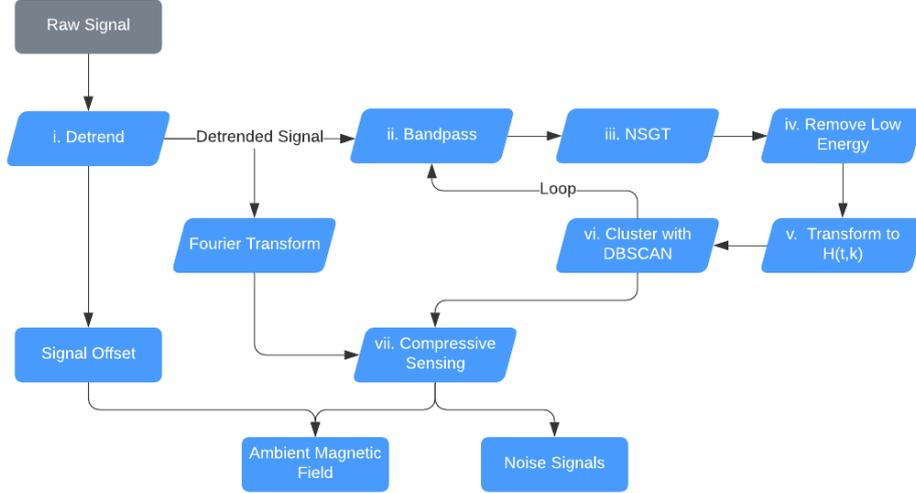
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Figure 5 details the process of identifying noise signals and reconstructing the ambient magnetic field. First (i), the signal offsets are subtracted to center the signals around 0 nT. Second (ii), the signals are bandpassed so the algorithm can analyze a more limited frequency range. Third (iii), the signals are transformed into the time-frequency domain using the Non-Stationary Gabor Transform to increase signal sparsity. Fourth (iv), low energy points are filtered out using Equation 6. Fifth (v), the signals are transformed into  $H(t,k)$  by projecting the magnitude,  $|B(t,k)|$  onto the unit hypersphere and concatenating it with the phase,  $\arg B(t,k)$ , via Equations 5, 7, and 8. Sixth (vi), the data,  $H(t,k)$ , are clustered using DBSCAN and the cluster centroids are found. This process loops back to step ii until the whole frequency spectrum has been swept. Finally, in the last step (vi), compressive sensing is used to reconstruct the ambient magnetic field. The minimum magnitude,  $\lambda$  in step iv, and the parameters  $\text{eps}$  and  $\text{MinPts}$  in step vi may need to be adjusted depending on the length and magnitude of the signals being analyzed.



**Figure 4.** Flow of processes involved in using cluster analysis to discover noise signals and compressive sensing to separate the ambient magnetic field from noise signals.

251 We evaluate the separation of noise signals via three metrics. The first metric is  
 252 the Pearson Correlation Coefficient. This measurement gives the covariance between the  
 253 normalized input and recovered signals.

$$\rho = \frac{\sum_{i=0}^{N-1} (x_i - \bar{x})(y_i - \bar{y})}{\sqrt{\sum_{i=0}^{N-1} |(x_i - \bar{x})|^2 \sum_{i=0}^{N-1} |(y_i - \bar{y})|^2}} \quad (10)$$

254 The second metric evaluated is the root mean squared error (RMSE). This met-  
 255 ric is proportional to the magnitude of the squared error. As a result, the RMSE is very  
 256 sensitive to large errors.

$$RMSE = \sqrt{\frac{\sum_{i=0}^{N-1} (x_i - y_i)^2}{N}} \quad (11)$$

257 The final metric is the normalized RMSE (NRMSE). This metric yields the RMSE  
 258 as a percentage of the magnitude of the signal being measured. It is used to compare  
 259 the relative error between signals on different orders of magnitude.

$$NRMSE = \frac{RMSE}{|y_{max}|} \quad (12)$$

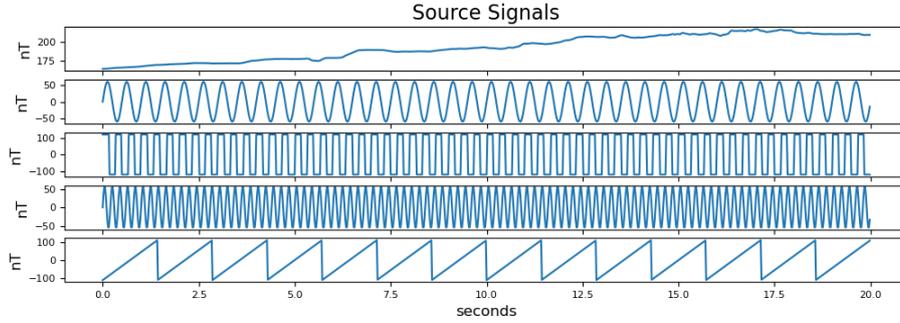
### 260 3.1 Experiment 1: Computer Simulation

261 In this experiment, we use four simulated noise signals,  $s(t) \supset [s_2(t), s_3(t), s_4(t), s_5(t)]$ ,  
 262 and three virtual magnetometers  $b(t) = Ks(t) = [b_1(t), b_2(t), b_3(t)]$ . The signal,  $s_1(t)$ ,  
 263 is residual magnetic field data created by subtracting data generated by the IGRF model  
 264 from SWARM magnetic field data. This process leaves only magnetic perturbations present  
 265 in the magnetosphere. The magnetic perturbation data we use were measured by the SWARM  
 266 A satellite on March 17th, 2015 between 8:53 and 8:55 UTC. This part of the orbit passes

267 between the 69th and 76th parallel south and was selected to capture perturbations in  
 268 the southern auroral zone. The proposed algorithm detailed in Figure 4 is tested on 100  
 269 seconds of data, although it may be applied to a signal of any length provided that there  
 270 are enough data points to cluster. The signals are combined through the complex mixing  
 271 matrix in Equation 13 with phases given in radians.

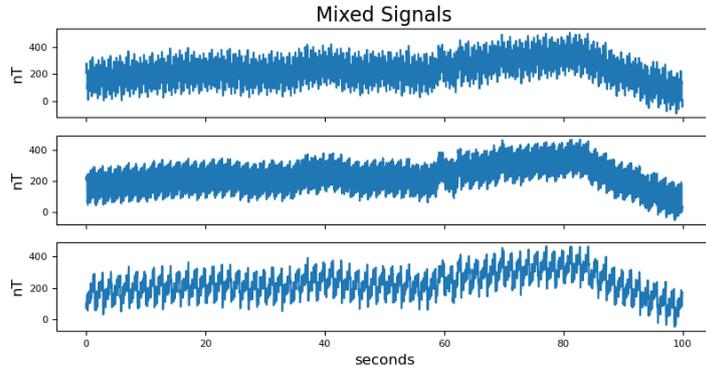
$$K = \begin{bmatrix} 1\angle 0 & 0.83\angle 0 & 0.56\angle 0 & 0.68\angle 0 & 0.30\angle 0 \\ 1\angle 0 & 0.50\angle 1.57 & 0.79\angle 0.523 & 0.29\angle 2.35 & 0.30\angle 0.314 \\ 1\angle 0 & 0.24\angle 1.04 & 0.24\angle 1.04 & 0.68\angle 3.14 & 0.90\angle 0.523 \end{bmatrix} \quad (13)$$

272 The values in the first column represent the ambient magnetic field signal which appears  
 273 identically at every magnetometer. Figure 5 shows the five source signals used in this  
 274 simulation. Two of the noise signals are sine waves with frequencies of 2 Hz and 5 Hz.  
 275 Sine waves are sparse signals that can be represented by a single point in the frequency  
 276 domain. This makes them easily identifiable by cluster analysis. The two remaining noise  
 277 signals used are a sawtooth wave with a frequency of 0.7 Hz, and a square wave with a  
 278 frequency of 3.0 Hz. These signals inhabit a broad frequency spectrum and diminish the  
 279 sparsity of the mixed signals.



**Figure 5.** Five computer generated source signals.

280 The signals are combined in the mixing system  $b(t) = Ks(t)$  with the mixing matrix  
 281  $K$  from equation 13. The resulting mixing signals are sampled by the virtual magnetometers  
 282 at a rate of 50 samples per second. A random normal signal with a standard deviation of  
 283 6 nT is added to each virtual magnetometer in order to simulate instrument noise. Fig-  
 284 ure 6 shows the sampled signals.

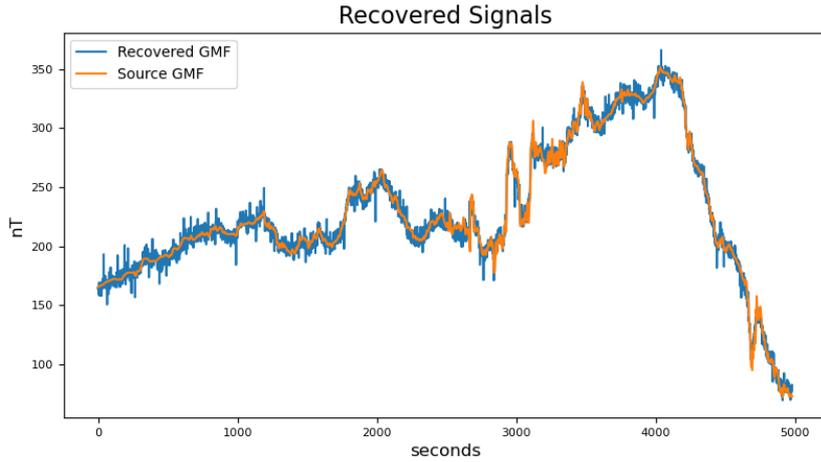


**Figure 6.** Three magnetometer signals created by mixing the five source signals in Figure 5.

285 Following the procedure in Figure 4, the signals were detrended and bandpassed  
 286 with frequency ranges of [0.01 Hz, 2.12 Hz] and [0.15 Hz, 25 Hz]. Overlapping frequency  
 287 ranges are analyzed to discover signals that may appear in multiple frequency bands. The  
 288 signals were then transformed into the Time-Frequency domain using the NSGT. The  
 289 NSGT is a type of constant-Q transform, so it requires the parameter  $Q$  which specifies  
 290 window size. In this experiment, we used  $Q = 20$ . In step 4, low energy points were  
 291 removed using a  $\lambda = 0.01$ . The resulting data were transformed into  $H(t,k)$  and clustered  
 292 by DBSCAN with parameters  $eps = 0.3$  and  $MinPts = 3$ . These parameters  
 293 were optimized experimentally using trial and error, however it may be possible to au-  
 294 tomate parameter selection based on the signals being analyzed. With this configura-  
 295 tion, DBSCAN discovered the five clusters corresponding to each noise source. The clus-  
 296 ters, shown below in the columns of  $\hat{K}$ , closely match the original mixing matrix.

$$\hat{K} = \begin{bmatrix} 1 \angle 0 & 0.83 \angle 0.00 & 0.57 \angle 0.00 & 0.62 \angle 0.00 & 0.308 \angle 0.00 \\ 1 \angle 0 & 0.50 \angle 1.57 & 0.70 \angle 0.31 & 0.33 \angle 2.63 & 0.31 \angle 0.33 \\ 1 \angle 0 & 0.24 \angle 1.02 & 0.39 \angle 0.56 & 0.70 \angle -3.1 & 0.90 \angle 0.51 \end{bmatrix} \quad (14)$$

297 Finally, in step 7, the mixed signals were separated by compressive sensing using  
 298 the recovered mixing matrix,  $\hat{K}$ , in Equation 15. The data,  $H(t,k)$ , are discarded and  
 299 the raw Fourier transform of the mixed signals is separated using the ECOS algorithm.  
 300 The reconstructed SWARM perturbation signal is shown in Figure 7 with the original  
 301 signal overlaid.



**Figure 7.** True magnetic perturbation signal in orange versus the recovered magnetic pertur-  
 bation signal in blue. The signal was reconstructed using the mixed signals in Figure 6 sampled  
 at a rate of 50 Hz.

302 The reconstructed ambient magnetic field signal resembles the original signal with some  
 303 additional error. In order to evaluate the reconstruction noise, the Pearson Correlation  
 304 Coefficient, RMSE, and NRMSE of each source signal are calculated. The ambient mag-  
 305 netic field was reconstructed with a RMSE of 5.79 nT. The results for each source sig-  
 306 nal are shown in the following table.

	Metrics				
	SWARM	Sine A	Square	Sine B	Sawtooth
$\rho$	0.9950	0.9954	0.9972	0.9996	0.8868
RMSE	5.79 nT	4.165 nT	17.00 nT	1.297 nT	33.49 nT
NRMSE	1.33%	6.94%	21.1%	2.26%	30.45%

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### 3.2 Experiment 2: Magnetic-Coil Generated Signal Separation

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In this experiment, we demonstrate the utility of the proposed algorithm on real magnetic field data. We use three PNI RM3100 magnetometers to record copper coil-generated noise signals. Four copper coils are driven by signal generators to create the source signals,  $s(t) \supset [s_2(t), s_3(t), s_4(t), s_5(t)]$ . The signals are combined in the unknown mixing system,  $b(t) = Ks(t) = [b_1(t), b_2(t), b_3(t)]$ . The SWARM residual magnetic field data, which is used in experiment one, is added to each magnetometer recording to generate the ambient magnetic field signal,  $s_1(t)$ .

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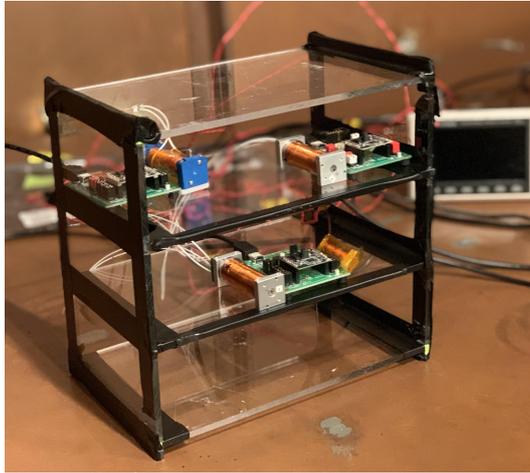
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The proposed algorithm detailed in Figure 4 is tested on 100 seconds of recorded data. The signals,  $s_2(t)$  and  $s_3(t)$ , are sine waves with frequencies of 0.4 Hz and 0.8 Hz. The signals,  $s_4(t)$  and  $s_5(t)$ , are square waves with frequencies of 1 Hz and 2 Hz. The three PNI RM3100 magnetometers and four copper coils are placed on the CubeSat apparatus as shown in Figure 8. Due to the location and orientation of the four copper coils and three magnetometers, each noise signal will appear at each magnetometer with a different magnitude and magnetic latitude induced phase. Additionally, this experiment was performed in a copper room lined with mu-metal in order to screen out magnetic fields from the surrounding environment.



**Figure 8.** Mock CubeSat Apparatus with three PNI RM3100 Magnetometers and four copper coils driven by signal generators. The Apparatus is placed inside a mu-metal lined copper room that acts as a large magnetic shield can.

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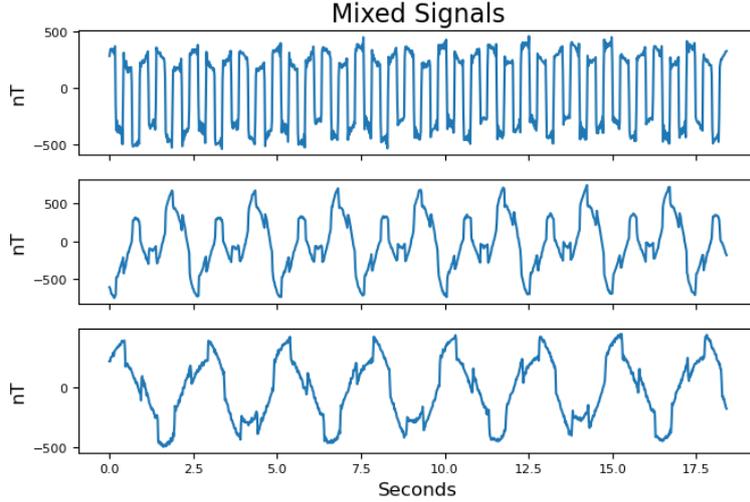
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The PNI RM3100 is a magneto-inductive magnetometer that measures the magnetic field by counting hysteresis loops with a comparator circuit, called a Schmitt Trigger, in an ASIC. The ASIC records magnetic field measurements by adding to a register every time the Schmitt trigger is saturated. This measurement renders the magnetic field when integrated with respect to time. The ASIC has a cycle count register that controls how many clock cycles pass between integrations. The error of the magnetometer will change with respect to the cycle count. In this experiment, each magnetometer is sampled at a rate of 50 Hz with a cycle count of 200 cycles. The PNI RM3100 is rated to have an error of 6 nT in this configuration. The mixed signals recorded by the PNI RM3100 magnetometers are shown in Figure 9 below.

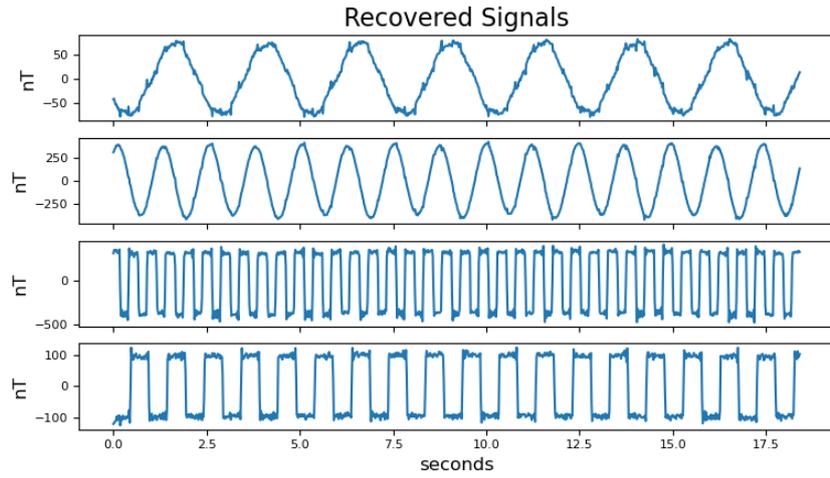


**Figure 9.** Three mixed signals recorded by PNI RM3100 magnetometers. The five signals present are two sine waves, two square waves, and the added residual magnetic field data.

The algorithm was run on this data following the same steps as in Figure 4 and section 3.1. The signals were detrended and bandpassed with frequency ranges of [0.01 Hz, 0.51 Hz], [0.07 Hz, 3.76 Hz], and [0.51 Hz, 25 Hz]. The signals were then transformed into the Time-Frequency domain using the NSGT with a quality factor of  $Q = 10$ . In step 4, low energy points were removed using a  $\lambda = 0.09$ . The resulting data were transformed into  $H(t,k)$  and clustered by DBSCAN with parameters  $eps = 0.3$  and  $MinPts = 3$ . DBSCAN discovered the following five clusters shown below in the columns of  $\hat{K}$ .

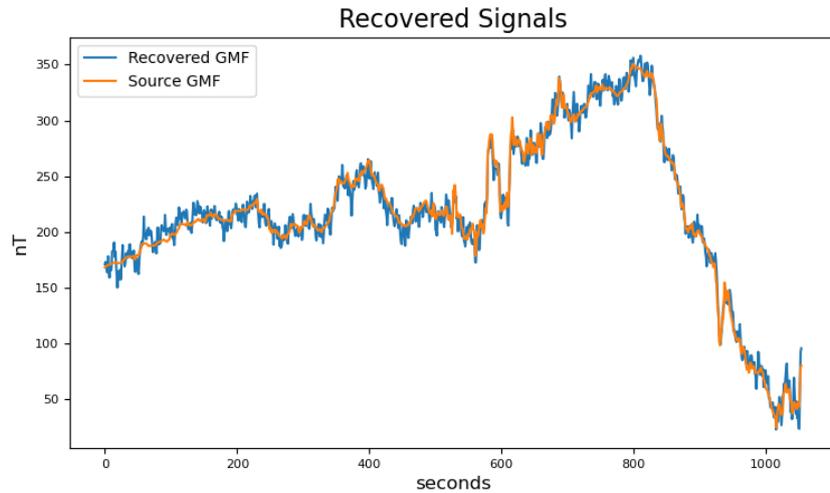
$$\hat{K} = \begin{bmatrix} 1 \angle 0 & 0.023 \angle 0 & 0.22 \angle 0 & 0.93 \angle 0 & 0.02 \angle 0 \\ 1 \angle 0 & 0.55 \angle 1.31 & 0.97 \angle 3.09 & 0.35 \angle 3.04 & 0.04 \angle 6.04 \\ 1 \angle 0 & 0.79 \angle 4.58 & 0.001 \angle 2.94 & 0.15 \angle 0.255 & 0.82 \angle 2.84 \end{bmatrix} \quad (15)$$

335 The PNI RM3100 magnetometer was experimentally found to have a lower noise  
 336 floor when sampled at a higher rate and decimated to a lower rate versus only being sam-  
 337 pled at a lower rate. We evaluated this effect by testing step 7, signal reconstruction, on  
 338 the original 50 Hz data, 10 Hz and 1 Hz data attained through downsampling, and 50  
 339 Hz data averaged with a moving mean ( $N = 10$ ). These signals were separated via com-  
 340 pressive sensing using the recovered mixing matrix,  $\hat{K}$ , in Equation 15. The four recon-  
 341 structed noise signals from the 50 Hz raw data are shown in Figure 10.



**Figure 10.** Reconstructed Sine and Square wave signals from 50 Hz mixed signals in Figure 9.

342 The reconstructed coil-generated signals closely resemble square and sine waves with  
 343 some additional noise. The recovered residual magnetic field data are shown in Figure  
 344 11. The recovered signal is overlaid with the true residual magnetic field signal. The  
 345 residual data in Figure 11 was reconstructed using the mixed signals decimated to a sam-  
 346 pling rate of 10 Hz.



**Figure 11.** True magnetic perturbation data in orange versus the recovered magnetic perturbation signal in blue. The signal was reconstructed using the mixed signals in Figure 9 decimated to a sampling rate of 10 Hz.

The reconstructed signal closely follows the true geomagnetic perturbation signal with some high frequency noise present. As a result of the geomagnetic field signal being artificially inserted into the magnetometer readings, we are able to calculate the RMSE and Pearson Correlation Coefficient with respect to the original signal. The results for the original, decimated, and moving-mean signals are shown in the following table.

Metrics				
	50 Hz	10 Hz	1 Hz	Moving Mean (N=10)
$\rho$	0.979	0.993	0.98	0.995
RMSE	14.7 nT	5.92 nT	3.73 nT	6.91 nT
NRMSE	3.37%	1.36%	0.85%	1.58%

## 4 Discussion

In this study, we introduced a signal processing algorithm based on UBSS and demonstrated the separation of magnetic noise from geomagnetic field data. In the first experiment, we separated four simulated noise signals from SWARM residual magnetic field data. The noise signals contained both sparse sine wave signals and wideband sawtooth and square wave signals. The algorithm was able to restore the residual magnetic field signal with a correlation coefficient of  $\rho = 0.9950$  and RMSE of 5.79 nT. This experiment was repeated without artificial instrument noise and yielded a RMSE of 3.88 nT for the ULF signal. In the second experiment, we created four magnetic noise signals using copper coils to generate real magnetic field data and placed PNI RM3100 magnetometers within the bus of a mock CubeSat apparatus. The same SWARM magnetic residual data were artificially inserted into the magnetometer measurements. This experiment mimicked the computer simulated experiment, with two sparse noise signals and two wideband noise signals. With a sampling rate of 50 Hz, the SWARM data had a reconstruction error of 14.7 nT using real magnetic field data as opposed to 5.79 nT in simulation. The signal separation algorithm was executed using several additional preprocessing techniques such as decimating the sampling rate and applying a moving mean to the magnetometer data. The lowest RMSE of 3.73 nT was achieved by decimating the sample rate to 1 Hz. At 1 Hz, the PNI RM3100 magnetometer is rated to have a measurement error of 1.2 nT due to instrument noise. This result places the reconstruction error near the noise floor of the magnetometer. These results show that the proposed UBSS algorithm is effective at removing spacecraft noise from magnetic field data.

In general, it is not feasible to adaptively cancel spacecraft noise when a single magnetometer is used. Adaptive noise cancellation requires the removal of noise signals that are time variable. The use of a single magnetometer requires that spacecraft noise be carefully characterized before launch. Otherwise, a change in spacecraft behavior may require special maneuvers to re-characterize noise signatures in situ (Miles et al., 2019). The use of multiple magnetometers allows for the discovery of noise signals through the comparison of magnetometer data. Sheinker and Moldwin (2016), Deshmukh et al. (2020), and Imajo et al. (2021) each propose algorithms for noise cancellation using multiple magnetometers. The algorithm proposed by Sheinker and Moldwin (2016) is effective at removing a single noise signal, but is not designed for multiple noise signals. Imajo et al. (2021) propose the use of ICA which is also limited by how many noise signals it can remove. ICA requires that the number of noise signals be less than the number of magnetometers. Spacecraft contain many electrical systems that could generate magnetic interference, so this condition is rarely met. The advantage of the proposed UBSS algorithm over Imajo et al. (2021) and Sheinker and Moldwin (2016) is that it can cancel noise signals in an underdetermined system. This means that there are more noise signals present than magnetometers. This property of the algorithm provides the flexibility necessary to be applied to many different spacecraft without prior characterization of spacecraft noise. The algorithm also does not require knowledge of magnetometer location and orientation. Finally, Deshmukh et al. (2020) designed a state estimation algorithm to trans-

395 form housekeeping data to magnetic noise signals. Housekeeping currents provide an in-  
 396 complete mapping of the distribution of currents within a spacecraft. The advantage of  
 397 the proposed UBSS algorithm over this approach is that it is a blind signal processing  
 398 algorithm. It requires no housekeeping data to identify and remove noise signals.

399 The proposed algorithm functions on the assumption that the noise signals are sparse,  
 400 meaning that only one noise signal is present at a given frequency. Multiple noise sig-  
 401 nals may be active at the same time, however, if a signal is not sparse in the frequency  
 402 domain, then its mixing vector cannot be accurately estimated by cluster analysis. Com-  
 403 pressive sensing also requires sparsity in order to accurately reconstruct the separate sig-  
 404 nals. Compressive sensing can fully reconstruct sparse signals, and approximately recon-  
 405 struct near sparse signals. In this work, we do not exhaustively explore the minimum  
 406 sparsity required for accurate reconstruction of the ambient magnetic field.

407 The proposed algorithm requires that several parameters be set by the user. In this  
 408 study, the parameters were manually selected based on the signals being analyzed, but  
 409 this process could also be automated. The first parameter is the quality factor,  $Q$ . This  
 410 parameter adjusts the window size used in the Non-Stationary Gabor Transform. We  
 411 experimentally selected it, but it may be chosen based on the length of the signal be-  
 412 ing processed. The parameter,  $\lambda$ , is used to remove low energy noise signals. Data points  
 413 that are below a fraction,  $\lambda$ , of the maximum energy data point are removed before clus-  
 414 tering occurs. We selected this parameter by analyzing the data projected onto the half-  
 415 unit hypersphere in Figure 2, and visually observing if the signals were clusterable. If  
 416  $\lambda$  is too small, then the hypersphere will be completely filled with data points, and the  
 417 noise signals will not be separable. If  $\lambda$  is too large, then small noise signals may not ap-  
 418 pear at all. Lastly, DBSCAN requires that two parameters,  $eps$ , and  $MinPts$ , be selected.  
 419 The parameter,  $eps$ , represents the maximum distance allowed for two data points to be  
 420 considered neighbors. The parameter,  $MinPts$ , represents the number of neighbors re-  
 421 quired for a data point to be considered a core.  $MinPts$  may be selected based on the  
 422 length of signal being processed. A disadvantage of using NSGT and DBSCAN together  
 423 is that more data points are created for higher frequency signals because the window size  
 424 is altered based on frequency. Therefore,  $MinPts$  should be selected based on the lower  
 425 frequency signals.

426 Most heliophysics missions require magnetic field accuracies of better than 1 nT  
 427 (e.g., the NASA MMS mission [Russell et al., 2016]). The lowest error achieved in this  
 428 experiment is 3.73 nT. This error is near the expected measurement noise for the PNI  
 429 RM3100 magnetometer at 1 Hz, indicating that the accuracy of the algorithm is limited  
 430 to the total error budget of the magnetometer. Nevertheless, the experiments performed  
 431 show successful reconstruction of magnetic perturbation signals measured from within  
 432 the bus of a mock CubeSat. These results demonstrate the utility of boomless CubeSats  
 433 for scientific investigation of magnetic field phenomena in the geospace environment. In  
 434 turn, the low cost of CubeSats enables the use of large constellations of small satellites  
 435 to measure the geomagnetic field with high temporal and spatial resolution.

## 436 5 Conclusions and Future Work

437 In this study, we propose an algorithm for separating spacecraft generated mag-  
 438 netic noise from geomagnetic field data using multiple magnetometers. The algorithm  
 439 does not require knowledge of the characteristics (location, orientation, amplitude, or  
 440 spectral signature) and allows the number of noise sources to exceed the number of mag-  
 441 netometers ( $n > m$ ). The algorithm identifies signals by looking at the relative gain and  
 442 phase of the magnetometer data in the Time-Frequency domain. If a noise signal is sparse  
 443 in this domain, the relative gain and phase is found using cluster analysis. Following the  
 444 same assumption of sparsity, the signal can be separated from the noisy data using the  
 445 cluster centroids in compressive sensing.

446 The algorithm is designed for underdetermined systems in which there are more  
 447 noise sources than magnetometers. An advantage of this approach is that the UBSS al-  
 448 gorithm can be integrated onto any satellite since no prior characterization of noise sig-  
 449 nals is required. This design eases the assimilation of magnetometers into spacecraft de-  
 450 signs by reducing the need for strict magnetic cleanliness requirements and long mechan-  
 451 ical booms.

452 There are several avenues of future development for this algorithm. The most im-  
 453 mediate step to be taken is for the selection of parameters to be automated. We present  
 454 an algorithm to automate the noise cancellation process, but some rudimentary analy-  
 455 sis is still required to select parameters for clustering and pre-processing. We think the  
 456 selection of parameters could be entirely automated. Another avenue of development is  
 457 to test the limits of the sparsity assumption. Sparsity is a very strict assumption that  
 458 may not always be met. In this work, we tested the algorithm using several wideband  
 459 signals. However, the threshold for minimum sparsity is unknown. This assumption can  
 460 be examined through examining signals with partially overlapping spectra to find a point  
 461 of failure. Finally, an interesting scenario to investigate is where several magnetometers  
 462 are mounted within the bus of a spacecraft, but one magnetometer is mounted on a short  
 463 boom, such as on the spacecraft Dellinger (Kepko et al., n.d.). In this scenario, the mea-  
 464 surements of one magnetometer may be more accurate than the others. It would be coun-  
 465 terproductive if the reconstructed magnetometer signal had more noise than the signal  
 466 measured by the magnetometer on the boom. It may be possible to account for this by  
 467 designing a programmable "trust" parameter at the compressive sensing stage. This pa-  
 468 rameter would indicate an elevated degree of trust in one magnetometer over the oth-  
 469 ers.

470 In this work, we performed two experiments to validate the algorithm. The first  
 471 experiment separated SWARM magnetic perturbation data from four computer simu-  
 472 lated signals. The algorithm was able to reconstruct the ambient magnetic field signal  
 473 with an RMSE near 5 nT and a correlation of  $\rho \approx 0.995$ . The reconstruction errors are  
 474 slightly less than the 6 nT intrinsic instrument noise that was added to each virtual mag-  
 475 netometer. The second experiment used real magnetic noise signals generated by cop-  
 476 per coils, and the same SWARM geomagnetic field data. This experiment was able to  
 477 separate four noise signals and reconstruct the background magnetic perturbation sig-  
 478 nal with a RMSE of 5.92 nT and a correlation of  $\rho = 0.993$  at a 10 Hz cadence.

479 These results show the potential of signal processing algorithms to identify and re-  
 480 move magnetic noise from spaceborne magnetometer data. The proposed algorithm di-  
 481 minishes the need to place a magnetometer on a boom. This enables the possibility of  
 482 low cost, boomless spacecraft to capture high fidelity magnetic field measurements.

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