# Imaging the Earth using time-domain surface-wave measurements: Evaluation and correction of the finite-frequency phase shift

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#### Abstract

Surface waves propagating from earthquakes, active sources or within the ambient noise wavefield are widely used to image Earth structure at various scales, from centimeters to hundreds of kilometers. The accuracy of surface-wave, phase-velocity measurements is essential for the accuracy of the Earth models they constrain. Here, we identify a finite-frequency phase shift in the phase travel time that causes systematic errors in time-domain, phase-velocity measurements. The phase shift arises from the approximation of monochromatic surface waves with narrow-band filtered surface waves. We derive an explicit formula of the finite-frequency phase shift and present a numerical method for its evaluation and for the correction of the measurements. Applications to high-frequency and long-period examples show that the phase shift is typically around  $\pi/60$ - $\pi/16$  for the common settings of ambient-noise imaging studies, which translates to 0.2-0.8% phase-velocity measurement errors. The finite-frequency phase shift depends on the (1) second derivative of the wavenumber with respect to frequency; (2) width of the narrow-band filter; (3) epicentral or interstation distance; (4) center frequency of the filter. In conversion to phase velocity, the last two factors cancel out. Frequency-domain methods for phase-velocity measurements have the advantage of not producing the finite-frequency phase shift. Both time- and frequency-domain measurements, however, can be impacted by a break-down of the far-field approximation (near-field phase shift), which our calculations also show. Our method offers an effective means of improving the accuracy of the widely used time-domain, phase-velocity measurements via the evaluation of and corrections for the finite-frequency phase shift.

1	Imaging the Earth using Time-domain Surface-wave Measurements: Evaluation and
2	<b>Correction of the Finite-frequency Phase Shift</b>
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10	Key Points:
11 12	• We identify a source of errors that can cause up to ~1% error in surface-wave phase-velocity measurements.
13	• The error applies to all the time-domain methods that use bandpass-filtered waveforms.
14 15	• We derive an explicit formula to evaluate the error and provide a numerical method to compute and remove it.

### 16 Abstract

Surface waves propagating from earthquakes, active sources or within the ambient noise 17 wavefield are widely used to image Earth structure at various scales, from centimeters to 18 hundreds of kilometers. The accuracy of surface-wave, phase-velocity measurements is essential 19 for the accuracy of the Earth models they constrain. Here, we identify a finite-frequency phase 20 shift in the phase travel time that causes systematic errors in time-domain, phase-velocity 21 22 measurements. The phase shift arises from the approximation of monochromatic surface waves with narrow-band filtered surface waves. We derive an explicit formula of the finite-frequency 23 phase shift and present a numerical method for its evaluation and for the correction of the 24 25 measurements. Applications to high-frequency and long-period examples show that the phase shift is typically around  $\pi/60-\pi/16$  for the common settings of ambient-noise imaging studies, 26 which translates to 0.2-0.8% phase-velocity measurement errors. The finite-frequency phase shift 27 depends on the (1) second derivative of the wavenumber with respect to frequency; (2) width of 28 the narrow-band filter; (3) epicentral or interstation distance; (4) center frequency of the filter. In 29 conversion to phase velocity, the last two factors cancel out. Frequency-domain methods for 30 phase-velocity measurements have the advantage of not producing the finite-frequency phase 31 32 shift. Both time- and frequency-domain measurements, however, can be impacted by a break-33 down of the far-field approximation (near-field phase shift), which our calculations also show. Our method offers an effective means of improving the accuracy of the widely used time-34 domain, phase-velocity measurements via the evaluation of and corrections for the finite-35 36 frequency phase shift.

### 37 Plain Language Summary

Surface waves sample the 'surface layer' of the Earth with the thickness of the layer depending 38 on the wave's wavelength. Combining surface waves of different wavelengths, or different 39 frequencies, can provide a detailed image of the Earth's structure over a large depth range. 40 Measuring the velocity at which surface waves travel is a crucial step in this process. In this 41 study, we identify a source of errors in the measurements that has not received much notice so 42 43 far. We first derive a formula for the possible bias and then develop a numerical method to evaluate and correct it. Applications of the numerical method reveal the effects of the bias in two 44 common scenarios, in the surface-wave studies of the shallow (kilometers deep) and deep 45 (hundreds of kilometers deep) structure of the Earth. Our results provide a means to improve the 46 accuracy of the surface wave measurements and, thus, the accuracy of the surface-wave imaging 47 of the Earth. 48

### 49 **1 Introduction**

Surface waves sample the Earth's interior at scales from centimeters to hundreds of 50 kilometers, with varying resolution depending on their frequency. Intermediate- and long-period 51 52 (>5 s) surface waves generated by earthquakes provide essential constraints on the shear-wave velocity structure and anisotropy of the crust (e.g., Agius & Lebedev, 2014, 2017; Bourjot & 53 Romanowicz 1992; Levshin & Ratnikova, 1984; U. Meier et al. 2007; Polat et al. 2012; Press & 54 55 Ewing, 1955), lithosphere and asthenosphere (e.g., Bonadio et al. 2021; Deschamps et al. 2008; Ekström & Dziewonski 1998; El-Sharkawy 2020; Masters et al. 1996; T. Meier et al. 2004; 56 Pasyanos et al. 2014; Shapiro & Ritzwoller 2002; Zhang et al. 2009), and crustal and upper-mantle 57 interfaces (e.g., Bartzsch et al. 2011; Beghein et al. 2019; Lebedev et al., 2013). High-frequency 58 (>5 Hz) surface waves generated by active sources have been used to constrain upper-crustal and 59 60 near-surface structure (e.g., Mi et al. 2020; Pan et al., 2019; Socco et al., 2010; Wathelet et al.,

2004; Xia et al., 1999). Ultrasonic (>20 kHz) surface waves image the top few centimeters beneath
the surface, providing information about hidden cracks in concrete and weathering in historical
sites (e.g., Aggelis et al., 2010; Bodet et al. 2005; T. Meier et al., 2017).

During the last two decades, ambient noise interferometry (cross-correlation of noise recorded 64 at two receivers yielding estimates of the Green's functions) has been widely adopted as an 65 additional approach for surface-wave imaging. It provides abundant surface wave observations 66 67 and fills the frequency gap between earthquakes and active sources. It also facilitates the imaging of regions where earthquakes and active sources cannot provide sufficient illumination (e.g., Li et 68 al., 2016; Mordret et al., 2013; Nicolson et al., 2014; Zhan et al., 2014). Ambient noise surface 69 70 wave tomography has been successfully applied to imaging subsurface structure and anisotropy from the crustal and upper mantle scale (e.g., Moschetti et al., 2007; Pawlak et al. 2012; Sabra et 71 al., 2005; Shapiro et al., 2005; Yao et al., 2006), to the scale of a basin, a volcano, or a fault region 72 (e.g., Brenguier et al., 2007; Delorey & Vidale, 2011; Inzunza et al., 2019; Martins et al., 2019; 73 Mordret et al., 2019; Roux et al., 2011), and to a mineral-deposit scale (e.g., Bellefleur et al., 2015; 74 Hollis et al., 2019; Mordret et al., 2013; Xu et al., 2021). The method is also applied in other fields, 75 such as cryoseismology (e.g., Lindner et al., 2019; Preiswerk & Walter, 2018). 76

Accurate group or phase velocity measurements are the foundation of most surface-wave studies at any scale. The measurement methods fall into two categories, with the measurements performed either in the time domain or in the frequency domain. Time-domain methods measure the arrival time or the instantaneous phase of surface waves in the time domain and then convert them to the velocity. One representative method is the frequency-time analysis (FTAN; Bensen et al., 2007; Dziewonski et al., 1969; Dziewonski & Bloch, 1972; Ritzwoller & Levshin, 1998; Yao et al., 2006). Using a set of narrow-band filters, the original, broadband surface waves are turned

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into a set of narrow-band surface-wave signals. One can then measure the phase travel time or instantaneous phase on the narrow-band seismograms to obtain phase velocities, or measure the group travel time on the envelopes to obtain group velocities. Using multiple stations can solve the ambiguity in the phase velocity measurement (e.g., Martins et al., 2019; Xia et al., 1999), even determine the direction of phase velocity (e.g., Kolínský et al., 2019).

The time-domain methods for the determination of the phase velocity implicitly assume that 89 90 the narrow-band signals represent the monochromatic surface waves at the center frequencies of the filters. The approximation can result in systematic errors in the measurements. By contrast, 91 frequency-domain methods measure the phase of the spectra using the Fourier transform (Bonadio 92 93 et al., 2018, 2021; Fry et al., 2010; Kästle et al., 2016; T. Meier et al., 2004; Molinari et al., 2015; Verbeke et al., 2012; Zhang et al. 2007). The frequency-domain methods do not rely on the 94 assumption of monochromaticity of narrow-band surface waves. However, they require effective 95 procedures for identifying the correct  $2\pi$  branch of the phase of the surface wave (e.g. Bonadio et 96 al., 2018, 2021; Soomro et al., 2016). 97

98 Both the time- and frequency-domain methods, originally developed for earthquake 99 seismograms, have been applied in ambient noise studies with minor modifications. The difference 100 is that the initial phase of virtual sources is zero (Bensen et al., 2007; Bonadio, 2019; Kästle et al., 101 2016; Yao et al., 2006), as the cross-correlation in noise interferometry cancels out the original initial phase from noise sources. Moreover, the zero initial phase leads to an alternative frequency-102 103 domain method as well (Aki, 1957; Ekström, 2014; Ekström et al., 2009). The spectrum of the noise cross-correlation functions (NCFs) is found to resemble a Bessel function with the argument 104 of  $\omega \Delta / c(\omega)$ , where  $\omega$  is angular frequency,  $\Delta$  is interstation distance and *c*—phase velocity. Phase 105 velocity can be obtained by fitting the Bessel function to the real part of the spectrum of NCFs. 106

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In this paper, we focus on the accuracy of phase velocity measurements using the time-domain methods, most popular due to their simplicity. Successful measurements of phase velocity are usually more accurate than those of group velocity and, also, can be related to Earth structure and anisotropy more unambiguously (Dahlen & Zhou, 2006). Phase-velocity measurements, however, are more complicated than group-velocity ones, even after the unknown initial phase is resolved.

Unlike with the group velocity, converting measured phase or phase travel time to correct phase velocity does not follow a simple relationship of  $t = \Delta/c$ , where t and c are phase travel time and phase velocity, respectively. Instead, misalignments have been long observed between the monochromatic surface wave and its corresponding Fourier component,  $\cos(\omega(t-\Delta/c))$  (Brune et al., 1961; Toksöz & Anderson, 1966; Tromp & Dahlen, 1992; Wang et al., 1993). The misalignments are generally referred to as phase shifts, which must be accounted for during the conversion; otherwise, the resulting phase velocity is biased.

We refer to phase shifts as phase advances or delays (Aki & Richards, 2002; Brune et al., 119 120 1961), where a phase advance refers to an event arriving earlier than expected and a phase delay refers to a late arrival. The representation is unambiguous regardless of the sign of frequency and 121 122 the convention of the Fourier transforms. The value of a phase shift is defined as the amount of 123 deviation of the measured phase from a predicted phase that usually from theoretical approximations. A phase advance, if not corrected, will result in a higher phase velocity, and vice 124 versa. Phase advances and delays corresponds to decreases and increases of the absolute magnitude 125 126 of the phase in frequency domain, respectively.

127 A number of types of the phase shifts have been identified. Quantifying and taking them into 128 account is essential for the accuracy of the measurements and for the accuracy of the Earth-129 structure models computed using the measurements. A phase delay of  $\pi/4$  is commonly used in

noise cross-correlation studies (e.g., Yao et al., 2006). The phase delay, which is physically 130 generated during interference of surface waves from different noise sources, is referred as (virtual) 131 source phase shift hereafter as it is analogous to the  $\pi/4$  phase delay in surface waves generated by 132 earthquakes. The  $\pi/4$  is an approximation in the far field (several wavelengths away) of the (virtual) 133 source. The amount of the phase shift changes with distance in the near field. Consequently, most 134 noise cross-correlation studies discard short-distance measurements, e.g., less than 1-3 135 wavelengths (Bensen et al., 2007; Luo et al., 2015; Shapiro et al., 2005). The phase delay turns to 136 a phase advance of  $\pi/4$  when using noise cross-correlation functions (NCFs; Kästle et al., 2016) 137 instead of empirical Green's functions (EGFs) that equals the opposite of the first derivative of the 138 NCFs with respect to time. 139

Another type of phase shift is the caustic phase shift. It is generated when surface waves pass 140 a caustic where rays of surface waves cross (e.g., Tromp & Dahlen, 1992; Wang et al., 1993). 141 Surface waves stack constructively at a caustic and change their phase. The caustic phase shift is 142 a  $\pi/2$  phase advance in the far field of the caustic. Each passage of a caustic causes a  $\pi/2$  phase 143 advance. One example of the caustic phase shift is the polar phase shift (Brune et al., 1961), which 144 occurs when surface waves travel across the antipode of the source and the polar area (the source). 145 The corresponding caustics are exactly at the source and its antipode in a spherically symmetric 146 Earth model and can deviate from the antipode for 10°-20° in a heterogeneous Earth model Earth 147 (Wang et al., 1993). The source phase shift can be regarded as a 'semi-caustic' as well. Its 148 149 difference from a caustic is that rays converge and diverge at a caustic but only diverge at the 150 source (Brune et al., 1961).

In the vicinity (near field) of a caustic or semi-caustic, the phase advance deviates from its
far-field value (Kästle et al., 2016; Pollitz, 2001; Schwab & Kausel, 1976; Tromp & Dahlen, 1993;

Wielandt, 1980). The exact amount of the phase shift can be either estimated analytically, by adding higher-order terms of Taylor expansions into the analysis (Herrmann, 1973; Wielandt, 1980), or computed numerically (Schwab & Kausel, 1976). In this paper, we use near-field phase shifts to refer to the difference between a (semi-)caustic phase shift and its far-field approximation.

In the time-domain methods for phase-velocity measurement, approximating monochromatic 157 surface waves by narrowband ones causes additional types of phase shifts due to the interference 158 between neighboring frequencies. The origins of such errors and corresponding solutions have 159 been discussed in the context of group-velocity measurements (Dziewonski & Bloch, 1972; 160 Herrmann, 1973; Levshin et al., 1992; Shapiro & Singh, 1999). The two origins identified are rapid 161 162 changes in the group-velocity dispersion curve and variations in the amplitude spectra. The proposed solutions for group velocity changes normally involve an iterative procedure that reduces 163 most of the changes in group velocity by subtracting the group velocity measured in the original 164 seismogram (Bensen et al., 2007; Dziewonski & Bloch, 1972; Ritzwoller & Levshin, 1998). 165 Solutions for non-constant amplitude spectra involve replacing the center frequency by an 166 instantaneous frequency (Ritzwoller & Levshin, 1998) or a centroid frequency (Shapiro & Singh, 167 1999). 168

The narrow-band approximation also has an effect on phase-velocity measurements. To our knowledge, however, there are no systematic studies on the associated phase shifts and their effects on the measurements and the resulting Earth models, especially in the context of noise crosscorrelations. Herrmann (1973) showed an additional phase term in the mathematical representation of Gaussian filtered surface waves, but he did not discuss its further implication.

The purpose of this paper is to present a systematic study of—and practical ways to correct for—the phase shift caused by approximating monochromatic surface waves by narrow-band

surface waves. We refer to the phase shift as the finite-frequency phase shift, as it originates from 176 a replacement of an infinitesimally narrow frequency band by a finite-width band. We first derive 177 an explicit expression of the phase shift, under certain assumptions, and then present a numerical 178 method to accurately evaluate the phase shift. We also demonstrate the effect of the finite-179 frequency phase shift on the phase velocity measurements and offer recipes for the correction of 180 181 the phase shift in order to obtain accurate phase-velocity measurements. The results apply to measurements with time-domain methods on surface waves from earthquakes, active sources and 182 ambient seismic noise. 183

### 184 **2 Finite-frequency phase shift**

Surface waves at different frequencies travel at different speeds. To measure phase velocities at different frequencies, a comb of narrow-bandpass filters is often used to isolate individual frequencies, such as in the multiple filter technique (Dziewonski et al., 1969). The filtered surface wave resembles a cosine function with a period of  $1/f_c$ , where  $f_c$  is the center frequency of the filters (Figure 1a). Assuming the narrowband surface waves share the same peaks with the monochromatic surface waves, the arrival time of the peaks can be written explicitly,

191 
$$t_n = \frac{\Delta}{c} + \frac{1}{8f_c} + \frac{n}{f_c} + \frac{\phi_s}{\omega_c}, \quad n = 0, \pm 1, \pm 2, ...,$$
(1)

where  $\Delta$  is the distance, *c* the phase velocity at the frequency  $f_c$ ,  $\omega_c = 2\pi f_c$  the angular frequency,  $\phi_s$  the initial phase of the source (Dahlen & Tromp, 1998; Yao et al., 2006). The 1/(8 $f_c$ ) is the manifestation of the  $\pi/4$  phase delay caused by the source term. We refer to *n* as the order of peaks in the narrowband surface waves, or 'ridges' in the frequency-time representation (Figure 1b). The Oth ridge is often referred as the 'correct' ridge (e.g., Wang et al., 2017; Yao et al., 2006), though other ridges can also generate correct phase velocity measurements if the time shift  $n/f_c$  is corrected (Bonadio et al., 2018; T. Meier et al., 2004; Soomro et al., 2016; Xu et al. 2021).

199 The finite-frequency phase shift,  $\delta\phi$ , corresponds to the time offset  $\delta t (= \delta\phi/2\pi f_c)$  between the 200 peaks of the narrowband and monochromatic surface waves (Figure 1c), giving a more accurate 201 prediction of the arrival time of the peaks,

202 
$$t_n = \frac{\Delta}{c} + \frac{1}{8f_c} + \frac{n}{f_c} + \frac{\phi_s}{\omega} + \delta t, \quad n = 0, \pm 1, \pm 2, \dots.$$
(2)

Unlike the 'systematic error' due to the variations in amplitude spectra, discussed by Shapiro and Singh (1999), the phase shift is non-zero even for constant amplitude spectra. It needs to be corrected along with the  $\pi/4$  phase delay to get an accurate measurement of phase velocities,

206 
$$c = \frac{\Delta}{t - 1/8f_c - n/f_c - \phi_s/\omega_c - \delta t},$$
 (3)

207 or

208 
$$c = \frac{\omega_c \Delta}{\omega_c t - \pi/4 - 2n\pi - \phi_s - \delta \phi}.$$
 (4)

Figure 2 illustrates the origin of the finite-frequency phase shift. Monochromatic surface waves are generated at three equal-spaced frequencies, 0.99, 1.00 and 1.01 Hz. Superposition of the three produces a narrow-band surface wave (Figure 2b, c). The three monochromatic surface waves have the same amplitude, so as to avoid the influence of the spectral amplitude variation. When the phase velocity dispersion curve is linear, the peak in the narrow-band surface wave arrives at the same time as the peak of the center-frequency (1 Hz) surface wave. By contrast, when the dispersion curve is not linear, the two peaks have a slight misalignment. The

- 216 misalignment is the finite-frequency phase shift. If not accounted for, the misalignment will result
- in a biased phase velocity measurement.





Figure 1 Time-domain phase velocity measurement and the finite-frequency phase shift. (a) Broadband and narrow-bandpass-filtered surface waves. The broadband surface wave is a synthetic seismogram generated using the velocity model ak135 (Kennett et al., 1995). For the narrow-band surface wave, a Gaussian filter with the center frequency of 0.03 Hz and  $\alpha = 48$  is used. The arrival times of the peaks are marked by vertical lines, with the peak corresponding to the correct phase travel time marked by a solid line and other peaks by dashed lines. (b) Frequency-time representation of the broadband surface wave.

Each row of the image corresponds to a narrow-band filtered surface wave. Connected peaks form ridges, with the 'correct' ridge marked by a solid line and other ridge by dashed lines. The separation between these ridges are n/f, or  $2n\pi$  in phase. (c) The finite-frequency phase shift. The measured phase travel time is  $f/8+\delta t$  s later than the predicted phase travel time of  $\Delta/c$ , equivalent to a  $\pi/4+\delta\phi$  phase delay, where  $\delta\phi$  is the finite-frequency phase shift.



Figure 2 Finite-frequency phase shift caused by using a bundle of frequencies to estimate the centre frequency. (a) Phase velocity curves used in the example. The black line denotes the curve that is linear, whereas the red line denotes a curve with a curvature (the kink at 1 Hz). (b) Monochromatic components at 0.99, 1.00 and 1.01 Hz and their superposition. The linear curve is used. The diamond and the dashed line mark the arrival time of the peak of the 1-Hz component. The arrow points to the arrival time of the peak of the superposition. (c) Same as b but using the curve with the kink.

### 238 **3 Theoretical derivation**

We can derive an explicit expression for the finite-frequency phase shift assuming the far field approximation and narrow frequency bands. By far field, we mean large  $|\omega|\Delta/c = 2\pi\Delta/\lambda$ , that is, a large number of wavelengths fitting between the source and station, or between two stations in the case of noise interferometry and two-station methods. Starting from the spectrum of surface waves, we integrate the spectrum over frequency in order to obtain the seismogram of surface waves, to which we refer as broadband surface waves. Then, we apply Gaussian filters to obtain the explicit expression for the narrow-band surface waves, from which, finally, we obtain the explicit expression for the finite-frequency phase shift.

247 3.1 Stationary phase approximation

The stationary phase approximation method is used repeatedly in the following derivation in order to approximate integrals. We briefly summarize the points that are relevant to our derivation. For more details, we refer the reader to Aki and Richards (2002). The method is used to estimate the integral of the form

252 
$$\int_{a}^{b} F(\omega) \exp(f(\omega)) d\omega, \qquad (5)$$

where  $F(\omega)$  and  $f(\omega)$  are real functions and  $\omega$  is a dummy variable that does not necessarily mean frequency. Both *a* and *b* can be infinity. This type of integral is dominated by several discrete points where  $f'(\omega) = 0$ . They are termed stationary phase points or saddle points (after the shape of the integrand surface near these points in the complex domain of  $\omega$ . If the  $|f''(\omega)|$  values at the saddle points are sufficiently large, the integral can be estimated as a summation of the contribution of the saddle points,

259 
$$\sum_{\omega_0 \in saddle \ points} F(\omega_0) \exp(f(\omega_0)) \sqrt{\frac{2\pi}{|f''(\omega_0)|}} \times \begin{cases} \exp\left(i\frac{\pi-\phi}{2}\right), & \phi \in (0,\pi] \\ \exp\left(i\frac{-\pi-\phi}{2}\right), & \phi \in (-\pi,0) \end{cases}$$
(6)

where  $\omega_0$  are saddle points within the interval [a, b] and  $\phi = \arg f''(\omega_0)$ . When a saddle point is at the end of the interval, its contribution should be halved.

- 262 3.2 Broadband time-domain waveforms
- 263 Surface waves can be written as a superposition of monochromatic surface waves,

264 
$$x(t) = \frac{1}{\pi} \Re \int_0^{+\infty} A(\omega) \exp\left(-i\frac{\omega\Delta}{c(\omega)} + i\varphi(\Delta)\right) \exp(i\omega t) d\omega, \qquad (7)$$

where  $\Re$  is the real part operator that arises from the reduction of the interval  $(-\infty, +\infty)$  to  $[0, +\infty)$ using the Hermitian symmetry of the spectrum,  $A(\omega)$  is the amplitude spectrum, and  $\varphi(\Delta)$ represents the overall phase shift regarding propagation of monochromatic surface waves, comprising the initial phase from the source mechanism, the source phase shift and the caustic phase shift when passing a polar or antipodal region. The Fourier transform we used is

270 
$$F(\omega) = \int_{-\infty}^{+\infty} f(t) \exp(-i\omega t) dt,$$

271 
$$f(t) = \frac{1}{2\pi} \int_{-\infty}^{+\infty} F(\omega) \exp(i\omega t) \, d\omega \,, \tag{8}$$

although the conclusion is independent of the convention of Fourier transform. For any given
distance, equation 7 can be evaluated using the stationary phase approximation,

274 
$$x(t) \approx \sqrt{\frac{2}{\pi\Delta |k''(\omega_0)|}} \times \begin{cases} \cos\left(\omega_0 t - k(\omega_0)\Delta + \varphi - \frac{\pi}{4}\right), & k''(\omega_0) > 0\\ \cos\left(\omega_0 t - k(\omega_0)\Delta + \varphi + \frac{\pi}{4}\right), & k''(\omega_0) < 0 \end{cases}$$
(9)

where  $k(\omega) = \omega/c(\omega)$  is the wavenumber and  $k'(\omega_0) = t/\Delta$ . It shows that the instantaneous phase of broadband surface waves deviates from its corresponding monochromatic component by  $\pm \pi/4$ , depending on the sign of  $k''(\omega_0)$ .  $k''(\omega_0)$  is positive when  $dc_g/dT > 0$ , where  $c_g = d\omega/dk$  is group velocity and  $T = 2\pi/\omega$  is period. The corresponding frequency for each time *t* can be found by solving  $k'(\omega_0) = t/\Delta$ .

### 280 3.3 Narrowband time-domain waveforms

## 281 3.3.1 Far-field approximation

Bandpass filtering can change the instantaneous phase of surface waves. Applying a Gaussian filter to the broadband surface wave (equation 7), we have

284 
$$x(t) = \frac{1}{\pi} \Re \int_0^{+\infty} A(\omega) \exp\left(-i\frac{\omega\Delta}{c(\omega)} + i\varphi(\Delta)\right) \exp\left(-\alpha \frac{(\omega - \omega_c)^2}{\omega_c^2}\right) \exp(i\omega t) d\omega, \quad (10)$$

where  $\omega_c$  is the center frequency of the filter and  $\alpha$  (> 0) is a parameter that controls the width of the filter. Using the stationary phase approximation, we can obtain the explicit expression for the time-domain waveform of the filtered surface wave,

$$\begin{aligned} x(t) &\approx \sqrt{\frac{2}{\pi \left| ik'' \Delta + \frac{2\alpha}{\omega_c^2} \right|}} A(\omega_0) \exp\left(-\alpha \frac{(\omega_0 - \omega_c)^2}{\omega_c^2}\right) \\ &\times \begin{cases} \cos\left(\omega_0 t - k\Delta + \varphi(\Delta) + \frac{-\pi - \beta}{2}\right), & k''(\omega_0) > 0\\ \cos\left(\omega_0 t - k\Delta + \varphi(\Delta) + \frac{\pi - \beta}{2}\right), & k''(\omega_0) < 0 \end{cases}$$

$$,(11)$$

where the stationary phase point  $\omega_0$  is determined by

290 
$$-ik'(\omega_0)\Delta + it - 2\alpha \frac{\omega_0 - \omega_c}{\omega_c^2} = 0, \qquad (12)$$

291 and

288

292 
$$\beta = \arg f''(\omega) = \arg \left( -\frac{2\alpha}{\omega_c^2} - ik''(\omega_0)\Delta \right).$$
(13)

When using a wide-band Gaussian filter (α→0), β in equation 11 approaches -π/2 for k"(ω₀)
0 and π/2 for k"(ω₀) < 0. Thus, equation 11 degenerates to its broadband counterpart, equation</li>
9. When using a narrow-band filter (α→∞), β→-π (k"(ω₀) > 0) and π (k"(ω₀) < 0), the cosine term</li>

in equation 11 in both cases become  $\cos(\omega_0 t - k\Delta + \varphi(\Delta))$ , which has the same phase as the monochromatic surface waves in equation 7. This is why narrow-bandpass filtered surface waves can be used to measure phase velocity at the center frequencies of the filters. However,  $\alpha$  cannot be  $\infty$  when making real measurements. It is crucial to know how much is the error for using a finite  $\alpha$ . As the saddle points move away from the real axis into the complex domain for  $0 < \alpha < \infty$ , it is not trivial to evaluate the phase shift using the stationary phase approximation, so we turn to another approximation under the narrow-band assumption.

303 3.3.2 Far-field and narrow-band approximation

To obtain an explicit expression for the finite-frequency phase shift, we re-evaluate the integral in equation 10 using Taylor expansions at the center frequency  $\omega_c$ . In additional to the farfield approximation, we limit ourselves to narrow-band filters. In this case, let

307 
$$F(\omega) = \frac{A(\omega)}{\pi}$$

308

$$f(\omega) = \omega t - k\Delta + \varphi(\Delta), \tag{14}$$

309 we can expand  $F(\omega)$  and  $\exp(if(\omega))$  at  $\omega_c$ ,

$$F(\omega) \approx F(\omega_c) + F'(\omega_c)(\omega - \omega_c) + \frac{1}{2}F''(\omega_c)(\omega - \omega_c)^2$$
  

$$\exp(if(\omega)) \approx \exp(if(\omega_c)) \left[1 + if'(\omega_c)(\omega - \omega_c) + \frac{1}{2}(if''(\omega_c) - f'^2(\omega_c))(\omega - \omega_c)^2\right].$$
(15)

Substituting equation 15 into equation 10, the integral can be organized as a series of integrals  $\int (\omega - \omega_c)^n \exp(-\alpha(\omega - \omega_c)^2) d\omega$ , which can be evaluated analytically. Summing the results yields the expression for the time-domain waveform of narrowband surface waves,

314 
$$x(t) \approx \frac{A(\omega)B}{\pi} \omega_c \sqrt{\frac{\pi}{\alpha}} \cos(i(\omega t - k\Delta + \varphi(\Delta) - \delta\phi)), \qquad (16)$$

315 where *B* and  $\delta\phi$  are the amplitude and phase, respectively, of a complex number given by

316 
$$B\exp(i\delta\phi) = F(\omega_c) + \frac{\omega_c^2}{2\alpha} \left[ -\frac{1}{2} F(\omega_c) f'^2(\omega_c) + \frac{1}{2} F''(\omega_c) \right] - i \frac{\omega_c^2}{2\alpha} \left[ \frac{1}{2} F(\omega_c) f''(\omega_c) + F'(\omega_c) f'(\omega_c) \right].$$
(17)

The  $\delta\phi$  is the finite-frequency phase shift we are looking for. We intentionally use  $-\delta\phi$  instead of  $\delta\phi$  in equation 16, so that  $\delta\phi > 0$  corresponds to phase delay and  $\delta\phi < 0$  corresponds to phase advance.

Assuming a constant amplitude spectrum,  $F'(\omega_c)$  and  $F''(\omega_c)$  are zero. Therefore, we can evaluate the finite-frequency phase shift as

322 
$$\delta\phi = \arg\left\{\frac{4\alpha}{\omega_c^2} - (t - k'(\omega_c)\Delta)^2 + ik''(\omega_c)\Delta\right\}.$$
 (18)

For narrow-band filters when  $\alpha$  is sufficiently large, the first term dominates the real part. We can therefore simplify the mathematical representation of  $\delta \phi$  to

325 
$$\delta \phi = \arctan \frac{k''(\omega_c)\Delta}{4\alpha/\omega_c^2} \approx \frac{\omega_c^2 k''(\omega_c)\Delta}{4\alpha}$$
(19)

The formula in equation 19 reveals four factors that affect the finite-frequency phase shift, namely, (1) the center frequency of the Gaussian filter  $\omega_c$ , (2) the second derivative of the wavenumber with respect to frequency  $k''(\omega_c)$ , (3) the epicentral distance  $\Delta$  and (4) the width of the Gaussian filter  $\alpha$ . Since  $\omega_c$ ,  $\Delta$  and  $\alpha$  are all positive, the sign of the phase shift is solely determined by  $k''(\omega_c)$ . Physically,  $k''(\omega_c) > 0$  means a positive curvature (with respect to frequency) in the phase dispersion curve or a positive slope (with respect to period) in the group dispersion curve.

### 332 3.4 Finite-frequency phase shift in noise cross-correlation functions

Here we show that the finite-frequency phase shift in the surface waves in the noise crosscorrelation functions (NCFs) shares exactly the same formula with ballistic surface waves. First, we compute the spectrum of NCFs by summing the cross-correlation of incoming plane waves over all the azimuths. Assuming that we have two stations, station A and station B, separated by the distance  $\Delta$ , and an incoming plane wave that arrives at the angle  $\theta$  (measured counter-clockwise from the east) (Figure 3), the cross-correlation spectrum of the plane wave at the station A with one at station B is  $\exp(i\omega\Delta\cos\theta/c)$ , where  $\omega$  is the angular frequency and *c* is the phase velocity at this frequency. Assuming a perfect illumination, when the amplitude of the incoming plane waves is constant over azimuth, the spectrum of the noise cross-correlation can be written as

342 
$$C(\omega) = \frac{1}{2\pi} \int_{-\pi}^{\pi} \exp\left(i\omega \frac{\Delta \cos\theta}{c(\omega)}\right) d\theta = J_0\left(\frac{\omega\Delta}{c(\omega)}\right), \tag{20}$$

where  $J_0(x)$  is the zeroth-order of Bessel functions of the first kind. Evaluating the integral using the stationary phase approximation yields the far-field approximation of the spectrum of the noise cross-correlation,

346 
$$C(\omega) \approx \sqrt{\frac{2}{\pi \frac{|\omega|\Delta}{c(\omega)}} \cos\left(\frac{|\omega|\Delta}{c(\omega)} - \frac{\pi}{4}\right)}.$$
 (21)

where far field implies a large  $\omega\Delta/c = 2\pi\Delta/\lambda$  and  $\lambda$  is the wavelength. Alternatively, the approximation can be obtained using asymptotic forms of Bessel functions (Gradshteyn & Ryzhik, 2014). The contributions of the causal branch and the acausal branch can also be separated in the far-field approximation (Table 1).



Figure 3 Incoming plane wave at a pair of stations. The plane wave arrives at the stations at an angle  $\theta$ .

The distance between stations A and B is  $\Delta$ . The plane wave needs to travel farther by  $\Delta \cos\theta$  to reach station

A compared to station B. The corresponding time delay is  $\Delta \cos\theta/c$  and phase delay is  $\omega \Delta \cos\theta/c$ .

355

Table 1 Spectra of the causal and acausal branches of the noise cross-correlation under the far-field approximation. The common factor  $\sqrt{2c(\omega)/\pi|\omega|\Delta}$  is omitted. The expressions correspond to the convention of Fourier transforms indicated by equation 8. Using other conventions will result in changes of signs or an additional constant factor.

Branch	$\omega > 0$	ω < 0
Causal	$\exp\left(-i\left(\frac{\omega\Delta}{c(\omega)}-\frac{\pi}{4}\right)\right)$	$\exp\left(-i\left(\frac{\omega\Delta}{c(\omega)} + \frac{\pi}{4}\right)\right)$
Acausal	$\exp\left(i\left(\frac{\omega\Delta}{c(\omega)}-\frac{\pi}{4}\right)\right)$	$\exp\left(i\left(\frac{\omega\Delta}{c(\omega)} + \frac{\pi}{4}\right)\right)$

360

Applying inverse Fourier transform to the far-field approximation of the spectrum of the causal branch (Table 1) yields the expression of broadband surface waves in the causal branch of NCFs,

364

$$C_{+}(t) \approx \frac{1}{2\pi^{2}} \Re \int_{0}^{\infty} \sqrt{\frac{2\pi}{k\Delta}} \exp(i\omega t - ik\Delta) \exp\left(i\frac{\pi}{4}\right) d\omega$$
$$\approx \frac{1}{\pi\Delta} \frac{1}{\sqrt{|k(\omega_{0})||k''(\omega_{0})|}} \times \begin{cases} \cos(\omega_{0}t - k(\omega_{0})\Delta), & k''(\omega_{0}) > 0\\ \cos\left(\omega_{0}t - k(\omega_{0})\Delta + \frac{\pi}{2}\right), & k''(\omega_{0}) < 0 \end{cases}$$
(22)

365 where  $k'(\omega_0) = t/\Delta$ . We can also obtain the expression for the surface waves in the acausal branch,

366 
$$C_{-}(t) \approx \frac{1}{\pi \Delta} \frac{1}{\sqrt{|k(\omega_{0})||k''(\omega_{0})|}} \times \begin{cases} \cos(\omega_{0}t + k(\omega_{0})\Delta), & k''(\omega_{0}) > 0\\ \cos\left(\omega_{0}t + k(\omega_{0})\Delta - \frac{\pi}{2}\right), & k''(\omega_{0}) < 0 \end{cases}$$
(23)

367 where  $k'(\omega_0) = -t/\Delta$  (t < 0). The two branches form an even function of t.

Unlike the ballistic surface waves, surface waves in NCFs have a known  $\pi/4$  advance instead 368 of an unknown phase shift of  $\phi(\Delta)$ . However, the  $\pi/4$  phase advance can be cancelled out by the 369  $\pi/4$  phase delay that arises in the frequency integration when  $k''(\omega_0) > 0$ , making the instantaneous 370 phase of the surface wave at a certain time t is in-phase (no phase shift) with the corresponding 371 monochromatic surface wave  $\cos(\omega_0 t - \omega_0 \Delta/c(\omega_0))$ . To illustrate the phenomenon, we generate a 372 broadband surface-wave synthetic using the exact spectrum in equation 20 and ak135 (Kennett et 373 al., 1995) and then compare it with the monochromatic surface wave (Figure 4). The alignment is 374 easier to examine at the peaks, so we chose the frequency 0.0355 Hz that is the saddle point 375 corresponding to the peak at t = 901.27 s. A good consistency is observed between the 376 monochromatic and broadband surface waves at 901.27 s, confirming their alignment in terms of 377 phase. Furthermore, the instantaneous frequency at 901.27 s is also 0.0355 Hz, which can be 378 verified by computing the first derivative of the instantaneous phase  $\phi(t) = \omega_0 t - k(\omega_0) \Delta$ , which is 379

380 
$$\omega(t) = \frac{\partial \phi(t)}{\partial t} = \omega_0 + \frac{\partial \omega_0}{\partial t} (t - k'(\omega_0)\Delta) = \omega_0(t)$$
(24)

in the causal branch. The second term is zero because the saddle point  $\omega_0$  follows the relationship  $k'(\omega_0) = t/\Delta$ .





Figure 4. Broadband and monochromatic surface waves. The broadband surface wave synthetic is computed using a trapezoid integration from 2 to 50 mHz, with an interval of 0.01 mHz. There is no misalignment between the peak at t = 901.27 s and its corresponding single frequency component, as the phase delay of  $\pi/4$  that arises from the frequency integration is cancelled by the phase advance of  $\pi/4$  that arises from the integration over azimuth.

The narrowband time-domain waveforms of NCFs can be computed using the same approachas in Section 3.3,

392

$$C(t) \approx \frac{1}{2\pi^2} \Re \int_0^\infty \sqrt{\frac{2\pi}{k\Delta}} \exp(i\omega t - ik\Delta) \exp\left(i\frac{\pi}{4}\right) \exp\left(-\alpha \frac{(\omega_0 - \omega_c)^2}{\omega_c^2}\right) d\omega$$
$$\approx \frac{B}{2\pi^2} \omega_c \sqrt{\frac{\pi}{\alpha}} \Re\left\{ \exp\left(i\left(\omega t - k\Delta + \frac{\pi}{4} - \delta\phi\right)\right) \right\}, \tag{25}$$

where *B* and  $\delta\phi$  share exactly the same definition as ballistic surface waves, with a slightly different definition of  $F(\omega)$  and  $f(\omega)$ ,

395 
$$F(\omega) = \frac{1}{2\pi^2} \sqrt{\frac{2\pi}{k\Delta}}$$

396 
$$f(\omega) = \omega t - k\Delta + \frac{\pi}{4}.$$
 (26)

397 Despite that difference in  $F(\omega)$  and  $f(\omega)$ , surface waves from noise interferometry share the 398 identical formula for the finite-frequency phase shift with surface waves from earthquakes and 399 active sources,

400 
$$\delta\phi \approx \frac{\omega_c^2 k''(\omega_c)\Delta}{4\alpha}.$$
 (27)

401 3.5 Finite-frequency phase shift in two-station methods

The two-station method is commonly used to measure phase velocities when the initial phase of the source is unknown (e.g., Brilliant & Ewing, 1954; T. Meier et al., 2004; Kolínský et al., 2019). It avoids the initial phase by measuring the travel time difference between two stations that are in line with the source. The difference can be captured by cross-correlating the surface waves on the two stations, whose spectrum has the following form,

407 
$$C(\omega) = \exp\left(-i\frac{\omega\Delta}{c(\omega)}\right).$$
 (28)

The narrowband surface waves can be obtained following the same procedure as in the ballistic and noise cross-correlation cases,

410 
$$C(t) \approx \frac{1}{\pi} \Re \int_0^\infty \exp(i\omega t - ik\Delta) \exp\left(-\alpha \frac{(\omega_0 - \omega_c)^2}{\omega_c^2}\right) d\omega \approx \frac{B}{\pi} \omega_c \sqrt{\frac{\pi}{\alpha}} \Re \left\{ \exp\left(i(\omega t - k\Delta - \delta\phi)\right) \right\}.$$
(29)

411 Again, the finite-frequency phase shift is,

412 
$$\delta\phi \approx \frac{\omega_c^2 k''(\omega_c)\Delta}{4\alpha}.$$
 (30)

### 413 **4** Numerical computation of the finite-frequency phase shift

To evaluate the finite-frequency phase shift accurately without the far-field and narrow-band assumptions, we now compute it numerically. The results can be used to correct the errors in phasevelocity measurements caused by this specific phase shift.

We compute the phase shift by comparing the measured phase travel times, obtained from surface-wave synthetics, to their far-field prediction, given by  $t_0 = \Delta/c(f_c) - 1/(8f_c)$ . The computation only needs a phase dispersion curve, c = c(f). As for the "measured" phase travel time, we first generate a synthetic surface wave by superposing monochromatic surface waves. Here, we use the exact expression of the causal branch of monochromatic noise cross-correlation functions,

423 
$$\sum_{i=0}^{N-1} w_i \Re\left[\left(H_0^{(2)}\left(\frac{\omega_i \Delta}{c(f_i)}\right)\right) \exp(i\omega_i t)\right] \mathrm{d}f, \qquad f_i = f_0 + i\mathrm{d}f, \qquad (31)$$

where  $H_0^{(2)}(x)$  is the zeroth-order Hankel functions of the second kind,  $\omega_i = 2\pi f_i$ , and  $w_i$  is the 424 weighting coefficient determined by the integration method used. The results apply to ballistic 425 surface waves as well. For two-station methods, one should replace the Hankel functions by cosine 426 functions, but they share the same far-field patterns. We use the trapezoidal integration, with  $w_i =$ 427 0.5 when i = 0, N-1 and  $w_i = 1$  when i = 1, ..., N-2. Next, we measure the phase travel time using 428 the method of Xu et al. (2021), who used a frequency-dependent  $\alpha = 2\pi f \gamma^2$ , with  $\gamma$  being an 429 empirical parameter (Soomro et al., 2016). Finally, we compute the difference  $\delta t$  between the 430 measured and predicted phase travel times and multiply it by  $2\pi f_i$  to get the finite-frequency phase 431 shift  $\delta \phi$ . The process should be repeated for each distance. For dense arrays, we can accelerate the 432 433 computation by interpolating a phase shift table pre-computed at a set of distance. The phase

velocity measurement method should be the same as the one used to obtain the real measurementsso as to avoid introducing errors due to the difference in the measurement methods.

In order to correct the finite-frequency phase shift in a real phase-velocity dataset, we need a phase dispersion curve. A good start is the average dispersion curve or a reference model inverted from the dataset. We recommend the reference-model approach as the dispersion curve it generates is free of unphysical bumps. Once the phase shift  $\delta\phi$  is computed, one can correct the phase velocity by

441 
$$\frac{1}{c} = \frac{1}{\tilde{c}} - \frac{\delta\phi}{\omega\Delta}$$
(32)

442 where  $\tilde{c}$  and c is the phase velocity before and after the correction.

Figure 5 illustrates the computation of the finite-frequency phase shift for a station pair 443 separated by 250 km. We used a phase dispersion curve calculated using ak135 to generate the 444 broadband surface-wave synthetic (Herrmann, 2013; Figure 5a). We integrated from 2 to 50 mHz 445 with an interval of 0.01 mHz. The phase travel time is measured on the narrow-band-passed 446 waveforms. The resulting phase shift is mostly positive (phase delay; Figures 5b,e), except for low 447 frequencies (Figures 5c,e). We found that this low-frequency anomaly is related to the near-field 448 phase shift, which we discuss further in Section 5.1. The phase shift causes noticeable 449 perturbations in the corresponding "measured" phase velocity curve (up to 0.02 km/s; Figures 450 451 5f,g).



Figure 5 Numerical computation of the finite-frequency phase shift. (a) Broadband synthetic and narrow-453 band filtered synthetics. We use  $\gamma = 16$  to determine the width of the Gaussian filters, the same as Soomro 454 455 et al. (2016) used for station pairs with similar distance ranges. Red and black diamonds denote the measured and predicted phase travel time, respectively. (b) Zoom-in around the measured phase travel time 456 of the filtered synthetic around 0.04 Hz. (c) Same as b, but for 0.01 Hz. (d) Phase travel time residual, the 457 458 difference between the measured (red) and predicted (black) phase travel time. (e) Corresponding phase 459 residual. (f) Corresponding phase velocity residual. (g) Measured and predicted phase velocity dispersion 460 curve.

### 4.1 High-frequency example (1-25 Hz)

We now compute the phase shift in a high-frequency scenario, relevant for the surface wave imaging of the shallow crust. We use this to demonstrate how to use the numerical method and to illustrate the factors that control the finite-frequency phase shift.

We use a model of the Dublin Basin, simplified from one obtained previously using receiver 465 functions (Licciardi & Piana Agostinetti, 2017). The model has 4 layers and a half space below 466 them (Figure 6a; Table 2). The P-wave velocity and density are converted from the S velocity 467 using the formulas in Brocher (2005). After computing the Rayleigh-wave phase-velocity 468 dispersion curve, we evaluate the phase shift for interstation distances from 0.5 to 4 km, at a 0.1 469 km step (Figure 6b). For each distance, we compute the synthetics using equation 31 and a 470 471 frequency range of 0.1-30 Hz, with an interval of 0.01 Hz (Figure 6c). We select 51 frequency points logarithmically distributed between 0.1 and 30 Hz as the center frequencies of the Gaussian 472 filters. Figure 6d shows an example of the finite-frequency phase shift measured for the Gaussian 473 filter with a center frequency of 5 Hz, which is 0.142 radians. 474

We use  $\gamma = 1$  to compute the finite-frequency phase shift over the distance range of 0.5-4 km 475 and the frequency range of 1-25 Hz (Figure 7; A slightly smaller  $\gamma = 0.5$  is used, for clarity, in 476 Figure 6c). The amplitude of the phase shift ranges from -0.015 to  $0.026 \pi$ , much smaller than the 477  $\pi/4$  phase shift caused by the source. The prominent features are the two high-amplitude anomalies 478 around 5 and 1.4 Hz. These are the frequencies of the two peaks in the second derivative of the 479 wavenumber,  $k''(\omega)$ , which confirms the effect predicted by the equation 27. The effect of the 480 distance is clear as well. The amplitudes of the two anomalies decrease with decreasing distance, 481 from 0.026  $\pi$  at 4 km to 0.0019  $\pi$  at 0.6 km. Additionally, the phase shift increases linearly with 482

frequency due to a combined effect of  $\omega^2$  and the frequency-dependent  $\alpha$ . It makes the 5-Hz anomaly stronger than the 1.4-Hz anomaly despite a smaller  $k''(\omega)$  at 5 Hz.

The corresponding phase-velocity perturbation (-0.79% to 2.3%) shows a pattern from that 485 for the phase shift (Figure 8). Firstly, the sign of the phase-velocity perturbation is opposite to the 486 phase shift. That is because a positive phase shift causes a delay in travel time, translating to a 487 lower phase velocity. Secondly, the change of amplitude with distance disappears and the change 488 489 with frequency is proportional to  $k''(\omega)$ . The reason is that the effects of distance and frequency cancel out when the phase shift is converted to phase velocity (equation 3). Therefore, the 490 amplitude variation in the phase shift table only depends on  $k''(\omega)$ . The frequency dependence is 491 cancelled when  $\alpha$  changes linearly with frequency. Using a constant  $\alpha$ , instead, results the velocity 492 perturbation depends linearly on frequency. The positive anomaly observed in the lower-right 493 corner of Figure 8 corresponds to low frequency and short distance or, equivalently, the near field 494 (small  $\Delta/\lambda$ ). The distinctive feature is a result of the near-field effects rather than the finite-495 frequency phase shift, as we discuss further in Section 5.1. 496

The finite-frequency phase shift is larger if a smaller  $\gamma$  is used, when the width of filter widens to include more frequencies (Figure 9). The phase shifts range from  $-\pi/128$  to  $7\pi/128$  for  $\gamma = 0.5$ , with a group of filters centered at 0.05, 0.1, 0.2 and 0.5 s. The phase shifts decrease when  $\gamma$ increases and converge to a small (non-zero) value determined by the near-field effects. However, using a large  $\gamma$  in real-data applications may reduce the signal-to-noise ratio in the filtered surface waves, hence increasing errors in phase velocity measurements. Therefore, the problem of the finite-frequency phase shift cannot be solved by simply adopting a large  $\gamma$ .

504

505 **Table 2**. Velocity model of the Dublin Basin simplified after Licciardi & Piana Agostinetti (2017).

Layer No.	Layer thickness (km)	Vp (km/s)	Vs (km/s)	Density (g/cm <sup>3</sup> )
1	0.15	4.17	2.44	2.42
2	0.5	4.85	2.88	2.51
3	1.35	5.49	3.25	2.62
4	8.0	5.96	3.5	2.71
5	$\infty$	6.34	3.7	2.79



Figure 6. Example of the evaluation of the finite-frequency phase shift using a simplified model of the Dublin Basin. (a) The velocity model (only the top 5 km portion of the shear-wave velocity model is shown); (b) Rayleigh wave phase velocity dispersion curve. The red dot denotes the frequency (5 Hz) used in panel d; (c) Broadband synthetic of the noise cross-correlation function at the interstation distance of 2.5 km; (d) Filtered waveform. The Gaussian filter is centered at 5 Hz, with  $\gamma = 0.5$ , or  $\alpha = 7.85$ . The finitefrequency phase shift is 0.142 radians. We used a smaller  $\gamma$  for a clearer illustration of the phase shift.



514

Figure 7. Phase shift (bottom) and the second derivative of  $k(\omega)$  (top). (Top) The red shaded region marks the positive  $k''(\omega)$ ; (Bottom) The positive phase shift indicates phase delay; the negative phase shift—phase advance.



Figure 8. Phase velocity perturbation corresponding to the phase shift in Figure 7. The perturbation is with
respect to the phase velocity dispersion curve that is used to generate the synthetics.



Figure 9. Phase shift as a function of *γ*. We compute the example using an interstation distance of 2.5 km
and Gaussian filtered centered at 2 Hz, 5 Hz, 10 Hz and 20 Hz.

### 524 4.2 Long-period example

521

The phase shift can be observed in long-period measurements as well. In this example, we use the phase velocity dispersion curve computed for the global reference model ak135. The phase shifts computed here illustrate the errors that can be incurred in long-period measurements performed with time-domain methods, which are widely used for crustal and lithospheric imaging. We also discuss a technique—ridge jumping—that can improve the quality of measurements, especially at shorter periods.

We evaluated the finite-frequency phase shift within the distance range of 100-3000 km (every 100 km) and the period range of 25-100 s. The broadband synthetic was computed by integrating over 2-50 mHz with an interval of 0.01 mHz, and the width of the Gaussian filters was set to  $\gamma =$ 16 (Soomro et al., 2016). We adopted the ridge jumping technique (Bonadio et al., 2018; T. Meier et al., 2004; Soomro et al., 2016; Xu et al., 2021), selecting high-amplitude ridges when scanning from low to high frequency, rather than staying on one ridge for the entire frequency band (Figure

537 10a). For the stability of the results, we only jump to the adjacent ridges and do so only when their 538 amplitude is 1.5 times higher than that of the current ridge (Xu et al., 2021). The ridge jumping 539 may produce discontinuities in the observed phase shift (Figure 10b), but it can reduce the phase 540 shift at higher frequencies (> 0.03 Hz).

The phase shift for the model ak135 ranges from  $-\pi/44$  to  $\pi/16$ , if we use multiple ridges (Figure 10d). This is ~18 times smaller than the values obtained when using the single, 0th ridge  $(-3\pi/2 \text{ to } \pi/40; \text{ Figure 10c})$ . The corresponding velocity perturbation is up to 0.2% at interstation or source-station distances above 300 km (Figure 11). Below 300 km, the near-field effect becomes dominant and increases the perturbation to 0.9%.



**Figure 10**. Phase shift in the measurements made on synthetic traces computed for ak135. (a) Frequencytime representation of the synthetic surface wave at 1750 km. Red and green solid lines denote the phase travel time measured using single ridge and multiple ridges, respectively. The green dashed line marks the ridge picked by the ridge jumping method. (b) Phase shift computed using the single-ridge and multipleridge phase travel time at the distance of 1750 km. (c) Phase shift computed using single ridges at the distance range of 100-3000 km. (d) Same as c, but using the ridge jumping method.



553

**Figure 11**. Phase velocity perturbations corresponding to the phase shifts shown in Figure 10.

### 555 **5 Discussion**

Using the calculations above, we found that the finite-frequency phase shift is relatively small in the range of distance, frequency and  $\gamma$  that are commonly used in the surface wave studies. It can be large, however, at (1) long distance, (2) high frequencies, (3) with relatively wide-band filters or (4) rapid changes with frequency in the group velocity curve. In terms of phase velocity perturbations, their dependences on the distance and frequency cancel out, so that only the bandwidth of the filters and the rate of group-velocity change—or, equivalently,  $k''(\omega)$ —have a significant effect. We can tune the bandwidth of the filters, but  $k''(\omega)$  is determined by the Earth's structure.

We also observed another type of phase shift, in addition to the finite-frequency phase shift. This phase shift dominates in the near field and is discussed below. We also discuss whether the finite-frequency phase shift exists in the frequency-domain method.

567 5.1 The near-field phase shift

The phase shift computed using the Dublin Basin model is negative at 1 Hz around the distance of 0.5 km, in contrast to the positive phase shift at the same frequency but longer distances  $(\Delta > 1 \text{ km})$ . Furthermore, it is seemingly inconsistent with the positive  $k''(\omega)$  at 1 Hz. The inconsistency is caused by a different type of phase shift, which we refer to as the near-field phase shift. The near-field phase shift arises from the far-field approximation, assumed when Bessel functions are replaced by cosine functions to represent monochromatic surface waves.

The phase shift computed by the numerical method described in Section 4 is the phase difference between the monochromatic cosine functions and narrowband Bessel functions. It comprises both the finite-frequency phase shift caused by the difference between monochromatic Bessel functions and narrowband Bessel functions and the near-field phase shift caused by the difference between monochromatic cosine functions and monochromatic Bessel functions.

We separated the two types of phase shift in Figure 12. In the isolated finite-frequency phase shift, the negative anomaly no longer exists in the near-field corner, which is more consistent with the prediction by equation 27 (Figure 12b). By contrast, the near-field phase shift is consistently negative and only visible in the near field (Figure 12c), which can be predicted by

583 
$$\delta\phi_{near} = -\arg H_0^{(2)} \left(\frac{\omega\Delta}{c}\right) - \left(\frac{\omega\Delta}{c} - \frac{\pi}{4}\right) \tag{33}$$

584 The phase of  $H_0^{(2)}\left(\frac{\omega\Delta}{c}\right)$  should be unwrapped to obtain a continuous phase, which approaches -585  $\omega\Delta/c + \pi/4$  at high frequencies, decreasing  $\delta\phi_{near}$  to zero.



586

Figure 12. The origins of the finite-frequency and near-field phase shifts. The frames show the phase differences (a) between narrow-band Bessel functions and monochromatic cosine functions; (b) between narrow-band and monochromatic Bessel functions; (c) between monochromatic Bessel functions and monochromatic cosine functions. The phase of monochromatic cosine functions is  $\omega/\Delta - \pi/4$ . The phase of narrow-band ones is measured using synthetics.

592 5.2 Time-domain method vs frequency-domain method

The finite-frequency phase shift only applies to measurement methods that use narrow-band waveforms to measure the phase travel time in the time domain. Frequency-domain methods (e.g., phase unwrapping method; T. Meier et al., 2004) do not have such phase shift. The difference between the two methods is that the phase unwrapping method measures the phase of the spectrum at the center frequency, so that its results are monochromatic measurements, instead of narrowband measurements. The measured phase is then unwrapped, converted to the phase travel time,and compared to the predicted phase travel time as in the time domain method.

Figure 13 shows a comparison of the phase shift associated with the time domain method and the phase unwrapping method. We can see that the phase shift associated with the frequency domain method is at constant values for different  $\gamma$ . These constant values are not zero, which reflects the near-field phase shift.

The frequency-domain method is an attractive alternative to time-domain ones as it is free of the finite-frequency phase shift. The time-domain methods, however, remain very popular due to their simplicity. We note that the near-field phase shift is present regardless of the approach chosen.



Figure 13. Phase shift as a function of  $\gamma$  for (a) the time-domain method and (b) the frequency-domain method.

### 611 6 Conclusions

The finite-frequency phase shift arises in the phase velocity measurements obtained using the 612 time-domain methods due to the approximation of the monochromatic surface waves by narrow-613 band surface waves. It applies to both ambient noise studies and those using ballistic surface waves 614 from earthquakes or active sources. The phase shift biases the measured phase travel time and, 615 hence, the measured phase velocity. The finite-frequency phase shift can be up to  $\pi/4$  when using 616 a very broadband filter and down to nearly zero when using a very narrowband filter. The exact 617 amount depends on four factors: (1) the second derivative of the wavenumber k with respect to  $\omega$ ; 618 (2) the width of the filter; (3) the distance; (4) the center frequency of the Gaussian filter. For 619 620 common settings in surface wave studies, the phase shift is about  $\pi/60-\pi/16$ , much smaller than the polar phase shift (phase advance of  $\pi/2$ ) and source phase shift, identified previously (phase 621 delay of  $\pi/4$ ). 622

The finite-frequency phase shift can cause non-negligible phase-velocity perturbations of around 0.2% in long-period (25-100 s) studies and around 0.8% in high-frequency (1-25 Hz) studies. The exact amount can vary depending on the filter parameters and local Earth structure. If the acceptable level of errors in the phase velocity measurements is comparable to or lower than the finite-frequency phase shift, the shift should be corrected.

The finite-frequency phase shift, and its corresponding perturbation in phase velocities, can be corrected once having an estimation of the phase shift. A dispersion curve, computed from the 1-D velocity model inverted from an average dispersion curve or from the entire dataset of dispersion curves, can be used to compute a good estimation of the phase shift. It can be done by comparing the measured phase travel time in surface wave synthetics generated by the dispersion curve to the far-field prediction of the phase travel time. The approach can also correct the near field phase shift when using Bessel functions instead of cosine functions in generating synthetics.

Because the finite-frequency phase shift results from the monochromatic approximation, it does not exist in the frequency-domain methods that do not rely on the approximation. In this sense, switching to frequency-domain methods is an alternative approach for increasing the accuracy of phase-velocity measurements.

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