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Sam Greenwood¹, Christopher J. Davies¹, and Anne Pommier²

 1 University of Leeds 2 UC San Diego

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Influence of thermal stratification on the structure and 1 evolution of the Martian core. 2

Sam Greenwood¹, Christopher J. Davies¹, Anne Pommier^{2,3}

¹School of Earth and Environment, University of Leeds, Leeds, UK
²Scripps Institution of Oceanography, University of California San Diego, La Jolla, CA, USA
³Earth and Planets Laboratory, Carnegie Institution for Science, Washington, DC, USA

Key Points:

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| 8 | • | Present day core temperature profile is conductive rather than the frequently as- |
|----|---|---|
| 9 | | sumed isentropic state. |
| 10 | • | End of internal magnetic field on Mars places limits on the thermal conductivity |
| 11 | | of the core. |
| 12 | • | Estimates of the mantle temperature are a useful additional constraint, limiting |
| 13 | | the range of mantle viscosities in successful solutions. |

 $Corresponding \ author: \ Sam \ Greenwood, \ {\tt s.greenwood@leeds.ac.uk}$

14 Abstract

The apparent end of the internally generated Martian magnetic field at 3.6-4.1 Ga 15 has been linked to insufficient core cooling. While the dynamo cessation time is a key 16 event in the Martian history, a large range of solutions exist to satisfy this observation, 17 limiting the insight it provides on the Martian interior. We produce a suite of models 18 improving our understanding of the evolution of Mars in three keys areas. Firstly, we 19 account for thermal stratification in the core, producing improved estimates on the core 20 thermal structure. Secondly, we match estimates for the present-day areotherm. Finally, 21 we consider recent experimental data for the core thermal conductivity, k_c , much lower 22 than previously thought for Mars. In order to yield a consistent dynamo cessation time 23 we require $k_{\rm c} \ge 18 \text{ W m}^{-1} \text{K}^{-1}$. Furthermore, the majority of our models indicate the 24 core is fully conductive at present and too hot to form any solid. 25

²⁶ 1 Introduction

Unlike Earth, Mars does not possess an internally generated global magnetic field. 27 However, analysis of vector magnetic measurements from the MGS and MAVEN satel-28 lites reveals remnant magnetisation characteristic of magnetisation formed in the pres-29 ence of a much stronger magnetic field than exists today (Acuna et al., 1998; Langlais 30 et al., 2019). The remnant magnetisation appears in crustal rocks older than an estimated 31 3.6-4.1 Ga (Acuna et al., 1998; Langlais et al., 2012; Milbury et al., 2012; Mittelholz et 32 al., 2020), leading to the common theory that an early dynamo on Mars generated a large 33 34 scale field prior to these age estimates (Stevenson, 2001). The dynamo process is produced by fluid convection of iron-alloy in the core, where thermal buoyancy is created 35 by the mantle conducting heat away from the core and potentially chemical buoyancy 36 provided by freezing liquid (Nimmo & Stevenson, 2000; Stevenson, 2001; Williams & Nimmo, 37 2004; Davies & Pommier, 2018). The magnetic history of Mars is therefore intimately 38 linked to the evolution of the planet as it cools over geological time. 39

Analysing the thermal and magnetic evolution of the Martian core requires two di-40 mensional (radius and time) parameterised thermal history models to simulate the long 41 timescales (Myrs-Gyrs) associated with the slow loss of heat from the planet. A key quan-42 tity is the heat extracted from the core by the mantle at the Core-Mantle Boundary (CMB), 43 $Q_{\rm c}$, relative to the heat flow down an isentropic temperature gradient resulting from con-44 vection, $Q_{\rm a}$. In the absence of freezing, a dynamo fails very close to the transition from 45 a super-isentropic heat flow $(Q_{\rm c} > Q_{\rm a})$ to a sub-isentropic heat flow $(Q_{\rm c} < Q_{\rm a})$ (Nimmo, 46 2015). As such, the thermal evolution of both the core and mantle must be solved to es-47 timate $Q_{\rm c}$ as a function of time, which in turn allows analysis of the magnetic history 48 of Mars. 49

A variety of solutions for the evolution of Mars have been proposed, exhibiting a 50 range of physical processes. Nimmo and Stevenson (2000) suggested that a brief period 51 of plate tectonics before a transition to stagnant lid tectonics was required to cool the 52 planet to power a dynamo prior to ~ 4 Ga. Due to a lack of evidence for plate tecton-53 ics on Mars, Williams and Nimmo (2004) instead showed that an initially super-heated 54 core relative to the mantle provides the required short period of rapid cooling to power 55 the dynamo. Growth of a large inner core would have likely restarted the dynamo (Williams 56 & Nimmo, 2004) but recent growth of a small inner core might not yet be able to pro-57 vide enough compositional buoyancy and could restart the dynamo in the future (Hemingway 58 & Driscoll, 2021). Depending upon the relative slopes of the core temperature and its 59 melting temperature, the core may instead start to freeze from the top-down rather than 60 bottom-up (Stewart et al., 2007). In this freezing regime, iron freezes as a snow at the 61 top of the core, sinking deeper into the core and remelting, releasing additional power 62 for a dynamo. The amount of power is relatively small compared to a growing inner core 63 and so a snow zone could be present today without restarting the dynamo (Davies & Pom-64 mier, 2018). All previous studies generally agree that the Martian core is required to have 65 undergone a short period of rapid cooling, powering the dynamo, before the cooling rate 66 of the planet becomes too low to sustain the dynamo after $\sim 3.6 - 4.1$ Ga. 67

There are three main issues that may alter our view of the Martian evolution. Firstly, 68 $Q_{\rm a}$ is proportional to the thermal conductivity of the core, $k_{\rm c}$. The magnetic history of 69 Mars is therefore very sensitive to $k_{\rm c}$, given the above condition on $Q_{\rm c}$ relative to $Q_{\rm a}$ for 70 dynamo action. Recent experimental studies on a variety of iron-alloys at conditions ap-71 propriate for Mars have yielded values for k_c from as low as 5 W m⁻¹K⁻¹ to around 30 72 W m⁻¹K⁻¹, depending on the precise composition (Pommier, 2018; Pommier et al., 2020). 73 These conductivities are lower than those used in previous models of Mars, which have 74 typically used 40 W m⁻¹K⁻¹ (Nimmo & Stevenson, 2000; Williams & Nimmo, 2004; Davies 75 & Pommier, 2018), whereas Hemingway and Driscoll (2021) consider a range of $k_{\rm c}$ = 76 $30-120 \text{ W m}^{-1} \text{ K}^{-1}$. A significantly lower k_c alters the ability for the core generate 77

78 a magnetic field (Pommier et al., 2020) and therefore can change our understanding of 79 the evolution of the planet.

Secondly, all previous models predict that the Martian core was heavily sub-isentropic 80 $(Q_{\rm c} < Q_{\rm a})$ for a significant proportion of its history, including at present. When sub-81 isentropic, the thermal state of the core deviates away from a convective state towards 82 a conductive one, resulting in a stable, thermally stratified layer that grows from the top 83 of the core downwards (Labrosse et al., 1997; Nimmo, 2015; Greenwood et al., 2021), as-84 suming chemical convection is not present or insufficient to mix the layer away. Previ-85 ous models for Mars have assumed that even when $Q_{\rm c} < Q_{\rm a}$, the core remains convect-86 ing, limiting predictions for the present day temperature of the core. The change in core 87 temperature from thermal stratification also alters the timing for freezing of solid as well 88 as influencing the evolution of $Q_{\rm c}$. By accounting for thermal stratification we can more 89 precisely estimate the present day core temperature, complimenting other modelling tech-90 niques (e.g. Rivoldini et al., 2011; Plesa et al., 2018; Khan et al., 2018) and observations 91 from missions such as InSight to understand the interior structure of Mars that are not 92 as sensitive to the core temperature. Thirdly, improved geophysical inversions for the 93 present day areotherm (Khan et al., 2018) offer an additional constraint upon evolution 94 models not previously utilised. In this paper we produce a suite of thermal history mod-95 els addressing each of these 3 areas. 96

97 2 Methods

We solve for the thermal evolution of Mars by coupling parameterised convection 98 models for the core and mantle. The core is assumed to be well mixed with an adiabatic 99 temperature profile. When $Q_{\rm c}$ becomes smaller than the heat conducted along the adi-100 abatic profile, a stratified layer grows beneath the CMB with a conductive temperature 101 profile. We used a common approach for the Martian mantle with an isothermal con-102 vecting interior bounded by thermal boundary layers above the CMB and beneath a stag-103 nant lid (Williams & Nimmo, 2004; Thiriet et al., 2019). Linear temperature profiles are 104 assumed in the thermal boundary layers and across the stagnant lid. 105

For the core, we use the model of Greenwood et al. (2021), which accounts for a stable layer in a standard energy balance to evolve the core temperature. An entropy balance is then used to estimate the ohmic dissipation produced by magnetic field generation, $E_{\rm J}$ (Gubbins et al., 2003; Williams & Nimmo, 2004; Greenwood et al., 2021):

$$E_{\rm J} = E_{\rm s} - E_{\rm k},\tag{1}$$

where $E_{\rm k}$, $E_{\rm s}$, and $E_{\rm J}$ refer to the changes in entropy arising from thermal conduction, 110 secular cooling, and ohmic dissipation within the core. Since $E_{\rm k} \propto k_{\rm c}$, a smaller $k_{\rm c}$ gives 111 a smaller $E_{\rm k}$ and hence a larger $E_{\rm J}$. Dynamo action is inferred when $E_{\rm J}$ becomes larger 112 than 1 MW K^{-1} which occurs close to, but not precisely, the condition $Q_c > Q_a$. Whilst 113 our model for the core can account for solidification of either a solid core or iron snow 114 (Davies & Pommier, 2018; Greenwood et al., 2021), we do not find scenarios where any 115 core fluid freezes and so do not include their associated terms in Equations 1. See sup-116 plementary text S1 for further details on the entropy budget. 117

The mantle is modelled using the parameterisation of stagnant lid convection of Thiriet et al. (2019). Temperature dependent mantle viscosity in the upper/lower thermal boundary layers are evaluated at the average temperatures within the relevant boundary layer given an Arrhenius equation, scaled by a reference viscosity η_0 at a reference temperature of 1600 K

$$\eta(T) = \eta_0 \exp\left(\frac{A}{R} \left[\frac{1}{T} - \frac{1}{1600}\right]\right),\tag{2}$$

where A is the activation energy, taken to be 300 kJmol⁻¹ assuming diffusion creep (Karato 123 & Wu, 1993), and R is the gas constant. The temperature of the upper mantle beneath 124 the stagnant lid, $T_{m,u}$, is scaled from the isothermal convecting mantle temperature as 125 $T_{\rm m,u} = T_{\rm m} - aRT_{\rm m}^2/A$, where a is a fixed constant. We take a = 2.54 with a correspond-126 ing β factor of 0.335 used for scaling the boundary layer thickness which are the best fit-127 ting values of Thiriet et al. (2019). In general, a larger η_0 or lower $T_{\rm m}$ thickens the ther-128 mal boundary layers, reducing $Q_{\rm c}$ for a given temperature difference between mantle and 129 core. The thickness of the stagnant lid was fixed to 300 km rather than being time de-130 pendent since we find this has no significant effect upon the evolution of Mars (Supple-131 mentary figure S1). Models are iterated from 4.5 Ga until present day from their initial 132 conditions. 133

Roughly 8 wt% nickel is expected in the Martian core (Wänke & Dreibus, 1994), 134 along with 10-20 wt% sulphur (Rivoldini et al., 2011; Khan et al., 2018) and as such we 135 assumed an Fe-Ni-S core. We used the melting data of Gilfoy and Li (2020), who observed 136 the melting point of Fe-Ni-S at ~ 1500 K with 10 wt% S at CMB pressure. This low 137 melting temperature suggests that the entire core is liquid at present and, as mentioned 138 above, we find no scenarios where any solid is formed. One consequence of no solid in 139 our calculations is that the composition of the liquid core is constant in time and the amount 140 of Ni/S only influence the material properties of the core. 141

A number of parameters for Mars are known well enough to be taken as constant 142 in our study, listed in table S1. For example, the radius and density of the core have been 143 constrained to 1730-1840 km and 6100-6500 kg m⁻³ (Khan et al., 2018). Changing these 144 parameters within their uncertainties does not appreciably alter the evolution of the planet 145 relative to some key unknowns, in particular the initial conditions. To address param-146 eters with large uncertainties, we perform Monte-Carlo simulations in order to search 147 the parameter space. We vary the initial temperature of the mantle and core, described 148 by $T_{\rm m,0}$ and the initial super-heat of the core relative to the mantle, $\Delta T = T_{\rm c} - T_{\rm m,0}$, 149 where $T_{\rm c}$ is the CMB temperature. There is little constraint upon the initial core and 150 mantle temperature and due to the thermostat effect, there is limited sensitivity of the 151 initial conditions on the present day state (Plesa et al., 2015). The initial conditions do 152 impact the early evolution of the planet and so are important when considering the longevity 153 of the dynamo. We therefore consider a wide range for $T_{\rm m,0}$ and ΔT . We also vary the 154 reference viscosity of the mantle, η_0 , which has a wide range of proposed values and sig-155 nificantly influences the cooling of the planet. Finally, we are interested in a range of core 156 thermal conductivities, k_c . We choose the range 5-40 W m⁻¹K⁻¹ based on the results 157 of (Pommier, 2018; Pommier et al., 2020; Pommier, 2020) representing a range of core 158 compositions. As mentioned, our core composition is constant in time in our models since 159 we have no formation of solid to unevenly partition alloying light elements. The effect 160 of composition is therefore limited to the impact upon the material properties of the core, 161 of which $k_{\rm c}$ is most significantly influenced. The density and specific heat capacity are 162 also composition dependent, however, they have an insignificant impact upon the ther-163 mal evolution relative to $k_{\rm c}$. 164

We ran a large number of models (n=100,000), drawing a random value from a uniform prior for each of the 4 variables between the ranges given in table 1. All other fixed parameters are listed in table S1.

Successful models satisfy two constraints. Firstly, the dynamo cessation time, de-168 noted t_{Φ} , must be consistent with the magnetic field history of Mars, where the dynamo 169 shut off between 4.1-3.6 Ga (400-900 Myr after core formation) (Acuna et al., 1998; Langlais 170 171 et al., 2012; Milbury et al., 2012; Mittelholz et al., 2020). Secondly, we choose models from our ensemble that are consistent with estimates of the present day temperature of 172 Mars, using the recent estimates of the areotherm from Khan et al. (2018) based on in-173 versions from geophysical data. Their model is not particularly sensitive to the CMB tem-174 perature since they cannot resolve the temperature change in the lower mantle thermal 175

| Table 1. \ | /ariables | for | the | parameter | search |
|------------|-----------|-----|-----|-----------|--------|
|------------|-----------|-----|-----|-----------|--------|

| Parameter | Symbol | Value | Units | Reference |
|---|---|---|---|--|
| Core thermal conductivity Core super heat Initial Mantle temperature Reference viscosity | $ \begin{array}{c} k_{\rm c} \\ \Delta T \\ T_{\rm m,0} \\ \eta_0 \end{array} $ | $5-40 \\ 0-500 \\ 1400-2200 \\ 10^{18} - 10^{21}$ | W m ⁻¹ K ⁻¹ K K Pa s | Pommier et al. (2020) - Breuer and Spohn (2006); Fraeman and Korenaga (2010) |

¹⁷⁶ boundary layer, and so instead we focus on the temperature at the base of the stagnant ¹⁷⁷ lid. We identify models with $T_{m,u} = 1650 - 1750$ K as successful in this regard.

178 **3 Results**



Figure 1. Time series for the 3 example cases described in the text. Panel a) shows the CMB heat flow, Q_c , (solid lines) and the heat flow down the adiabatic temperature gradient at the CMB, Q_a . Panel b) shows the entropy due to ohmic dissipation, E_J . Finally, c) shows the growth of the thermally stratified layer by plotting the radius of the base of the layer, r_s , normalised to the core radius, r_c . The reference case is an example of a successful model, yet the low k_c and high η_0 cases are both unsuccessful.

¹⁷⁹ We first show the time series of three example cases to demonstrate the impact of ¹⁸⁰ varying thermal conductivity and mantle viscosity on the evolution of the planet (Fig. ¹⁸¹ 1) as these will be important for interpreting the trends seen in the Monte-Carlo results. ¹⁸² The reference case is a successful model taken from the Monte-Carlo simulation ($T_{\rm m} =$ ¹⁸³ 2327 K, $\Delta T = 192$ K, $k_c = 24$ W m⁻¹K⁻¹, $\eta_0 = 2.5 \times 10^{20}$ Pa s), whereas the other ¹⁸⁴ two cases are unsuccessful. A low conductivity case uses the same input parameters as ¹⁸⁵ the reference case, with the exception that k_c is lowered to 5 W m⁻¹K⁻¹, the lowest value ¹⁸⁶ we consider. Finally a high viscosity case uses the same input parameters as the refer-¹⁸⁷ ence case except that η_0 is raised to 10^{21} Pa s, the largest value we consider.

In all cases there is an initially super-isentropic heat flow that drops rapidly, be-188 fore becoming more steady for the majority of time (Fig. 1a). Comparing the reference 189 case to the low conductivity case shows the identical evolution of Q_c until ~ 500 Myr. 190 After this time, the reference case becomes sub-isentropic $(Q_{\rm c} < Q_{\rm a})$ and a stable layer 191 begins to grow causing the evolution between them to diverge. The introduction of the 192 stable layer in the reference case relatively elevates the core temperature, leading to a 193 larger temperature difference between the core and mantle, driving a larger heat flow at 194 the CMB. A stable layer never grows in the low conductivity case due to the extremely 195 low values for $Q_{\rm a}$. Whilst the stable layer elevates the core temperature, the resulting 196 increase in Q_c increases core cooling to offset this initial increase in temperature. Mod-197 els that grow a stable layer are generally ~ 30 K hotter at present than if a stable layer 198 were not accounted for. This difference in temperature is small relative to uncertainties 199 in geophysical estimations of the interior temperature but at the low cooling rates of the 200 core still represents ~ 250 Myr worth of core cooling. 201

Comparing next the high viscosity case to the reference case, as expected, Q_c is de-202 creased since the more viscous mantle produces thicker thermal boundary layers, through 203 which less heat is conducted. $Q_{\rm c}$ drops off more rapidly, although $Q_{\rm c}$ is comparable to 204 the reference case at the present day (Fig. 1a). Figure 1c shows the growth of the sta-205 ble layer through time. The lower heat flows in the high viscosity case result in the sta-206 ble layer growing sooner and faster than the reference case. The whole core is stratified 207 in both the reference and high viscosity cases by the present day. When the stable layer 208 is thin, the expected growth rate is $\propto \sqrt{\text{time}}$, however, as the heat flow continues to drop 209 and the layer grows there is an acceleration in the growth rate when only a small pro-210 portion of the core is still convecting $(r_s/r_c < 0.4)$. This acceleration is due to the fact 211 that as the convecting region becomes smaller, its mass decreases $\propto r^3$, whereas the heat 212 extracted from it is $\propto r^2$. This results in rapid cooling of the convecting region relative 213 to the stable layer and subsequent rapid movement of $r_{\rm s}$. 214

The effects of η_0 and k_c on E_J can be seen in Figure 1b. The low conductivity case 215 predicts a dynamo operating at all times due to the low entropy associated with ther-216 mal conduction, $E_{\rm k}$, and is therefore inconsistent with observations. The reference and 217 high viscosity case both drop quickly early on, falling below 1 MW K^{-1} (dashed line), 218 our assumed limit for dynamo action, coinciding with the growth of the stable layer. Note 219 that in our entropy budget $E_{\rm J}$ does not fall below 0, as is physically expected, since ac-220 counting for the correct temperature profile when sub-isentropic ensures entropy is bal-221 anced (see supplementary text S1 for more details). 222

The left panel of Figure 2 shows the correlation between the dynamo cessation time, 223 t_{Φ} , with the present day upper mantle temperature $T_{m,u}$ for the whole ensemble of mod-224 els. Many models fit either the constraint upon $T_{m,u}$ (n=26,180) or t_{Φ} (n=9040) but only 225 2010 models fall within the limits for both. No correlation between $T_{m,u}$ and t_{Φ} exists 226 as t_{Φ} is primarily sensitive to heat flows rather than temperatures. The colour scale shows 227 that there is also no correlation between models that fit the dynamo constraint ($t_{\Phi} =$ 228 400-900 Myr) and the mantle viscosity. There is however a strong correlation between 229 $T_{m,u}$ and η_0 where higher viscosities limit the heat release through the upper mantle ther-230 231 mal boundary layer, insulating the planet and producing a hotter present day mantle by approximately $T_{\rm m,u} \propto \log(\eta_0)$. As such, the present day areotherm offers a comple-232 mentary constraint to the dynamo cessation time since it limits the reference viscosity 233 in our models to $\eta_0 \sim 10^{20} - 10^{21}$ Pa s. 234



Figure 2. Monte-Carlo simulation results. Left panel shows cessation time, t_{Φ} , plotted against present day upper mantle temperature, $T_{m,u}$. White lines indicate the limits from observational constraints and the colour scale indicates the value of $\log(\eta_0)$. On both panels, successful models are indicated by the larger opaque circles. Right panel shows t_{Φ} against core conductivity, with the same limits on t_{Φ} as the left panel. Models where the dynamo is active at present have no cessation time and so do not appear on the figure. Colour scale indicates the proportion of the core that is convecting at present, given by the ratio of radii of the base of the stable layer, r_s , and the CMB, r_c (0 = fully conductive core, 1 = fully convecting core). Downwards arrow indicates how t_{Φ} varies with η_0 if all other input parameters are fixed.

The right panel of Figure 2 shows how all 2010 successful models are limited to the 235 upper half of core conductivities we have considered. At $k_{\rm c} < 20 \ {\rm W} \ {\rm m}^{-1} {\rm K}^{-1}$, there are 236 two branches between models that have dynamo that fails too early or lives too long. The 237 upper branch can be explained by the long term decaying trend in Q_c and the approx-238 imately constant value of $Q_{\rm a}$, as can be seen in the reference example case in Figure 1a. 239 Since t_{Φ} occurs when $Q_{\rm c} \sim Q_{\rm a}$, as k_c (and hence $Q_{\rm a}$) is decreased, dynamo failure is 240 delayed. At the lower branch where the dynamo is short lived, models have the highest 241 viscosities (high η_0 and low $T_{m,0}$) and/or low initial superheats ΔT . These conditions 242 lead to low CMB heat flows that quickly become sub-isentropic and hence an early t_{Φ} . 243 The absence of models inbetween the branches arises from the behaviour of Q_c at higher 244 mantle viscosities, as seen in the high viscosity case in Figure 1a. At low k_c , a sufficiently 245 large viscosity is needed to produce $Q_{\rm c} < Q_{\rm a}$. However, this results in the mantle heat-246 ing up early in the evolution since heat cannot be efficiently moved out the top of the 247 mantle to counter the radiogenic heating. This heating in turn reduces the viscosity, al-248 lowing Q_c to increase over time before falling again at a later time (see high viscosity 249 case in Fig.1a). The inflexion in $Q_{\rm c}$ ensures that t_{Φ} is either very late on, or very early 250 after the initial drop in Q_c since this plateau lasts for ~ 1 Gyr. For $k_c > 20$ W m⁻¹K⁻¹, 251 $Q_{\rm a}$ is sufficiently large that lower viscosities not exhibiting this inflexion in $Q_{\rm c}$ are suf-252 ficient to provide the desired range of t_{Φ} . 253

The colour-scale on the right panel of Figure 2 indicates the proportion of the core 254 that is convecting at present day. We find all successful models with $k_{\rm c} > 24 \ {\rm W} \ {\rm m}^{-1} {\rm K}^{-1}$ 255 are fully stratified, with successful models with a lower $k_{\rm c}$ having a stable layer compris-256 ing at least the top half of the core. Typically models that are fully stratified at present, 257 have been fully stratified for 100's Myr, cooling purely by conduction. In all of our mod-258 els the core is far hotter than the melting point observed by Gilfoy and Li (2020), with 259 the successful models giving $T_{\rm c} = 1940 - 2080$ K. Our temperatures are also above the 260 melting point given by Stewart et al. (2007) and those used by Rivoldini et al. (2011); 261 Hemingway and Driscoll (2021) for sulphur concentrations consistent with interior mod-262 els, > 10 wt% (Rivoldini et al., 2011; Khan et al., 2018). 263

For the mantle thermal conductivity, we have used the recent experiments on iron 264 rich olivine predicted for the Martian mantle (Zhang et al., 2019) (Table S1) although 265 this differs from the typical value of 4 W $m^{-1}K^{-1}$ used in thermal evolution models (e.g. 266 Williams & Nimmo, 2004; Breuer & Spohn, 2003; Thiriet et al., 2019). We ran our Monte-267 Carlo simulations with the mantle thermal conductivity set to 4 W $m^{-1}K^{-1}$ to inves-268 tigate the impact. The same behaviour was observed with regards to where successful 269 models are located in the parameter space. The successful model with the lowest k_c was 270 12.5 W m⁻¹K⁻¹, as opposed to 17.5 W m⁻¹K⁻¹ seen in Figure 2b. Since the study of 271 Zhang et al. (2019) account for the higher iron content of Martian mantle as well as the 272 extended olivine phase due to lower gravity than Earth, we focus on the results that are 273 based on their estimates. 274

Figure 3 demonstrates the general impact of varying any one of the four variables in Table 1 upon t_{Φ} and $T_{m,u}$ relative to the reference case in Figure 1. The present day temperature of the mantle is almost exclusively controlled by η_0 which also exerts some control on the dynamo cessation time. The other inputs, $T_{m,u}$, k_c , and ΔT , instead almost solely influence the cessation time, with the largest influence on t_{Φ} coming from k_c .

Finally, successful models all predict a heat flow conducted through the stagnant lid of around 15 mW m², although this is a consequence of the thermal evolution being insensitive to the size of the stagnant lid and a constrained temperature at the base of the lid. If we had imposed a different stagnant lid size, the predicted heat flow would change accordingly, as we have assumed a linear temperature gradient across it.



Figure 3. Influence of the 4 varied inputs $(T_{m,0}, \Delta T, k_c, \eta_0) t_{\Phi}$ and $T_{m,u}$. Shaded regions indicate constraints upon t_{Φ} and $T_{m,u}$. The star marks the reference case shown in Figure 1. Arrows and circular data points show the influence of the variable (indicated by colour) if only that variable is changed from the reference case. For example, the bottom right point marked 10^{21} , shows the results using all inputs the same as the reference case, except that η_0 is changed to 10^{21} Pa s.

²⁸⁶ 4 Discussion and Conclusions

Our results suggest that a value of $k_c \geq 18 \text{ W m}^{-1} \text{ K}^{-1}$ is required for the dy-287 namo to stop between 400 and 900 Myrs after core formation. Studies of pure iron have 288 suggested k_c upwards of 80 W m⁻¹ K⁻¹ (Deng et al., 2013; Pommier, 2018; Ezenwa & 289 Yoshino, 2021), with alloying light elements reducing k_c (Pommier, 2020) and so our lower 290 limit of 18 W m^{-1} K⁻¹ can be related to the light elements in the core. Using electri-291 cal measurements, Pommier (2018) obtained a value of $k_c \approx 40 \text{ W m}^{-1} \text{ K}^{-1}$ for Fe with 292 5 wt% S (Fe-5S). Due to the large amount of FeO in the Martian mantle (Wänke & Dreibus, 293 1994), significant amounts of oxygen may have dissolved into the core (Tsuno et al., 2007) 294 and an additional 0.5 wt% oxygen to Fe-5S drastically reduces k_c to ≈ 18 W m⁻¹ K⁻¹ 295 at 2000 K (Pommier et al., 2020). Furthermore, nickel in the core, whilst weakly impact-296 ing many properties of iron such as density, can significantly reduce $k_{\rm c}$ as well as the melt-297 ing temperature (Gilfoy & Li, 2020). Pommier (2020) observed 10 wt% Ni alloyed with 298 Fe-5S also halves k_c to ≈ 20 W m⁻¹ K⁻¹ compared to just Fe-5S. Although the exper-299 iments discussed in this section were conducted at 8-10 GPa, lower than the 20-40 GPa 300 in the Martian core, k_c reduces by approximately 10% when extrapolated to 20-40 GPa 301 (Pommier et al., 2020). Since > 15 wt% of sulphur is predicted based on density esti-302 mates in the Martian core (Rivoldini et al., 2011; Khan et al., 2018), a lower k_c than 18 303 W m⁻¹ K⁻¹ may be expected, highlighting the need to further explore k_c as a function 304 of composition and pressure to interpret the magnetic history of Mars. 305

Inference of the dynamo cessation time from our evolution models is dependent upon 306 the scenario for cooling of the planet, where we have assumed stagnant lid convection 307 in the mantle. Early plate tectonics has been proposed based upon observations of ge-308 ological structures in the northern lowlands (Sleep, 1994) and magnetic anomalies in the 309 southern highlands (Connerney et al., 1999) that were hypothesised to indicate ancient 310 sea floor spreading. Plate tectonics would allow the mantle to cool more rapidly, increas-311 ing the heat flow from the core (Nimmo & Stevenson, 2000). Little evidence of plate tec-312 tonics has been subsequently discovered and any significant period of plate tectonics ap-313 pears incompatible with the present day crustal thickness (Breuer & Spohn, 2003). Given 314 available information, assuming the stagnant lid regime for all time seems reasonable. 315

An alternative scenario proposes that a series of large impacts on Mars heated the 316 mantle (Roberts et al., 2009) and thermally stratified the top of the core (Arkani-Hamed 317 & Olson, 2010; Roberts & Arkani-Hamed, 2014) which could have triggered an already 318 sub-critical dynamo to quickly fail (Kuang et al., 2008). The core may take 10's Myr to 319 1 Gyr (Arkani-Hamed & Olson, 2010; Roberts & Arkani-Hamed, 2014) for convection 320 to re-establish in the entire core, hence $Q_{\rm c}$ may be super-isentropic for up to 1 Gyr whilst 321 still being compatible with the inferred cessation time for Mars. Taking the most gen-322 erous estimate that impacts could have inhibited a super-isentropic heat flow from pro-323 ducing a dynamo for 1 Gyr would change our interpretation by essentially shifting the 324 results in Figure 2 down on the y-axis by 1 Gyr. Due to the rapid increase in t_{Φ} with 325 decreasing k_c , the right panel of Figure 2 would instead give a lower bound on success-326 ful models of $\sim 15 \text{ W m}^{-1} \text{ K}^{-1}$, rather than 18 W m⁻¹ K⁻¹. We therefore expect gi-327 ant impacts to not significantly alter our results, assuming the evolution of the mantle 328 on the Gyr timescale is also not significantly altered. 329

In writing equation 2 we have included only a temperature dependence on the viscosity. Water content of olivine crystals can significantly impact η (Mackwell et al., 1985), particularly in the Fe rich Martian mantle (Kohlstedt & Mackwell, 2010), which to some extent is captured by our consideration of a wide range for η_0 . What we fail to account for is any time dependence on the viscosity except through the temperature, yet in the absence of sufficient evidence of changing water content in the mantle we cannot include this effect at this stage.

All of our successful models contain a thermally stratified layer at least comprising the top half of the core, with the majority producing a fully conductive core. Inversions for the Martian interior typically assume the core is isentropic (e.g. Khan et al., 2018) but we suggest this constraint should be relaxed by studies in the future. Our estimates on the CMB temperature based on successful models $(2010 \pm 70 \text{ K})$ may also help in this regard.

In summary, we have conducted a suite of models for the thermal evolution of Mars 343 including thermal stratification in the core and considering a range of core thermal con-344 ductivities based on recent experimental data. We demonstrated that in order to match 345 estimates of the termination of the Martian dynamo, the thermal conductivity is lim-346 ited to $k_{\rm c} < 18 \text{ W m}^{-1} \text{K}^{-1}$. This limit will aid future constraints upon the composi-347 tion of the core since light elements core strongly influence k_c . We find at least the up-348 per 50% of the core to be thermally stratified, with the majority of models predicting 349 the entire core to be conductive with a CMB temperature of 2010 ± 70 K. Finally, we 350 utilised recent temperature constraints of the present day mantle as an additional con-351 straint which limits the range of successful solutions since it constrained the viscosity 352 of the mantle to $\eta_0 = 10^{20} - 10^{21}$ Pa s in our modelling framework. 353

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Supporting Information for "Influence of thermal stratification on the structure and evolution of the Martian core."

Sam Greenwood¹, Christopher J. Davies¹, Anne Pommier^{2,3}

 $^1\mathrm{School}$ of Earth and Environment, University of Leeds, Leeds, UK

²Scripps Institution of Oceanography, University of California San Diego, La Jolla, CA, USA

³Earth and Planets Laboratory, Carnegie Institution for Science, Washington, DC, USA

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Text S1.

The entropy budget is used to estimate the ohmic dissipation, $E_{\rm J}$, produced by magnetic field generation (Gubbins et al., 2003; Williams & Nimmo, 2004; Greenwood et al., 2021):

$$\overbrace{\int k_{\rm c} \left(\frac{\nabla T}{T}\right)^2 \mathrm{d}V_{\rm c}}^{E_{\rm k}} + \overbrace{\int \frac{\Phi}{T} \mathrm{d}V_{\rm c}}^{E_{\rm J}} = \overbrace{-\int \left(\frac{1}{T_{\rm c}} - \frac{1}{T}\right) \rho_c C_{p,c} \frac{\partial T}{\partial t} \mathrm{d}V_{\rm c}}^{E_{\rm s}},\tag{1}$$

Corresponding author: S. Greenwood (s.greenwood@leeds.ac.uk

where T is temperature and T_c is the temperature at the CMB. Terms are integrated over the volume of the entire core, V_c , with the temperature and cooling rate defined by a conduction solution in the stable layer ($r_s \leq r \leq r_c$) or by the isentropic value in the convecting region ($0 \leq r \leq r_s$). Φ is the heat released by ohmic dissipation.

The entropy gain in the core from ohmic dissipation must be > 0; the process is a dissipative one and so can only act to increase entropy. Assuming the entire core is convecting at all times can lead to an inconsistency producing negative values for $E_{\rm J}$ (Pozzo et al., 2012). We note that when including a thermally stable layer with a conduction profile rather than an isentropic profile when $Q_{\rm c} < Q_{\rm a}$, ensures $E_{\rm J} \ge 0$ as is physically expected (as seen in the main document).

Typically, the condition $E_{\rm J} > 0$ is used to infer dynamo action (Williams & Nimmo, 2004, e.g.) but we cannot use this since we do not obtain $E_{\rm J} \leq 0$. Physically, dynamo action would not necessarily be expected at some small value of $E_{\rm J}$ since a dynamo requires sufficiently established, self-sustaining feedback between the magnetohydrodynamic processes. Such an established process would produce a certain minimum of ohmic dissipation that for the Earth has been estimated to be on the order of 1 MW K⁻¹ (Jackson et al., 2011). Therefore, we take $E_{\rm J} > 1$ MW K⁻¹ as our requirement for an active dynamo. The precise value of this lower bound does not significantly change t_{Φ} since the variations of $E_{\rm J}$ brought about by the secular cooling of the core are generally much larger than this value.

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Figure S1. Recreation of results from Figure 2 of Thiriet et al. (2019) showing the CMB heat flow through time. All parameters are the same, as well as using the same core model (simple secular cooling of an isothermal core), as Thiriet et al. (2019), with the only difference being that we assumed a fixed stagnant lid of 300 km, rather than implementing their time dependent calculation. Our solution does not appreciably change when using a lid thickness between 200-400 km.

 Table S1. Table S1 lists all fixed parameters using for all models produced in our Monte-Carlo simulation.



Figure S2. Models fitting our temperature constraint (red) and models that fit both the temperature and magnetic history constraints (red) with combinations of the 4 variables: $T_{m,0}$, ΔT , k_c , and η_0 . Axis labels indicate the variable on the axis in that row/column.

| Table 51. Tixed input parameter | | mouel runs. | | |
|-----------------------------------|----------------|----------------------|---|-------------------------|
| Parameter | Symbol | Value | Units | Reference |
| Core radius | r_c | 1750 | km | Khan et al. (2018) |
| Core density | $ ho_c$ | 6100 | $\rm kgm^{-3}$ | Khan et al. (2018) |
| Core thermal expansivity | $\alpha_{T,c}$ | 10^{-5} | K^{-1} | - |
| Core heat capacity | $C_{p,c}$ | 1089 | $\rm Jkg^{-1}K^{-1}$ | Gilfoy and Li (2020) |
| Radius of Mars | r_m | 3400 | km | - |
| Stagnant lid thickness | $D_{\rm sl}$ | 300 | km | Khan et al. (2018) |
| Mantle density | $ ho_m$ | 3550 | $\rm kgm^{-3}$ | Khan et al. (2018) |
| Upper mantle thermal conductivity | $k_{m,u}$ | 2 | $\mathrm{W}~\mathrm{m}^{-1}\mathrm{K}^{-1}$ | Zhang, Yoshino, |
| | | | | Yoneda, and Osako |
| | | | | (2019) |
| Lower mantle thermal conductivity | $k_{m,l}$ | 5 | $\mathrm{W}~\mathrm{m}^{-1}\mathrm{K}^{-1}$ | Zhang et al. (2019) |
| Mantle thermal expansivity | $\alpha_{T,m}$ | 2.65×10^{-5} | K^{-1} | Zhang et al. (2019) |
| Mantle heat capacity | $C_{p,m}$ | 798 | $\rm Jkg^{-1}K^{-1}$ | Zhang et al. (2019) |
| Activation energy | A | 300 | $\rm kJmol^{-1}$ | - |
| Convection scaling parameters | a, β | 2.54, 0.335 | - | Thiriet et al. (2019) |

 Table S1.
 Fixed input parameters for all model runs.