# Hydrothermal Exploration of the southern Chile Rise: Sediment-hosted venting at the Chile Triple Junction.

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#### Abstract

We report results from a hydrothermal plume survey along the southernmost Chile Rise from the Guamblin Fracture Zone to the Chile Triple Junction encompassing two segments (93km cumulative length) of intermediate spreading-rate mid-ocean ridge axis. Our approach used *in situ* water column sensing (CTD, optical clarity, redox disequilibrium) coupled with sampling for shipboard and shore based geochemical analyses ( $d^{3}$ He, CH<sub>4</sub>, TDFe, TDMn) to explore for evidence of seafloor hydrothermal venting. Across the entire survey, the only location at which evidence for submarine venting was detected was at the southernmost limit to the survey. There, the source of a dispersing hydrothermal plume was located at 46°16.5'S, 75°47.9'W, coincident with the Chile Triple Junction itself. The plume exhibits anomalies in both  $d^{3}$ He and dissolved CH<sub>4</sub> but no enrichments in TDFe or TDMn beyond what can be attributed to resuspension of sediments covering the seafloor where the ridge intersects the Chile margin. From comparison with the Escanaba Trough on the southern Gorda Ridge, we infer that the anomalies we report here arise from sediment-hosted venting at the Chile Triple Junction.

#### Table S1: Water Column Analytical Data, RV Melville Cruise MV1003 (2010)

Lacation         Cast#         Bottle #         Latitude         Longitude         Depth         33He         CH4         TOFe         TOM           Seg2         27         1         45%145         76%21W         442         28.00         0.5           Seg2         27         3         999         28.66         0.5           Seg2         27         4         45%1.65         76%21W         3756         26.74         0.4           Seg2         27         6         50%2         776         26.74         0.4           Seg2         27         7         4         45%1.65         76%1.6W         3000         0.6           Seg2         27         7         4         45%4.58         76%47.7W         3000         0.6           Seg2         27         10         45%0.78         76%46.7W         3005         1.1           Seg2         27         14         45%0.4%         76%45.7W         3000         1.1           Seg2         27         16         45%1.7%         76%45.5W         3200         1.1           Seg2         27         16         45%1.7%         76%45.5W         3200         2.14										
m         (m)         (k)         (mM)         (m)         (	Location	Cast#	Bottle #	Latitude	Longitude	Depth	∂3He	CH4	TDFe	TDMn
Seg 2         2T         1         45%1.4%         76%2.1%         4142         28.80         0.5           Seg 2         2T         3         3999         28.66         0.5           Seg 2         2T         4         45%1.4%         75%1.8%         3956         26.74         0.4           Seg 2         2T         4         45%1.5%         76%1.8%         3956         26.79         0.5           Seg 2         2T         6         3500         0.6         3000         0.6           Seg 2         2T         7         6         45%4.5%         76%4.7W         300         0.4           Seg 2         2T         8         45%5.6%         76%4.6W         3000         1.1           Seg 2         2T         10         45%5.6%         76%4.6W         3000         1.1           Seg 2         2T         14         45%5.6%         76%4.6W         3000         1.1           Seg 2         2T         18         45%5.4%         76%4.6W         3000         1.1           Seg 2         2T         18         45%5.4%         76%4.6W         3000         2.74         0.5           Seg 2         2T						(m)	(%)	(nM)	(nM)	(nM)
Seg 2         21         1         4541.45         0"52.1"W         4142         20.80         0.5           Seg 2         21         3         3         3099         26.66         0.6           Seg 2         21         3         3         3099         26.66         0.6           Seg 2         21         4         4541.65         7651.47         3999         26.6         0.6           Seg 2         21         6         4546.55         76"47.8"         3990         26.6         0.6           Seg 2         21         6         45'46.55         76"47.8"         3000         0.6         3000           Seg 2         21         6         45'46.55         76"47.8"         3000         27.35         0.6           Seg 2         21         10         3250.45         70"46.6"         3000         1.5         300           Seg 2         21         14         45'56.6%         70"46.5"         3000         1.5         300           Seg 2         27         16         45'57.0%         70"45.5"         300         1.6         300           Seg 2         27         16         45'57.3%         70"3.8"W	00	07	4	15111 110	70250 45**	4440	00.00	0.5	r	
Jampa         Jampa <th< td=""><td>Seg 2</td><td>21</td><td>1</td><td>45'41.4'S</td><td>16"52.1"W</td><td>4142</td><td>26.80</td><td>0.5</td><td></td><td></td></th<>	Seg 2	21	1	45'41.4'S	16"52.1"W	4142	26.80	0.5		
Seg2         1         3         4         4541.6S         7651.6W         3566         20.76         0.51           Seg2         2T         5         4545.5S         7647.6W         3775         0.6           Seg2         2T         6         5         4545.5S         7647.6W         3775         0.6           Seg2         2T         6         4545.5S         7647.7W         3300         0.3           Seg2         2T         6         4546.5S         7647.7W         3300         0.3           Seg2         2T         10         520.72         50.6         520.72         50.6           Seg2         2T         11         3200         271.22         0.6         535.82           Seg2         2T         13         4556.75         7645.6W         3000         1.1         55.82           Seg2         2T         16         3500         1.1         3566         320.74         0.5           Seg2         2T         18         4554.1%         7645.6W         3000         1.1         356           Seg2         2T         19         457.0%         7645.8W         3500         2.744         0.5	Seg 2	21	2			3999	20.00	0.0		
Seg 2         2T         5         45'45.55         76'47.5''         20'5         0.5           Seg 2         2T         5         45'45.55         76'47.5''         3600         0.6           Seg 2         2T         7         6         3800         0.4           Seg 2         2T         7         7         3600         0.5           Seg 2         2T         7         7         3200         0.3           Seg 2         2T         9         45'46.95'         76'45.6W         3600         0.3           Seg 2         2T         10         54'40.95'         76'45.6W         3000         0.3           Seg 2         2T         10         45'50.4''         70'45.6W         3000         1.1           Seg 2         2T         14         45'50.4'''         70'45.5W         3000         1.1           Seg 2         2T         16         3000         1.1         1.5           Seg 2         2T         16         45'51.7'''         70'45.5W         3000         1.1           Seg 2         2T         16         45'51.1''         75'58.3'W         3200         27.44         0.5           S	Seg 2	21	4	45°41 6'9	76°51 8'\^/	3506	26.79	0.4		
leng 2         2T         5         45%45.55         76%47.5W         3775         0.6           Seg 2         2T         7         7         300         0.6           Seg 2         2T         7         7         300         0.6           Seg 2         2T         7         7         300         0.3           Seg 2         2T         7         7         45%45.65         76%47.7W         300         0.3           Seg 2         2T         10         45%45.65         76%46.5W         3050         22.55         0.6           Seg 2         2T         11         45%5.6%         76%46.5W         3000         1.5           Seg 2         2T         14         45%5.6%         76%45.5W         3000         1.5           Seg 2         2T         16         3500         1.5         3000         1.1           Seg 2         2T         18         45%1.75         76%45.5W         3200         2.74         0.5           Seg 2         2T         18         45%1.75         76%45.5W         3200         2.74         0.5           Seg 2         2T         24         575.73%         76%38.W         <	Jeg z	21		43 41.03	70 31.0 W	3380	20.75	0.5		
Seg2         2T         6         300         0.6           Seg2         2T         7         3450         0.4           Seg2         2T         8         454585         7647.7W         3300         0.3           Seg2         2T         10         3450         2725         0.6           Seg2         2T         10         3205         2725         0.6           Seg2         2T         11         3205         2220         0.7           Seg2         2T         13         4550.4S         7646.6W         2020         0.7           Seg2         2T         15         3200         1.1         350         320         0.7           Seg2         2T         16         4550.4S         7646.6W         2000         1.5         300         1.1           Seg2         2T         16         4551.7S         7645.5W         220         0.7         300           Seg2         2T         19         4557.7S         7645.5W         3200         27.44         0.5           Seg2         2T         23         4557.7S         7653.2W         3200         2.442         2.1           A </td <td>Seg 2</td> <td>2T</td> <td>5</td> <td>45°45.5'S</td> <td>76°47.8'W</td> <td>3775</td> <td></td> <td>0.6</td> <td>1</td> <td></td>	Seg 2	2T	5	45°45.5'S	76°47.8'W	3775		0.6	1	
Seg 2         2T         7         450         0.4           Seg 2         2T         8         454585         76477.W         3300         0.3           Seg 2         2T         9         4546.95         76477.W         3300         0.5           Seg 2         2T         10         4546.97         7646.6W         3200         27.35         0.6           Seg 2         2T         11         4550.45         7646.6W         2200         27.15         0.6           Seg 2         2T         12         3075         28.20         0.7         5360         7645.6W         200         2.816         0.4           Seg 2         2T         16         4550.65         7645.6W         3000         1.1         5500         1.1           Seg 2         2T         19         4557.03         7640.3W         3000         27.44         0.5           Seg 2         2T         20         4557.35         7653.8W         3300         27.44         0.5           Seg 2         2T         23         4557.35         7558.3W         320         2.442         2.1           Seg 2         2T         23         4557.35 <t< td=""><td>Seg 2</td><td>2T</td><td>6</td><td></td><td></td><td>3600</td><td></td><td>0.6</td><td></td><td></td></t<>	Seg 2	2T	6			3600		0.6		
Seg2         2T         9         4545.85         7547.7W         3300         0.3           Seg2         2T         9         4549.95         7546.7W         300         27.35         0.6           Seg2         2T         10         3250         27.25         0.6           Seg2         2T         11         3250         27.25         0.6           Seg2         2T         11         3250         27.21         0.3           Seg2         2T         14         4556.95         7646.6W         2022         28.16         0.4           Seg2         2T         16         3500         1.1         3586.2         37.6         1.1           Seg2         2T         16         4556.75         7646.5W         3500         1.1           Seg2         2T         16         457.73         7645.5W         3200         2.74         0.5           Seg2         2T         10         457.73         7645.5W         3200         2.74         0.5           Seg2         2T         12         457.73         77645.5W         3200         2.435         1.0           Seg2         2T         12         457	Seg 2	2T	7			3450		0.4		
Seg 2         2T         9         45'40.9"         76'46.6"         3600         27.35         0.6           Seg 2         2T         10         3425         27.25         0.6           Seg 2         2T         11         3250         27.21         0.3           Seg 2         2T         12         3075         28.29         0.7           Seg 2         2T         14         45'50.4"         76'46.6"         2021         28.16         0.4           Seg 2         2T         14         45'50.4"         76'46.6"         2021         28.16         0.4           Seg 2         2T         16         5000         1.1         500         1.1           Seg 2         2T         16         45'51.75         75'64.5"         27.44         0.5           Seg 2         2T         19         45'51.1'5         75'58.3'W         3200         27.44         0.5           Seg 2         2T         23         45'51.1'5         75'58.3'W         3200         24.45         1.0           A         1T         4         45'51.1'5         75'54.3'W         200         26.66         0.3           Seg 2         2T	Seg 2	2T	8	45°45.8'S	76°47.7'W	3300		0.3		
Seg 2         21         9         4'54.92's         7'6'46'W         3600         27.35         0.6           Seg 2         21         10										
Seg 2         21         10         342.5         27.45         0.6           Seg 2         21         11         346.5         77.45         0.6           Seg 2         21         13         4550.45         76.46.6W         2002         28.16         0.4           Seg 2         21         13         4550.45         76.46.6W         2002         28.16         0.4           Seg 2         21         15         5000         1.1         15           Seg 2         21         16         3000         0.7           Seg 2         21         16         3000         1.1           Seg 2         21         18         4551.15         76*45.5W         220         0.8           Seg 2         21         19         45*51.7S         76*45.5W         220         0.8           Seg 2         21         20         5000         27.68         0.3           Seg 2         21         22         3000         24.42         2.1           A         17         4         45*51.25         75*58.3W         3200         26.64         1.5           B         17         6         46*01.25         75*54.	Seg 2	21	9	45°49.9'S	76°46.6'W	3600	27.35	0.6		
Jampa 2         2.1         1.2         Jampa 2         2.1         0.3           Seg2 2         2T         12         4550.45         76'46.5W         2002         28.16         0.4           Seg2 2         2T         13         45'50.45         76'46.5W         2002         28.16         0.4           Seg2 2         2T         16         45'56.65         76'46.5W         3000         1.1           Seg2 2         2T         16         3000         1.1         35'5         322'5         0.5           Seg2 2         2T         18         45'54.15         76'45.5W         3200         0.7         35'5           Seg2 2         2T         18         45'54.15         76'45.5W         3200         2.7.44         0.9           Seg2 2         2T         20         55'53.2W         3500         2.7.44         0.3           Seg2 2         2T         22         45'57.35         75'38.2W         328         2.44         2.1           A         1T         4         45'51.15         75'58.2W         3800         2.7.68         0.3           Seg2 2         2T         23         45'51.25         75'54.2W         286	Seg 2	21	10			3425	27.25	0.5		
Curry -         2.         -<	Seg 2	21 2T	12			3075	28.20	0.3		
S         1         1         1         1         1         1           Seg 2         2T         14         4556.68         7645.6W         3705         1.1           Seg 2         2T         15         3600         1.1         3           Seg 2         2T         16         3600         1.1         3           Seg 2         2T         16         3600         1.1         3           Seg 2         2T         18         45'54.15         76'45.5W         2260         0.5           Seg 2         2T         18         45'57.05         76'40.5W         3600         27.44         0.9           Seg 2         2T         20         3600         27.66         0.3         3500         27.66         0.3           Seg 2         2T         23         45'57.35         76'39.6W         3500         27.66         0.3           Seg 2         2T         23         45'51.15         75'58.2W         3200         24.42         2.1           A         1T         4         45'51.25         75'58.2W         3200         24.42         2.1           A         1T         6         46'01.2'5	Seg 2	2T	13	45°50.4'S	76°46.6'W	2902	28.16	0.4		
Seg2         2T         14         4596.65         76'45.8''         3706         1.1           Seg2         2T         16         3000         1.5           Seg2         2T         19         45'51.7'S         76'40.3''         3900         27.44         0.9           Seg2         2T         20         3050         27.47         0.5         3900         27.44         0.9           Seg2         2T         23         45'51.1'S         75'58.3''W         3200         24.42         1.0           A         1T         4         5'51.1'S         75'58.3'W         3200         24.42         1.0           A         1T         4         5'51.1'S         75'58.3'W         3200         24.42         1.0           A         1T         7         5'58.3'W         3200         24.42         1.0           A         1T         7         75'58.3'W         3200         24.42         1.0           A <td>oog z</td> <td></td> <td>10</td> <td>.0 00.40</td> <td></td> <td>LUUL</td> <td>20.10</td> <td>0.4</td> <td>L</td> <td></td>	oog z		10	.0 00.40		LUUL	20.10	0.4	L	
Beg 2         2T         15         3600         1.5           Seg 2         2T         16	Seg 2	2T	14	45°56.6'S	76°45.8'W	3705		1.1	ſ	
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Seg 2	2T	16			3500		1.1		
Beg 2         2T         18         455.415         7043.5W         3250         0.8           Seg 2         2T         19         4557.0S         7040.5W         3950         27.44         0.9           Seg 2         2T         20         3756         27.47         0.5           Seg 2         2T         21         3652         27.47         0.3           Seg 2         2T         22         3650         27.68         0.3           Seg 2         2T         23         4557.3S         7579.38.7W         3280         24.42         2.1           A         1T         1         4551.15         75758.3'W         3280         24.42         2.1           A         1T         2         4571.25         75758.3'W         3200         26.44         1.5           B         1T         4         4571.25         75754.3'W         3000         26.44         1.5           B         1T         7         8         7700         27.65         0.4         0.3           C         1T         10         46701.75         7575.17W         200         27.65         0.6           C         1T         10<	Seg 2	2T	17			3400		0.7		
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Seq 2         2.1         10         45 5/35         70 40 3/3         3300         27.44         0.9           Seg 2         21         20         3706         27.47         0.3           Seg 2         21         22         3602         27.47         0.3           Seg 2         21         22         3602         27.47         0.3           Seg 2         21         23         457.735         76 93.67         3500         27.68         0.3           A         11         4         551.15         7578.37%         3000         42.42         2.1           A         11         2         3000         27.68         0.3         3000         42.43         1.0           A         11         4         6551.125         7558.37%         2000         24.42         2.1           A         11         6         4551.25         7554.37%         2000         24.64         1.0           A         17         6         4601.25         7554.37%         200         27.46         0.4           B         17         6         4601.75         7551.7%         200         27.46         0.4           B </td <td>Sec. 2</td> <td>27</td> <td>10</td> <td>45%57.0%</td> <td>76°40 2%4</td> <td>2050</td> <td>27.44</td> <td>0.0</td> <td>r</td> <td></td>	Sec. 2	27	10	45%57.0%	76°40 2%4	2050	27.44	0.0	r	
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	Seq 2	21 2T	22			3500	27.68	0.3		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Seg 2	2T	23	45°57.3'S	76°39.8'W	3350	27.99	0.3		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					//					
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	А	1T	1	45*51.1'S	75*58.3'W	3228	24.42	2.1		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	A	1T	2			3000	24.35	1.0		
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	A	1T	4	45*51.2'S	/5"58.2'W	2499	26.64	1.5	l	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$										
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	В	1T	6	46*01.2'5	75*54.3'W	3200	26.48	0.9	1	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	в	1T	7			2999	26.09	0.3		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	в	1T	8			2750	28.44	0.4		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	в	1T	9			2700	27.65	0.4		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	В	1T	10	46*01.7'S	75*54.1'W	2500	27.94	2.0		
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$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	C	1T	11	46*08.3'S	/5*51.9'W	3007	26.86	0.8		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	c c	11	12			2900	27.55	0.5		
C         11         16         46'12.8'S         75'49.8'W         2860         28.43         5.6           D         1T         16         46'12.8'S         75'49.8'W         2800         28.43         5.6           D         1T         17         2001         28.43         5.6           D         1T         19         46'13.0'S         75'49.6'W         2000         28.43         5.6           D         1T         19         46'13.0'S         75'49.6'W         2000         34.58         26.3           E         1T         20         46'16.4'S         75'47.6'W         2000         34.58         26.3           E         1T         20         46'16.5'S         75'47.6'W         2000         34.58         26.3           E         1T         24         46'16.5'S         75'47.6'W         2000         34.58         26.3           F         12V         9         46'16.4'S         75'47.6'W         2000         28.06         4.4           E         1T         24         46'16.5'S         75'47.6'W         2000         28.5         2.3         5.8         2.8           F         12V         6	c	11	14	46*08 5'5	75*51 7'W	2799	27.99	-0.2		
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	D	1T	17			2801	28.43	5.8		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	D	1T	18			2700	31.00	18.1		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	D	1T	19	46*13.0'S	75*49.6'W	2600	28.56	1.8		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$									r	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	E	1T 4T	20	46°16.4'S	/5°47.9'W	2600	34.58	26.3		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	E	1T 4T	21			2/00	38.92	52.2		
L	F	11	22			2800	28.66	20.9		
F         12V         9         46*15.4*S         75*48.4*W         2500         28.21         2.3         25.4         2.9           F         12V         6         2600         2000         2.3         59.8         2.8           F         12V         6         2600         2000         2.3         59.8         2.8           F         12V         5         2700         30.51         13.5         75.6         4.6           F         12V         4         2790         30.55         25.5         53.9         4.7           F         12V         3         2800         208.3         12.1         95.4         5.5           F         12V         2         2000         22.60         10.5         70.6         4.9           F         12V         1         46*15.4*3         75*48.4*W         2954         28.8         8.0         79.5         5.2	E	1T	23	46*16.5'S	75*47.8'W	2500	30.82	7.7		
F         12V         9         46°15.4%         75°48.4%         2500         28.21         2.3         25.4         2.9           F         12V         6         2600         200         2.3         5.8         2.8           F         12V         5         2600         2.00         5.8         2.8           F         12V         5         2700         30.51         13.5         75.6         4.6           F         12V         4         2700         33.55         25.5         5.9         4.7           F         12V         3         2800         28.83         12.1         95.4         5.5           F         12V         3         2800         28.03         10.5         70.6         4.9           F         12V         1         46°15.4%         75°48.4W         2900         28.6         8.0         79.5         5.2	-		24	0.00		2200			L	
F         12V         6         2600         200         2.3         59.8         2.8           F         12V         5         2700         30.51         1.35         75.6         4.6           F         12V         4         2700         30.51         1.35         75.6         4.6           F         12V         4         2700         30.55         25.5         53.9         4.7           F         12V         2         2800         28.8         12.1         95.4         5.5           F         12V         2         2000         2900         12.5         0.6         4.9           F         12V         1         46*15.4%         75*48.4W         2954         28.8         8.0         79.5         5.2	F	12V	9	46°15.4'S	75°48.4'W	2500	28.21	2.3	25.4	2.9
F         12V         5         2700         30.51         13.5         75.6         4.6           F         12V         4         2790         33.55         25.5         53.9         4.7           F         12V         3         2850         29.83         12.1         95.4         5.5           F         12V         2         2900         29.05         10.5         7.6         4.9           F         12V         1         46*15.4°S         75*48.4W         2954         28.8         8.0         79.5         5.2	F	12V	6			2600	29.09	2.3	59.8	2.8
F         12V         4         2790         33.55         25.5         53.9         4.7           F         12V         3         2850         29.83         12.1         95.4         5.5           F         12V         2         2900         29.50         10.5         70.6         4.9           F         12V         1         46°15.4°S         75'48.4°W         2954         28.88         8.0         79.5         5.2	F	12V	5			2700	30.51	13.5	75.6	4.6
F         12V         3         2850         29.83         12.1         95.4         5.5           F         12V         2         2900         29.50         10.5         70.6         4.9           F         12V         1         46°15.4°S         75′48.4°W         2954         28.88         8.0         79.5         5.2	F	12V	4			2790	33.55	25.5	53.9	4.7
F         12V         2         2900         29.50         10.5         70.6         4.9           F         12V         1         46°15.4°S         75°48.4′W         2954         28.88         8.0         79.5         5.2	F	12V	3			2850	29.83	12.1	95.4	5.5
F 12V 1 46"15.4'S 75"48.4'W 2954 28.88 8.0 79.5 5.2	F	12V	2	10010 11-	BELLO 18.1	2900	29.50	10.5	70.6	4.9
	F	12V	1	46°15.4'S	75°48.4'W	2954	28.88	8.0	79.5	5.2

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2	Hydrothermal Exploration of the southern Chile Rise: Sediment-hosted venting at
3	the Chile Triple Junction.
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20	Key Points:
21 22	• Hydrothermal exploration along the southernmost Chile Rise has revealed evidence for venting located at the Chile Triple Junction.
23 24	• Hydrothermal plume signals include dissolved methane enrichments co-registered with diagnostic mantle-like Helium isotope signatures.
25 26 27	• Seafloor morphology, turbidity and TDFe, TDMn data all provide evidence that this is a sediment-hosted hydrothermal vent-field.

## 28 Abstract

- 29 We report results from a hydrothermal plume survey along the southernmost Chile Rise from the
- 30 Guamblin Fracture Zone to the Chile Triple Junction encompassing two segments (93km cumulative
- length) of intermediate spreading-rate mid-ocean ridge axis. Our approach used *in situ* water column
- 32 sensing (CTD, optical clarity, redox disequilibrium) coupled with sampling for shipboard and shore based
- 33 geochemical analyses ( $\delta^3$ He, CH<sub>4</sub>, TDFe, TDMn) to explore for evidence of seafloor hydrothermal
- 34 venting. Across the entire survey, the only location at which evidence for submarine venting was
- 35 detected was at the southernmost limit to the survey. There, the source of a dispersing hydrothermal
- 36 plume was located at 46°16.5'S, 75°47.9'W, coincident with the Chile Triple Junction itself. The plume
- 37 exhibits anomalies in both  $\delta^3$ He and dissolved CH<sub>4</sub> but no enrichments in TDFe or TDMn beyond what
- 38 can be attributed to resuspension of sediments covering the seafloor where the ridge intersects the Chile
- 39 margin. From comparison with the Escanaba Trough on the southern Gorda Ridge, we infer that the
- 40 anomalies we report here arise from sediment-hosted venting at the Chile Triple Junction.

## 41 Plain Language Summary

Since their first discovery in the 1970s, submarine hot-springs have now been located in every 42 ocean basin on Earth. But vast tracts (at least 75-80%) of the globe-encircling mid-ocean ridge 43 44 volcanic chain remain completely unexplored which means that the majority of vents, and probably an increasing diversity of styles of submarine venting, remain to be discovered. The 45 absence of discoveries is particularly acute in the southern hemisphere. Here we report results 46 47 from the southern Chile Rise, close to the Chile Margin, where a segment of volcanic mid-ocean ridge crust is actively being subducted beneath the over-riding South American continental 48 margin. The setting is unique in present-day tectonics, giving rise to unusual hydrothermal 49 signatures. But the same processes may have recurred consistently around the rim of the Pacific 50 throughout its ~200My history. 51

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## 57 **1 Introduction**

Hydrothermal activity has been demonstrated to exist in all ocean basins and along ridges of all spreading 58 59 rates [Baker & German, 2004] but the vast majority of mid-ocean ridges remain unexplored for seafloor venting; this is particularly the case in the southern hemisphere [Beaulieu et al., 2013]. Further, as 60 exploration for seafloor venting has continued along different ridge-crests, the range in geologic diversity 61 of known submarine hydrothermal fields has expanded [German & Seyfried, 2014; German et al., 2016]. 62 The southern Chile Rise represents a particularly intriguing target from this perspective because, at its 63 southernmost limit, it intersects the Peru-Chile Trench at the Chile Triple Junction (Fig.1a). This setting 64 is geologically unique because it represents the only location on Earth at which a mid-ocean ridge is 65 currently being subducted beneath a continental margin [Cande et al., 1987]. It is to be expected, 66 however, that such processes have recurred throughout the ~200My history of the Pacific Ocean. 67 Mapping of the southernmost four segments of the Chile Rise in 2010 provided new insights into the 68 interplay among processes associated with crustal production at the Chile Rise ridge-crest and recycling 69 70 of that ocean crust at the adjacent Peru-Chile Trench subduction zone [Blackman et al., 2012]. Here, we 71 describe results from hydrothermal exploration conducted in conjunction with that mapping effort and in 72 follow-up studies completed during a follow-on cruise in 2012. Although our geophysical investigations 73 [Blackman et al., 2012] covered the four southernmost segments of the Chile Rise (numbered 74 consecutively starting from the Chile Triple Junction), our hydrothermal investigations were restricted to 75 the southernmost two second-order ridge-segments (Fig.1b.c). 76





**Figure 1.** (a) *Inset:* regional map of the SE Pacific showing the location of the Chile Triple

Junction in broad tectonic context. *Main figure*: map of the southernmost four segments of the

80 Chile Rise mapped by Blackman et al. (2012); (b) detailed map of Segment 2 of the Chile Rise

showing track-line of CTD tow-yo completed in 2010; (c) detailed map of Segment 1 of the Chile

82 Rise showing trackline of CTD tow-yo completed in 2010, including (A-E) start/end locations for

83 five mini-profiles of water column samples that were collected along-track. Box outlines region

of 2012 field operations illustrated in Fig.3.

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86 The Chile Rise is an intermediate spreading rate mid-ocean ridge with a half spreading rate of 30mm/yr 87 which places it at a threshold in terms of underpinning geophysical processes that can impact morphology [Cande et al., 1987]. As a result of this spreading rate, variability in along-axis ridge morphology is 88 apparent between segments [Blackman et al., 2012]. Segment 2, for example (Fig.1b) is anomalously 89 deep for an intermediate spreading-rate ridge and exhibits a rift valley that is close to 1000 m deep 90 91 relative to its flanks. Its axial depth is ~3800 m toward the center of this 43 km long segment and deepens to >4000 m at either end. In contrast, Segment 1 (Fig.1c), which is offset from Segment 2 by 92 93  $\sim$ 50 km along the Darwin Fracture Zone, is notably shallower with an axial rift-valley floor depth of  $\sim$ 3200 m at its northern end near  $45^{\circ}50^{\circ}$ S. In prior work, the southern limit of Segment 1 and, hence, the 94 location of the Chile Triple Junction (CTJ) had been estimated to occur at 46°09'S [Bourgois et al., 2000] 95 where high back-scatter volcanic structures are juxtaposed against a scarp at the toe of the continental 96 97 slope. With the higher resolution mapping conducted as part of our 2010 survey [Blackman et al., 2012], 98 it was possible to identify fault scarps within the western rift-valley wall of Segment 1 that allow us to extend its length south to  $\sim 46^{\circ}16$ 'S (Fig.1c). The rift-valley floor reveals a chain of volcanic structures 99 each <400 m in diameter that fall along the center-line of the graben at the northern end of the segment. 100 101 Further south, beyond  $\sim 46^{\circ}05$ 'S, such features are increasingly obscured by terrigenous sediment shed 102 from the adjacent continental margin. From 46°06'-46°12'S, some small volcanic features (diameter ~1 103 km each) are still discernible rising above the sediment fill [Blackman et al., 2012] but the morphology of 104 the rift-valley floor becomes monotonously flat and featureless from  $\sim 46^{\circ}12^{\circ}$  to the triple junction at 105 ~46°16'S (Fig1c).

### 106 2 Materials and Methods

107 2.1 At Sea Operations & Sample Collection

The hydrothermal plume investigations described in this study were all conducted aboard RV Melville 108 109 during two short cruises of opportunity conducted in 2010 (MV 1003) and 2012 (MV 1205). Surveys 110 along the axis of the ridge-crest were first conducted using the ship's Seabird 911+ CTD rosette which 111 was equipped with a transmissometer and - specific to our work – two different *in situ* redox probes that 112 were provided from NOAA-PMEL in 2010 and from AIST-Japan in 2012. Initially, the entire sensor suite was mounted to a 24-position rosette and towed at speeds of ~1.5 kt along the full length of each of 113 114 Segment 2 and Segment 1 (Fig.1b, c) lowering and raising the package through the deep portion of the water column in "tow-yo" mode between depths of ~2500 m and a safe operating altitude above the 115 116 seafloor (typically ~50m). Traditionally, such approaches have proven very effective at intercepting hydrothermal plumes dispersing away from high temperature hydrothermal fields [Baker & German, 117

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118 2004] although it is now increasingly recognized that such approaches, in isolation, may under-report the 119 full extent of submarine venting present along fast and intermediate spreading ridges [Baker et al., 2016; 120 Chen et al., 2020]. In addition to these initial tow-yo surveys, vertical casts of the CTD-rosette package were conducted in 2010 while in 2012, a combination of tow-yo, vertical casts and "pogo" stations were 121 employed. For the latter deployment type, the ship was repositioned over short distances to different 122 123 locations to collect a series of vertical mini-profiles through the deep (>2500m) water column, within a single deployment. Importantly, an ultra-short baseline (USBL) navigation beacon was attached to the 124 CTD-rosette for all deployments in 2010 and 2012 to ensure that we could navigate precisely where all 125 samples and ancillary data were collected, as well as their sample depths (Suppl. Tables 1 & 2). 126

127

128 In parallel with our *in situ* sensing approach to hydrothermal plume detection, water samples were 129 collected routinely. Initially, short mini-profiles (4-5 samples each) were collected at key way-points along the length of each of our segment-long "tow-yo" surveys, for a combination of shipboard and 130 131 shore-based geochemical analyses diagnostic of submarine vent influence. First, from each Niskin, water samples were drawn for shore-based helium isotope analyses. Immediately upon recovery of the CTD-132 rosette, air-free water samples were flushed through 24 inch long sections of refrigeration-grade Cu 133 134 tubing, with duplicate half-sections, and cold-weld sealed for on-shore laboratory determinations of He 135 concentrations and isotope ratios [Young and Lupton, 1983]. Next, 100 mL of bubble-free fluid was 136 drawn directly into 140 mL syringes for shipboard methane analysis. Any air bubbles were removed 137 immediately after drawing the fluid into the syringe and this was followed by the addition of 40 mL headspace gas of ultrapure helium to the samples. The samples were then shaken vigorously and allowed 138 139 to warm to room temperature (~ 30 min) to reach equilibrium for  $CH_4$  between the water and gas phase, prior to shipboard analysis. In 2010, samples for total dissolvable Fe and Mn analyses were also archived 140 141 into double-bagged 500mL polypropylene bottles that had been acid-washed for trace metal analyses prior to the cruise. Samples were drawn directly from the rosette into these sample bottles which were 142 triple-rinsed with sample and then filled, unfiltered. Samples were transferred to Woods Hole 143 Oceanographic Institution (WHOI) immediately upon completion of the cruise for trace-metal clean 144 145 processing.

146

## 147 2.2 Laboratory Analyses of Samples

148

149 After the expedition, samples collected for Helium analyses were processed at the NOAA/PMEL Helium

150 Isotope Laboratory in Newport, OR. The gas and liquid phases of the cold-welded samples were

separated using a high-vacuum extraction line. The content of each sealed Cu tube was dropped into an

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152 evacuated flask and continuously stirred with a magnetic stirrer during the extraction process. A

- 153 combined charcoal- $LN_2$  trap was then used to pump the gas phase into aluminosilicate ampoules during
- the 15 minute-long gas extraction process. The ampoules were subsequently sealed with a hot flame and
- stored dry until analysis. Isotope ratios and concentrations of helium were determined using a dual
- 156 collector, 21 cm radius, sector-type mass spectrometer specially designed for helium isotope analyses.
- 157 The precision for the helium isotope ratios in seawater samples averaged 0.2% in  $\delta^3$ He, where  $\delta^3$ He is the
- 158 percentage deviation of  ${}^{3}\text{He}/{}^{4}\text{He}$  from the atmospheric ratio.
- 159
- 160 Methane concentrations were determined at sea. After equilibration, the headspace gas was injected into a
- 161 SRI 8610C gas chromatograph. Separation of CH<sub>4</sub> was done using a 15 m long Molecular Sieve 5A
- 162 column and CH<sub>4</sub> concentrations were measured with a flame ionization detector. The measured
- 163 background seawater CH<sub>4</sub> concentration was 0.4 nM. Sampling and analytical precision, determined
- 164 through replicate draws, was <2.5% of the measured concentrations or  $\pm0.1$  nM, whichever is greater.
- 165

Analyses for total dissolvable iron (TDFe) and manganese (TDMn) were conducted on samples selected 166 from Cruise MV1003 (2010) based on shipboard dissolved CH<sub>4</sub> data. Those analyses were conducted 167 using Mg-precipitation, isotope dilution, and inductively coupled plasma mass spectrometry (ICP-MS) 168 following standard methods described elsewhere [Saito and Schneider, 2006; Noble et al., 2008]. Briefly, 169 unfiltered seawater samples were acidified to pH 1.7 using high purity HCl (SeaStar Inc) and then left for 170 4 months to allow the dissolution of labile metals in weak acid. For each analysis 13.0mL of processed 171 sample was decanted into a centrifuge tube, spiked with <sup>57</sup>Fe stable isotope and precipitated using a small 172 amount of high-purity ammonia (SeaStar Inc.) then centrifuged for 3 min at 3000 rpm (1460 x g) and 173 174 decanted. The sample was resuspended in 5% high-purity nitric acid with 1ppm indium (In) and analysis 175 was conducted on an Element 2 ICP-MS using an Aridus desolvator and platinum X-cones. Fe and Mn concentrations were calculated using the <sup>57</sup>Fe for isotope dilution and In as a recovery tracer [Saito and 176 177 Schneider, 2006]. Precisions in the measurements were typically better than  $\pm 1.0$  nM for Fe and  $\pm 0.2$  nM 178 for Mn.

- 179 **3 Results & Discussion**
- 180

#### 181 *3.1 Along-axis Surveys of the southern Chile Rise*

182 Perhaps the most remarkable result from the initial tow-yo surveys conducted in 2010 (tow-yo tracks

183 marked as white lines in Fig.1b, 1c) was that no *in situ* anomalies indicative of mid-water hydrothermal

184 plumes were observed along the cumulative ~93km of survey. This was a surprise because prior work

had shown that at least one site of high temperature hydrothermal venting should have been expected,

186 statistically, during a survey of this length along an intermediate spreading-rate ridge [Baker & German,

- 187 2004; Beaulieu et al., 2013]. Further, shipboard and shore-based geochemical analyses for dissolved
- 188 methane concentrations and He isotope composition also failed to detect hydrothermal signals throughout

189 Segment 2 (*Supp.Table S1*).

190 Within Segment 1, by contrast, analyses for these dissolved gas species revealed clear evidence for 191 seafloor hydrothermal inputs (Fig.2). Mini-profiles of water samples were collected at five locations 192 along the length of this segment at 45°51'S, 46°01'S, 46°08'S, 46°13'S and 46°16'S (positions labelled A 193 through E in Fig.1c, respectively). Throughout the northern half of the segment (locations A, B & C) no evidence for hydrothermal plume activity was apparent and values for both tracers fell into the same 194 background range as was observed in Segment 2 (Supp. Table S1). This was the case at least as far as 195 196 46°08'S where sediment begins to obscure the underlying ridge-axis morphology [Blackman et al., 2012]. Further south, however, at locations D and E a clear mid-water plume is apparent in both the  $\delta^3$ He 197 198 anomaly profile and that for dissolved methane.



199



In both cases, the maximum anomalies observed are at a depth of ~2700m with lower concentrations
below and above that depth. Further, these anomalies occur at a height of ~200-300m above the seafloor

- at the southern end of Segment 1 consistent with the heights of rise that might be expected for a
- 206 hydrothermal plume rising above a high-temperature vent-source before attaining a level of neutral

207 buoyancy and being dispersed by prevailing deep ocean currents [Lupton, 1995]. For dissolved methane, 208 the contrast between the background concentrations to the north of Segment 1 and the plume anomalies to 209 the south are marked. Further, the range of concentrations observed (20-50nmol/L) is directly comparable to that observed for non-buoyant plumes overlying other high-temperature Pacific Ocean 210 211 vent-sites [Lilley et al., 1995]. Along the Chile margin, immediately to the north of the Chile Triple Junction, thermal destabilization of gas hydrates beneath the sediments of the continental margin arises 212 213 due to the increased heat-flow that results from subduction of young oceanic crust. This thermal destabilization leads to the accumulation of large amounts of gas hydrate in an extremely thin bottom-214 simulating reflector (BSR) layer at shallow depths within the sediment and can also lead to the release of 215 dissolved methane via cold seep activity [Brown et al., 1996]. At the southern end of Segment 1, 216 217 however, the presence of  $\delta^3$ He anomalies that are unambiguously indicative of a mantle source [Lupton, 218 1983] coincident with the mid-water methane plume provides strong evidence that release of dissolved 219 methane, here, is not due to cold seep activity. A high-temperature vent source is most consistent with the combination of mid-water mantle-signature  $\delta^3$ He and dissolved CH<sub>4</sub> anomalies reported here. 220

221

#### *3.2 Hydrothermal venting at the Chile Triple Junction.*

223 We returned to the southern part of Segment 1 in 2012 to continue our exploration for this inferred hydrothermal source. Those operations began with a repeat tow-yo along the southern portion of the 224 section occupied in 2010, between 46°16'S and 46°13'S (Fig.3) which, once again, revealed no in situ 225 optical or redox anomalies indicative of hydrothermal venting but *did* exhibit mid-water plumes in  $\delta^3$ He 226 and dissolved  $CH_4$ . For both dissolved gas species, highest mid-water plume concentrations were 227 observed at the southern end of the survey, closest to the intersection of the ridge-axis and margin (Supp. 228 229 Table S2). Next, to confirm that the methane signals reported here were not related to cold-seep activity, a series of 4 vertical casts were occupied along the base of the scarp that defines the continental margin, 230 231 immediately to the east of the ridge-crest (Area G). All samples from those mini-profiles yielded background values for both  $\delta^3$ He (29.4±0.4%) and dissolved methane (4.4±1.4nmol/L) comparable to 232

values from northern Segment 1 (Fig.4, Supp. Table S2).



Figure 3. Map of the southernmost portion of Segment 1, southern Chile Rise (contour intervals: 100 m). White line denotes track of 2012 CTD tow-yo that reoccupied the southernmost portion of the 2010 tow-yo (underlying black line). Circles in areas F, G, H refer to vertical CTD profiles discussed in text. F (white): station sampled for  $\delta^{3}$ He, CH<sub>4</sub>, TDFe & TDMn in 2010; G (blue): stations along the Chile margin (2012); H (yellow, red): stations at the Chile Triple Junction (2012). Red circle represents point of closest approach to seafloor venting.

243 Three further sets of CTD-deployments were then undertaken, targeting the ridge-margin intersection at the CTJ (Area H). This yielded nine sets of vertical casts through the deep portion of the water column 244 between  $46^{\circ}16$ 'S and  $46^{\circ}17$ 'S and between  $75^{\circ}46.5$ 'W and  $75^{\circ}48.0$ 'W (Supp. Tab. 2). All of these 245 246 stations showed plume-height  $\delta^3$ He anomalies that fell in the range 30-40%, compared to background values of 25-30% in northern segment 1, and dissolved CH<sub>4</sub> concentrations in the range 15-50nmol/L, 247 clearly in excess over background (Fig.4). For both tracers, maximum anomalies were observed at 248  $\sim$ 2700m in a mini-profile that was occupied at 46°16.5'S, 75°47.9'W, collected quasi-synoptically with 249 four other mini-profiles as part of a single CTD deployment. At this location,  $\delta^3$ He and dissolved CH<sub>4</sub> 250 251 values reached 38% and 46nmol/L respectively, marking the highest concentrations detected during our 252 2012 investigations and converging with our highest values from 2010 at the same location (Figs.2, 4).



**Figure 4.** Vertical profiles of (*left*)  $\delta^3$ He, and (*right*) dissolved CH<sub>4</sub> concentrations measured in southern Segment 1 in 2012. Color coding for symbols matches grouping of station locations shown in Fig.3. Blue = profiles from Chile margin with background values at all depths (Area G); Yellow, Red = profiles from Chile Triple Junction (Area H) that show hydrothermal anomalies in both  $\delta^3$ He and CH<sub>4</sub> at plume depths; Red circles = profile with the highest plume anomalies.

- From the much higher spatial resolution afforded from our 2012 surveys, we consider this location, as
- indicated by the red circle in Fig.3 (46°16.5'S, 75°47.9'W), to be our point of closest approach, thus far,
- to the source of seafloor venting at the Chile Triple Junction. Importantly, from an inter-comparison of
- $\delta^{3}$ He and dissolved CH<sub>4</sub> concentrations in all of our samples from southern Segment 1, we can be

confident that there is only one such source. As shown in **Fig.5**, all of our hydrothermal plume data

- collected over both expeditions, from throughout the southern Segment 1 region (46°13-16'S) fall on a
- single linear trend that characterizes samples from both years. This can be taken as indicative that there is
- a single source of venting generating the plume signatures observed and, further, that this source was
- 268 invariant over the timescale of repeat investigations of the region, consistent with a high-temperature
- vent-source located precisely at the Chile Triple Junction, where the southernmost Chile Rise ridge-axis is
- 270 being subducted.



Figure 5. Plot of dissolved  $CH_4$  concentrations vs  $\delta^3$ He values for water-column stations at which hydrothermal plume anomalies were detected in both 2010 (Red Circles: Areas D, E, F) and 2012 (Blue Circles: Area H) all of which fall along a common linear trend (black line).

However, if the methane and  $\delta^3$ He anomalies at the southern end of Segment 1 derive from a high-

temperature hydrothermal source, a question that arises is why we could not detect the presence of ionic

- 277 species arising from chemical (redox) equilibrium between the vent-fluids and the water-column using
- our *in situ* redox sensors that were mounted on the CTD-rosette. Remembering that all the hydrothermal
- 279 plume signals from this study coincide with the southernmost portion of Segment 1, where sediment
- cover is sufficiently thick to obscure all volcano-tectonic morphologies [Blackman et al., 2012] provides a
- possible explanation for these observations. Examination of a cross-section of suspended particle
- concentrations, as determined from transmissometer data collected during the initial tow-yo survey in
- 283 2010 (**Fig.6a**), reveals that in addition to the seafloor being covered in thick sediment as the ridge-axis

approaches the continental margin (Fig.1c), the overlying deep waters are characterized by a benthic

- nepheloid layer south of ~46°14'S that extends up to 2600m. These anomalies, which increase
- progressively toward the seafloor, are quite distinct from the particle-laden mid-water plumes that are
- typically observed overlying high-temperature "black smoker" vents.
- The inference that there is extensive sediment resuspension in the deep waters of southern Segment 1 is 288 supported by our analyses from a vertical CTD-station that was occupied toward the center of this region 289 of Segment 1 in 2010 - station F (Fig.3). There, profiles for  $\delta^3$ He and dissolved methane show diagnostic 290 mid-water hydrothermal plumes (Fig.6b). Unlike those profiles, however, total dissolvable Fe and Mn 291 292 data for the same samples show no coherent plume-like structure and, instead, exhibit a general increase toward the seafloor, reminiscent of the transmissometer cross-section (Fig.6a). Further, within the scatter 293 of the data (which is far greater than the analytical precision of the measurements), there is even a 294 suggestion that TDFe and TDMn concentrations exhibit a *decrease* at the depth at which highest  $\delta^3$ He 295 values and dissolved methane concentrations are observed. When interpreting these data, it is important 296 297 to remember that TDFe and TDMn analyses were specifically adopted during early hydrothermal plume 298 studies because this approach allows for the determination of both dissolved and recently-precipitated Fe 299 and Mn concentrations in hydrothermal plumes at mid-ocean ridge settings where minimal terrigenous 300 sediment is to be expected [Klinkhammer et al, 1985]. At the Chile Triple Junction, by contrast, sediment cover south of  $\sim 46^{\circ}10^{\circ}$ S is sufficient to mask any underlying volcano-tectonic morphology [Fig.1c; 301 302 Blackman et al., 2012] and there is clear evidence for a thick benthic boundary layer that extends upward beyond the height of the non-buoyant hydrothermal plume height (Fig.6). This is important to consider 303 because the level of acidification used during our sample processing was more than sufficient to 304 redissolve authigenic FeMn-oxyhydroxide component of any sedimentary material incorporated into our 305
- 306 samples [Bayon et al., 2002].



Figure 6. (a) Vertical cross-section of deepwater particle anomalies overlying the southern end 308 of Segment 1 as detected from in situ transmissometer data collected during 2010 CTD tow-yo. 309 Highest particle concentrations (lowest transmissometer values) are observed at the same 310 latitudes where volcano-tectonic seafloor morphologies are obscured by sediment (Fig.1c, 2a). 311 Vertical red bar shows location of CTD profile "F" (Fig.3); (b) vertical profiles from location "F" 312 showing (left)  $\delta^3$ He values & dissolved CH<sub>4</sub> with diagnostic mid-water hydothermal plumes and 313 314 (right) TDFe & TDMn concentrations that, by contrast, increase progressively toward the seafloor. 315

## 317 3.3 Evidence for sediment-hosted venting at the Chile Triple Junction

318 A final consideration that arises concerning the TDFe and TDMn data reported here, is whether the 319 absence of pronounced "black smoker" hydrothermal plume anomalies is because such signals are 320 *masked* by the presence of inputs associated with sediment re-supension at the southern end of Segment 1, or whether such hydrothermally-sourced metal enrichments are altogether *absent*. If the source of the 321 322  $\delta^3$ He and dissolved methane concentrations observed at Station F was a typical "black smoker" vent, then we might predict plume-height  $CH_4$ : Mn ratios in the range 0.2-1.0, as reported previously from the 323 northern East Pacific Rise [Baker et al., 1994]. In that case, for dissolved CH4 anomalies of ~25nM 324 (Fig.6b) we might expect corresponding TDMn anomalies of 25-125nM at hydrothermal plume height -325 *much* higher than the <10nM TDMn concentrations that we do observe. Instead, we argue that a more 326 analogous setting to consider here is the Escanaba Trough at the southern limit of the Gorda Ridge 327 [Atwater & Mudie, 1973]. Despite obvious differences in tectonic setting, what the Escanaba Trough 328 329 shares in common with southernmost Segment 1 of the Chile Rise is that its axial rift-valley floor is also buried by terrigenous sediments, derived from the adjacent continental margin [Vallier et al., 1973]. In 330 early water column studies at the Escanaba Trough, Baker et al. [1987] reported plume-like dissolved 331 332 methane anomalies, at 200-300m above the seafloor, with no accompanying enrichments in Fe or Mn. 333 While that study did not collect helium isotope samples to confirm the hydrothermal origins of the 334 methane plume, subsequent Alvin dives located active vents at the NESCA hydrothermal field, 335 discharging hot, clear fluids at temperatures up to  $217\pm2^{\circ}C$  [Campbell et al., 1994]. Those fluids were distinct from other mid-ocean ridge vents because they were (a) situated atop a thick sediment pile and (b) 336 both cooler than, and highly depleted in transition metals compared to, typical "black smokers". 337 Subsequent work showed that Fe and Mn are anomalously enriched in seafloor sediments at the same 338 NESCA site, consistent with the sequestration of hydrothermally-sourced Fe and Mn that precipitate from 339 340 the Escanaba vent-fluids into the sediments that the fluids percolate up through. Similar processes have also been documented at Middle Valley (Juan de Fuca Ridge) where ocean drilling has led to the 341 characterization of extensive horizons of polymetallic sulfide within the subsurface at that ridge segment, 342 which is also buried in terrigenous sediments [Zierenberg et al., 1998]. We hypothesize that the Chile 343 Triple Junction hosts another example of the same style of venting; one in which high temperature vent-344 345 fluids circulating through young ocean crust at depth rise through the overlying sediment column, transporting their dissolved gas contents all the way to the seafloor but depositing their metal contents 346 within the sediment column that they percolate up through. Upon reaching the seafloor, the emitted fluids 347 348 - as at Escanaba Trough - remain sufficiently hot to form a buoyant hydrothermal plume that rises up 349 above the seafloor until a level of neutral buoyancy is attained. This hypothesis would account for the

- 350 generation of a plume that is enriched in <sup>3</sup>He and methane but devoid of high metal concentrations
- dispersing at mid-water depth away from a source of venting. In the case of the Chile Triple Junction our
- inference is that the source of this venting is located at the seafloor close to 46°16.5'S, 75°47.9'W.

## 353 4 Conclusions

We have conducted systematic exploration for evidence of hydrothermal venting along the 354 southernmost two segments of the Chile Rise, from the Guamblin Fracture Zone to the Chile 355 Triple Junction. Our results are consistent with a single source of high-temperature venting 356 357 anywhere within this survey, at the southernmost end of Segment 1, immediately adjacent to 358 where the mid ocean ridge-crest is being subducted, actively, beneath the Chile Margin. Hydrothermal plume signals in this vicinity are enriched in dissolved methane and helium 359 isotope anomalies diagnostic of mantle influence in a mid-water lens consistent with a high-360 temperature vent-source at the underlying seafloor. But multi-beam bathymetry data for the 361 same region provide evidence for thick terrigenous sediment sufficient to blanket neo-volcanic 362 ridge axis morphologies. Further, optical back-scatter, TDFe and TDMn profiles overlying the 363 364 sedimented southern-most portion of the ridge all show evidence for a benthic boundary layer, indicative of suspended sediment load, that extends upward from the seafloor to depths shallower 365 than the hydrothermal plume layer. Importantly, however, the concentrations of TDFe and 366 TDMn observed within this benthic boundary layer are too low to mask what would be expected 367 in the non-buoyant plume of a conventional "black smoker" hydrothermal vent. Instead, we 368 conclude that the most likely source of venting at the Chile Triple Junction is a sediment-hosted 369 vent-site, emitting high-temperature fluids that are enriched in dissolved gases but depleted in 370 dissolved metals. That vent-site, to within  $\leq 1$  km, is predicted to be located at the seafloor close to 371 46°16.5'S, 75°47.9'W. 372

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- 380

## 381 **Open Research**

- All data presented in this research are included in Supplementary Tables S1 and S2 appended to
- 383 this submission.
- 384
- 385

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Table	S2:
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Water Column Analytical Data, RV Melville Cruise MV1205 (2012)

Location	Cast#	Bottle #	Latitude	Longitude	Depth	∂3He	CH4
					(m)	(%)	(nM)
TowYo	1T	1	46°16.49'S	75°47.96'W	2866	29.4	8.1
TowYo	1T	2			2785	30.1	8.3
TowYo	1T	3			2689	33.6	22.7
TowYo	1T	4			2595	28.1	1.7
TowYo	1T	5	46°16.15'S	75°48.20'W	2500	28.7	1.4
TowYo	1T	6	46°15.74'S	75°48.30'W	2901	29.0	7.8
TowYo	1T	7			2797	32.6	13.7
TowYo	1T	8			2698	32.3	13.8
TowYo	1T	9			2602	27.7	1.9
TowYo	1T	10	46°15.50'S	75°48.40'W	2499	28.4	1.6
TowYo	1T	11	46°14.80'S	75°48.74'W	2901		1.6
TowYo	1T	12			2800	30.2	7.2
TowYo	1T	13			2700	30.7	8.2
TowYo	1T	14			2598	28.6	2.3
TowYo	1T	15	46°14.64'S	75°48.85'W	2502	27.5	0.7
TowYo	1T	16	46°14.14'S	75°49.08'W	2507	28.8	1.1
TowYo	1T	17			2602	29.3	1.5
TowYo	1T	18			2701	29.5	4.1
TowYo	1T	19			2800	31.6	10.5
TowYo	1T	20	46°14.02'S	75°49.12'W	2901	30.1	6.3
TowYo	1T	21	46°12.94'S	75°49.67'W	2800	30.0	6.7
TowYo	1T	22			2700	30.8	4.3
TowYo	1T	23			2602	29.9	10.8
TowYo	1T	24	46°12.76'S	75°49.78'W	2500	30.4	2.1
r							
G	2P	1	46°15.49'S	75°47.95'W	2896	28.4	5.2
G	2P	2			2800	30.0	5.8
G	2P	3			2697	28.5	3.4
G	2P	4	46°15.49'S	75°47.95'W	2600	29.8	3.3
G	2P	5	46°15.75'S	75°47.93'W	2900	28.9	5.4
G	2P	6			2790	29.5	8.0
G	2P	7			2700	29.7	5.0

G	2P	8			2600	29.0	2.7
G	2P	9	46°15.75'S	75°47.93'W	2500	29.4	3.2
G	2P	10	46°16.00'S	75°47.83'W	2898	29.2	5.3
G	2P	11			2800	29.7	5.8
G	2P	12			2697	29.4	4.5
G	2P	13			2598	30.2	2.2
G	2P	14	46°16.00'S	75°47.83'W	2500	30.2	4.0
G	2P	15	46°16.27'S	75°47.80'W	2888	29.1	4.4
G	2P	16			2796	29.9	6.2
G	2P	17			2699	28.9	3.2
G	2P	18			2602	29.1	3.1
G	2P	19	46°16.27'S	75°47.80'W	2500	29.7	3.6
Н	3P	1	46°16.33'S	75°47.99'W	2803	30.2	16.5
н	3P	2			2748	32.4	21.7
н	3P	3			2699	34.4	32.6
н	3P	4	46°16.33'S	75°47.99'W	2649	33.7	26.1
Н	3P	5	46°16.52'S	75°47.11'W	2800	30.8	16.5
н	3P	6			2750	31.6	20.5
н	3P	7			2702	35.3	39.9
н	3P	8	46°16.52'S	75°47.11'W	2649	31.9	16.2
Н	3P	9	46°16.51'S	75°47.89'W	2918	29.0	8.4
н	3P	10			2850	31.2	12.0
н	3P	11B			2800	30.7	18.2
н	3P	12			2750	32.6	17.9
н	3P	13			2700	37.1	45.0
н	3P	14	46°16.51'S	75°47.89'W	2650	38.1	46.2
Н	3P	15	46°16.53'S	75°47.62'W	2800	31.7	12.5
н	3P	16			2750	33.8	19.9
н	3P	17			2702	32.8	28.0
н	3P	18	46°16.53'S	75°47.62'W	2650	33.6	37.0
Н	3P	19	46°16.74'S	75°47.75'W	2799	33.1	23.0
н	3P	20			2748	32.5	30.0
н	3P	21			2699	32.4	19.0
н	<u>3</u> P	22	46°16.74'S	75°47.75'W	2648	32.6	26.3
Н	3P	23	46°16.83'S	75°47.70'W	2700	34.8	33.6

Н	3P	24	46°16.83'S	75°47.70'W	2649	35.0	31.8
Н	4V	1	46°16.99'S	75°48.15'W	2905	31.4	18.9
Н	4V	3			2875	34.1	28.4
Н	4V	4			2854	34.8	32.9
Н	4V	6			2802	35.6	33.8
Н	4V	8			2751	34.8	33.9
н	4V	10			2700	34.3	28.2
н	4V	12			2650	32.0	12.7
н	4V	14			2600	30.6	8.6
Н	4V	16			2549	29.8	3.5
Н	4V	17	46°16.99'S	75°48.15'W	2500	29.8	2.5
Н	5P	1	46°16.52'S	75°47.88'W	2900	30.4	11.8
Н	5P	2			2849	33.4	26.3
Н	5P	3			2800	35.0	31.6
Н	5P	4			2749	33.9	25.3
Н	5P	5			2723	34.0	25.7
Н	5P	6			2700	33.2	21.1
н	5P	7			2679	33.2	20.8
н	5P	8			2650	30.5	12.0
н	5P	9			2625	29.7	7.6
н	5P	10			2599	29.3	5.0
н	5P	11			2549	28.9	2.5
Н	5P	12	46°16.52'S	75°47.88'W	2498	29.6	2.8
Н	5P	13	46°16.47'S	75°47.81'W	2900	30.9	15.7
Н	5P	14			2848	33.5	26.0
Н	5P	15			2822	33.8	28.7
Н	5P	16			2798	33.7	29.2
Н	5P	17			2773	33.9	26.0
Н	5P	18			2750	33.0	20.3
н	5P	19			2722	31.7	13.8
н	5P	20			2700	31.7	14.4
Н	5P	21			2672	31.2	13.2
Н	5P	22			2650	30.9	10.4
Н	5P	23			2598	29.9	5.4
Н	5P	24	46°16.47'S	75°47.81'W	2502	28.3	3.1