Investigation of flow characteristics of landslide materials through pore space topology and complex network analysis

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Abstract

Unlike embankments, earth dams, and other man-made structures, most landslide dams are formed by rapid accumulation of rock or debris rather than mechanical compaction; thus, they are loose and pose a great risk of seepage failure. Landslide materials usually have complex pore structures with randomly distributed pores of various sizes, making the flow and transport processes very complex. Aiming at these challenges, we have studied the influences of pore structure on the micro-and macro-scale flow characteristics of landslide materials. First, landslide materials are simplified as spherical granular packings with wide grain size distributions. Then, we use finite difference method (FDM) and lattice Boltzmann method (LBM) to simulate the fluid flow through granular packings and calculate their permeability. We find that both the correlation between pore-scale velocity and throat diameters and the correlation between macroscopic permeability and average throat diameters follow a power-law scaling with an exponent close to 2, in agreement with the Hagen–Poiseuille equation for laminar flow in pipes, suggesting that the relationships in complex pore structures are conformed with the simple theory. Moreover, we propose a new method by combining pore networks and complex networks to characterize the pore structure. The network analysis illustrates that granular packings with different permeability display distinctive distributions of pore throat size and pore connectivity and their correlations. Compared with disassortative pore networks, assortative ones generally have higher permeability. Furthermore, pores with larger closeness centrality have higher flow efficiency that results in higher macroscopic permeability.

Investigation of flow characteristics of landslide materials through pore space 1 topology and complex network analysis 2 Jia Zhang^{1,2}, Gang Ma^{1,2}, Zhibing Yang^{1,2}, Qirui Ma³, Wenyu Zhang^{1,2}, Wei Zhou^{1,2} 3 ¹ State Key Laboratory of Water Resources and Hydropower Engineering Science, Wuhan 4 University, Wuhan 430072, China. 5 ² Kev Laboratory of Rock Mechanics in Hydraulic Structural Engineering of Ministry of 6 Education, Wuhan University, Wuhan 430072, China. 7 ³ Changjiang Institute of Survey, Planning, Design and Research, 430010, Wuhan, China. 8 Corresponding author: M. Gang (magang630@whu.edu.cn) 9 10 **Key Points:** 11 • Conventional topological measures except tortuosity fail to explain the influence of pore 12 structure on flow characters in low permeability. 13 14 • The relationship between permeability and throat diameter spanning nine orders of magnitude is consistent with the Hagen–Poiseuille theory. 15 Complex network theory is proven useful to unveil the topological characteristics of pore • 16 networks.

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19 Abstract

Unlike embankments, earth dams, and other man-made structures, most landslide dams are 20 21 formed by rapid accumulation of rock or debris rather than mechanical compaction; thus, they are loose and pose a great risk of seepage failure. Landslide materials usually have complex pore 22 23 structures with randomly distributed pores of various sizes, making the flow and transport processes very complex. Aiming at these challenges, we have studied the influences of pore 24 25 structure on the micro-and macro-scale flow characteristics of landslide materials. First, landslide materials are simplified as spherical granular packings with wide grain size 26 distributions. Then, we use finite difference method (FDM) and lattice Boltzmann method 27 (LBM) to simulate the fluid flow through granular packings and calculate their permeability. We 28 29 find that both the correlation between pore-scale velocity and throat diameters and the correlation between macroscopic permeability and average throat diameters follow a power-law 30 scaling with an exponent close to 2, in agreement with the Hagen–Poiseuille equation for laminar 31 flow in pipes, suggesting that the relationships in complex pore structures are conformed with 32 the simple theory. Moreover, we propose a new method by combining pore networks and 33 complex networks to characterize the pore structure. The network analysis illustrates that 34 granular packings with different permeability display distinctive distributions of pore throat size 35 and pore connectivity and their correlations. Compared with disassortative pore networks, 36 assortative ones generally have higher permeability. Furthermore, pores with larger closeness 37 38 centrality have higher flow efficiency that results in higher macroscopic permeability.

39 **1 Introduction**

Landslide dams are common worldwide, especially in tectonically active mountain regions, 40 which are usually caused by natural hazards, such as mountain collapse, earthquakes, and 41 42 mudslides. Landslide dams are mainly composed of loose soil and fragmented rocks with grain size spanning several orders of magnitude (Sun et al., 2016). The blockage of river channels by 43 44 landslide dam results in raising water in upstream areas. With the increase of water level in dammed lake, the loose dam body will collapse catastrophically, causing anomalous destructive 45 46 flood waves and posing a significant threat to downstream life and properties (Peng & Zhang, 2012). Therefore, the study of landslide dams and their consequences has acquired significant 47 48 relevance in scientific research to predict and prevent landslide dam collapse. Many factors 49 influencing the stability of landslide dam have been studied comprehensively, such as dam 50 geometry (Chen et al., 2015), grains composition (Okeke & Wang, 2016), the angle of dam 51 downstream face (Gregoretti et al., 2010) and permeability, which is considered as one of the 52 critical factors affecting the stability of landslide dam (Costa & Schuster 1988).

Previous studies on the hydraulic properties of landslide materials through experimental 53 54 and field tests (Okeke & Wang, 2016) and numerical simulations (Zhu et al., 2020) have revealed that the grain size distribution of the dam accumulation has significant impacts on the seepage 55 stability of landslide dams. However, the relationship between pore structure and hydraulic 56 properties of landslide materials has not been fully understood, mainly due to the difficulties of 57 58 characterizing the pore structure of landslide materials. The complex pore structure is originated from the quick deposits of landslide materials composed of poorly graded soils and fragmented 59 rocks. The existing test results have shown 1~2 orders of magnitude permeability variation for 60 approximately the same porosity. This variation has been attributed to the complex pore structure 61 of landslide materials (Miller et al., 2015; Thomson et al., 2018). 62

Characterization of the pore structure is of great interest in many scientific and 63 technological areas. Many techniques have been developed to examine the pore space of porous 64 medium, such as scanning electron microscopy (SEM) (Peters, 2009), mercury injection capillary 65 pressure (MICP) (Xiao et al., 2016), nuclear magnetic resonance (NMR) (Li et al., 2021), and X-66 ray (Zambrano et al., 2019). By the aid of the nondestructive and quantitative methods, the 67 inhomogeneity coefficient, curvature coefficient, critical pore radius (Nishiyama & Yokoyama, 68 2017), tortuosity (Ahmadian et al., 2019) have been used to characterize the microscopic pore 69 70 structure and link to macroscopic permeability. On the numerical modeling side, several pore-scale methods have been widely used, such as the pore network model (PNM) (Dong & Blunt, 2009; 71 Fatt, 1956). The PNM and its variants have been extensively used in characterization of pore space 72 geometry and topology as well as simulation of multiphase and single-phase flows in porous media 73 (An et al., 2016; Esmaeilpour et al., 2021; Steinwinder & Beckingham, 2019; Zhang et al., 2019). 74

Besides the pore throat size distribution, the pore connectivity and pore spatial distribution have been found to play important roles in fluid flow through porous media (Cai et al., 2019). Pore connectivity can be quantified by either coordination number (Thomson et al., 2018) or connectivity factor (Cai et al., 2019; Hunt, 2004). Coordination number can be evaluated by medial axis analysis, which reduces the macropore space to a medial axis and calculates the average

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number of branches at a junction (Hormann et al., 2016). Recently, Zhang et al. (2021) extracted the pore networks from samples slices and proposed two connectivity indexes based on generated pseudo MICP curves to evaluate the connectivity of 2D pore networks quantitatively. Bernabé et al. (2010) proposed a new model based on network simulations and percolation theory and highlighted the importance of pore connectivity and pore size heterogeneity on fluid flow in porous media (Bernabé et al., 2011).

Despite the advances in previous studies, there is a lack of detailed analysis on robust 86 multiscale descriptors of pore connectivity and their relationship to fluid flow characteristics 87 88 (Bernabé et al., 2010; Cai et al., 2019). Complex network analysis provides a new perspective to study pore connectivity and the multiscale characterization of pore network. For example, Van 89 Der Linden et al. (2016) developed a framework to characterize the internal pore structure and 90 fluid transmission efficiency of porous media using complex network theory; by combining the 91 92 particle's complex network and its pore network, Russell et al. (2016) proposed a framework to characterize the coupled evolution for planar deformation considering the geometry and 93 94 connectivity of pores; Jimenez-Martinez and Negre (2017) proposed an measure called eigenvector centrality based on complex network theory to characterize the geometric and 95 topological characterization of porous media; Valera et al. (2018) developed an approach to 96 describe transport in fractured rock based on node centrality of complex network. 97

This study aims to develop a framework to investigate the effect of pore structure on 98 microscale flow characteristics and macroscopic hydraulic properties of landslide materials. 99 100 Because the landslide materials are very complex and the grain size exceeds the limitation of 101 current experimental techniques, we simplify the landslide materials as granular packings and perform a large set of numerical simulations. The workflow of this study is shown in **Figure 1**. 102 We firstly generate granular packings with different grain size distributions to represent typical 103 landslide materials. Then, the pore space of the granular packing is extracted, and the fluid flow 104 through granular packing is numerically simulated. Finally, the pore space topology, pore network 105 model, and complex network analysis are used to link the pore structure and micro- and 106 macroscopic flow characteristics of landslide materials. 107

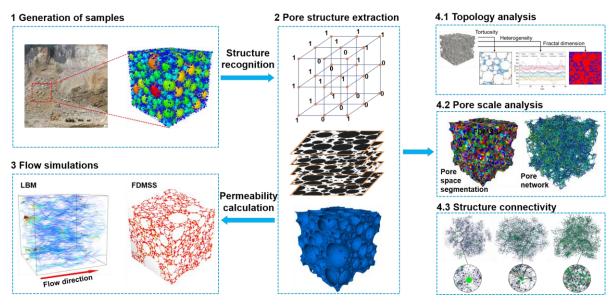


Figure 1 Workflow of this study.

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2 Permeability evaluation of landslide deposits 111

2.1 Typical samples of landslide deposits 112

We collected grain size distributions (GSDs) of 32 landslide dams located all over the 113 114 world. As shown in **Figure 2a**, the GSD of natural landslide deposits varies significantly. With the increase of fine grains, the grain gradation curve gradually changes from a convex shape to a 115 116 concave one. In this study, we select seven GSDs to represent the typical landslide deposits. Samples 1 and 2 have more fine grains; Samples 4~7 have more coarse grains; Sample 3 is 117 characterized by a relatively uniform size distribution. 118

The discrete element method (DEM) was used to generate the widely graded granular 119 packings shown in Figure 2b. The grain diameter ranges from 2 mm (d_{\min}) to 80 mm (d_{\max}) 120 following the distributions illustrated in Figure 2a. Firstly, loose assemblies of nonoverlapping 121 grains with a dimension of $0.4 \times 0.4 \times 0.4$ m were generated randomly. Then, the grain assemblies 122 were triaxially compressed to an equilibrium state under the confining pressure of 1MPa (Ma et 123 al., 2016). The input parameters for the DEM simulations of granular packing are summarized in 124 Table 1. 125

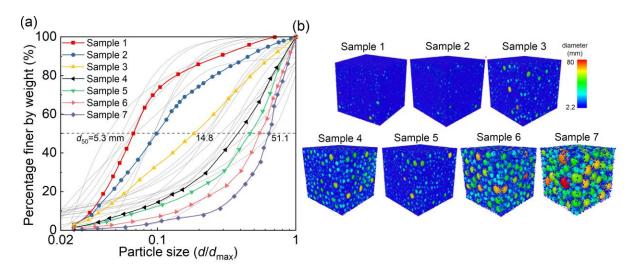


Figure 2 (a) Grain size distributions collected from 32 landslide dams (grey color) and seven
GSDs used in this study (colored lines); (b) Granular packings with different GSDs and particles

130 are colored by their diameter.

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132	Table 1 Input parameters 1	for DEM simulation	of granular packing
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Parameters	Symbol	Units	Values
Grain density	ρ	kg/m ³	2600
Young's module	E	GPa	65
Timestep	Δt	S	1e-7
Initial size of samples	Н	m	0.4
Target confining pressure	Р	MPa	1
Poisson ratio	ν	-	0.2
Friction	μ	-	0.1
Contact model		-	Hertz-Mindlin

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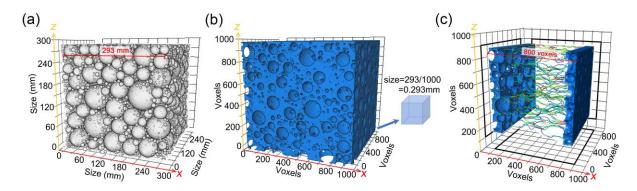
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2.2 Fluid flow simulation using FDMSS

Take one granular packing as an example, the granular packing was divided into 137 $1000 \times 1000 \times 1000$ voxels, as shown in **Figure 3a**. The voxel size is approximately 0.3 mm, about 138 1/7 of the smallest grain. To extract the pore space, we converted $1000 \times 1000 \times 1000$ voxels into a 139 three-dimensional matrix according to grain position and grain size, in which each element has a

value of either 0 (void voxel) or 1 (solid voxel). Figure 3b and Figure 3c show the pore space 140 extracted from the granular packing and several fluid streamlines for illustration. The finite-141 difference method Stokes solver (FDMSS) is used to simulate the fluid flow (Gerke et al., 2018). 142 The FDMSS uses the finite difference method to directly solve the Navier-Stokes equation, which 143 has been verified and proven to be efficient and accurate. Compared with other methods, such as 144 classic FDM (Shabro et al., 2012) and LBM (Khirevich et al., 2015), FDMSS has higher accuracy 145 and convergence speed and lower computational cost. The interested readers may refer to Gerke 146 et al. (2018) for the details of FDMSS. 147

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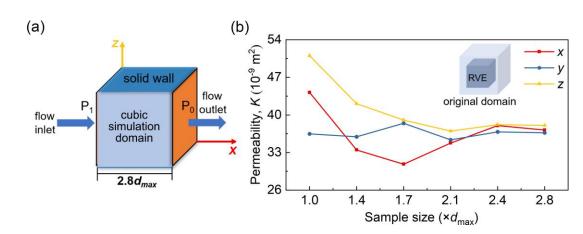
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Figure 3 (a) Granular packing; (b) Extraction of pore space; (c) Illustration of the fluid flow
paths.

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Flow velocity fields are modeled by applying pressure gradients across three principal 153 directions while treating all other sides of the granular packing as impermeable walls (see Figure 154 4a). The permeability along flow direction can be calculated using Darcy's equation 155 $K = \mu LQ/(\Delta pS)$, where μ is fluid viscosity, L is the distance of fluid flow, Q is flow rate, Δp 156 is pressure difference between inlet and outlet boundaries, and S is the cross-sectional area. To 157 eliminate the boundary effects on fluid flow simulation, a subset of manually binarized images 158 159 was cropped from the original stack for simulations resulting in 3D modeling domains containing $300^3 \sim 800^3$ voxels. The representative volume element (RVE) is obtained when the measured or 160 calculated permeability plotted versus increasing sample size reaches a plateau (Figure 4b). 161 Meanwhile, grid sensitivity analysis is also performed (Figure 5). It can be seen that the 162 permeability becomes stable when the resolution is less than 0.35 mm/voxel. Thus, the resolution 163

we choose is accurate enough for the flow simulations. The granular packing porosity ϕ , mean grain size d_{50} , permeability calculated by FDMSS K_{FDMSS} are summarized in **Table 2**.



169 Figure 4 (a) Simulation domain and boundary conditions of the fluid flow simulation; (b) RVE

170 size effect on the permeability of granular packing.

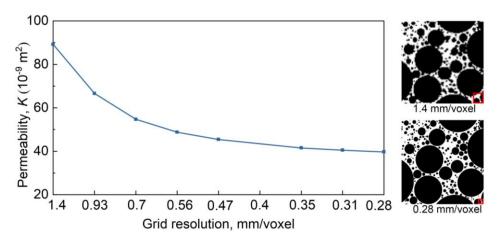


Figure 5 Grid sensitivity analysis (The lattice number is $200^3 \sim 1000^3$ corresponding to the

- resolution of 1.4~0.28 mm/voxel).

	Porosity ϕ	d_{50} (mm)	Permeability K_{FDMSS} (×10 ⁻⁹ m ²)	Range
Sample 1	0.29	5.33	5.15	
Sample 2	0.24	7.81	4.73	1< <i>K</i> <10
Sample 3	0.19	14.84	3.65	
Sample 4	0.19	30.80	16.49	
Sample 5	0.22	37.28	39.70	10< <i>K</i> <100
Sample 6	0.26	43.73	76.77	
Sample 7	0.31	51.13	306.27	K>100

181 **Table 2** Basic information of the granular packings and their permeability

The permeability of the seven granular packings covers nearly two orders of magnitude. 183 We can divide the granular packings into three categories according to their permeability to 184 facilitate the following analysis. Sample 2, Sample 5 and Sample 6 have the similar porosity, but 185 they show an order of magnitude difference in permeability. Sample 3 and Sample 4 have the same 186 porosity, but display a distinct difference in permeability. This means that the porosity alone 187 cannot reflect the effect of pore structure on permeability. Therefore, a more thorough 188 investigation of the effect of pore structure on flow characteristics of landslide materials is 189 190 necessary. Besides FDMSS, we also use LBM to simulate the fluid flow through the porous space. The LBM simulation with the D3Q19 lattice model achieves a good balance between stability and 191 192 efficiency. The permeabilities calculated by FDMSS and LBM are nearly the same. However, the 193 computational efficiency of FDMSS is much higher than that of LBM.

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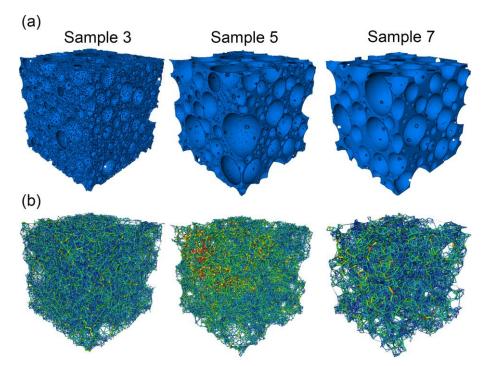
2.3 Construction of pore-throat structure and complex network

The pore space topology of the granular packing is analyzed by the pore network model (PNM) and complex network approach, respectively. The pore network of the granular packing is extracted using the maximal sphere method developed by Dong & Blunt (2009). According to the maximal sphere algorithm, the pore space is divided into pore bodies and throats. Then the PNM consisting of the network of pores and throats is constructed, in which throats are the local constrictions that connect the adjacent pores. The pore network model provides an effective way of analyzing the geometry and topology of the pore space. The topology and geometry information about the pore structures of granular packings are summarized in **Table 3**. Using Sample 3, Sample 5 and Sample 7 as examples, we show the pore space and pore network model of these three granular packings in **Figure 6**. It is clear that the pore network of Sample 3 is relatively concentrated, while Sample 5 and Sample 7 are relatively loose, indicating the pore distribution is scattered and coarse.

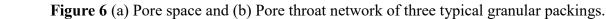
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Table 3 Parameters of different samples simulated by the pore network modeling

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	Sample 1	Sample 2	Sample 3	Sample 4	Sample 5	Sample 6	Sample 7
Size (mm)	283	278	272	273	278	282	293
Pores number	79396	59739	40226	10718	6615	3846	1692
Throats number	428315	297364	184380	45815	28075	16079	6765
Average pore connection number	10	10	9	8	8	8	8
Max pore connection number	45	39	35	25	21	20	21
Average pore diameter (mm)	1.77	1.81	1.82	2.78	3.75	5.17	8.21
Max pore diameter (mm)	4.00	3.90	3.91	6.00	8.84	10.53	14.39
Average pore volume (mm ³)	10.12	11.42	12.42	48.88	98.06	208.90	647.27
Max pore volume (mm ³)	115.00	103.61	154.79	497.49	944.09	1866.88	4516.30
Average throat diameter (mm)	0.94	0.97	0.99	1.52	2.04	2.84	4.54
Max throat diameter (mm)	3.20	3.31	3.36	5.44	7.31	8.21	13.41
Average throat volume (mm ³)	5.89	6.78	7.62	31.29	62.73	136.19	424.52
Max throat volume (mm ³)	110.33	124.44	166.62	434.58	851.76	2018.39	5514.10
Average throat length (mm)	7.30	7.42	7.48	10.69	12.87	15.57	21.39
Max throat length (mm)	24.51	24.30	27.40	30.63	37.28	45.78	58.60







212 **3 Topological characteristics of pore structure**

Landslide materials are highly complex systems characterized by significant variability of grains and pore sizes. Although landslide materials have been idealized as spherical granular packing with different GSDs, their internal structures are significantly different due to the significant differences in the GSD of the granular packings. It has been well recognized that the fluid flow in porous media is affected by its internal structure (Alim et al., 2017). In this section, we use several measures to characterize the topological properties of the pore structure.

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3.1 Conventional topological measures

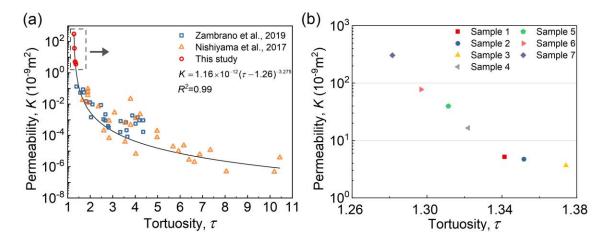
Tortuosity is an intrinsic property of a porous material usually defined as the ratio of actual flow path length to the straight distance between the ends of the flow path (Ghanbarian et al., 2013). It has been reported that tortuosity is an important factor affecting flow and transport in porous media (Cai et al., 2019). As the tortuosity τ becomes larger, the flow path will be more tortuous and longer. We first show how tortuosity affects the permeability of landslide materials. Instead of using its geometric definition, we calculate the tortuosity using the velocity vector of the flow field. The tortuosity along the flow direction (*x*-direction) is defined as:

$$\tau_{x} = \frac{\sum_{i=1}^{N} \sqrt{v_{xi}^{2} + v_{yi}^{2} + v_{zi}^{2}}}{\sum_{i=1}^{N} v_{xi}}$$
(1)

Where τ_x is the tortuosity in the x-direction; the subscript *i* denotes the *i*-th node in the flow field; *N* is the total number of nodes in the flow field; v_{xi} , v_{yi} , and v_{zi} are the *x*, *y*, and *z* components of the velocity vector. The local tortuosity at each node can be calculated analogically as $\tau_{xi} = \sqrt{v_{xi}^2 + v_{yi}^2 + v_{zi}^2} / v_{xi}$.

The relationship between tortuosity and permeability is plotted in **Figure 7**. Although the 232 permeability spans eight orders of magnitude, these data points collapse to a master curve with a 233 determination coefficient of 0.99. The permeability demonstrates a decreasing trend with the 234 increase of tortuosity, which is consistent with previous studies (Nishiyama & Yokoyama, 2017; 235 Zambrano et al., 2019). We then analyze the influencing mechanism of tortuosity on permeability. 236 As shown in **Figure 8a**, the curvature of the streamlines gradually decreases due to the increase of 237 coarse grains in the granular packing. Take Sample 7 as an example, coarse grains take up most of 238 239 the space, and large pore space is generated without the filling of fine grains. Therefore, there is no obstruction of fine grains when the fluid flows, leading to straight flow path and high flow 240 velocity between large pores (Figure 8b). With the increase of fine grains, local blocking 241 structures are formed by the filling of fine grains. Thus, due to the more tortuous flow paths, the 242 243 fluid flow through the porous media becomes difficult and results in lower permeability. Figure 8c shows the local tortuosity at the cross-section of the three granular packings. As shown, the 244 front and rear regions of pores show higher tortuosity. Therefore, the porous media consisting of 245 more pores display a higher tortuosity, which explains the relationship between permeability and 246 247 tortuosity.

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Figure 7 The relationship between tortuosity and permeability. The right panel (b) is an enlarged

view of the dotted box shown in (a).

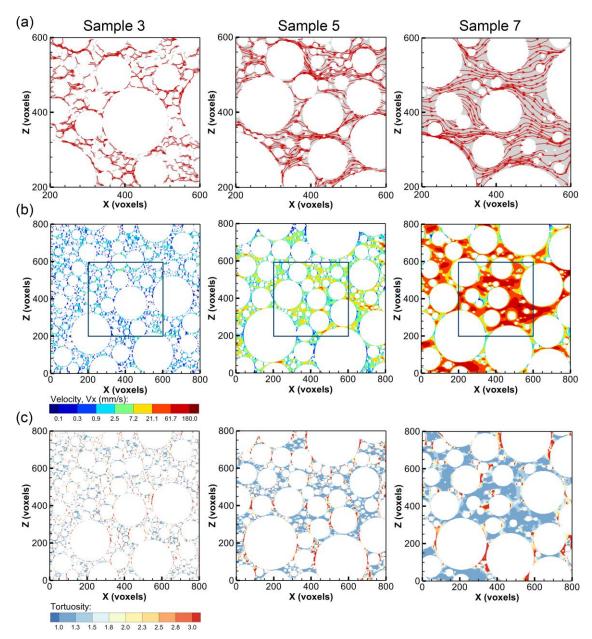


Figure 8 The distributions of (a) Streamline, (b) Flow velocity, and (c) Tortuosity of each node at the cross-section of the three typical granular packings.

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Disorder is another intrinsic property of porous media, which profoundly influences the stress transmission and failure (Huang et al., 2021; Zaiser, 2017), flow and transport characteristics (Zami-Pierre et al., 2018). The disorder of porous media can be manifested as the heterogeneity of pore size distribution or local porosity distribution. Porous media with non-uniformly distributed pore size and local porosity generally have a higher degree of disorder. As suggested by Laubie (2017), the domain containing the granular packing is divided into several subdomains to facilitate the calculation of local porosity (see **Figure 9a**). A heterogeneity index can be defined as the standard deviation of the local porosity of each subdomain (Laubie, Radjai, et al., 2017; Wang et al., 2016).

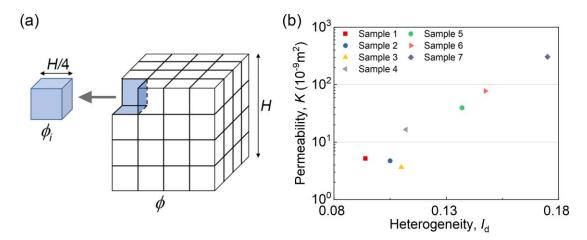
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$$I_d = \sqrt{\left\langle \phi_i^2 \right\rangle - \phi^2} \tag{2}$$

where I_d is the heterogeneity index, ϕ is the global porosity of the granular packing, and ϕ_i is the local porosity of the *i*-th subdomain.

The relationship between pore heterogeneity and permeability is plotted in **Figure 9b**. The permeability shows an overall increasing trend with I_d in samples 4~7, suggesting that granular packings with the increasing of coarse grains showing more obvious pore aggregation have higher permeabilities. However, the heterogeneity does not display an obvious trend when the proportion of fine grains is large (as in Samples 1~3). This means that I_d is determined by the GSD when there are more coarse grains in samples, but it is not applicable to the samples composed of more fine grains.

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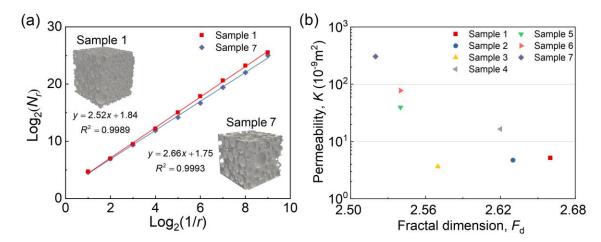
Figure 9 (a) Illustration of the pore heterogeneity calculation; (b) The relationship between
heterogeneity and permeability.

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Besides tortuosity and heterogeneity, we further use fractal dimension to characterize the pore space topology. Many studies have shown that the pore space of porous media has a typical fractal structure (Yu & Cheng, 2002; Yun et al., 2009). The fractal dimension of the pore space is calculated using the box-counting method (see **Figure 10a**). The overall tendency is that the fractal

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dimension increases with the increasing proportion of fine grains in porous media with low permeability (**Figure 10b**). The fractal dimension does not appear to be a robust metric to describe the pore structure for characterization of hydraulic properties; e.g., samples 1~3, having a similar permeability, display quite different fractal dimensions. Therefore, we propose a new method based on microscopic analysis with pore networks and complex networks in Section 4 and 5.



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Figure 10 (a) Illustration of the calculation of fractal dimension of pore space; (b) The
relationship between fractal dimension and permeability.

3.2 Characterization of the complex pore network

This section focus on analyzing the topological characteristics of pore structure using the 295 complex network theory (Papadopoulos et al., 2018). A complex network is a graph, which can 296 help to simplify the pore structure and give insights into the flow and transport properties in porous 297 media (Jimenez-Martinez & Negre, 2017; Van Der Linden et al., 2016, 2019). As shown in Figure 298 11, a complex network is constructed to represent the pore throat network, in which the nodes 299 represent pores (centroid of the pore) and edges represents throats determined by the medial axis 300 method. In order to relate the complex network features to the flow characteristics of porous media, 301 some studies constructed weighted complex network to represent the pore throat structure. 302 303 Different choices of edge weight have been proposed, such as conductance (Van Der Linden et al., 2016) and throat cross-section area (Jimenez-Martinez & Negre, 2017). 304

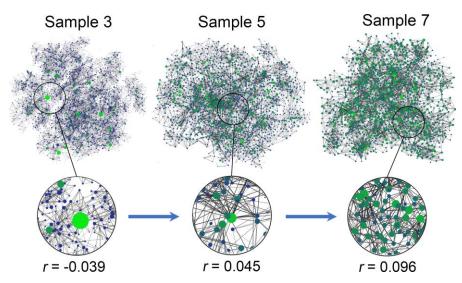


Figure 11 Complex network representation of the pore structure of three typical granular packings. r is the degree correlation coefficient. complex networks tend to be assortative with the increase of r.

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The complex network constructed in this way is physically representative and can be 310 viewed as a "fingerprint" of the porous media. The complex pore network is denoted as a graph 311 G=(V, E), where $V = \{1, ..., N\}$ is the set of nodes (pores) and $E \subseteq V \times V$ is the set of edges that 312 represents throats. We use several overall network features to characterize the transport efficiency 313 314 and flowing capacity in the network, such as global efficiency, entropy, and transitivity. The global efficiency represents the average of the reciprocal path lengths of all nodes in the complex network 315 and can be interpreted as a measure of how well the flow is transmitted through a network. The 316 global efficiency \overline{E}_{glob} is defined as: 317

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$$\bar{E}_{glob} = \frac{1}{N(N-1)} \sum_{i,j} \frac{1}{d_{ij}}$$
(3)

where *N* is the number of nodes; d_{ij} is the shortest path length between node *i* and *j*, representing the shortest number of steps necessary to get from node *i* to *j*. The flow transmission rate is dependent upon d_{ij} , and lower d_{ij} corresponds to higher transmission efficiency.

The entropy of degree distribution is an important concept that measures the node connection inhomogeneity in the complex network (Reichl & Luscombe, 1999). It is defined as:

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$$H = -\sum_{k} P(k) \log P(k)$$
(4)

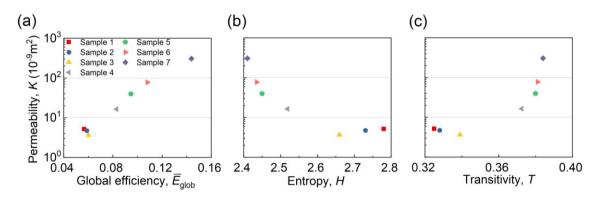
Where *k* is the degree that represents the number of edges connected to a node; P(k) is the fraction of nodes in a network with degree *k*. The entropy achieves the maximum value when the degree distribution is uniform (wide), and the minimum value of entropy is 0 when the nodes have the same degree.

The transitivity is defined by the fraction of all possible triangles present in the graph (Zlatić et al., 2012). Possible triangles are identified by the number of triads composed of two edges with a shared node. Suppose that a node *i* has k_i neighbors. The maximum number of edges are $k_i(k_i - 1)/2$. The transitivity can be calculated as:

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$$T = \frac{3t(G)}{\sum_{i \in V} \frac{k_i(k_i - 1)}{2}}$$
(5)

Where t(G) is the number of triangles in *G*; k_i is the degree of node *i*. The transitivity reflects the probability that two random neighbors of one node are neighbors with each other and can be used to measure how well nodes tend to be clustered.

As shown in Figure 12a, the network with higher global efficiency has better flow 337 338 transmission efficiency, thus, demonstrating larger permeability. Specifically, in Samples 1~3, the nodes that are not close to one another are separated by multiple edges and have longer path length, 339 therefore, the connectivity between nodes is weakened. In Samples 4~7, the length of the shortest 340 path connecting two nodes is shorter, and the fluid can reach another node through fewer edges. 341 342 Thus, the fluid can communicate, transform, and transmit in each node with greater efficiency, which ultimately lead to higher permeability. With the increase of fine grains, the entropy 343 344 reflecting the node connection inhomogeneity increases. The complex networks with higher entropy demonstrate lower permeability (see Figure 12b). The networks with larger transitivity 345 also display higher permeability (see Figure 12c). We can conclude from this analysis that 346 granular packings with relatively clustered pores that are linked by high connectivity throats have 347 high permeability. 348



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Figure 12 The relationships between permeability and three complex network features: (a)
Global efficiency; (b) Entropy; (c) Transitivity.

4 Microscopic investigation by pore network analysis

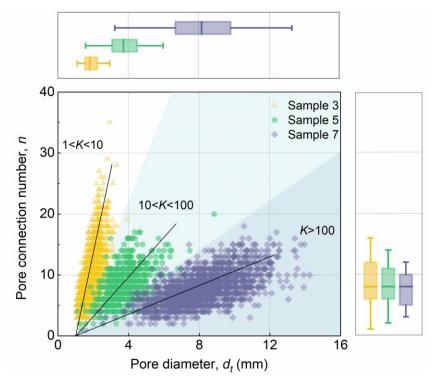
The above analysis indicates that both conventional topological parameters and complex network measures can be used to investigate the relationship between pore structure and permeability at the macroscopic scale. Among these metrics, tortuosity and global efficiency perform better than others. We further investigate the relationship between the microscopic pore structure and pore scale flow dynamics. In this section, the pore and throat geometry obtained from PNM are analyzed in detail. We mainly focus on the pore and throat size distributions of different granular packings and their correlations with pore connectivity and flow dynamics.

Using Sample 3, Sample 5 and Sample 7 as typical examples, the distributions of pore size 360 and pore coordination number and their correlations of different granular packings are shown in 361 Figure 13. The pore connection number represents the number of throats connected to a pore. 362 With the increase of coarse grains, the pore size gradually increases and varies in a wider range. 363 The connection number increases with increasing pore size, indicating that larger pores tend to 364 connect more throats. In Sample 3, the pore sizes scatter in a quite narrow range, while the pore 365 connection numbers show a relatively wide range. Thus, the relationship between pore size and 366 pore connection number is fitted by a line with a larger slope, indicating that small pores with few 367 connection numbers are more likely to link to large pores with multiple connection numbers. 368

The distributions of throat diameter and throat length and their correlations of different granular packings are presented in **Figure 14**. It clearly outlines the positive correlation between pore throat size and permeability, suggesting that longer and larger throats generally result in higher permeability of granular packing. With the increase of fine grains, the void space can be

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filled by finer grains, the cross-section area of throat becomes smaller, which hinders the flow in granular packing. As the proportion of coarse grain increases, the granular packing tends to generate large void space without filling of finer grains, therefore, the pore space are manifested by larger pore and throat size with relatively evenly distributed connection number. We can categorize the granular packings into three groups according to the features of the pore throat geometry and their correlations. The significant difference in pore throat geometry and their connectivity results in permeability difference of orders of magnitude.



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Figure 13 Scatter plot of pore diameter and pore connection number with marginal boxplots of

different granular packings (Permeability K, 10^{-9} m²).

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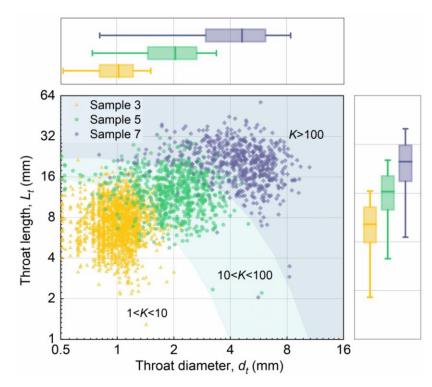
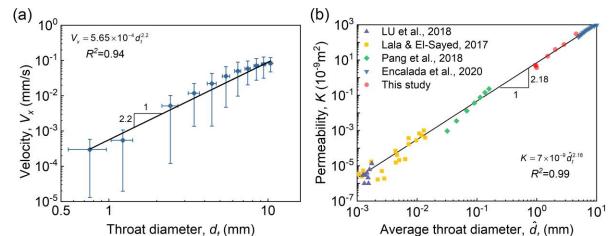




Figure 14 Scatter plot of throat diameter and throat length with marginal boxplots of different granular packings (Permeability K, 10⁻⁹ m²).

387 The correlations between pore throat geometry and flow characteristic are also analyzed at both the pore scale and the macroscale. The flow velocity at the throat center is plotted as the 388 function of throat diameter (Figure 15a). At the pore scale, the flow velocity increases 389 approximately linearly with throat diameter in the log-log scales with a slope of about 2.2, i.e. 390 $V_r \propto d_r^{2.2}$, which is in close agreement with Hagen–Poiseuille equation: the velocity of the fluid is 391 392 proportional to the square of the pipe diameter. This demonstrates that the relationship between velocity and throat diameter in complex porous media is basically conformed with the simple 393 theory. At the macroscopic scale, we observe a strong correlation between the average throat 394 diameter and macroscopic permeability of various porous media. The data points from different 395 sources (Encalada et al., 2020; Lala & El-Sayed, 2017; LU et al., 2018; Pang et al., 2018) collapse 396 onto a single master curve shown in Figure 15b. The slope of the fit is 2.18, which is basically in 397 accordance with the results of $K \propto D^2$ by combining the Hagen-Poiseuille equation and Darcy's 398 Law (Ozgumus et al., 2014). This indicates that there are strong connections between the pore 399



400 structure and the fluid flow characteristics, and that the connections exist at both micro-and macro-

401

scales.

402

Figure 15 (a) The relationship between throat diameter and pore-scale velocity plotted with error
bars (b) The relationship between average throat diameter and macroscopic permeability. Data
points from different sources are colored differently. Solid lines are a guide to the eye.

406 **5 Connectivity analysis based on complex pore network**

The connectivity among nodes with different degrees has been found to play an important 407 role in the transportation and communication within a network. These dependencies can be related 408 to the degree-degree correlations or assortativity, which measures the likelihood that nodes link to 409 nodes of similar or dissimilar nodal degree. The degree correlations can be simply characterized 410 using the degree correlation coefficient r proposed by Newman (2002). It varies between 411 $-1 \le r \le 1$: for r < 0 the network is disassortative, for r = 0 the network is neutral and for r > 0412 the network is assortative. Another way to quantify the degree correlations is to measure for each 413 node i the average degree of its neighbors (Pastor-Satorras et al., 2001): 414

415
$$k_{nn,i} = \frac{1}{k_i} \sum_{j \in V_i} k_j = \frac{1}{k_i} \sum_{j \in V} A_{ij} k_j$$
(6)

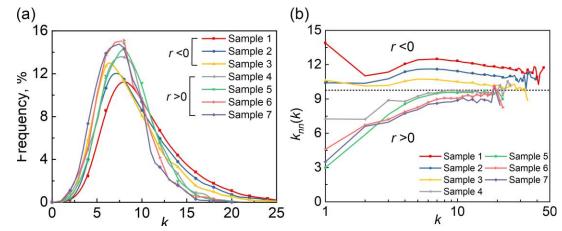
where k_i, k_j are the connectivity degree of node *i* and *j*, respectively. Define *V* as the set of nodes in the complex network, and V_i denote the set of neighbors of node *i*. *A* is the adjacency matrix of the complex networks. If node *i* is connected with node *j*, then A_{ij} =1; otherwise, A_{ij} =0.

For all nodes with degree k, $k_{nn}(k)$ is the average degree of the neighbors of all nodes with degree k.

$$k_{mn}(k) = \frac{1}{N_k} \sum_{i \in V_k} k_{mn,i}$$
⁽⁷⁾

where V_k is the subset of nodes with degree value equal to k, and $N_k = |V_k|$ is the number of nodes with degree equal to k. A subset of nodes with degree equal to k is more likely to be connected with a subset of nodes with degree equal to $k_{nn}(k)$.

We can inspect the dependence of $k_{nn}(k)$ on k to quantify the degree correlations (Newman, 2002). As shown in **Figure 16**, we discover a slightly overall decreasing trend in $k_{nn}(k)$ for samples 1~3, which indicates nodes of high degree prefer to link with low-degree nodes (see **Figure 11**). For samples 4~7, $k_{nn}(k)$ increases gradually with the increasing degree value, indicating that nodes of comparable degree tend to link to each other, i.e., small-degree nodes to small-degree nodes and hubs to hubs, and the network is called assortative. Thus, the networks for samples 1~3 are disassortative, and networks for samples 4~7 are assortative.



432

421

Figure 16 (a) The distributions of nodes degree; (b) The relationships between $k_{nn}(k)$ and node degree.

435

For disassortative networks (Samples 1~3), the wide and inhomogeneous distributions of node degree implies complicated pore connection patterns. The fluid has a tendency to flow from low-degree pores to high-degree pores. These networks show a scattered and messy distribution of flow paths that results in the flow process tending to be disordered and of high entropy. Thus, more energy will be dissipated during flow, which ultimately leads to low permeability. The assortative networks (Samples 4~7) have relatively simple connection patterns. The flow paths are relatively regular, and the flow process is in an orderly manner, indicating that less energy will bedissipated and the permeability tends to be high.

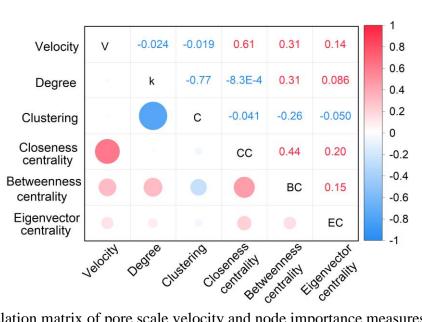
Then, we analyze local correlations between the complex network measures of each pore 444 and the pore scale velocity. These measures are summarized in Table 4 and are calculated in terms 445 of the adjacency matrix and node degree, in which A is the adjacency matrix of the graph G with 446 eigenvalue λ ; σ_{ik} is the number of paths between node *j* and *k*; $\sigma_{ik}(i)$ is the number of paths 447 between node *i* and *k* that pass through node *i*; λ is the eigenvalue of matrix *A*. The local 448 clustering coefficient C_i measures the local density of 3-cycles surrounding a node (Watts & 449 Strogatz, 1998). Closeness centrality CC_i is used to describe the importance of a node to transport 450 across the network, which is calculated as the reciprocal of the shortest path length (Bavelas, 1950). 451 A node with high closeness centrality indicates it has close relationships with many nodes (Metcalf 452 & Casey, 2016). Betweenness centrality BC_i is a measure of traffic flow that represents the total 453 454 fraction of all-pairs shortest paths that pass through node *i* (Brandes, 2001). Eigenvector centrality EC_i describes the qualitative aspect of the connections of node *i*. It is based on the assumption 455 that connections to more critical nodes are more momentous than to less critical nodes (Parau et 456 al., 2017). 457

Figure 17 shows the correlation matrix of pore scale velocity and measures reflecting node 458 importance. Correlations exist between flow velocity and the node features extracted from 459 complex network analysis, especially the closeness centrality. The results in Figure 18 suggest 460 that pores with higher closeness centrality have shorter shortest path length and larger flow 461 velocity. On the contrary, pores with lower closeness centrality have longer shortest path length 462 and smaller flow velocity. That is, porous media with more centered pores connected with others 463 make a positive contribution to the fluid flow and show a high permeability. We adopt the 464 closeness centrality of nodes to measure the importance of pore space for fluid flow and reveal the 465 interplay between fluid flow, shortest paths, and pore size in the microcosmic scale. 466

- 467
- 468
- 469
- 470

Parameter	Variable	Equation
Velocity	V	-
Degree	k	$k_i = \sum_{j=1}^N A_{ij}$
Clustering	С	$C_{i} = \frac{1}{k_{i}(k_{i}-1)} \sum_{j,k} A_{ij} A_{jk} A_{ki}$
Closeness centrality	СС	$CC_{i} = \frac{n-1}{N-1} \frac{n-1}{\sum_{j=1}^{n-1} d_{ij}}$
Betweenness centrality	BC	$BC_{i} = \frac{2}{(N-1)(N-2)} \sum_{\substack{j,k \in V \\ i \neq j \neq k}} \frac{\sigma_{jk}(i)}{\sigma_{jk}}$
Eigenvector centrality	EC	$EC_i = rac{1}{\lambda} \sum_{j \in V} A_{ij} ullet EC_j$

Table 4 Local parameter calculation formula



- Figure 17 Correlation matrix of pore scale velocity and node importance measures of complex
- 476 network.

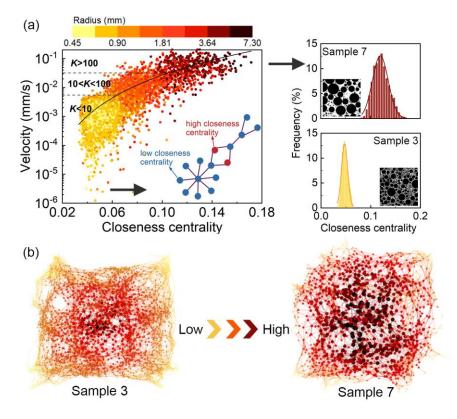


Figure 18 (a) Scatter plots of the node closeness centrality and pore-scale flow velocity and the
distributions of the closeness centrality of two granular packings. Dots are colored by pore size;
(b) Two typical complex networks. The node size and color depth represent the closeness
centrality value.

484 6 Conclusions

We report a systematic investigation on the influences of pore structure on the flow characteristics of landslide deposits from both micro-and macroscopic perspectives. Seven granular packings with significantly different grain gradations are constructed to represent typical landslide materials. Both pore-space topological measurements and complex network analysis are employed to characterize the pore structure of the idealized landslide materials. The main findings are as follows:

(1) Due to the complex pore structure of landslide materials, there is 1~2 orders of magnitude permeability variation for approximately the same porosity, indicating that porosity alone is not sufficient to determine the macroscopic permeability. The topological characterization of pore structure using tortuosity, heterogeneity, and fractal dimension shows correlation with macroscopic permeability. This is especially evident for pore tortuosity, which demonstrates a 496 clear relation with permeability that covers eight orders of magnitude for permeability on a variety497 of porous medium.

(2) The pore network modeling is a powerful tool in analyzing the pore structure of 498 landslide materials. With the increase of coarse grains, the pore throat size becomes larger and the 499 distributions are wider and more heterogeneous, resulting in a high permeability. The pore throat 500 geometry displays clearly three distinctive distributions in the scope of this study. The 501 correspondence between pore throat size distribution and pore connectivity and permeability range 502 503 suggests the importance of pore size heterogeneity and pore connectivity on the fluid flow. The 504 pore-scale flow velocity and macroscopic permeability show power law growth with throat diameter and its ensemble average value, respectively, with an exponent close to 2, which is in 505 accordance with the Hagen-Poiseuille equation. This means that the relationship between fluid 506 characteristics and complex pore structures is conformed with the simple theory. 507

(3) The pore space topology is also explored by using complex network approach. The overall measures of complex networks, such as network entropy, global efficiency, and transitivity show significant correlations with macroscopic permeability. The careful inspection of connection patterns between pores reveals that disassortative pore networks have lower permeability and assortative pore networks generally have higher permeability. The closeness centrality is a good measure to link the internal connectivity and the efficiency of transmission pathways across spatial scales.

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520 Data Availability Statement

521 The data supporting this paper can all be found at the corresponding author's github 522 repository (https://github.com/tinazhangjia/Samples-imformation).

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