

Linking Intra-Plate Volcanism to Lithospheric Structure and Asthenospheric Flow

Thomas Duvernay¹, D. Rhodri Davies¹, Christopher Robert Mathews¹, Angus H. Gibson¹, and Stephan C Kramer²

¹Australian National University

²Imperial College London

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Abstract

Several of Earth's intra-plate volcanic provinces are hard to reconcile with the mantle plume hypothesis. Instead, they exhibit characteristics that are more compatible with shallower processes that involve the interplay between uppermost mantle flow and the base of Earth's heterogeneous lithosphere. The mechanisms most commonly invoked are edge-driven convection (EDC) and shear-driven upwelling (SDU), both of which act to focus upwelling flow and the associated decompression melting adjacent to steps in lithospheric thickness. In this study, we undertake a systematic numerical investigation, in both 2-D and 3-D, to quantify the sensitivity of EDC, SDU, and the associated melting to key controlling parameters. Our simulations demonstrate that the spatio-temporal characteristics of EDC are sensitive to the geometry and material properties of the lithospheric step, in addition to the magnitude and depth-dependence of upper mantle viscosity. These simulations also indicate that asthenospheric shear can either enhance or reduce upwelling velocities and the associated melting, depending upon the magnitude and orientation of flow relative to the lithospheric step. When combined, such sensitivities explain why step changes in lithospheric thickness, which are common along cratonic edges and passive margins, only produce volcanism at isolated points in space and time. Our predicted trends of melt production suggest that, in the absence of potential interactions with mantle plumes, EDC and SDU are viable mechanisms only for Earth's shorter-lived, lower-volume intra-plate volcanic provinces.

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Thomas Duvernay¹, D. Rhodri Davies¹, Christopher R. Mathews¹, Angus H. Gibson¹, Stephan C. Kramer²

¹Research School of Earth Sciences, The Australian National University, Canberra, ACT, Australia
²Department of Earth Science and Engineering, Imperial College London, London, UK

Key Points:

- Edge-driven convection is sensitive to upper-mantle viscosity and the geometry and material properties of lithospheric steps.
- Asthenospheric flow magnitude and orientation dictate whether edge-driven cells are enhanced through asthenospheric shear or suppressed.
- Melting associated with edge-related processes can account for Earth's shorter-lived and lower-volume intra-plate volcanic provinces.

Corresponding author: Thomas Duvernay, thomas.duvernay@anu.edu.au

Abstract

Several of Earth’s intra-plate volcanic provinces are hard to reconcile with the mantle plume hypothesis. Instead, they exhibit characteristics that are more compatible with shallower processes that involve the interplay between uppermost mantle flow and the base of Earth’s heterogeneous lithosphere. The mechanisms most commonly invoked are edge-driven convection (EDC) and shear-driven upwelling (SDU), both of which act to focus upwelling flow and the associated decompression melting adjacent to steps in lithospheric thickness. In this study, we undertake a systematic numerical investigation, in both 2-D and 3-D, to quantify the sensitivity of EDC, SDU, and the associated melting to key controlling parameters. Our simulations demonstrate that the spatio-temporal characteristics of EDC are sensitive to the geometry and material properties of the lithospheric step, in addition to the magnitude and depth-dependence of upper mantle viscosity. These simulations also indicate that asthenospheric shear can either enhance or reduce upwelling velocities and the associated melting, depending upon the magnitude and orientation of flow relative to the lithospheric step. When combined, such sensitivities explain why step changes in lithospheric thickness, which are common along cratonic edges and passive margins, only produce volcanism at isolated points in space and time. Our predicted trends of melt production suggest that, in the absence of potential interactions with mantle plumes, EDC and SDU are viable mechanisms only for Earth’s shorter-lived, lower-volume intra-plate volcanic provinces.

Plain Language Summary

Intra-plate volcanoes, which occur away from plate boundaries, are common across Earth’s surface (e.g. Hawaii, Reunion, Cameroon, Eastern Australia), but their origin remains debated. The classically invoked hypothesis for their genesis centres around mantle plumes – buoyant columns of hot rock that ascend through Earth’s mantle. Upon reaching the base of tectonic plates, plumes generate extensive melting and remain comparatively fixed, providing a mechanism for generating linear volcanic tracks that grow older in the direction of plate motion. Several intra-plate volcanic regions, however, exhibit characteristics that are inconsistent with the mantle plume hypothesis: their eruptions are usually short-lived, non-age-progressive, and only generate minor volumes of lava. Therefore, they are more likely to be driven by shallower processes, such as small-scale convective instabilities that develop adjacent to step-changes in the thickness of Earth’s lithosphere, its rigid outermost shell. In this study, we utilise both 2-D and 3-D computational models to simulate these shallow processes, and we analyse their sensitivity to a range of key controlling parameters. Our results help to solve the puzzle of why such processes only produce volcanism at isolated locations and, in the absence of interactions with mantle plumes, limit their applicability to Earth’s shorter-lived, lower-volume volcanic provinces.

1 Introduction

Most of Earth’s volcanism is concentrated at tectonic plate boundaries, representing the surface manifestation of either passive decompression melting at mid-ocean ridges (e.g. Sengör & Burke, 1978; Phipps Morgan et al., 1987) or volatile-induced melting at subduction zones (e.g. Tatsumi et al., 1986; Peacock, 1990). However, a significant and widespread class of volcanism occurs within plates or across plate boundaries. These so-called *intra-plate* volcanic provinces cannot be explained through plate tectonic processes and require an alternative generation mechanism. Mantle plumes – hot, buoyant columns that rise from Earth’s core-mantle boundary to its surface (e.g. Morgan, 1971) – are commonly invoked to explain age-progressive volcanic tracks that grow older in the direction of plate motion. At the young end of these tracks, volcanism localises within a radius of a few tens of kilometres and has persisted for tens of millions of years, implying

64 a self-renewing source that lies below the region where the mantle moves with the sur-
 65 face plate (e.g. Richards et al., 1989; Farnetani & Richards, 1995; Courtillot et al., 2003;
 66 Davies & Davies, 2009; French & Romanowicz, 2015). Classic examples include the vol-
 67 canic tracks terminating at Hawaii in the Pacific, Reunion in the Indian Ocean and Cos-
 68 grove in eastern Australia (e.g. Duncan & Richards, 1991; Davies et al., 2015; Jones et
 69 al., 2017; Bredow et al., 2017). However, many intra-plate volcanic provinces are hard
 70 to reconcile with the mantle plume hypothesis, for example the Colorado Plateau in North
 71 America, the Moroccan Atlas Mountains in northern Africa and the Newer Volcanics Province
 72 of southeastern Australia (e.g. Demidjuk et al., 2007; Missenard & Cadoux, 2012; Davies
 73 & Rawlinson, 2014; Klöcking et al., 2018). At these locations, volcanism is often short-
 74 lived (< 20 Myr), non-age-progressive, and of low eruptive volume, all of which point to-
 75 wards alternative generation mechanisms (e.g. King & Ritsema, 2000; Conrad et al., 2011;
 76 Davies & Rawlinson, 2014; Ballmer et al., 2015).

77 Most proposed mechanisms involve the interplay between shallow mantle flow and
 78 the base of Earth’s heterogeneous lithosphere. The two most commonly invoked are (i)
 79 edge-driven convection (EDC) – a small-scale convective instability, associated with a
 80 step in lithospheric thickness, driven by lateral density variations between a thick litho-
 81 sphere and adjacent asthenosphere (e.g. Buck, 1986; King & Anderson, 1998; King &
 82 Ritsema, 2000; Till et al., 2010; Davies & Rawlinson, 2014; Ballmer et al., 2015; Liu &
 83 Chen, 2019); and (ii) shear-driven upwelling (SDU) – defined here as a sub-lithospheric
 84 ascending flow, induced by topography at the base of the lithosphere in the presence of
 85 asthenospheric shear (e.g. Conrad et al., 2010, 2011; Bianco et al., 2011; Davies & Rawl-
 86 inson, 2014; Ballmer et al., 2015). For the latter, we acknowledge that Conrad et al. (2010)
 87 formulated SDU in the context of low-viscosity pockets within the shallow asthenosphere,
 88 but we focus solely on the role of lithospheric topography herein. While both EDC and
 89 SDU have been linked to the generation of intra-plate volcanism, their applicability and
 90 relative importance remain unclear and likely vary from one volcanic province to the next,
 91 owing to regional differences in their primary controlling parameters (e.g. King & Rit-
 92 sema, 2000; Conrad et al., 2011; Davies & Rawlinson, 2014). To complicate matters fur-
 93 ther, EDC and SDU may interact with upwelling mantle plumes and pockets of low-viscosity
 94 asthenosphere to produce intricate volcanic patterns at the surface (e.g. Conrad et al.,
 95 2011; Davies et al., 2015; Kennett & Davies, 2020).

96 To better assess the origin of some of Earth’s intra-plate volcanic provinces and un-
 97 derstand possible interactions between different driving mechanisms, it is necessary to
 98 analyse, in isolation, how EDC, SDU, and their associated melting depend on several plau-
 99 sible controlling parameters. Accordingly, in this study, we use a systematic series of 2-
 100 D and 3-D numerical models to quantify the sensitivity of EDC and SDU to a subset
 101 of these parameters. We focus on the role of (i) the topography of the lithosphere-asthenosphere
 102 boundary (LAB), especially the geometry and orientation of lithospheric steps and their
 103 material properties; (ii) uppermost mantle viscosity, both in terms of its magnitude and
 104 depth-dependence; and (iii) the intensity, depth distribution and orientation of plate mo-
 105 tion and asthenospheric flow. These models allow us to identify the fundamental con-
 106 trols on shallow edge-related processes and highlight, in particular, what determines the
 107 location and intensity of melt production at depth. Our results allow us to place quan-
 108 titative bounds on the conditions under which EDC and SDU can explain intra-plate vol-
 109 canism in the absence of other melt-generating processes.

110 2 Methods

111 2.1 Governing Equations and Solution Strategy

112 We set up a numerical study of thermo-chemical convection applied to Earth’s man-
 113 tle in both 2-D and 3-D Cartesian domains with dimensions 4000:[4000]:1000 km (x:[y]:z).
 114 We use Fluidity – a finite-element, control-volume computational modelling framework

115 (e.g. Davies et al., 2011; Kramer et al., 2012) – to solve the equations governing man-
 116 tle convection for pressure, velocity, temperature and material volume fraction fields, on
 117 anisotropic, adaptive, simplex meshes. Mesh optimisation is controlled by a metric that
 118 depends on the Hessian of the temperature, velocity and material volume fraction fields.
 119 It provides increased resolution in areas of dynamical significance, with coarser resolu-
 120 tion elsewhere, thus ensuring computational efficiency whilst maintaining solution ac-
 121 curacy (e.g. Davies et al., 2007). The resulting mesh satisfies a minimum edge-length
 122 condition of 5 km, a maximum edge-length of 200 km and a 20% edge-length gradation
 123 (i.e. the maximum allowable jump in edge-length from element to element).

124 We simulate incompressible (Boussinesq) Stokes flow in an Eulerian reference frame,
 125 incorporating spatial variations of viscosity. In this context, we solve the following gov-
 126 erning equations:

$$0 = \nabla \cdot \mathbf{u}, \quad (1)$$

$$\mathbf{0} = \nabla p - \nabla \cdot \left[\mu (\nabla \mathbf{u} + (\nabla \mathbf{u})^\top) \right] + \left[\rho_0 \alpha (T - T_S) - \Delta \rho_c \right] \mathbf{g}, \quad (2)$$

$$\mu = \left[A_1 \times \exp \left(- \frac{E^* + \rho_0 g z V_1^*}{RT^*} \right) + A_2 \times \exp \left(- \frac{E^* + \rho_0 g z V_2^*}{RT^*} \right) \right]^{-1}, \quad (3)$$

$$T^* = T + \psi z. \quad (4)$$

127 We model energy conservation through a simple advection-diffusion equation including
 128 a heat source term:

$$\frac{\partial T}{\partial t} + \mathbf{u} \cdot \nabla T = \kappa \Delta T + \phi. \quad (5)$$

129 Distinct materials are initialised and tracked using material volume fraction fields (Wilson,
 130 2009; Garel et al., 2014), described by a linear advection equation:

$$\frac{\partial \Gamma}{\partial t} + \mathbf{u} \cdot \nabla \Gamma = 0. \quad (6)$$

131 In the above equations, \mathbf{u} denotes velocity, p dynamic pressure, μ dynamic viscosity, T
 132 temperature, z depth, ρ density, $\Delta \rho_c$ the density contrast between different materials,
 133 and Γ volume fraction. Other symbol names and values are presented in Tables 1 and
 134 2. Although our models are incompressible, when determining viscosity, we update tem-
 135 perature to account for an adiabatic gradient (Equation 4); a similar update is performed
 136 to determine melt fractions (Section 2.4). Our computational domain includes three dif-
 137 ferent materials: continental crust, continental lithosphere (excluding the crust) and man-
 138 tle (incorporating oceanic lithosphere). Each has a distinct density (Table 1; Artemieva,
 139 2009), but they all obey the same viscosity law, albeit with continental lithosphere that
 140 is intrinsically 100 times more viscous than adjacent mantle (e.g. Lenardic & Moresi, 1999;
 141 Currie & van Wijk, 2016).

142 2.2 2-D Reference Case

143 We begin by simulating idealised 2-D flow around thermally and compositionally-
 144 defined steps in lithospheric thickness, which separate thick continental lithosphere from
 145 thin oceanic lithosphere – this is analogous to a passive margin setting.

146 We consider viscosity, μ , to be isotropic and model it through a diffusion creep rhe-
 147 ology. To describe this mechanical behaviour, we combine two empirical Arrhenius laws
 148 (Hirth & Kohlstedt, 2004; Korenaga & Karato, 2008) inside which we account for both
 149 the temperature increase through the adiabatic gradient, ψ , and the effect of lithostatic
 150 pressure (Equations 3 and 4). We fix a common activation energy, $E^* = 350 \text{ kJ mol}^{-1}$,
 151 for both laws but vary the activation volumes, V_i^* , and viscosity pre-factors, A_i . Setting
 152 distinct V_1^* and V_2^* in Equation 3 allows us to incorporate a low-viscosity channel in the

Table 1. *Model parameters common to all simulations*

Name	Symbol	Value	Units
Reference Density	$\rho_0 \rho_0^{Cont} \rho_0^{Crust}$	3370 3300 2900 ^a	kg m ⁻³
Gravity	g	9.8	m s ⁻²
Gas Constant	R	8.3145	J K ⁻¹ mol ⁻¹
Thermal Expansion	α	3×10^{-5b}	K ⁻¹
Surface Temperature	T_S	290	K
Mantle Temperature	T_M	1650 ^{c,d}	K
Adiabatic Gradient	ψ	4×10^{-4e}	K m ⁻¹
Thermal Diffusion	κ	6×10^{-7f}	m ² s ⁻¹
Internal Heating (Cont. Crust)	ϕ	2.6×10^{-13g}	K s ⁻¹
Internal Heating (Elsewhere)	ϕ	4×10^{-15h}	K s ⁻¹
Activation Energy	E^*	350 ⁱ	kJ mol ⁻¹
Upper Mantle Viscosity at ULMB	μ_{660}	10^{21}	Pa s
Lower Mantle Viscosity	μ_{LM}	2×10^{22}	Pa s
Viscosity Bounds	$\mu_{min} \mu_{max}$	$10^{18} 10^{24}$	Pa s
Water Content (Melting)	X_{H_2O}	300	ppm

Note. Parameters for the rheological law are guided by Korenaga and Karato (2008); additional values used in the upper mantle can be found in Table 2.

^a Artemieva (2009). ^b Ye et al. (2009). ^c Putirka (2016). ^d Sarafian et al. (2017). ^e Katsura et al. (2010).

^f Gibert et al. (2003). ^g $\equiv 1.3 \times 10^{-6}$ W m⁻³ (Jaupart & Mareschal, 2005). ^h $\equiv 2 \times 10^{-8}$ W m⁻³ (Pollack & Chapman, 1977). ⁱ A value of 550 kJ mol⁻¹ is used for the dislocation creep regime (Section 2.3.1).

153 sub-lithospheric mantle (e.g. Richards et al., 2001). Conversely, specifying identical pa-
 154 rameters leads to a single law with a pre-factor twice as large. Either way, to determine
 155 V_i^* and A_i and, thereby, establish our upper mantle viscosity profile, we consider the ther-
 156 mal structure generated by a half-space cooling model (Parsons & Sclater, 1977) of age
 157 40 Myr. Then, we define target values that the profile should satisfy: (i) μ_{660} , the value
 158 at the upper-lower mantle boundary (ULMB), which we set to 10^{21} Pa s (e.g. Mitrovića
 159 & Forte, 2004); and (ii) μ_{min}^0 , the profile’s minimum value in the sub-lithospheric man-
 160 tle (e.g. Iaffaldano & Lambeck, 2014). Using these constraints, we iteratively determine
 161 the values of A_i and V_i^* (Table 2). To complete our profile, we fix the lower-mantle vis-
 162 cosity, μ_{LM} , to 2×10^{22} Pa s, resulting in a factor of 20 increase through the ULMB. Fi-
 163 nally, we restrict viscosity values between $\mu_{min} = 10^{18}$ Pa s and $\mu_{max} = 10^{24}$ Pa s. The
 164 resulting reference profile (representative of our initial oceanic domain), alongside the
 165 other profiles examined (Section 2.3.1), are illustrated in Figure 1a. All profiles are com-
 166 patible with estimates derived from models of global isostatic adjustment (e.g. Paulson
 167 & Richards, 2009).

168 For our reference model, we impose no-slip velocity boundary conditions at the bot-
 169 tom of the domain and free-slip boundary conditions elsewhere. Temperature is set to
 170 $T_S = 290$ K at the surface and $T_M = 1650$ K at the base, with insulating sidewalls –
 171 $\frac{\partial T}{\partial n} = 0$. Initial temperature conditions incorporate a sub-lithospheric mantle of tem-
 172 perature T_M and differentiate between oceanic and continental realms (Figure 1c). Oceanic
 173 lithosphere is treated as a surface thermal boundary layer, where the temperature dis-
 174 tribution follows a half-space cooling model of age 40 Myr; the 1620 K isotherm, which
 175 we use to identify the LAB, is located at a depth of 90 km. Thicker continental litho-
 176 sphere, including a 41 km-thick crust, extends down to 200 km depth and is described
 177 by a conductive geotherm (e.g. Pollack & Chapman, 1977), which we determine by solv-
 178 ing a 1-D steady-state heat equation. We use a value of 3 W m⁻¹ K⁻¹ for the thermal
 179 conductivity (Schatz & Simmons, 1972) and account for internal heat generation through
 180 an exponential decrease of characteristic length-scale 9 km (e.g. Lachenbruch, 1970). We

181 set the surface crustal heat production to $6 \times 10^{-6} \text{ W m}^{-3}$ (McLaren et al., 2003), which
 182 is compatible with the internal heating, ϕ , defined in Equation 5 as it yields a compa-
 183 rable heat flux upon spatial integration (Nicolaysen et al., 1981; Jaupart & Mareschal,
 184 2005). Oceanic and continental segments are connected via two 200 km-wide thermo-chemical
 185 steps located between 1150 km and 1350 km to the left, and 2650 km and 2850 km to the
 186 right of the continent; the material boundary is halfway through both steps. Within these
 187 steps, the depth of a given isotherm follows an error function of the horizontal coordi-
 188 nate, x . Such a definition ensures a smooth, diffusive transition between the continen-
 189 tal area and adjacent lithosphere (Figure 1c), and it leads to instabilities that develop
 190 as they would naturally do in this type of system.

2.3 Parameter Space

2.3.1 2-D Cases

193 To assess possible expressions of flow adjacent to lithospheric steps, we first con-
 194 duct a systematic study around our reference case, exploring the effect of varying val-

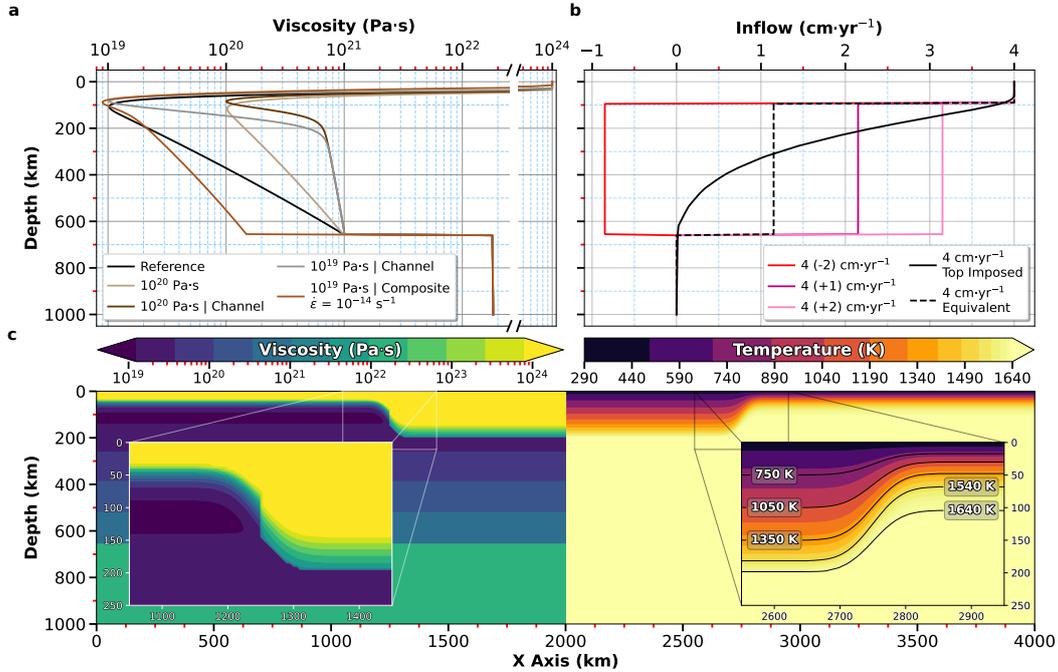


Figure 1. 2-D model setup: (a) Viscosity profiles considered in the 2-D parameter space study, calculated according to the temperature distribution of the reference 40 Myr old oceanic lithosphere. These profiles are for representation purposes only: our models include strong lateral viscosity contrasts. (b) Velocity profile within the oceanic realm resulting from a purely plate-driven model (solid black line) and its simplified counterpart (dashed black line), which is used as a basis for inflow boundary conditions (Section 2.3.1). Remaining profiles incorporate additional asthenospheric shear (number between parentheses), either aligned with (+ sign) or opposite to (- sign) the direction of plate motion. (c) Initial distribution of viscosity (left) and temperature (right) inside the 2-D domain. The viscosity inset illustrates the separation between continent and ocean through the $\times 100$ continental viscosity increase, while the temperature inset highlights the smooth paths taken by isotherms at the step.

Table 2. *Model Parameters Varied Across 2-D Simulations*

Geometry				
Name (Abbreviation)		Values		Units
Oceanic Lithosphere Age (Oce.)		20 and 40		Myr
Continent Depth (Cont.)		140 and 200		km
Step Width (Step)		200 and 400		km
Step Material Proportion (Step)		Equal and $\frac{2}{3}$ Oce.		–
Viscosity ^a				
Profile ^b	Minimum viscosity μ_{min}^0 (Pa s)	Channel	Activation volume V_1^*, V_2^* ($\text{m}^3 \text{mol}^{-1}$) ^c	Pre-factor A_1, A_2 (Pa s) ^c
	10^{19}	No	6.8×10^{-6}	1.9×10^{-8}
	10^{19}	Yes	$25 \times 10^{-6}, 3 \times 10^{-6}$	$2.1 \times 10^{-6}, 2.1 \times 10^{-10}$
	10^{20}	No	4.7×10^{-6}	1.1×10^{-9}
	10^{20}	Yes	$25 \times 10^{-6}, 3 \times 10^{-6}$	$2 \times 10^{-7}, 2.1 \times 10^{-10}$
Plate Motion				
Name		Values		Units
Plate Speed		0 , 2, 4 and 6		cm yr^{-1}
Additional Shear		–2, 0 , 1 and 2		cm yr^{-1}

Note. Reference case values are in bold.

^a Diffusion creep regime only; refer to Section 2.3.1 for the composite regime.

^b Refer to Figure 1a for visualisation of the profiles.

^c In the absence of a channel, activation volumes and pre-factors are identical in both laws (Equation 3).

195 uses for potential key controlling parameters (Table 2). We vary four geometric param-
 196 eters: the initial age of oceanic lithosphere (i.e. the thickness of the lithospheric lid), the
 197 depth of the continent (i.e. the extent of the continental guide), the width of the litho-
 198 spheric step (effectively changing its slope), and the location of the material interface
 199 between continent and ocean within the step (modifying the density distribution within
 200 the step). We also examine cases with five distinct viscosity configurations (Figure 1a):
 201 four account for diffusion creep only, as described in Section 2.2, and differ in their value
 202 of μ_{min}^0 and the inclusion or exclusion of a sub-lithospheric viscosity channel (Table 2),
 203 while the remaining case accounts for deformation through a composite diffusion and dis-
 204 location creep rheology, calculated via a harmonic mean:

$$\mu = 2 \times \left(\frac{1}{\mu_{diff}} + \frac{1}{\mu_{disl}} \right)^{-1}. \quad (7)$$

205 The diffusion creep component, μ_{diff} , is identical to the reference case (Equation 3), while
 206 the dislocation creep component, μ_{disl} , introduces a (non-linear) dependence on the sec-
 207 ond invariant of the strain-rate tensor, $\dot{\epsilon}_{II}$, according to

$$\mu_{disl} = \left[A \times \dot{\epsilon}_{II}^{\frac{n-1}{n}} \times \exp\left(- \frac{E^* + \rho_0 g z V^*}{nRT^*} \right) \right]^{-1}. \quad (8)$$

208 For dislocation creep, we increase the activation energy to 550 kJ mol^{-1} , the activation
 209 volume to $12 \times 10^{-6} \text{ m}^3 \text{ mol}^{-1}$ and set the values of A and n to $2.2 \times 10^{-4} \text{ Pa s}$ and 3.6
 210 respectively, guided by Korenaga and Karato (2008).

211 In addition, we investigate the effect of plate motion and asthenospheric shear through
 212 kinematic boundary conditions. We first consider purely plate-driven cases by impos-

ing horizontal motion of 2, 4 and 6 cm yr⁻¹ at the surface and opening both side boundaries (whilst imposing a lithostatic pressure condition); the flow generated is akin to a classical Couette profile. We subsequently explore the effect of asthenospheric shear whilst keeping plate motion imposed. To do so, we consider the horizontal velocity profile generated within the oceanic realm in the 4 cm yr⁻¹ plate-driven case (solid black line, Figure 1b) and generate an equivalent, albeit simplified, profile. We impose a constant velocity, equal to the plate speed, from the surface down to the LAB at 90 km depth, and we close side-boundaries in the lower mantle. For the upper mantle, we integrate the plate-driven velocity profile between depths of 90 km and 660 km, and average the result over that depth range. Using the obtained value (≈ 1.15 cm yr⁻¹) as an asthenospheric inflow boundary condition (dashed black line, Figure 1b), we replicate the dynamical behaviour produced by the plate-driven case (Figures S1 and S2), demonstrating that results are largely insensitive to the depth-dependence of the inflow profile prescribed within the asthenosphere – the flow is redistributed in line with the underlying physics. Subsequently, to provide additional shear either in the direction of plate motion, or opposite to it, we increase, or decrease, the constant asthenospheric flow by 2 cm yr⁻¹. Additionally, to illustrate the balance between the plate-driven flow and asthenospheric shear, we include a case with a smaller 1 cm yr⁻¹ increase (Figure 1b). For completeness, we also consider an end-member case that incorporates shear only by using our increased asthenospheric flow scenario and setting the coefficient of thermal expansion to zero, which prevents the development of edge-driven instabilities. For all cases incorporating plate motion, we prescribe the temperature at the inflow boundary using the initial thermal structure of oceanic lithosphere. We also increase the domain size from 4000 km to 6000 km to prevent any interaction between the continental block and sidewalls of the domain.

2.3.2 3-D Cases

We extend our analyses to 3-D to quantify the sensitivity of EDC and SDU to more complex continental geometries and a broader spectrum of plate motion and asthenospheric flow directions, relative to the continent. Other model parameters remain identical to our reference 2-D case.

We examine four continental geometries for which the shape of the continent is based on a 200 km-thick cuboid located between $x, y = 1250$ km and $x, y = 2750$ km (Figure 2). Similar to our 2-D models, lithospheric steps connect continent to ocean along continental boundaries, including the four ‘corners’. Each case differs in the following way: (i) *Case U400* incorporates a 400 km-wide oceanic indent inside the continent, between $x = 2350$ km, $y = 1800$ km and $x = 2750$ km, $y = 2200$ km, with additional steps at inner edges and corners; (ii) *Case U600* is similar to Case U400, albeit with a wider indent of 600 km, located between $x = 2150$ km, $y = 1700$ km and $x = 2750$ km, $y = 2300$ km; (iii) *Case U400-Grad* builds on Case U400 but differs by the presence of a linear gradient in the y -direction, from $z = 130$ km to $z = 230$ km depth, to represent the continental LAB; (iv) *Case Complex* does not incorporate an indent but, instead, combines a similar gradient as Case U400-Grad (same direction, different amplitude) with sinusoidal variations and local anomalies to define the continental LAB. In particular, the smaller-scale variations in LAB topography included in Case Complex allow us to investigate the flow regime and melt patterns in a more realistic scenario that better approximates the nature of the LAB inferred through seismic techniques and probabilistic inversion of combined geophysical datasets (e.g. Afonso et al., 2016; Rawlinson et al., 2017).

To explore the effects of background asthenospheric flow, we select Case U400 as our basis and impose both plate motion and asthenospheric inflow in four different directions: positive x at $x = 0$ km, negative x at $x = 6000$ km, positive y at $y = 0$ km and both positive x and y (which we will refer to as oblique) at $x, y = 0$ km. We follow the same strategy to produce the velocity inflow profile as for our 2-D cases but only consider 4 cm yr⁻¹ plate motion with a 2 cm yr⁻¹ increase of the constant asthenospheric in-

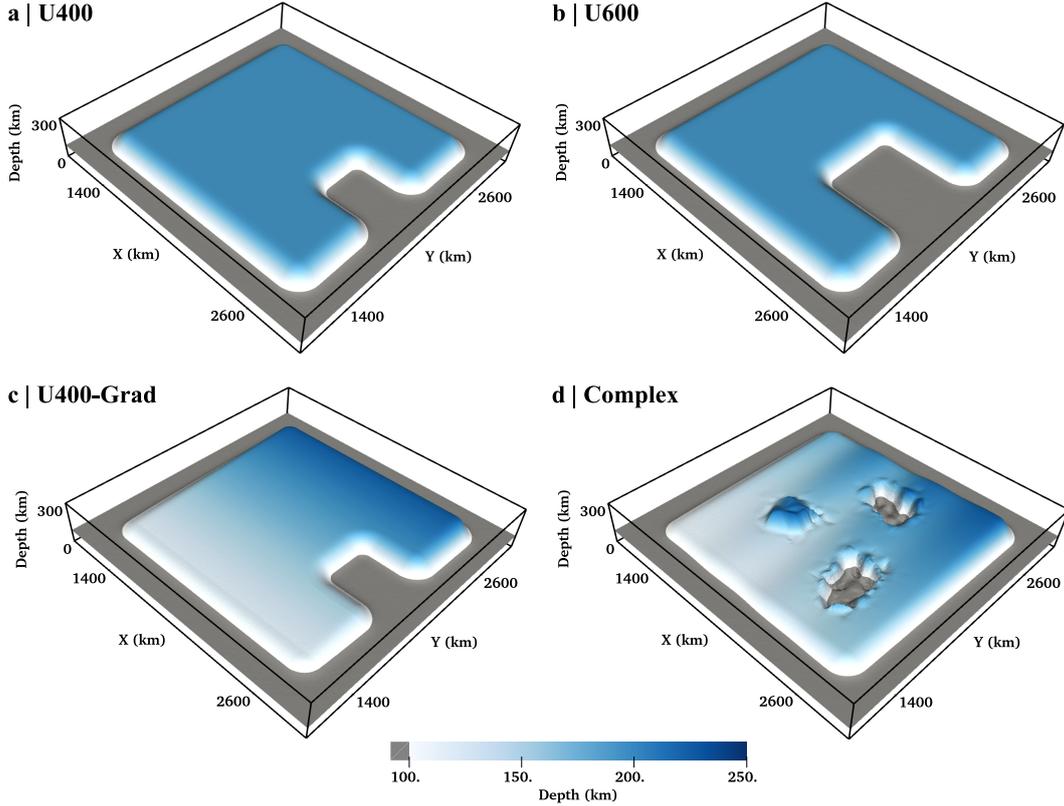


Figure 2. Initial topography of the LAB, as delineated by the 1620 K isotherm, for continental geometries used in our 3-D simulations. On each panel, the view is from below, looking at the base of the continent. (a) Case U400. (b) Case U600. (c) Case U400-Grad. (d) Case Complex.

265 flow (Section 2.3.1). In the oblique case, we also apply the inflow profile at the outflow
 266 boundaries to ensure flow remains oblique inside the domain.

267 2.4 Model Diagnostics

268 2.4.1 Edge-Driven Cells

269 For our 2-D cases, we identify the edge-driven cells generated adjacent to steps in
 270 lithospheric thickness and quantify their strength. When plate motion and asthenospheric
 271 shear are imposed, we uncover cells by subtracting from the velocity field a vertical pro-
 272 file of u_x , sampled through the centre of the continental realm. Following Coltice et al.
 273 (2018), we calculate at each mesh node the angle of the velocity vector relative to the
 274 x-axis and the horizontal derivative of the vertical component of velocity, $\frac{\partial u_z}{\partial x}$. We next
 275 divide the domain into large squares inside which we analyse angle and derivative val-
 276 ues. For a cell to exist, velocity vectors must be oriented such that they form the shape
 277 of an ellipse. Accordingly, we require the equivalent condition that vector directions dis-
 278 tribute in all four quadrants of the unit circle, which we interpret in terms of the dis-
 279 tribution of angles. Moreover, we apply a threshold to the absolute value of the deriva-
 280 tive (e.g. $3 \times 10^{-15} \text{ s}^{-1}$ for the reference viscosity profile), filtering out squares with only
 281 low-intensity features. We test each square for both conditions and either discard those
 282 that do not meet our criteria or decompose others into four sub-squares. We iterate through
 283 the process until we reach the desired threshold of squares with 10 km sides. At this stage,
 284 we consider the remaining squares to contain the centre of a cell, approximately defined

by the square’s centroid. With the centre of each cell accurately known, relevant velocity profiles can be drawn and compared across multiple cases.

2.4.2 Melting

To track the occurrence of melting, we use the particle-in-cell method recently implemented and validated in Fluidity (Mathews, 2021). We adopt the batch melting parameterization for wet upper-mantle peridotite from Katz et al. (2003), which addresses both the exhaustion of clinopyroxene and water saturation in the rock. Our implementation considers the pressure to be lithostatic, incorporates the adiabatic temperature increase with depth (similar to our viscosity formulation) and makes use of an algorithm for root-finding (Brent, 2013). Moreover, to account for the latent heat of fusion, we couple the melting parameterisation of Katz et al. (2003) to a modified version of the thermodynamic framework from McKenzie (1984) (Supplementary Information).

Particles are randomly initialised throughout the domain, with a denser distribution adjacent to lithospheric steps where melting is expected. We typically use 2×10^5 and 2×10^7 particles in 2-D and 3-D simulations, respectively. For each particle, we determine the onset of melting and track the evolution of both melt fraction, F , and the temperature change due to the latent heat of fusion. At the beginning of the simulation, F is calculated according to the pressure and temperature conditions of the initial state. Particles subsequently record a new value of F at each time-step and keep track of the maximum value experienced, F_{max} , with melting only occurring when the current F is greater than any previous F (i.e. $F > F_{max}$). A melting rate, M , is calculated using the current time-step, δt :

$$M = \max\left(0, \frac{F - F_{max}}{\delta t}\right). \quad (9)$$

As melting occurs, the temperature on a particle not only varies according to the local temperature gradient but also changes through latent heating; both contributions can be distinguished. Consequently, temperatures on nodes of the underlying finite element mesh are updated through the source term of the heat equation (Equation 5). We do not attempt to simulate melt extraction or ‘re-freezing’.

For all simulations, we calculate the cumulative melt production beneath a region of interest, surrounding the continent. To do so, at each time-step, we select particles within a given depth range where melting is occurring (e.g. between 30 km and 160 km) and construct a piecewise linear interpolant from the obtained melting rate. We then evaluate the interpolant onto a 5 km-resolution structured grid and use Simpson’s rule to integrate along any space dimension, as well as multiply by the current model time-step to integrate in time. We obtain cumulative melt thicknesses/areas/volumes by summing results from each time-step. To account for continental motion in cases with a prescribed inflow, we advect the grid according to the displacement of a particle that is located within the rigid continent. We ignore melting from the first time-step as it represents an equilibration process between the originally unmolten rocks and the pressure-temperature-velocity conditions of the model.

3 Results

3.1 Two-Dimensional Simulations

We first examine results from our 2-D simulations. Our reference case incorporates 40 Myr old oceanic lithosphere, a 200 km thick continent and 200 km wide steps, with the material interface between continent and ocean halfway along the step. The initial viscosity distribution, purely in the diffusion creep regime, reaches a minimum of 10^{19} Pa s in the sub-lithospheric oceanic mantle and does not include a low-viscosity channel; domain boundaries are closed.

332 We focus on the dynamics at the right step, illustrated for 30 Myr in Figure 3. A
 333 cell-like flow develops, adjacent to the continent, driven by the negative buoyancy of oceanic
 334 material at the step. Flow rapidly intensifies, with peak vertical velocities increasing by
 335 a factor of ~ 3 from 7 to 15 Myr. Continental lithosphere, owing to its lower density and
 336 increased viscosity, guides downward motion that, in turn, generates upwelling beneath
 337 adjacent oceanic lithosphere. A secondary instability initiates away from the step after
 338 ~ 15 Myr and persists throughout the remainder of the model's evolution. Melting oc-
 339 curs where upwelling material impinges beneath oceanic lithosphere, leading to melting
 340 rates of, on average, a few 100 ppm Myr^{-1} , with some particles recording over $\sim 1 \text{ ‰ Myr}^{-1}$
 341 at 30 Myr; melt fractions reach maximum values of 1%. Melting is initially induced by
 342 the main edge-driven flow and subsequently sustained by the secondary instability, which
 343 delays lithospheric thickening and locally enhances upwelling velocities.

344 We next examine the role of background asthenospheric flow using a 4 cm yr^{-1} plate-
 345 driven case, alongside two cases with additional 2 cm yr^{-1} shear in the asthenosphere,
 346 aligned with, or opposite to, the direction of plate motion, and a similar case with 2 cm yr^{-1}
 347 shear aligned with plate motion for which the coefficient of thermal expansion is set to
 348 0. Figure 4 compares the dynamics around both lithospheric steps after 20 Myr, with ar-
 349 row glyphs illustrating a modified velocity field: the horizontal component is relative to

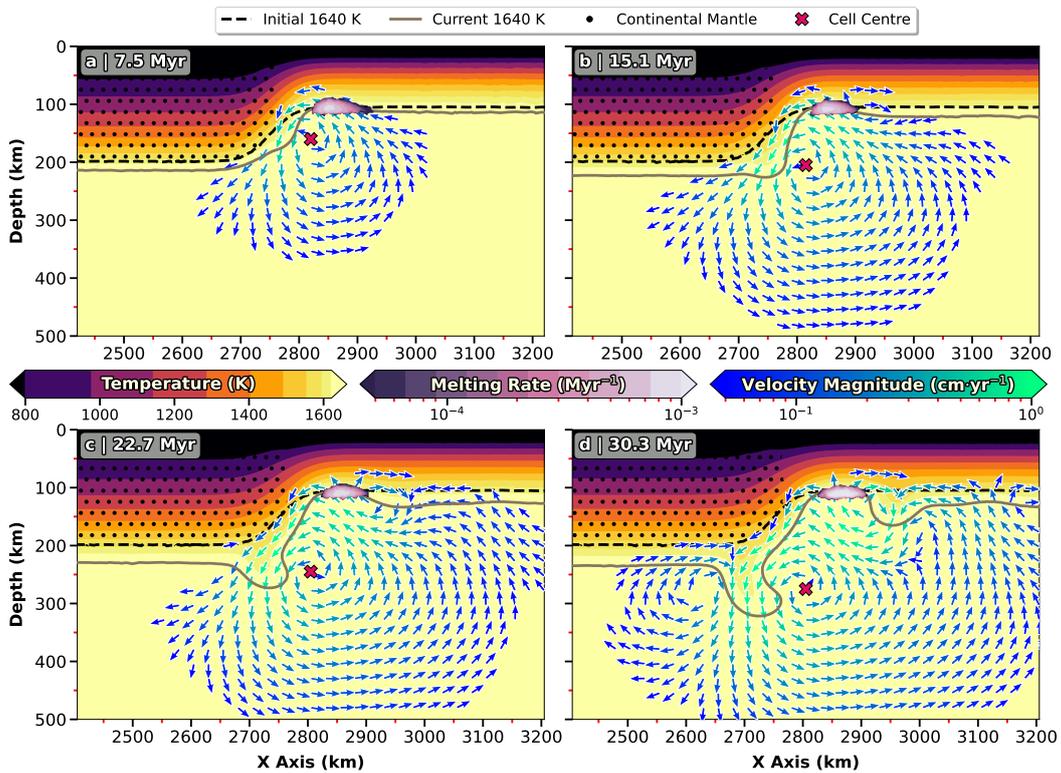


Figure 3. Development of an instability adjacent to the right step of the reference 2-D case. Background colours represent temperature, with the current and initial location of the 1640 K isotherm – a convenient proxy for downwellings – highlighted by solid grey and dashed black lines, respectively. Black dots depict the location of continental mantle. Arrow glyphs highlight the areas of most intense velocity, where the magnitude is higher than 0.5 mm yr^{-1} , as indicated by their colour. Areas experiencing melting are represented as a superimposed surface, coloured by melting rate. The red cross denotes the centre of the cell.

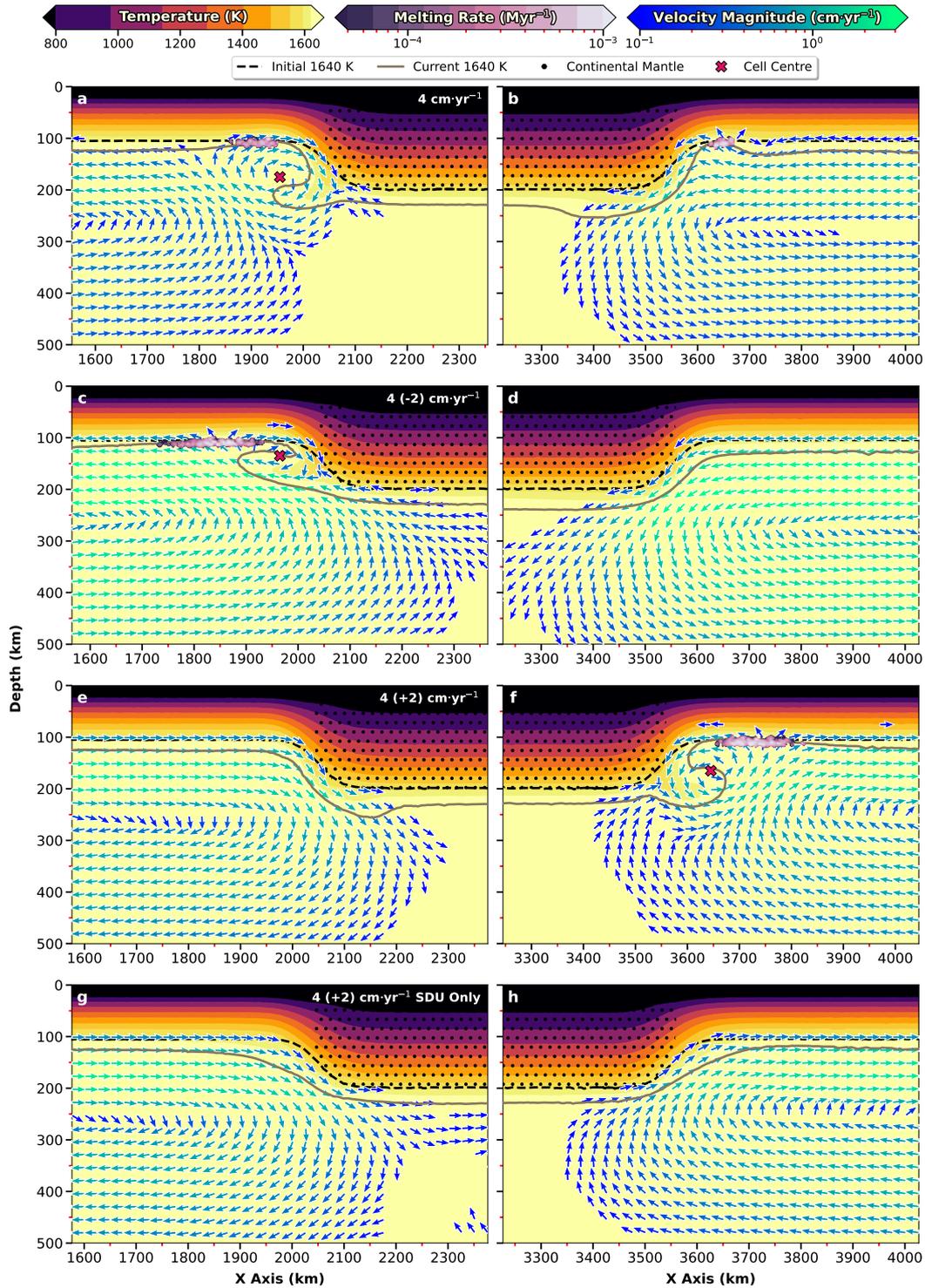


Figure 4. Effect of asthenospheric flow on edge-related dynamics. (a) & (b) 4 cm yr^{-1} purely plate-driven scenario. (c) & (d) A case with additional shear in the asthenosphere, directed opposite to plate motion. (e) & (f) Similar to (c) & (d), but with asthenospheric shear aligned with plate motion direction. (g) & (h) Similar to (e) & (f), but with the coefficient of thermal expansion set to 0, thus negating edge-driven instabilities. All models are displayed after 20 Myr of model evolution. Graphics illustration as in Figure 3, with the horizontal component of velocity relative to that of a vertical transect through the centre of the continent.

350 that of the profile beneath the centre of the continent (refer to Figure S3 for the full ve-
 351 locity field). In the purely plate-driven case (Figure 4a-b), the location of the 1640 K isotherm
 352 indicates that instabilities develop at both steps, although a clear cell is only identifi-
 353 able adjacent to the left step. For this simulation, relative to the overlying plate, the Cou-
 354 ette flow-component associated with plate motion (Figure S2) drives asthenospheric ma-
 355 terial to the left. As such, at the left step, the instability is displaced sideways, away from
 356 the step, and asthenospheric flow enhances the upwelling component of the edge-driven
 357 cell. Conversely, at the right step, asthenospheric motion acts against the cell, with the
 358 resulting downwelling driven horizontally below the continent. The differences between
 359 left and right steps increase in proportion to the magnitude of imposed plate motion, as
 360 reflected in Figure 5a-b where we plot the vertical component of velocity along a hor-
 361 izontal transect through the centre of each cell. These flow patterns explain why melt-
 362 ing is enhanced at the left step relative to the right (quantified in Figure 6a-d and dis-
 363 cussed further below).

364 Additional shear in the asthenosphere, in the direction opposite to plate motion
 365 (Figure 4c-d), increases the aforementioned contrast in behaviour between left and right
 366 steps. Under this scenario, both Couette and asthenospheric shear components act in
 367 the same direction, relative to the overlying plate. As such, at the left step, edge-driven
 368 convection, Couette flow and shear-driven flow combine to increase upwelling rates ('4
 369 (-2)' curve on Figure 5a). We note that the style of upwelling is modified – upwelling flow
 370 becomes dominantly shear-driven, as reflected in the lateral displacement of the insta-
 371 bility and the limited depth extent of the edge-driven cell. Regardless, melting is enhanced
 372 (both in intensity and spatial extent), with the melt region displaced away from the step.
 373 Conversely, at the right step, Couette and shear-driven flow combine to drive material
 374 beneath the continent, preventing upwelling (and melting) in this region.

375 The case where asthenospheric shear is aligned with the direction of plate motion
 376 incorporates counteracting flow regimes: at the left step, the Couette component of flow,
 377 associated with plate motion, acts to enhance the edge-driven cell, but the asthenospheric
 378 shear component acts to dampen it, with opposite trends at the right step. Nonetheless,
 379 as illustrated in Figure 4e-f, the asthenospheric shear component dominates on both steps,
 380 forcing material below the continent and shutting off melting at the left step, but increas-
 381 ing upwelling rates and melting adjacent to the right step. Interestingly, across the pa-
 382 rameter space examined, the largest upwelling velocity recorded along the cell-centre tran-
 383 sects (Figure 5) occurs for this specific model ('4 (+2)') where Couette and shear com-
 384 ponents of flow counteract. In this case, the edge-driven instability is able to develop more
 385 naturally: the drip descends more vertically and acquires a larger volume than in the '4
 386 (-2)' case where flow components combine (compare Figure 4c with Figure 4f). We note
 387 that relative motion between continental lithosphere and underlying asthenosphere is far
 388 greater when they move in opposite directions (relative motion of 5 cm yr^{-1} in case '4
 389 (-2)' compared to 1 cm yr^{-1} in case '4 (+2)', at 250 km depth – see Figure S2). As such,
 390 EDC is able to operate alongside asthenospheric shear in case '4 (+2)', rather than be-
 391 ing completely dominated by it. Nevertheless, melting intensity is similar between these
 392 two cases, albeit occurring over a smaller spatial extent in case '4 (+2)'.

393 To further highlight the delicate balance between different flow components, we il-
 394 lustrate in Figure 4g-h the temperature and flow fields for a case identical to '4 (+2)',
 395 except that the coefficient of thermal expansion has been set to 0. As a result, temper-
 396 ature gradients no longer generate the density changes required to drive an edge insta-
 397 bility at either step. Consequently, the shear-driven flow simply dives beneath the con-
 398 tinent at the left step and rises at the right step. However, it is noteworthy that, dur-
 399 ing the first ~ 7.5 Myr, maximum upwelling velocities at the right step are elevated com-
 400 pared to the case that incorporates buoyancy, indicating that the descending edge-driven
 401 instability partially counteracts shear-driven upwelling at this step (Figure S6). Over time,
 402 this situation reverses: upwelling velocities increase for the case that does incorporate

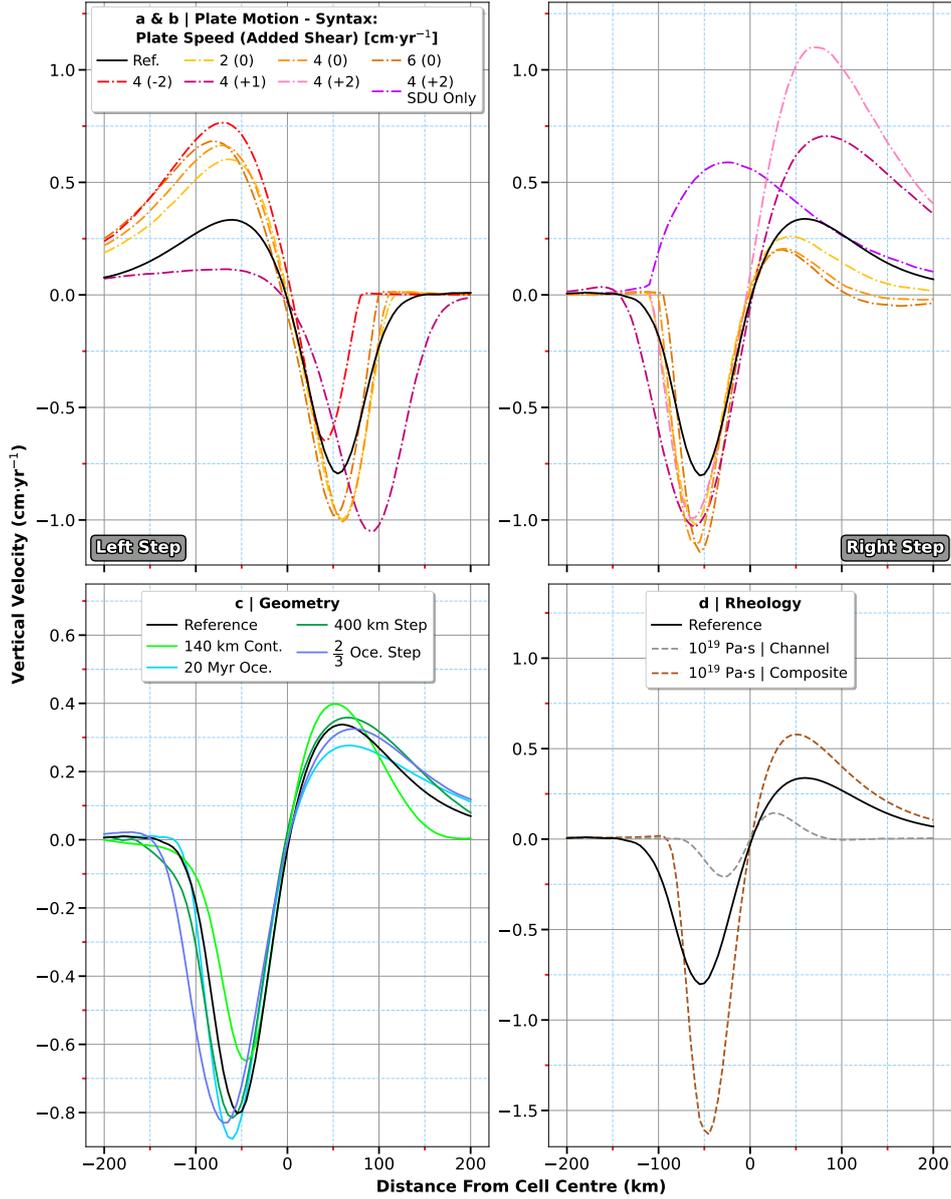


Figure 5. Comparison of vertical velocity in the vicinity of the cell centre (see Figure S4 for computed locations) at the right step (if not specified) for the 2-D simulations examined herein. As instabilities develop over different time-scales for different cases, we identify the centre of the cell in each simulation (Figure S4) at the time of maximum downwelling velocity (Figure S5), prior to the onset of secondary instabilities, to provide a meaningful comparison. Each profile represents a 400 km horizontal transect passing through the centre of the cell. (a) & (b) Influence of background asthenospheric flow – ‘Reference’ corresponds to an enclosed simulation. At the right step, purely plate-driven cases do not develop a full circulating cell and, accordingly, velocity profiles are displayed at depths picked to allow for illustration of upwelling velocities in a way that is comparable to other cases. Moreover, the case with SDU only does not generate a cell at all and we use the cell centre from the equivalent case (‘4 (+2)’) to draw the profile to allow for a representative comparison. (c) Effect of step geometry – ‘Reference’ corresponds to ‘40 Myr Oce.’, ‘200 km Step’, ‘200 km Cont.’, and a material boundary halfway along the step. (d) Role of viscosity – ‘Reference’ corresponds to a purely diffusion creep channel-free profile with a minimum viscosity of 10^{19} Pa.s.

403 buoyancy, as the instability grows, but upwelling velocities systematically decrease in the
 404 SDU-only case, as the upper thermal boundary layer thickens through diffusion, reduc-
 405 ing the pressure difference between regions of thick and thin lithosphere. As a consequence,
 406 after ~ 15 Myr, the lid has sufficiently thickened to prevent any decompression melting
 407 in the SDU-only case (Figure 6c). The interplay between buoyancy and mantle flow at
 408 lithospheric steps is further reflected in case ‘4 (+1)’ (Figure 5a), for which asthenospheric
 409 shear is sufficient to counteract the Couette component of flow: horizontal flow within
 410 and just below the continent are of similar intensity (Figure S2). As a result, edge-driven
 411 instabilities develop akin to these of the reference case, and a weak cell is observed at
 412 the left step, despite it being strongly modulated by asthenospheric shear. Nevertheless,
 413 the presence of a weak cell enhances melting as it focusses upwelling velocities at shall-
 414 lower depths, closer to the solidus. Taken together, these results highlight that there is
 415 a threshold point at which EDC and SDU combine to maximise upwelling velocities ad-
 416 jacent to lithospheric steps. Where the shear-driven component is reduced, relative to
 417 this point, upwelling velocities decrease. Conversely, where the shear-driven component
 418 is increased, relative to this point, downwelling instabilities are unable to develop at litho-
 419 spheric steps and, accordingly, the contribution from EDC is eliminated and upwelling
 420 is purely shear-driven.

421 We next compare the vigour of edge-driven instabilities across the remainder of our
 422 parameter space. Although we have examined a broad suite of models, we focus on rep-
 423 resentative end-members for clarity. As illustrated in Figure 5c, geometric parameters
 424 generally have only a moderate influence on the downwelling velocity, upwelling veloc-
 425 ity and cell width (i.e. the distance between maximum downwelling and upwelling speeds
 426 along the profile) along these horizontal transects, with all profiles displaying similar char-
 427 acteristics. Nonetheless, in comparison to the reference case, the thinner continent (‘140 km
 428 Cont.’) yields a smaller cell, both in depth and lateral extent, with peak downwelling
 429 velocities reduced but peak upwelling velocities enhanced. Such differences arise primar-
 430 ily from the shorter continental guide at depth, which limits instability growth and down-
 431 welling velocities. As a result, flow circulation concentrates closer to the step and the
 432 extent of horizontal motion beneath the lithosphere decreases, facilitating an earlier on-
 433 set of secondary instabilities. Accordingly, although peak upwelling velocities are initially
 434 smaller, they eventually overcome those of the reference case. In general, we find that
 435 increased space available along the continental guide (e.g. ‘20 Myr Oce.’) and greater vol-
 436 umes of unstable oceanic lithosphere (e.g. ‘400 km Step’ and ‘ $\frac{2}{3}$ Oce. Step’) lead to slightly
 437 stronger downwelling instabilities. Corresponding peak upwelling velocities, however, are
 438 not necessarily higher, but the lateral extent of the cells increases. In Figure 5d, we il-
 439 lustrate the important role of upper mantle viscosity and its depth-dependence. At a min-
 440 imum viscosity of 10^{20} Pa s no comparable cell forms over the simulation times examined.
 441 The presence of a low-viscosity channel limits the vertical space over which an instabil-
 442 ity can develop and, accordingly, stabilises the lithosphere, reducing the intensity and
 443 scale of edge-driven instabilities. In the composite diffusion-dislocation creep regime, the
 444 intensity of the cell is enhanced, as a result of lower viscosities in the vicinity of the drip:
 445 a voluminous and focussed instability forms, generating a broad, robust upwelling (Fig-
 446 ure S7).

447 To understand how these flow patterns influence melting, we present both instan-
 448 taneous melting rates and cumulative melt diagnostics in Figure 6. Melting trends in cases
 449 with plate motion and asthenospheric shear are generally consistent with the flow fields
 450 highlighted above. For the first ~ 20 Myr of model evolution, instantaneous melting rates
 451 are enhanced at the left step for cases with plate motion, and further enhanced when favourable
 452 asthenospheric shear is included. At the right step, plate-driven cases generate less melt-
 453 ing than the reference case, but favourable asthenospheric shear once again enhances melt
 454 production. We note that a small amount of melting occurs at the left step for case ‘4
 455 (+1)’, as expected from the flow field highlighted above. For all cases with plate motion
 456 or asthenospheric shear, the onset of secondary instabilities is delayed and, hence, the

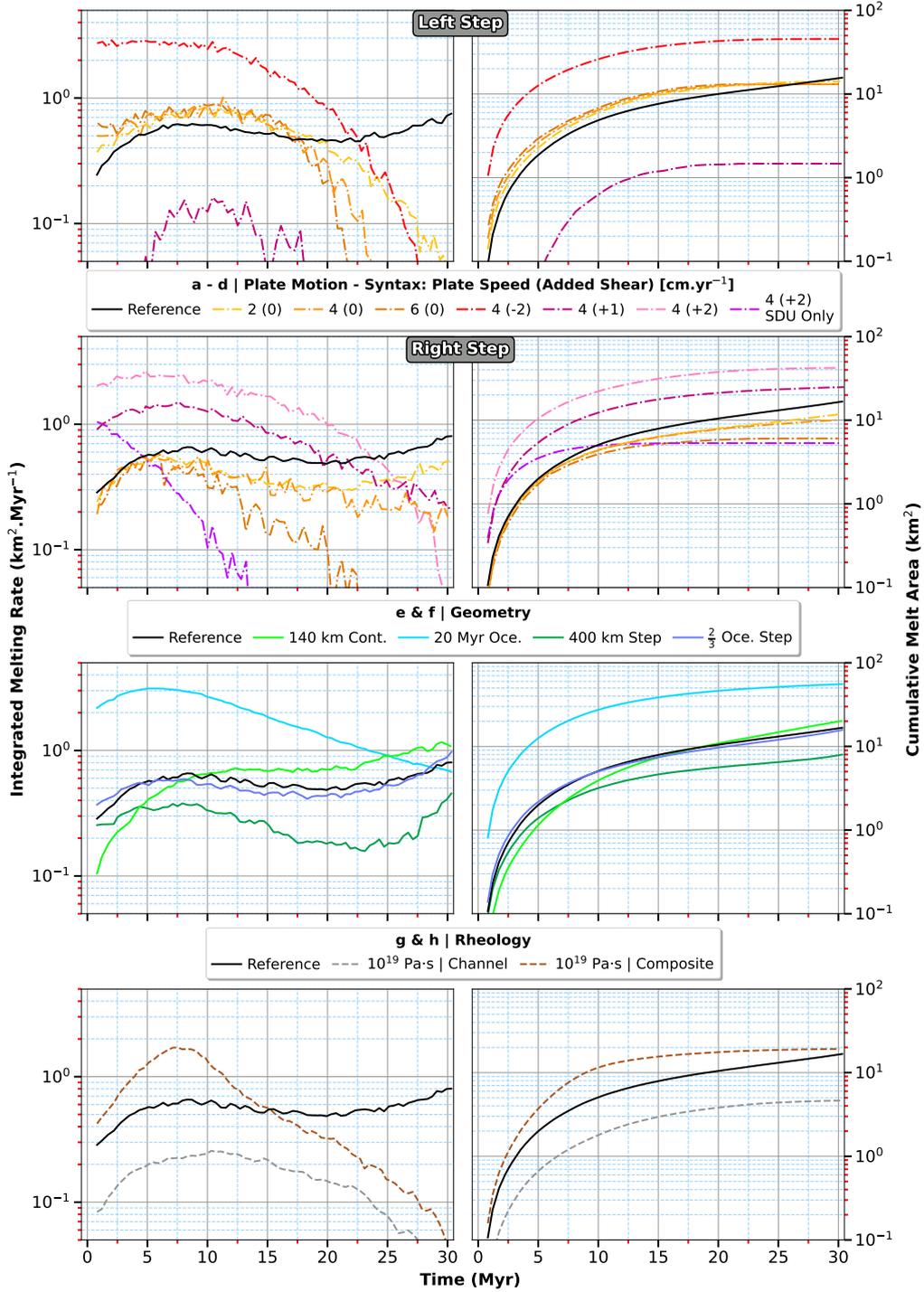


Figure 6. (a), (c), (e) & (g) Integrated melting rate measured at the right step (if not specified), as a function of time. Values correspond to the full integral in space of interpolated melting rates as recorded by particles. (b), (d), (f) & (h) Cumulative melt area, corresponding to the cumulative sum of melting rate additionally integrated in time. (a), (b), (c) & (d) Influence of asthenospheric flow – ‘Reference’ corresponds to an enclosed simulation. (e) & (f) Effect of step geometry – ‘Reference’ corresponds to ‘40 Myr Oce.’, ‘200 km Step’, ‘200 km Cont.’, and a material boundary halfway along the step. (g) & (h) Role of viscosity – ‘Reference’ corresponds to a purely diffusion creep channel-free profile with a minimum viscosity of 10^{19} Pa.s.

lithospheric lid thickens more rapidly than in cases without shear. As a consequence, instantaneous melting rates drop below the reference case beyond ~ 20 Myr of model evolution – melting occurs over a shorter temporal duration for cases with a large component of asthenospheric shear. Such trends are further amplified in the absence of EDC, as illustrated by the SDU only case.

We find that most of the alternative step geometries analysed generate a comparable ‘melt area’ to that of the reference case, apart from the thinner lid (‘20 Myr Oce’) which enhances decompression melting (Figure 6e-f). Nonetheless, in the case of a wider step (‘400 km Step’), melting rates are $\sim 50\%$ less than the reference case: the more gradual step generates a more-rounded cell, with upwelling flow less vertical at the LAB and, accordingly, less intense melting. Geometries such as ‘140 km Cont.’ promote a more rapid onset of secondary instabilities, which thin the lithospheric lid and locally increase upwelling velocities. Such cases, therefore, initially display lower instantaneous melting rates, but eventually melt more than the reference case. Finally, cases with a minimum viscosity of 10^{20} Pa s exhibit no, or very limited, melting, whilst the incorporation of a low-viscosity channel reduces melting rates significantly, as expected from the aforementioned flow field (Figure 6g-h). In the composite viscosity regime, melting rates are higher for the first ~ 15 Myr of model evolution. However, the broader and more intense cell delays the onset of secondary instabilities (due to increased shear beneath the lithosphere) and, thus, the cumulative melt curve flattens after ~ 15 Myr, leading to a similar melt area to that of the reference case after 30 Myr.

3.2 Three-Dimensional Simulations

Our 2-D results highlight the importance of the orientation of asthenospheric shear in controlling the flow regime and associated melt production at lithospheric steps. Nonetheless, the 2-D geometry limits the range of scenarios that can be examined. Accordingly, we extend our analyses to 3-D, allowing for the incorporation of more complex geometries and greater flexibility in the orientation of asthenospheric flow. We separate our results into cases that neglect (Section 3.2.1) or incorporate (Section 3.2.2) background asthenospheric flow, respectively.

3.2.1 No Prescribed Asthenospheric Flow

We first examine the velocity field generated after 15 Myr: this is sufficient to capture the development of primary instabilities whilst avoiding complications linked to the onset of secondary instabilities, allowing us to focus upon 3-D effects that arise from more complex continental geometries. Nonetheless, for completeness, we illustrate through Figure S8, which is directly comparable to Figure 2, the development of secondary instabilities after 30 Myr in all 3-D geometries examined. Figure 7a displays the flow regime for Case U400, which exhibits edge-driven instabilities of comparable intensity adjacent to the entire continental boundary, except within the indent where darker red glyphs highlight more vigorous upwelling. At this location, the geometry of the interface between ocean and continent brings upwelling flows associated with three adjacent steps into close proximity: these coalesce (Figure S9a), enhancing upwelling velocities by as much as 70% in comparison to those in other parts of the domain (Table 3).

Figure 7b displays results for Case U600. Although similar high-intensity upwelling velocities are present within the indent, they are restricted to the inner corners: in this case, the distance between edge-driven cells exceeds the width of the cells and, accordingly, cells on opposite steps are unable to coalesce and influence each other to the same extent as in Case U400 (Figure S9b). Figure 7c illustrates results from Case U400-Grad, with a complementary cross-section presented in Figure S10. Consistent with our 2-D cases (Figure 5c), downwelling velocities are enhanced adjacent to thicker parts of the continent, with upwellings broader and marginally less vigorous. Figure 7d illustrates

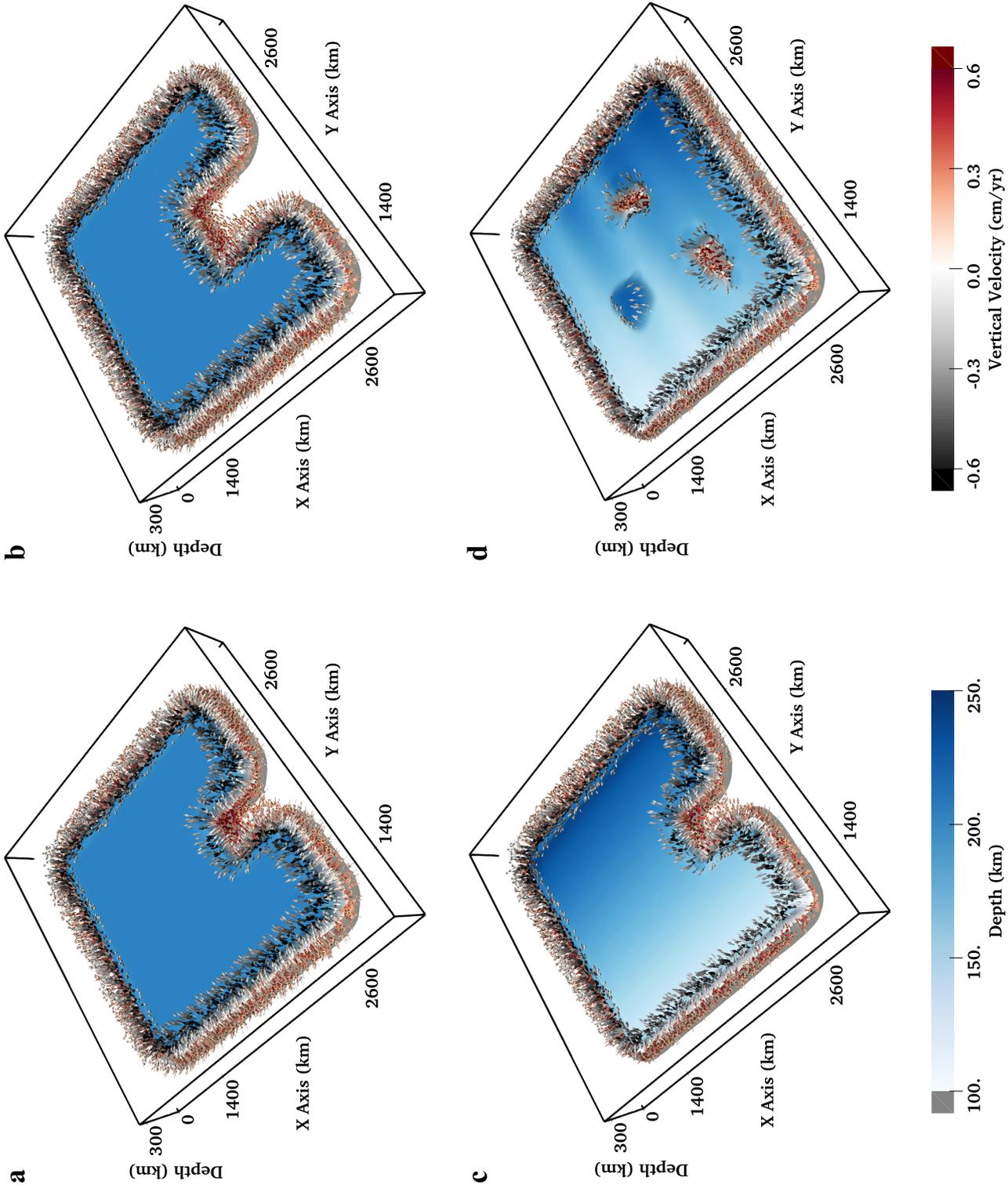


Figure 7. 3-D representation of the velocity field around the continent at 15 Myr, illustrated through a view looking at the base of the continent, from below. Surface colours correspond to the depth of the 1620 K isotherm – our proxy for lithospheric thickness – while arrow glyphs illustrate the velocity field. For visualization purposes, glyphs are only drawn at locations where the velocity magnitude is larger than 2 mm yr^{-1} ; glyphs all have the same length, are uniformly distributed and are coloured according to the vertical component of velocity. (a) Case U400. (b) Case U600. (c) Case U400-Grad. (d) Case Complex.

507 flow patterns for Case Complex and clearly demonstrates that regions of anomalously
 508 thin continental thickness trigger localised and strong upwelling flows. However, only mod-
 509 erate downwelling flows develop adjacent to the anomalously thick continental area: con-
 510 tinental material resists deformation through its higher viscosity. Instabilities along con-
 511 tinental boundaries are consistent with those in Case U400-Grad, as expected.

512 We now analyse the cumulative melt production for these cases. Results, presented
 513 in Figure 8, are expressed as a cumulative thickness, which results from the integration
 514 of melting rates both in time (over 15 Myr) and along the vertical axis (Section 2.4). Most
 515 melting occurs between 90 km and 120 km depth, consistent with the 2-D cases, except
 516 where the lithosphere is sufficiently thin to host shallower melting. For Case U400 (Fig-
 517 ure 8a), we observe three distinct melting trends: (i) weak melting, adjacent to the ex-
 518 ternal corners of the continent, producing less than ~ 0.12 km of melt; (ii) moderate melt-
 519 ing, at external steps away from the corners, producing up to ~ 0.20 km of melt; and (iii)
 520 enhanced melting, within the indent, producing up to ~ 0.45 km of melt, with the most
 521 intense melting concentrated at the indent’s inner corners. Full spatial integration around
 522 the indent’s lower-left corner (Figure 8a, 150 km-side black square) yields a cumulative
 523 volume of ~ 3000 km³ distributed over an area of $\sim 15,600$ km² (Table 3). Melt fractions
 524 peak at 1%, consistent with our 2-D cases. These trends are as expected from the in-
 525 tensity of upwelling at these locations.

526 In Figure 8b, we illustrate the spatial distribution of melt obtained for Case U600.
 527 We observe similar trends as for Case U400 and note, in particular, that comparable melt-
 528 ing is recorded adjacent to the indent’s inner corners, despite weaker flow coalescence
 529 (Figure S9), indicating that the geometry of the corners is sufficient to sustain melting.
 530 For Case U400-Grad (Figure 8c), steps adjacent to thicker parts of the continent gen-
 531 erate around 30% more melt than those adjacent to thinner parts, with a gradient in
 532 between, in agreement with Figure 6c – recall how the primary melting of ‘140 km Cont.’,
 533 relative to our reference case, is initially reduced, but eventually enhanced through the
 534 action of secondary instabilities. Finally, for Case Complex (Figure 8d), trends at ex-
 535 ternal steps are consistent with Case U400-Grad. Within the continent, significant melt-

Table 3. *Diagnostics Across 3-D Models*

Case	Maximum downwelling		Maximum upwelling		Maximum melt thickness ^a		Melt volume ^b (km ³) & area ^c (km ²) at the indent’s corner
	inside outside indent (cm yr ⁻¹)	inside outside indent (km)	inside outside indent (km)				
U400	-1.03 -1.10	0.70 0.42	0.47 0.20	0.47 0.20	2976 & 15,594		
U600	-1.01 -1.11	0.67 0.42	0.47 0.20	0.47 0.20	2977 & 15,861		
U400-Grad	-1.07 -1.15	0.64 0.49	0.46 0.20	0.46 0.20	2951 & 15,850		
Complex ^d	-0.61 -1.17	0.87 0.48	0.70 0.20	0.70 0.20	3936 & 15,256		
Pos. x	-0.97 -1.40	1.31 0.84	0.66 0.33	0.66 0.33	5646 & 20,044		
Neg. x	-1.13 -1.41	0.39 0.92	0.21 0.35	0.21 0.35	837 & 7389		
Pos. y	-1.19 -1.37	1.11 0.91	0.60 0.33	0.60 0.33	4676 & 18,689		
Oblique	-0.96 -1.75	1.75 0.95	0.81 0.31	0.81 0.31	8103 & 21,080		

^a Cumulative thickness over the first 15 Myr of model evolution, obtained by integration of the melting rate carried by particles both in time and along the vertical axis (Figures 8 and 10). ^b Integration of the cumulative thickness in both x and y directions; only nodes (Section 2.4) with a cumulative thickness greater than 0.04 km and that are closest to the bottom-left inner corner of the indent (e.g. black square in Figure 8a) are considered. ^c Area defined by the nodes considered in the melt volume calculation.

^d For the first three columns, ‘inside | outside the indent’ is swapped for ‘inside | outside the continent’, while the last column ‘indent’s corner’ is replaced by ‘right trough’ (black rectangle in Figure 8d).

536 ing is restricted to the two anomalous troughs, in agreement with the vigorous upwellings
 537 highlighted in Figure 7d. As a result of the initially thin continental lithosphere at these
 538 locations (60 km in places, as opposed to 90 km for surrounding oceanic lithosphere), we
 539 record up to 0.7 km of cumulative melt production, which is 50 % higher than observed
 540 at the indent's inner corners in Case U400. Additionally, melt volume within the right
 541 trough, recorded over a similar area (Table 3), is 30 % higher.

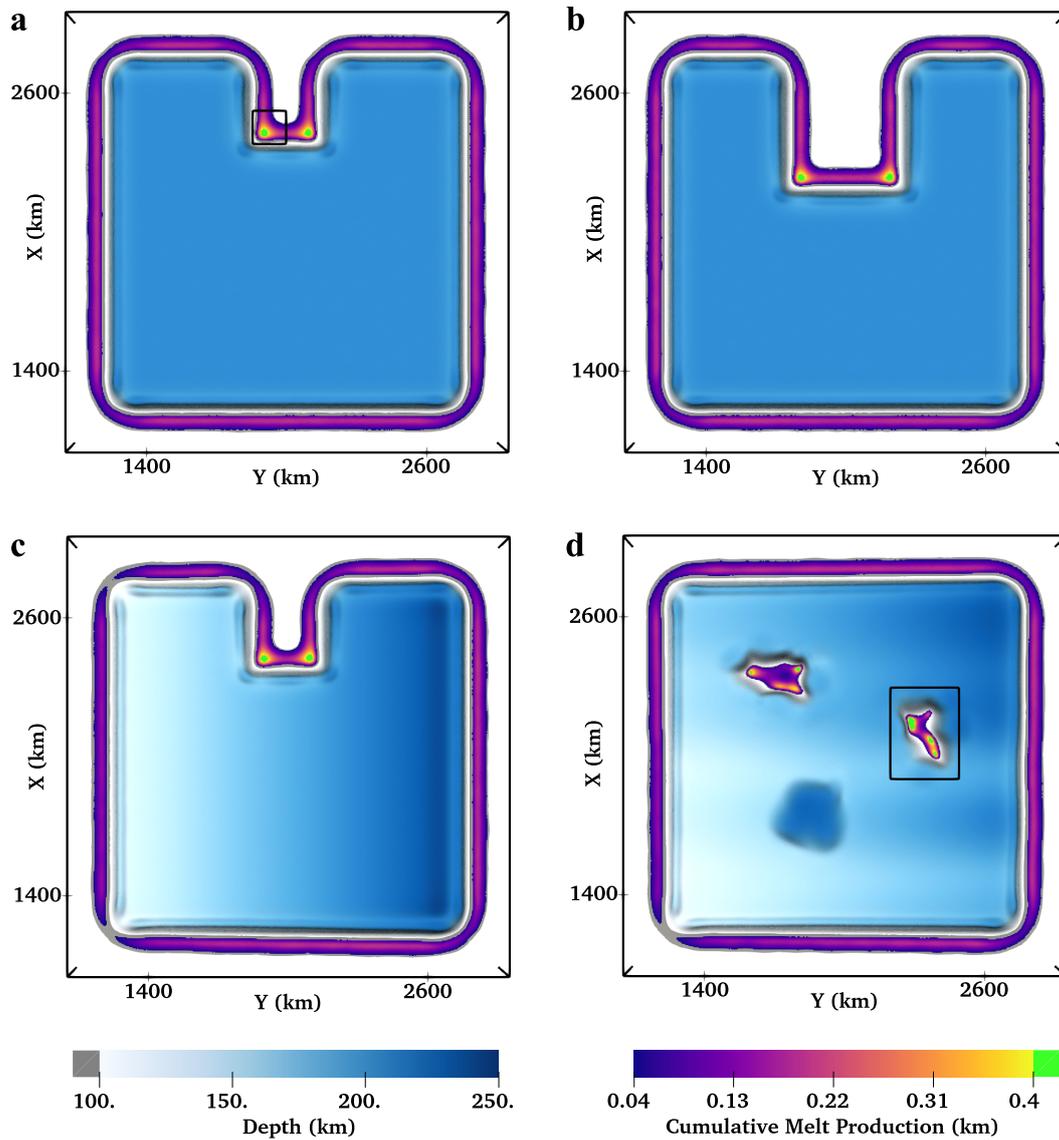


Figure 8. Cumulative melt production adjacent to the continent for cases without plate motion, after 15 Myr. Surface colours correspond to the depth of the 1620 K isotherm, our proxy for lithospheric depth; lithospheric erosion is identified by the grey tone, which depicts portions thinner than 100 km. Purple-to-yellow colours represent the cumulative melt production as obtained after integration along the vertical axis (Section 2.4); major locations of melting are indicated by the green tone. Black rectangles illustrate zones of interest used for calculations in Table 3. (a) Case U400. (b) Case U600. (c) Case U400-Grad. (d) Case Complex.

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3.2.2 Prescribed Asthenospheric Flow

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We next examine cases that incorporate prescribed asthenospheric flow and focus on how its orientation, relative to the continent, affects dynamical instabilities throughout the domain. We use Case U400 as our reference and systematically prescribe flow in the positive x, negative x, positive y, and both positive x and y (oblique) directions. We illustrate our results initially through the flow field (Figure 9) and, subsequently, through its influence on melting (Figures 10 and 11).

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We find that velocities align with the prescribed inflow direction, in agreement with 2-D behaviour (Figure S3). Accordingly, to better highlight buoyancy-driven instabilities and allow for a consistent comparison with our 2-D cases, we modify the velocity field such that, at all depths, horizontal components are relative to those sampled on a vertical profile transecting through the centre of the continent. Figure 9a illustrates the resulting dynamics when asthenospheric shear is prescribed in the positive x-direction. Compared to Case U400 (Figure 7a), we observe enhanced upwelling velocities, increasing by up to $\sim 90\%$ inside the indent and $\sim 100\%$ where the asthenosphere flows away from the continent (i.e. the trailing edge). Conversely, where the asthenosphere flows toward the continent (i.e. the leading edge), upwelling velocities are reduced substantially by $\sim 70\%$. The leading edge exhibits a clear downwelling, no associated upwelling, and divergent flow at continental corners. Conversely, intense upwelling takes place along the trailing edge and flow is convergent around the corners. Divergent and convergent flows at the continent's external corners occur due to the higher pressure beneath the continent, which drives material around continental margins and, accordingly, also contributes toward upwelling flow at the continent's lateral edges.

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Figure 9b illustrates the flow field resulting from prescribed inflow in the negative x-direction. Trends are generally identical to the previous case on leading, trailing and outer lateral steps. However, upwelling velocities within the indent are no greater than those along the continent's lateral margins (Table 3): asthenospheric shear of this magnitude and orientation overcomes the dynamics of edge-driven convection imposed by the indent's geometric configuration. In Figure 9c, we illustrate the effect of incorporating shear in the positive y-direction. Both strong upwelling and downwelling velocities are observed within the indent (compared to Figure 7a), as the flow first upwells from below and then dives beneath the continent. Peak upwelling velocity is intermediate between Case U400 and the positive-x inflow case. For our oblique case (Figure 9d), the notion of leading and trailing edges evolves into the idea of pairs of edges adjacent to leading and trailing corners. Accordingly, downwellings concentrate alongside outer edges connected to the leading corner, whereas upwellings distribute adjacent to the opposite edges. Within the indent, we observe intense upward motion. Flow within the asthenosphere is favourably oriented to enhance upwellings at both steps adjacent to the lower-left inner corner (Figure 10d). Consequently, the vertical velocities recorded are the largest across all cases examined, a $\sim 250\%$ increase relative to Case U400.

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We next analyse the cumulative melt production for these cases. In Figure 10a, we recover the three melting trends previously described for our reference 3-D case (Case U400). However, relative to the reference case, melting is absent at the continent's leading edge and enhanced at its trailing edge (by $\sim 65\%$). Inside the indent, the maximum melt thickness increases by $\sim 40\%$ relative to Case U400, and melting takes place over a larger area, leading to a $\sim 90\%$ increase in local melt volume (Table 3). Inflow prescribed in the opposite direction (Figure 10b) yields similar trends at leading, trailing and lateral edges. In this case, melt production inside the indent is comparable to that observed at the continent's lateral edges and is less than that observed at the trailing edge. The calculated melt volume at the indent's lower-left corner falls to $\sim 840 \text{ km}^3$, equivalent to a $\sim 70\%$ decrease from Case U400. For inflow in the positive y-direction (Figure 10c), the distribution of melt production corresponds closely to locations of upwelling flow, especially within the indent where the recorded melt volume at the lower-left inner cor-

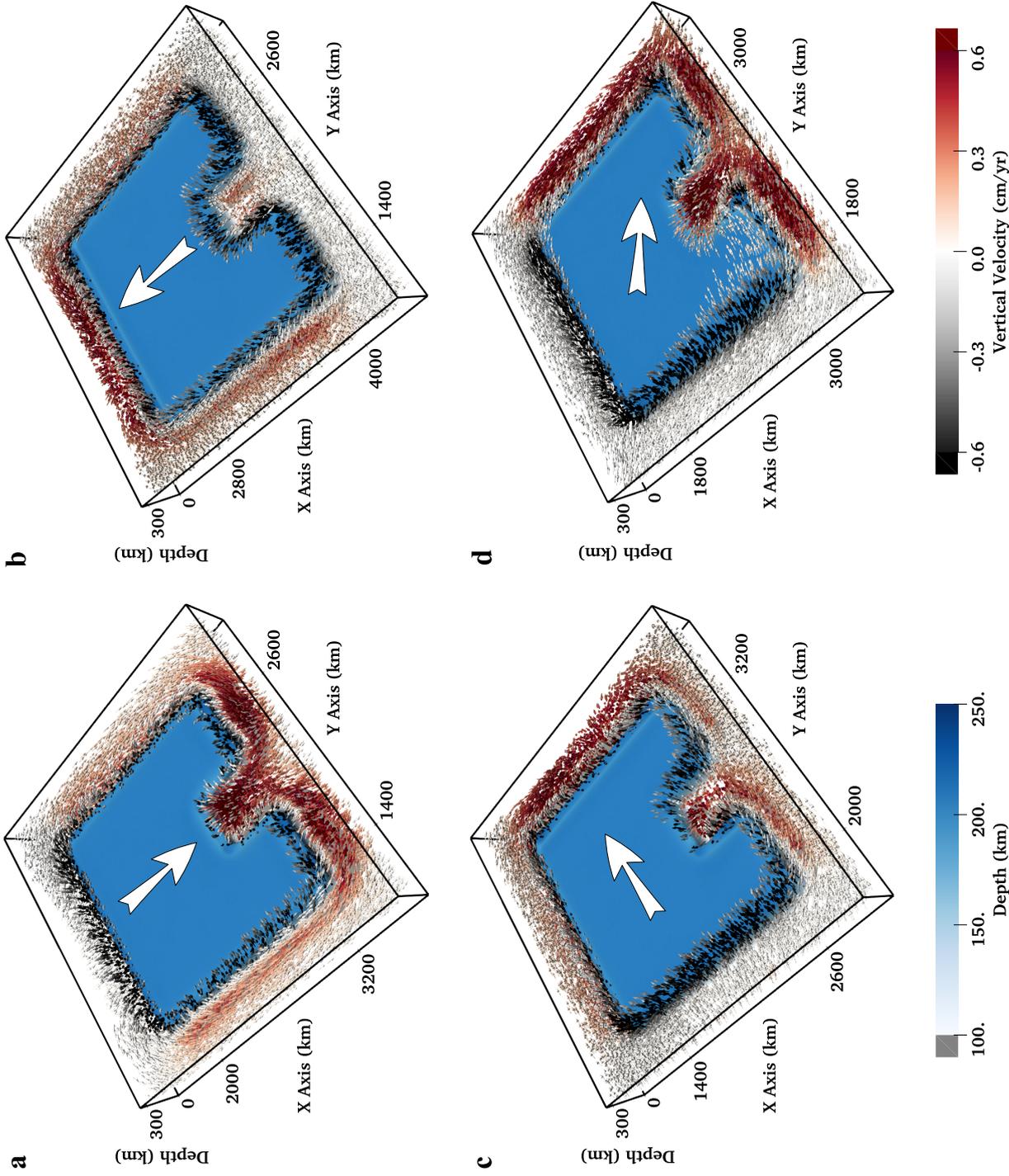


Figure 9. 3-D representation of the velocity field around the continental area after 15 Myr. Graphic illustration is similar to Figure 7; glyphs are only drawn where the velocity magnitude is greater than 4 mm yr^{-1} . Similar to Figure 4, horizontal components of velocity are relative to that sampled on the vertical profile centred through the continent, uncovering dynamical instabilities. Additionally, large white arrows represent both the direction of plate motion and the direction of asthenospheric flow relative to the continent, thereby pointing from the continent's leading edge to its trailing edge. (a) Prescribed flow in the direction of positive x . (b) Direction of negative x . (c) Direction of positive x . (d) Direction of both positive x and y .

595 ner represents $\sim 80\%$ of that measured for the positive-x inflow. For our oblique case (Fig-
 596 ure 10d), melting is absent at the pair of edges adjacent to the leading corner. At op-
 597 posite edges, melt production is marginally lower than at a trailing edge experiencing
 598 purely normal flow (e.g. in the case of positive x-inflow) but still noticeably higher than
 599 at a comparable edge in the absence of asthenospheric flow (e.g. Case U400). As expected
 600 from the velocity field, a large area around the lower-left inner corner of the indent dis-
 601 plays intense melt production, up to $\sim 70\%$ higher than in Case U400. The calculated
 602 cumulative melt volume in this region is $\sim 270\%$ higher than Case U400 and is the high-
 603 est recorded across the parameter space examined.

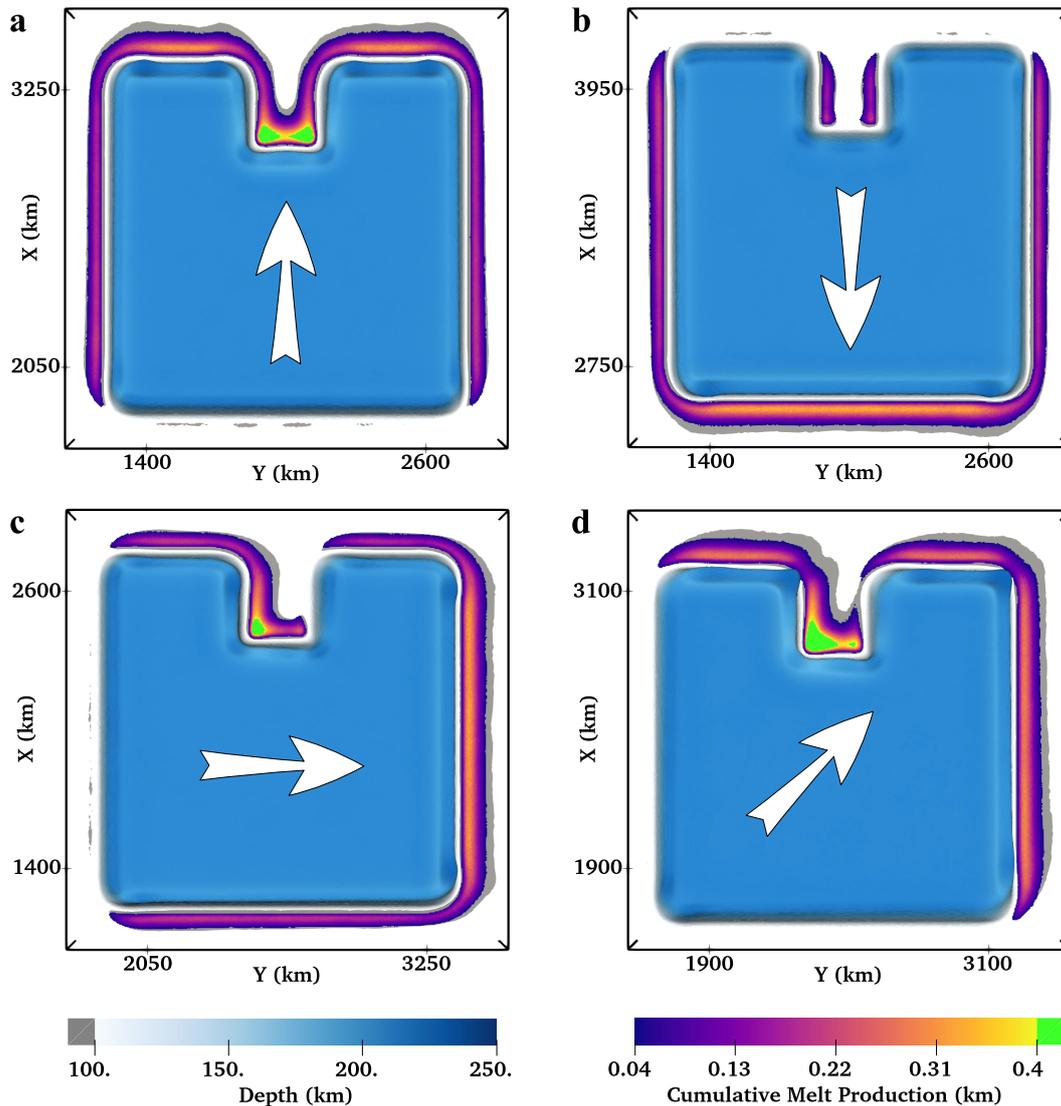


Figure 10. Cumulative melt production adjacent to the continent for cases with prescribed inflow, after 15 Myr. Graphic illustration is similar to Figure 8. Additionally, large white arrows represent both the direction of plate motion and the direction of asthenospheric flow relative to the continent, thereby pointing from the leading edge to the trailing edge. (a) Positive x. (b) Negative x. (c) Positive y. (d) Oblique.

604 Finally, we compare the spatial distribution of melts produced in our 3-D cases that
 605 incorporate asthenospheric flow (Figure 10) with Case U400 (Figure 8a). For each panel
 606 in Figure 10, we subtract the melt production from Figure 8a and illustrate the result
 607 in the corresponding panel of Figure 11. We make several important observations: (i)
 608 the leading edge of a continent is identified by a substantial decrease in melt production
 609 (dark pink colours) as material descends beneath the continent; (ii) trailing edges dis-
 610 play an increase in melt production (green tones) as material rises from beneath the con-
 611 tinent; (iii) lateral edges see no significant change in melt production; and (iv) the ef-
 612 fect of flow direction is reflected in melting locations within the indent, with melting in-

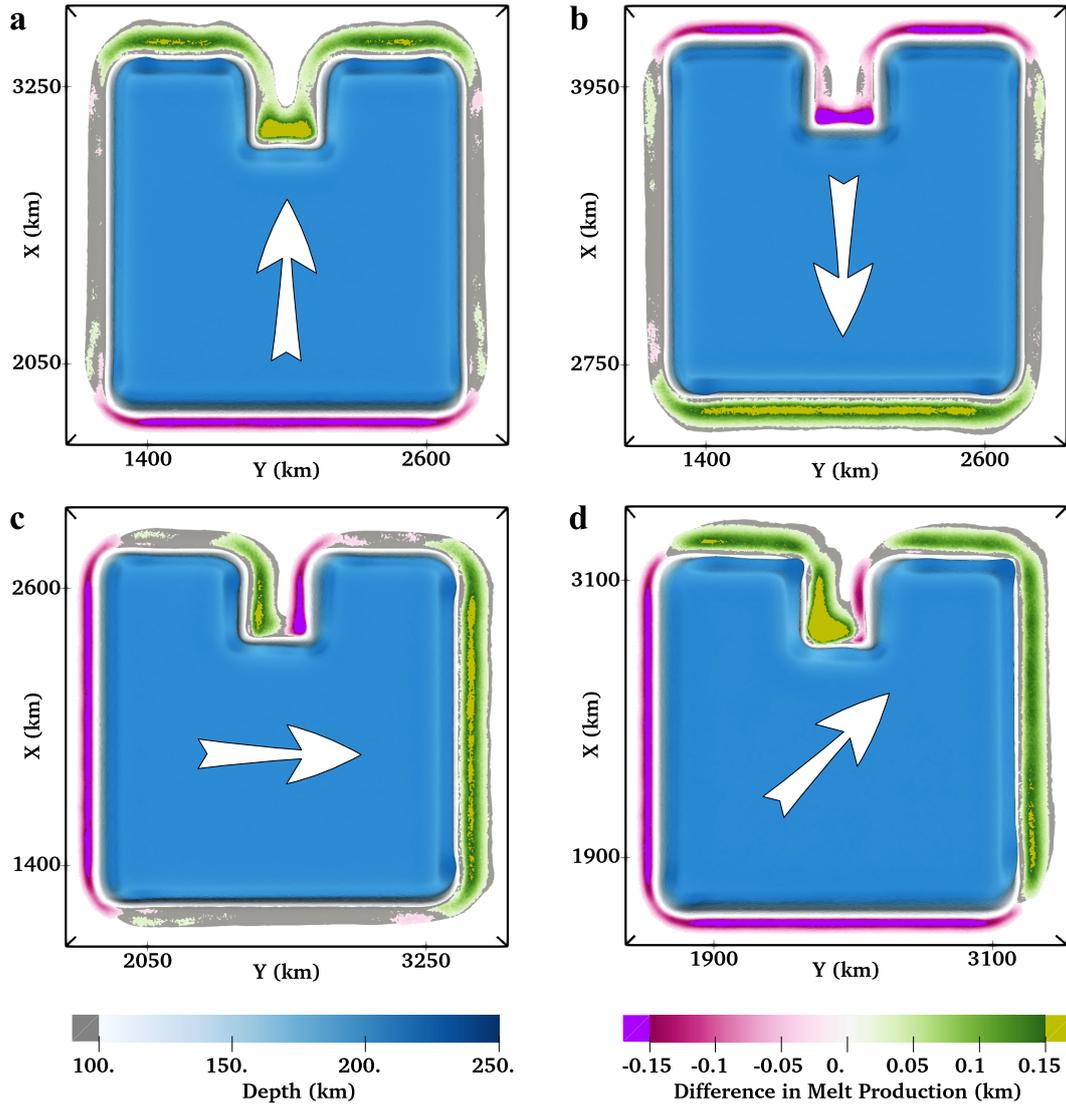


Figure 11. Relative production of melt between cases with prescribed inflow and Case U400. Each panel is generated as a difference between the corresponding panel in Figure 10 and Figure 8a; values in the range -0.02 km to 0.02 km are not represented. Pink tones denote areas where melting is weakened by asthenospheric flow, while green tones highlight zones of enhanced melting. Large white arrows are consistent with Figure 10. (a) Positive x. (b) Negative x. (c) Positive y. (d) Oblique.

613 creasing significantly where interactions between upwelling currents are facilitated by the
614 geometric configuration.

615 4 Discussion

616 We have quantitatively examined mantle flow and melt generation in the vicinity
617 of lithospheric steps, using a suite of 2-D and 3-D numerical models. Our models reveal
618 the dominant controls on edge-driven convection (EDC) and shear-driven upwelling (SDU),
619 how these shallow processes interact, and under which conditions they can be linked to
620 intra-plate volcanism.

621 We find that EDC is strongly sensitive to uppermost mantle viscosity and its depth
622 dependence. At minimum viscosities $\geq 10^{20}$ Pa s, only weak edge-driven cells develop over
623 the timescales of our simulations. If low viscosities are restricted to a narrow astheno-
624 spheric channel, the length-scale and vigour of edge-driven cells are reduced. These find-
625 ings are consistent with several previous studies, which report that significant small-scale
626 convection only develops at viscosities of less than 10^{19} - 10^{20} Pa s (e.g. van Hunen et al.,
627 2003; Currie et al., 2008; Le Voci et al., 2014; Davies et al., 2016). We find that the ge-
628 ometry and material properties of the step are also important in controlling EDC. Con-
629 tinental lithosphere guides downwelling flow and, thus, cases with deeper continental guides
630 drive larger-scale cells. Other geometrical parameters, including the width of the step,
631 the age (thickness) of oceanic lithosphere and the location of the interface between con-
632 tinent and ocean along the step, control the volume of lithospheric instabilities and, hence,
633 the rate at which they develop and the vigour of the resulting cell. These findings build
634 on those across a number of previous studies (e.g. Farrington et al., 2010; Till et al., 2010;
635 Ballmer et al., 2011; Davies & Rawlinson, 2014; Kaislaniemi & van Hunen, 2014; Rawl-
636 inson et al., 2017).

637 By analysing EDC in the presence of plate-motion and asthenospheric shear, we
638 have been able to shed light on how EDC and SDU interact. In 2-D, we find that Cou-
639 ette flow, induced by plate-motion, can enhance EDC where the asthenosphere flows away
640 from the lithospheric step and suppress it where the asthenosphere flows toward the step.
641 Depending upon its orientation, the addition of further asthenospheric shear can enhance
642 or diminish the contrast in dynamics between leading and trailing continental edges. Where
643 both processes combine, we find that melting is enhanced, even if the contribution from
644 EDC is minimal. Under this scenario, EDC drives a small-scale upwelling at shallow depths,
645 close to the step (e.g. Figure 4c), which enhances decompression melting. We empha-
646 size that there is a threshold beyond which SDU dominates and EDC is suppressed: in
647 our models with an imposed surface velocity, we find that EDC is largely overcome when
648 relative motion between the continent and underlying asthenosphere exceeds $\sim 2 \text{ cm yr}^{-1}$.
649 At this stage, downwelling instabilities cannot drip vertically and are swept horizontally,
650 with the morphology of upwelling flow also modified as a result. Although we have not
651 undertaken an exhaustive parameter space study, we note that this threshold is sensi-
652 tive to a number of parameters, including the geometry and material properties of the
653 step, as well as uppermost mantle viscosity and its depth-dependence. Interestingly, as
654 one approaches this threshold point, the negative buoyancy of lithospheric material at
655 the step partially counteracts shear-driven upwelling: at times, upwelling velocities at
656 depth are reduced in comparison to cases where buoyancy is not considered (Figure S6).

657 In 3-D, we find that the distribution of lithospheric steps and their relative orien-
658 tation exert a key control on the system's dynamics: edge-driven cells at steps that are
659 in close proximity can coalesce and, thereby, enhance and localise upwelling flow, with
660 our models yielding upwelling velocities that are up to $\sim 70\%$ higher than would oth-
661 erwise be the case – this corroborates the conclusions of Davies and Rawlinson (2014).
662 In addition, cells are strongly sensitive to the orientation of background mantle flow. Con-
663 sistent with our 2-D results, we find that edge-driven upwelling currents are strength-

664 ened through SDU where asthenospheric mantle flows away from the continent, but are
665 suppressed where the asthenosphere flows toward the continent. Moreover, where asthenospheric
666 flow is parallel to a lithospheric step, the modulation of edge-driven instabilities
667 by asthenospheric shear does not strongly affect melting. We emphasise, however, that
668 this may not be the case with more vigorous asthenospheric flow than examined herein.
669 Our results demonstrate that, although lithospheric steps are an essential prerequisite
670 for the development of edge-driven cells, the orientation and strength of asthenospheric
671 flow determines whether or not these cells can form, their spatial extent and, ultimately,
672 the location and degree of decompression melting. As an example, even though the struc-
673 ture of the indent is consistent across all 3-D cases examined, the orientation of the ve-
674 locity field, relative to the continent, either promotes or impedes magmatism, leading
675 to an order of magnitude variation in cumulative melt production at the indent's lower-
676 left corner (Table 3).

677 The strong sensitivity of EDC and the associated melting to asthenospheric flow
678 has important implications for our understanding of spatial and temporal patterns of intra-
679 plate volcanism at lithospheric steps. Importantly, our results imply that magmatism,
680 generated in the presence of SDU, should be shorter-lived than that induced by EDC,
681 given that increased shear at the LAB delays the development of secondary instabilities,
682 which thin overlying lithosphere and, thus, prolong decompression melting. In addition,
683 we find that magmatism induced by SDU is displaced further away from lithospheric steps,
684 in the direction of asthenospheric shear. In Earth's vigorously convecting mantle, asthenospheric
685 flow directions and magnitudes are likely to be time-dependent (e.g. Coltice et
686 al., 2018; Iaffaldano et al., 2018; Coltice et al., 2019), with a strong sensitivity to changes
687 in plate motion (e.g. Müller et al., 2016) and the shallow Poiseuille component of man-
688 tle flow (e.g. Phipps Morgan et al., 1995; Höink et al., 2011; Stotz et al., 2017, 2018).
689 Our simulations suggest that these changes in asthenospheric flow directions and mag-
690 nitudes will strongly modulate edge-driven cells and the associated magmatism. To il-
691 lustrate this further, in Figure S11 we present results from an additional 3-D simulation,
692 where the direction of plate motion and asthenospheric shear is rotated by 90° after 16 Myr.
693 Under such a scenario, edge-driven flow and the associated magmatism could be enhanced,
694 reduced or even suppressed, within only a few million years of the plate motion change,
695 at any given location along a lithospheric step. In particular, an edge that was originally
696 orientated parallel to asthenospheric mantle flow records a clear and substantial increase
697 (decrease) in melt production as it has transitioned to a trailing (leading) edge. We note
698 that these trends are visible in our melting diagnostics within only a few million years
699 of the plate motion change (Figure S11b-c). It is noteworthy that the original leading
700 edge does not display a substantial increase in melt production following the plate mo-
701 tion change, suggesting a longer lag for steps dominated by downwelling currents prior
702 to a change in the asthenospheric flow direction, thus pointing towards a history depen-
703 dence in the system. The history of mantle flow, therefore, becomes important to un-
704 derstanding why specific locations generate magmatic trends that deviate from their ex-
705 pected behaviour based upon present-day estimates of lithospheric geometries, plate mo-
706 tion and asthenospheric flow directions. This reinforces the notion that volcanic provinces
707 likely controlled by EDC and SDU will be comparatively short lived and time-dependent.
708 We note that these mechanisms are in addition to those identified in previous studies
709 that lead to a periodicity in edge-driven melting (e.g. Kaislaniemi & van Hunen, 2014).

710 Our study builds on and complements previous studies, for example, Till et al. (2010)
711 and Davies and Rawlinson (2014), by (i) examining the interaction between EDC and
712 asthenospheric shear over a wider range of asthenospheric flow intensities, distributions
713 and orientations; (ii) examining more complex lithospheric structures and step geome-
714 tries in 3-D, which allow for the coalescence and localisation of upwelling; (iii) incorpo-
715 rating an improved treatment of mantle melting that accounts for melt history using La-
716 grangian particles; and (iv) accounting for the time-dependence of these systems, which
717 differs from the instantaneous flow models of Davies and Rawlinson (2014). Nonethe-

718 less, consistent with these, and other, studies, our results support EDC and SDU as vi-
 719 able mechanisms for intra-plate volcanism in the vicinity of lithospheric steps, particu-
 720 larly where the geometry, material properties and orientation of these steps, relative
 721 to each other and asthenospheric mantle flow, are favourable. Over 15 Myr of model evo-
 722 lution, our simulations neglecting the role of asthenospheric shear predict melt thicknesses
 723 of up to 0.20 km adjacent to continental margins, up to 0.47 km at an indent’s inner corner,
 724 and 0.70 km inside the anomalous continental trough of our more complex LAB case
 725 (Table 3). When asthenospheric flow is incorporated, trailing edges, where the astheno-
 726 sphere flows away from the continent, record up to 0.35 km, while production at the indent’s
 727 inner corners increases up to 0.81 km. Although melt volumes recorded adjacent
 728 to the indent’s inner corners are reasonably consistent for all cases that neglect astheno-
 729 spheric flow ($\sim 3000 \text{ km}^3$), they are strongly modulated by the orientation of astheno-
 730 spheric flow when it is present: up to $\sim 8100 \text{ km}^3$, within an area of $\sim 21,100 \text{ km}^2$ (Ta-
 731 ble 3), is predicted for the 3-D oblique case over 15 Myr of model evolution. Such a vol-
 732 ume corresponds to a mean magmatic production rate of $\sim 0.54 \text{ km}^3 \text{ kyr}^{-1}$. We note that
 733 these rates are further modulated by secondary instabilities.

734 Our predicted melt volumes and melting rates suggest that, in isolation, EDC and
 735 SDU are suitable mechanisms only for Earth’s lower-volume intra-plate volcanic provinces.
 736 Taking into account the sensitivity of melting to the thickness of the overlying lid (Fig-
 737 ure 6c), the composition and water content of upper-mantle rocks, in addition to the po-
 738 tential impact of rheological uncertainties in our models (as indicated by different melt-
 739 ing rates in our diffusion versus composite viscosity models), our results suggest that EDC

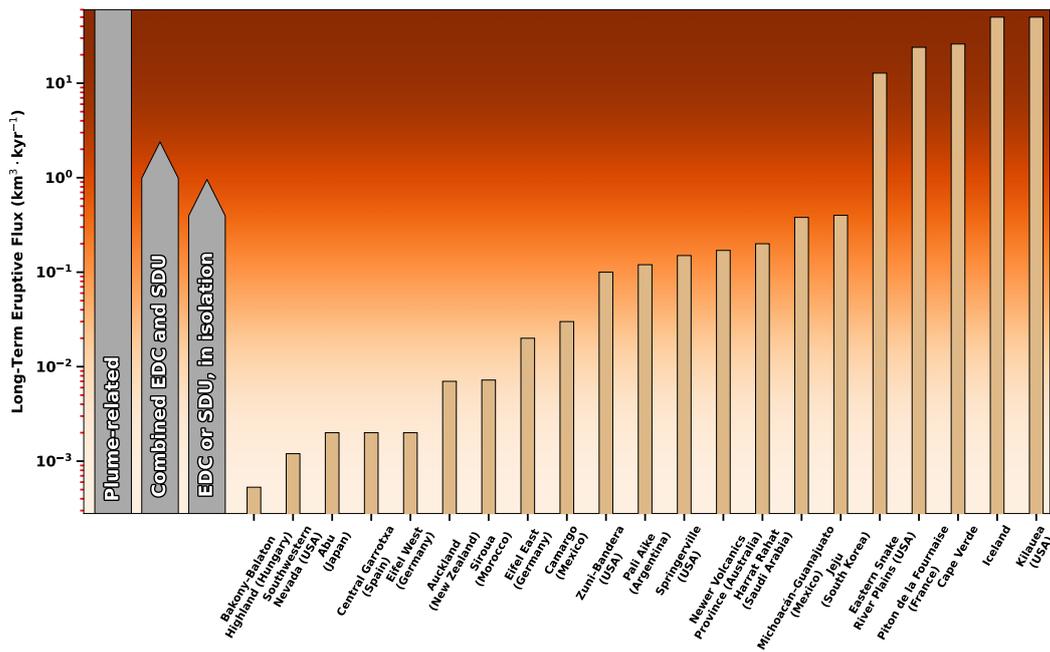


Figure 12. Long-term eruptive flux for a selection of intra-plate volcanic fields (building on van den Hove et al., 2017). Vertical grey arrows indicate the expected long-term flux that can be accounted for by given melt-generating mechanisms; we infer that mantle plumes are required to explain the largest fluxes observed. Values for province fluxes are taken from van den Hove et al. (2017), or as follows: Kilauea (Dvorak & Dzurisin, 1993), Iceland (Thordarson & Höskuldsson, 2008), Piton de la Fournaise (Roult et al., 2012), Cape Verde (Holm et al., 2008), Siroua (Missenard & Cadoux, 2012).

740 or SDU, in isolation, can account for magmatic production rates of up to $\sim 1 \text{ km}^3 \text{ kyr}^{-1}$,
 741 whilst EDC enhanced by SDU should sustain up to $\sim 2.5 \text{ km}^3 \text{ kyr}^{-1}$, the latter value be-
 742 ing a simple $\times 2.5$ increase as deduced from Table 3. Accordingly, such shallow processes
 743 cannot explain, for example, eruptive rates at Earth’s largest intra-plate volcanic provinces,
 744 including the Hawaiian Ridge, Iceland, Reunion and Cape Verde, where effusion rates
 745 exceed $10 \text{ km}^3 \text{ kyr}^{-1}$ (e.g. Dvorak & Dzurisin, 1993; Thordarson & Höskuldsson, 2008;
 746 Holm et al., 2008; Roult et al., 2012). However, as illustrated in Figure 12, the magmatic
 747 rates predicted herein are comparable to those determined from field observations at a
 748 number of Earth’s smaller intra-plate volcanic provinces, including the Newer Volcanics
 749 Province of Victoria and South Australia, the old Springerville volcanic field within the
 750 Southern Colorado Plateau, and the Siroua volcanic field of the Moroccan Atlas Moun-
 751 tains, all of which lie in close proximity to step-changes in lithospheric thickness and ex-
 752 hibit a long-term eruptive flux smaller than $0.2 \text{ km}^3 \text{ kyr}^{-1}$ (e.g. Condit et al., 1989; Mis-
 753 senard & Cadoux, 2012; van den Hove et al., 2017; Cas et al., 2017).

754 It is important to emphasise that such comparisons should be nuanced and are in-
 755 dicative only. Firstly, our models yield magmatic fluxes at depth, whereas observations
 756 focus on eruptive fluxes at the surface. In addition, many of our chosen model param-
 757 eters may not be appropriate at a given location. For example, in our 3-D simulations,
 758 we set the initial depth of oceanic lithosphere to $\sim 90 \text{ km}$, which increases over time through
 759 thermal diffusion – most of the aforementioned provinces are located above thinner litho-
 760 sphere, which would increase predicted melting rates and volumes (e.g. Davies & Rawl-
 761 inson, 2014; Priestley et al., 2018). Furthermore, all numerical models have limitations,
 762 and some of our model assumptions may influence results. In particular:

- 763 1. In our melting calculations, for simplicity, we assume a peridotitic composition –
 764 magmatism may be locally enhanced (or reduced) through the presence of more
 765 enriched (or depleted) compositions. Furthermore, we assume a wet peridotite batch
 766 melting parameterisation and make no attempt to simulate the dynamics of melt
 767 transport and extraction. Whilst melt extraction has been considered in other mod-
 768 elling studies (e.g. Ballmer et al., 2011; Jain et al., 2019), the strategies used to
 769 model this process remain under development, particularly in the context of single-
 770 phase Stokes flow.
- 771 2. Although our models capture the effect of latent heating, they do not include di-
 772 rect feedbacks between melting and key material properties, such as density and
 773 viscosity. The low melting rates observed in our simulations, however, suggest that
 774 such feedbacks will have only a minor impact on our model predictions.
- 775 3. We model the continent as a rigid and viscous block, that is not dramatically im-
 776 pacted by edge-driven processes. It is possible that parts of the continental edge
 777 behave weakly, modifying the edge-driven process and associated melting (e.g. Liu
 778 & Chen, 2019).
- 779 4. Our study has focused on simulations with short evolution times, to isolate the
 780 sensitivity of EDC and SDU to the controlling parameters examined. In reality,
 781 lithospheric steps, particularly those at cratonic margins, are likely long-lived (e.g.
 782 Hoggard et al., 2020). Simulations with longer evolution times develop secondary
 783 instabilities that make it more challenging to isolate the signals highlighted herein.
 784 However, as illustrated in Figure S12 which compares both flow dynamics and melt-
 785 ing patterns for Case U400 after 15 Myr and 30 Myr, the first order trends that
 786 we predict should remain consistent, with melting enhanced within the indent rel-
 787 ative to external steps.
- 788 5. The strength and scale of edge-driven cells in our simulations is strongly depen-
 789 dent on the magnitude and depth-dependence of viscosity, which remain uncer-
 790 tain (e.g. Korenaga & Karato, 2008; Paulson & Richards, 2009; Iaffaldano & Lam-
 791 beck, 2014; Rudolph et al., 2015). Nonetheless, we have examined the sensitivity

of our results under a range of different scenarios, all of which are within the estimated range (e.g. Iaffaldano & Lambeck, 2014; Lau et al., 2016).

6. We neglect other important aspects of mantle convection, including compressibility, phase transitions, global mantle flow and the impact of mantle plumes (e.g. Tackley et al., 1993; Gassmüller et al., 2020).

Each of these points requires further investigation to quantify their effect on the flow field and associated melting diagnostics. Nonetheless, our results suggest that EDC and SDU are capable of generating magmatic rates of $0.1\text{-}2.5\text{ km}^3\text{ kyr}^{-1}$ under favourable conditions. As illustrated in Figure 12, this is compatible with eruptive rates determined for a number of intra-plate volcanic provinces on Earth that lie adjacent to step-changes in lithospheric thickness, supporting EDC and SDU as viable mechanisms. At other provinces, where substantially enhanced melting rates are measured, alternative mechanisms, such as mantle plumes, are likely more applicable. Additionally, there is increasing evidence that the shallow mechanisms examined herein interact with upwelling mantle plumes at some locations to produce complex volcanic patterns at the surface (e.g. Davies et al., 2015; Rawlinson et al., 2017; Kennett & Davies, 2020). Understanding these interactions is an important avenue for future research.

5 Conclusion

This study systematically documents the behaviour of EDC and SDU in 2-D and 3-D geodynamical models. Our 2-D simulations demonstrate that EDC, which results from the negative buoyancy of lithospheric mantle adjacent to a rigid continental block at a lithospheric step, is sensitive to the geometry and material properties of that step, in addition to the upper mantle viscosity profile – given sufficient space, EDC cells can develop at viscosities below 10^{20} Pa.s. Furthermore, we have highlighted how EDC can be enhanced, suppressed or, under certain conditions, completely eclipsed by SDU.

By examining the interaction between EDC and SDU in 3-D, we have demonstrated that edge-driven cells developing at adjacent lithospheric steps can modulate each other to enhance and localise upwelling. Additionally, flow in the asthenosphere can either intensify or weaken edge-driven upwellings, depending on the intensity of asthenospheric currents and their orientation relative to the moving continent. In our models, these flow patterns control the observed melting trends: increased melting occurs at locations of intense upwelling. Our predicted melt volumes suggest that, in the absence of potential interactions with mantle plumes, EDC and SDU are viable mechanisms only for Earth’s shorter-lived and lower-volume intra-plate volcanic provinces. Altogether, our results illustrate the importance of local variations in lithospheric thickness and the orientation and magnitude of asthenospheric flow in controlling the location and timing of EDC and SDU-generated intra-plate volcanism. Most importantly, although changes in lithospheric thickness provide a favourable setting for EDC, edge-driven cells can be enhanced, displaced or overwhelmed by asthenospheric flow. As such, our study helps to explain why step changes in lithospheric thickness, which are common along cratonic edges and passive margins, only produce volcanism at isolated points in space and time.

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842 was used for the simulations presented herein, has been archived at Zenodo (Kramer et
 843 al., 2021). Similarly, example input files required to reproduce the simulations presented
 844 herein have been made available (Duvernay, 2021). The authors are grateful to two anony-
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 849 ures have been prepared using Matplotlib, ParaView and Inkscape.

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Supporting Information for ‘Linking Intra-Plate Volcanism to Lithospheric Structure and Asthenospheric Flow’

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Thomas Duvernay¹, D. Rhodri Davies¹, Christopher R. Mathews¹, Angus H.

Gibson¹, Stephan C. Kramer²

¹Research School of Earth Sciences, The Australian National University, Canberra, ACT, Australia

²Department of Earth Science and Engineering, Imperial College London, London, UK

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Corresponding author: Thomas Duvernay, Research School of Earth Sciences, The Australian National University, 142 Mills Rd, Acton ACT 0200, Australia. (thomas.duvernay@anu.edu.au)

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Melting Parameterisation

McKenzie (1984) defined a framework to calculate the amount of melt produced through decompression at constant entropy. Writing the total differential of entropy as a function of temperature, pressure and melt fraction, the following two governing equations are obtained:

$$\left. \frac{dF}{dP} \right|_S = \frac{-\frac{c_P dT}{T dP} \Big|_F + \frac{\alpha_s}{\rho_s} + F \left(\frac{\alpha_f}{\rho_f} - \frac{\alpha_s}{\rho_s} \right)}{\Delta S + \frac{c_P dT}{T dF} \Big|_P}, \quad (1)$$

$$\left. \frac{dT}{dP} \right|_S = \frac{\frac{\alpha_s}{\rho_s} + F \left(\frac{\alpha_f}{\rho_f} - \frac{\alpha_s}{\rho_s} \right) - \Delta S \left. \frac{dF}{dP} \right|_S}{\frac{c_P}{T}}. \quad (2)$$

In the above expressions, P , T and F represent the pressure, temperature and fraction of melt, respectively. The coefficient of thermal expansion, density and the specific heat at constant pressure are denoted by α , ρ and c_P , while S corresponds to entropy and ΔS to the entropy of fusion. Subscripts s and f differentiate between the solid and fluid phase, respectively, while derivative sub-scripts indicate variables that are held constant.

In the absence of melting, Equations 1 and 2 become:

$$\left. \frac{dF}{dP} \right|_S = 0, \quad (3)$$

$$\left. \frac{dT}{dP} \right|_S = \frac{\alpha_s T}{\rho_s c_P}. \quad (4)$$

In particular, Equation 4 represents the temperature change of a parcel of rock ascending adiabatically through Earth's mantle. However, in our numerical models, we can already calculate a temperature change as we are solving the heat equation for temperature. To ensure consistency between the evolution of temperature obtained through the melting

framework and the thermal state of our model, we modify the framework's governing equations: we replace the adiabatic gradient term by the actual temperature gradient derived from the temperature field calculated by Fluidity. Mathematically, using thermodynamical identities, our modification translates to

$$\frac{\alpha}{\rho} = - \left. \frac{dS}{dP} \right|_T = \left. \frac{dS}{dT} \right|_P \left. \frac{dT}{dP} \right|_S \sim \frac{c_P}{T} \left. \frac{dT}{dP} \right|^{Fluidity},$$

and, in the absence of melting, it leads to

$$\left. \frac{dT}{dP} \right|_S \sim \left. \frac{dT}{dP} \right|^{Fluidity}.$$

Incorporating this change within Equations 1 and 2, we obtain the following system of coupled equations:

$$\left. \frac{dF}{dP} \right|_S = \frac{\left. \frac{dT}{dP} \right|^{Fluidity} - \left. \frac{dT}{dP} \right|_F^{Katz}}{\frac{T\Delta S}{c_P} + \left. \frac{dT}{dF} \right|_P^{Katz}} \quad (5)$$

$$\left. \frac{dT}{dP} \right|_S = \left. \frac{dT}{dP} \right|^{Fluidity} - \frac{T\Delta S}{c_P} \left. \frac{dF}{dP} \right|_S. \quad (6)$$

In the above expressions, derivative super-scripts signal where the expression/value for the derivative is sourced from.

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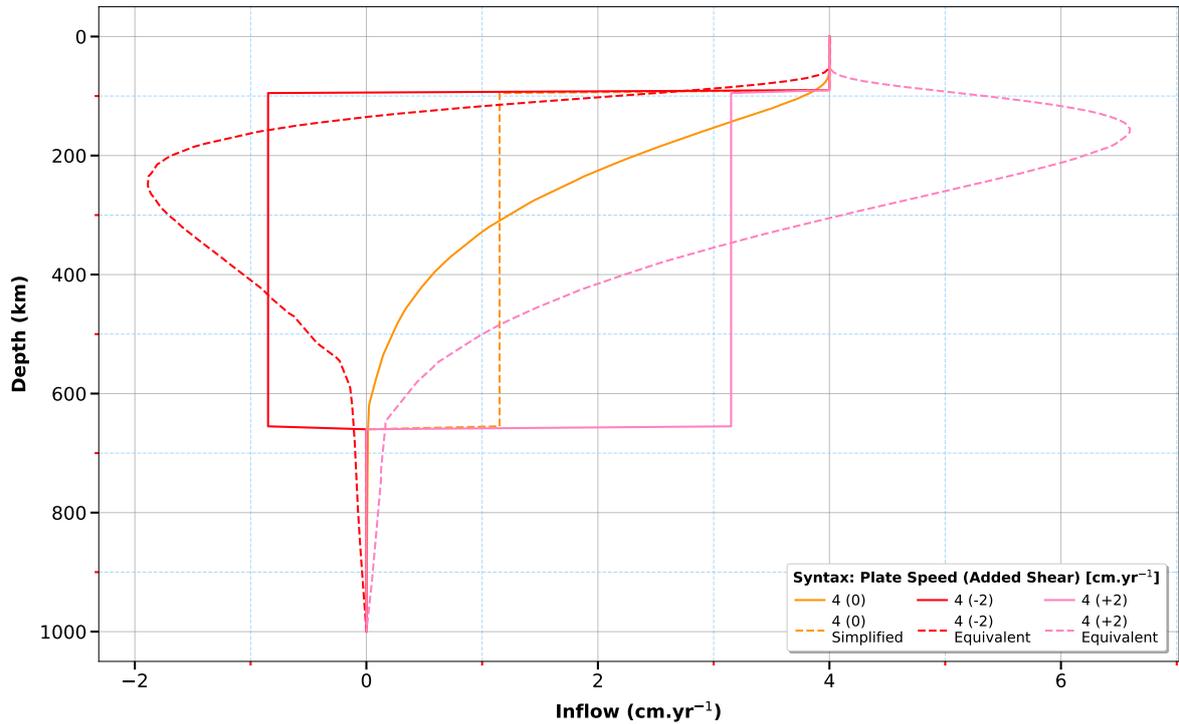


Figure S1. Velocity inflow profiles considered in the study (solid lines) and their counterparts used to demonstrate equivalent flow patterns (dashed lines). The ‘4 (0)’ profile is measured within the oceanic realm of the purely plate-driven model. The ‘4 (0) Simplified’ profile corresponds to a step-like version of the ‘4 (0)’ profile, with plate velocity imposed from the surface down to 90 km (our initial LAB), constant velocity imposed within the asthenosphere (where the integral of velocity is identical to the ‘4 (0)’ profile over this depth range), and zero flow imposed in the lower mantle. Profiles ‘4 (-2)’ and ‘4 (+2)’ build on the ‘4 (0) Simplified’ profile by adding 2 cm yr⁻¹ asthenospheric shear, either aligned with (+2) or opposite to (-2) plate motion. Profiles ‘4 (-2) Equivalent’ and ‘4 (+2) Equivalent’ are measured within the oceanic realm, from simulations where the ‘4 (-2)’ and ‘4 (+2)’ profiles are imposed at the inflow boundary.

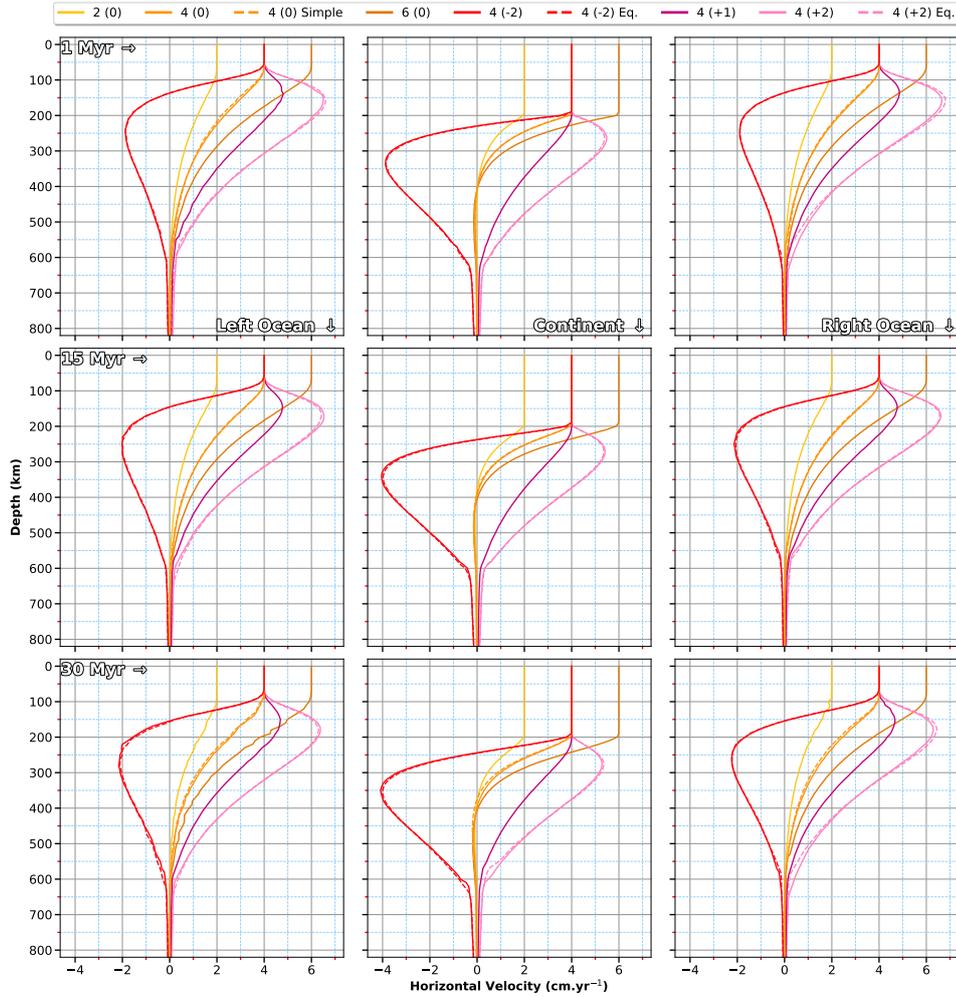


Figure S2. Velocity profiles generated within the numerical domain when plate motion and, in some cases, additional asthenospheric shear, are prescribed. Specifically, the profiles displayed in Figure S1 are prescribed as inflow boundary conditions for different models, in addition to cases with increased ($6 (0)$) or decreased ($2 (0)$) plate velocities. The resulting flow field is sampled below oceanic lithosphere to the left of the continent (left), below the continent (centre) and below oceanic lithosphere to the right of the continent (right). Additionally, different rows display profiles measured at 1 Myr, 15 Myr and 30 Myr, respectively. We find that cases where simplified step-function profiles are imposed at the inflow boundary yield results that are practically indistinguishable from the smoother profiles. This demonstrates that results are largely insensitive to the depth-dependence of the inflow profile prescribed within the asthenosphere – the flow is redistributed in line with the underlying physics.

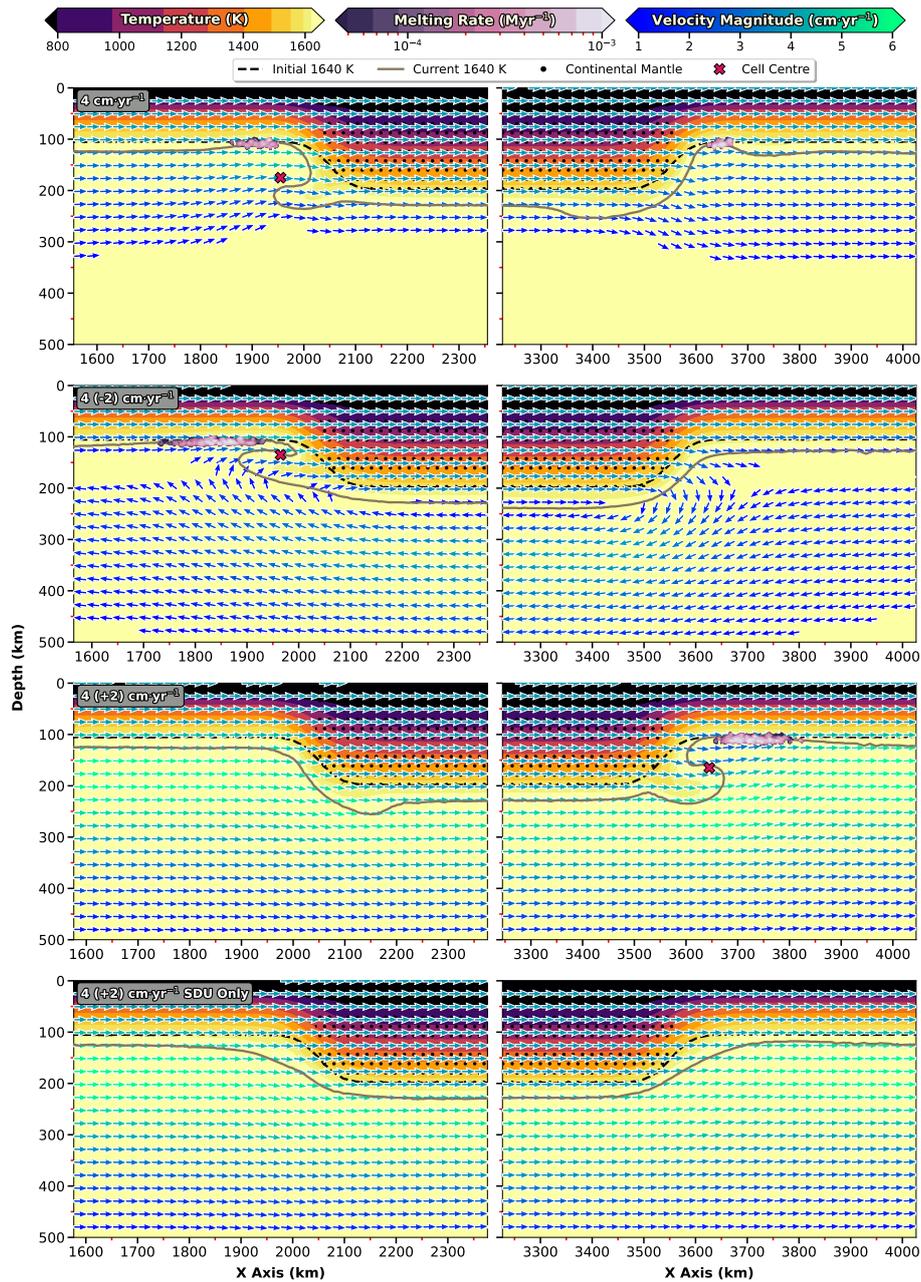


Figure S3. Effect of plate motion and asthenospheric flow on dynamics adjacent to lithospheric steps. The top row illustrates our 4 cm yr^{-1} purely plate-driven scenario, while the subsequent two rows display results following the addition of momentum within the asthenosphere, opposite to and aligned with plate motion, respectively. The bottom row is equivalent to the third row, except that the coefficient of thermal expansion has been set to 0; all models are displayed after 20 Myr. Graphic illustration similar to Figure 4, with glyphs only drawn where velocities exceed 1 cm yr^{-1} ; the velocity field is that directly output from the model.

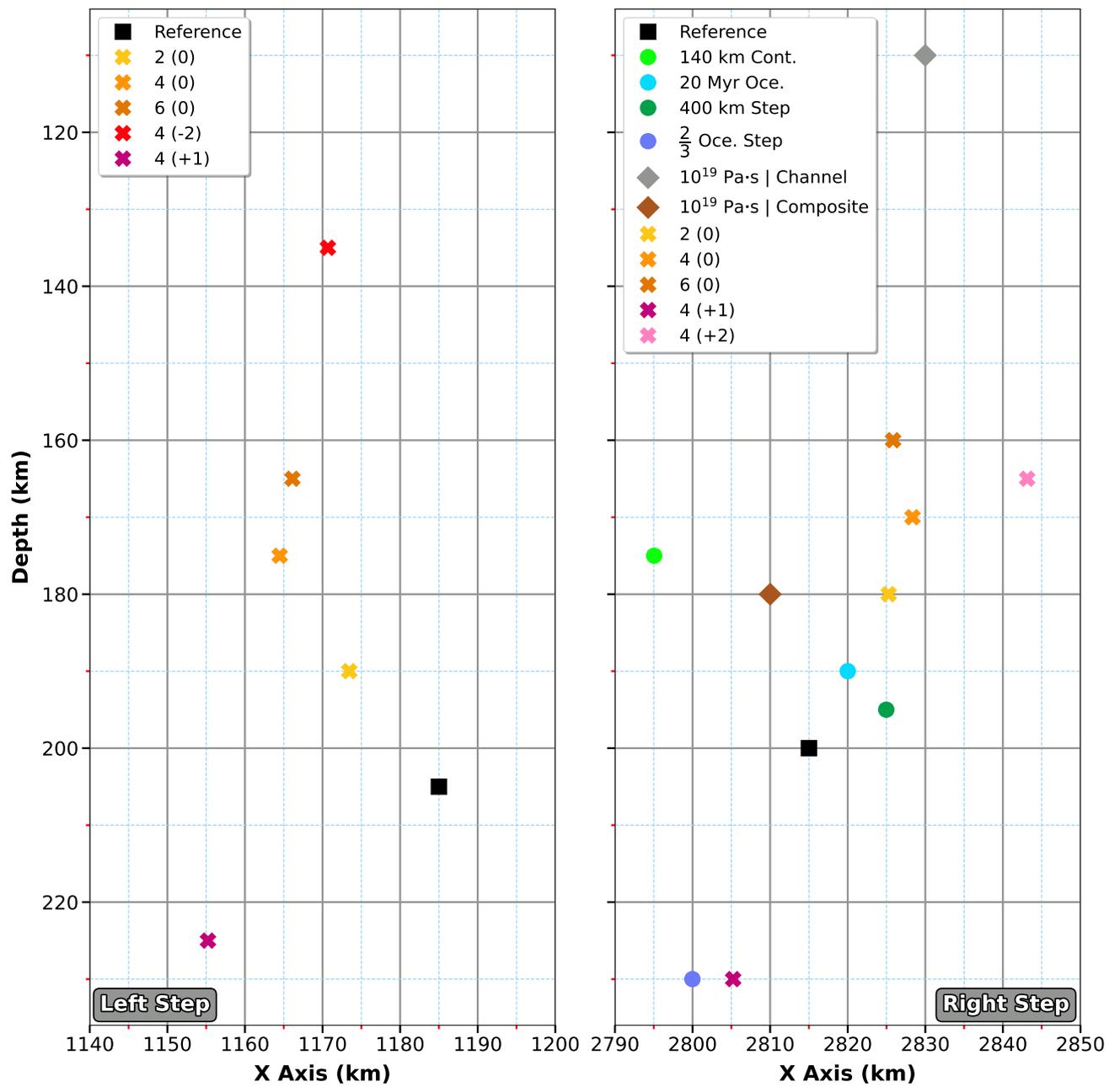


Figure S4. Location of cell centres used as a basis for vertical velocity profiles in Figure 5, determined at the time of maximum downwelling velocity as illustrated in Figure S5. Cases with plate motion are corrected for plate advection through time.

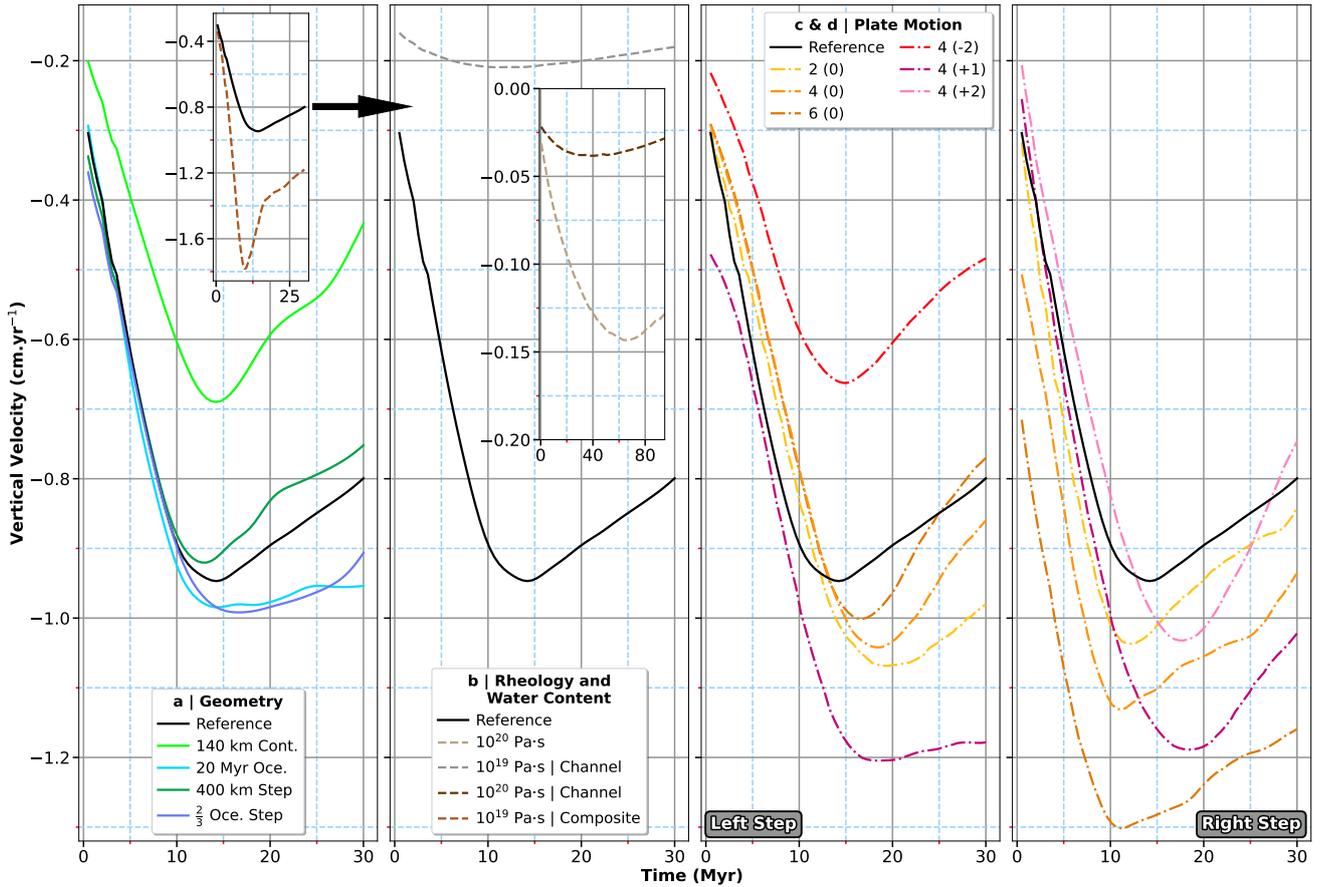


Figure S5. Maximum downwelling velocity, as a function of time, at the right step (if not specified). The velocity field is analysed over an area surrounding the step, no deeper than continental depth. Each curve has a local minimum, which we use to determine the time at which we compare the vigour of edge-driven instabilities cases across our chosen parameter space (Figure 5). Such a strategy allows for a meaningful comparison between different cases. (a) Effect of step geometry. The inset compares the reference case to the composite rheology model and, therefore, belongs with the cases shown on panel b as indicated by the black arrow. (b) Role of viscosity. The inset corresponds to a zoom on the 10²⁰ Pa-s cases, with a similar aspect ratio as the original panel. (c) & (d) Influence of plate motion and asthenospheric shear.

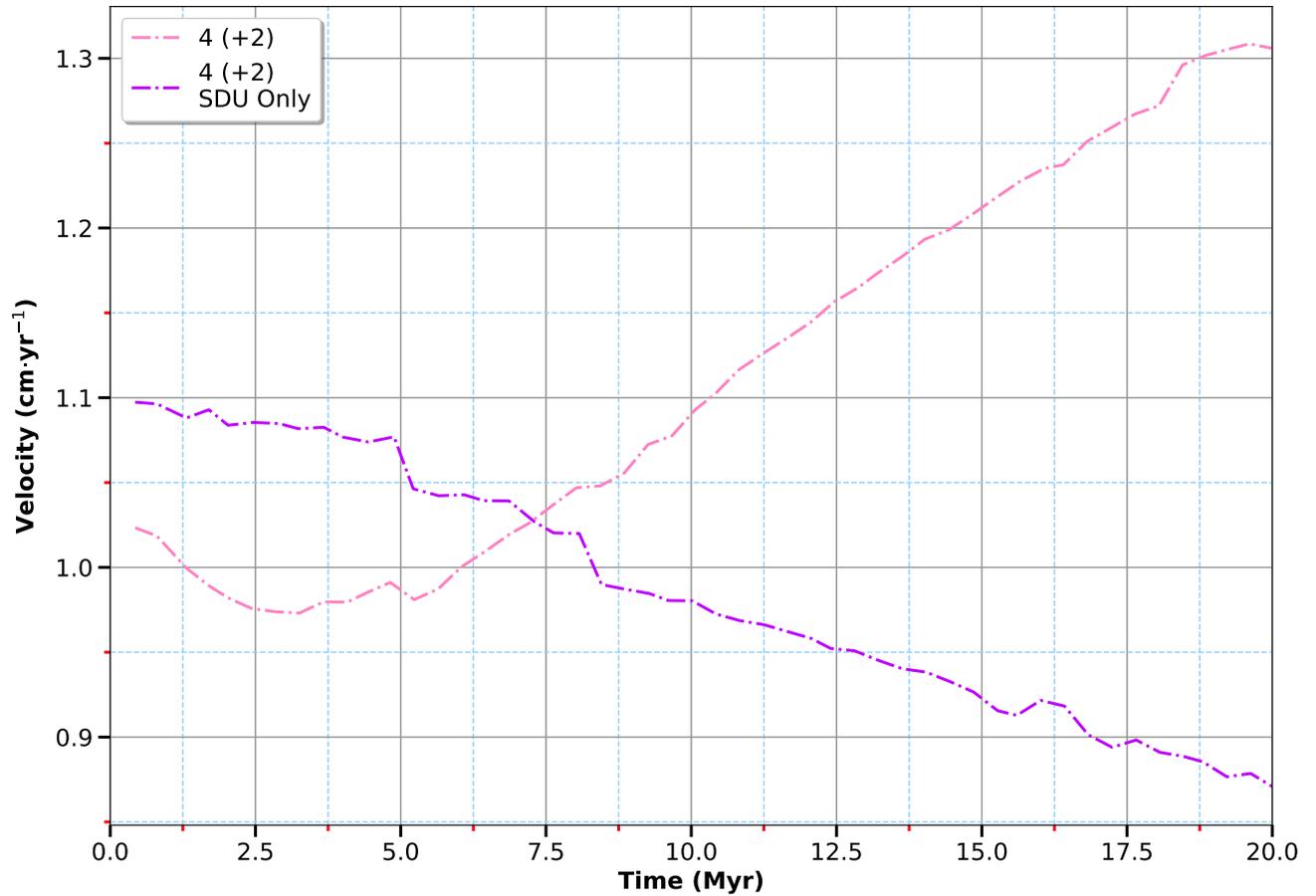


Figure S6. Temporal evolution of the maximum upwelling velocity recorded at the right step for cases with additional asthenospheric shear of 2 cm yr^{-1} prescribed at the inflow boundary. Case ‘4 (+2)’ incorporates both EDC and SDU mechanisms, while case ‘4 (+2) SDU Only’ solely features SDU (the coefficient of thermal expansion is set to 0).

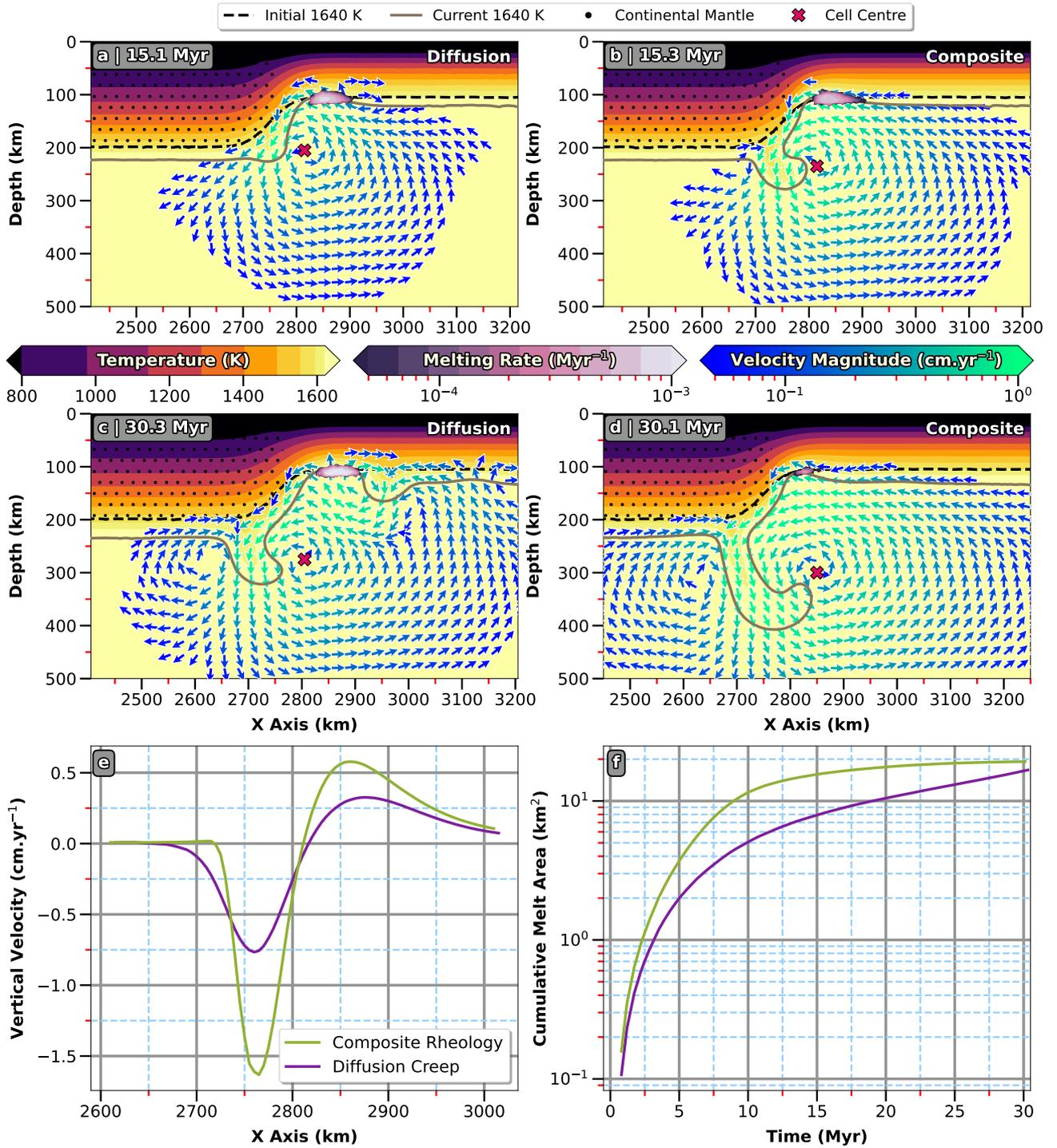


Figure S7. Dynamics (a-e) and melt production (f) compared between the reference case (a & c) and the model incorporating a composite rheology (b & d).

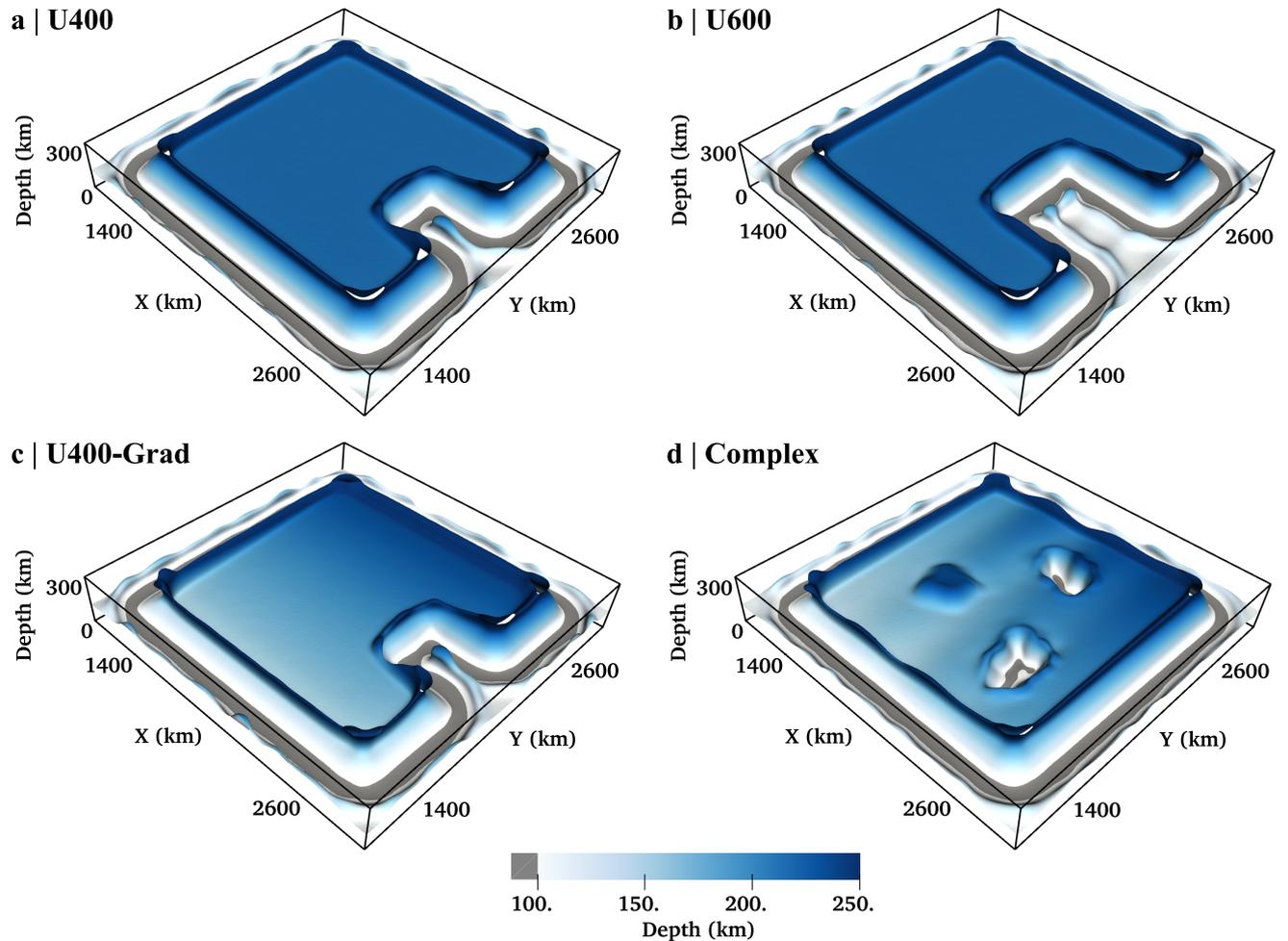


Figure S8. Topography at the LAB, as delineated by the 1620 K isotherm, for continental geometries used in 3-D simulations. Cases are illustrated after 30 Myr of model evolution. (a) Case U400. (b) Case U600. (c) Case U400-Grad. (d) Case Complex.

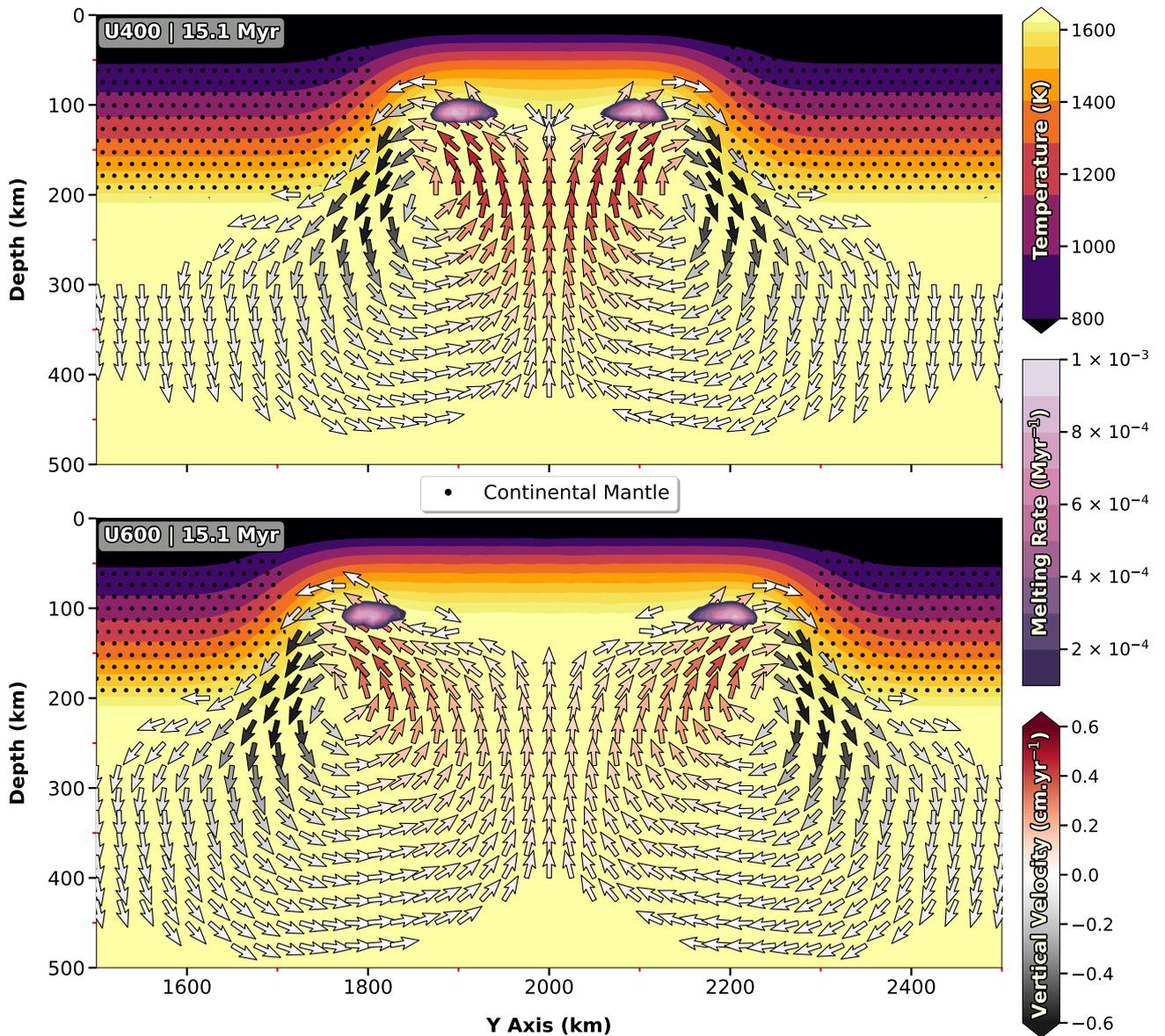


Figure S9. Influence of the indent’s width on the flow dynamics, as observed after 15 Myr. Background colours represent temperature. Black dots depict the location of continental mantle. Arrow glyphs illustrate the velocity field and their colour indicates the strength of flow. Areas experiencing melting are represented as a superimposed surface, coloured by melting rate.

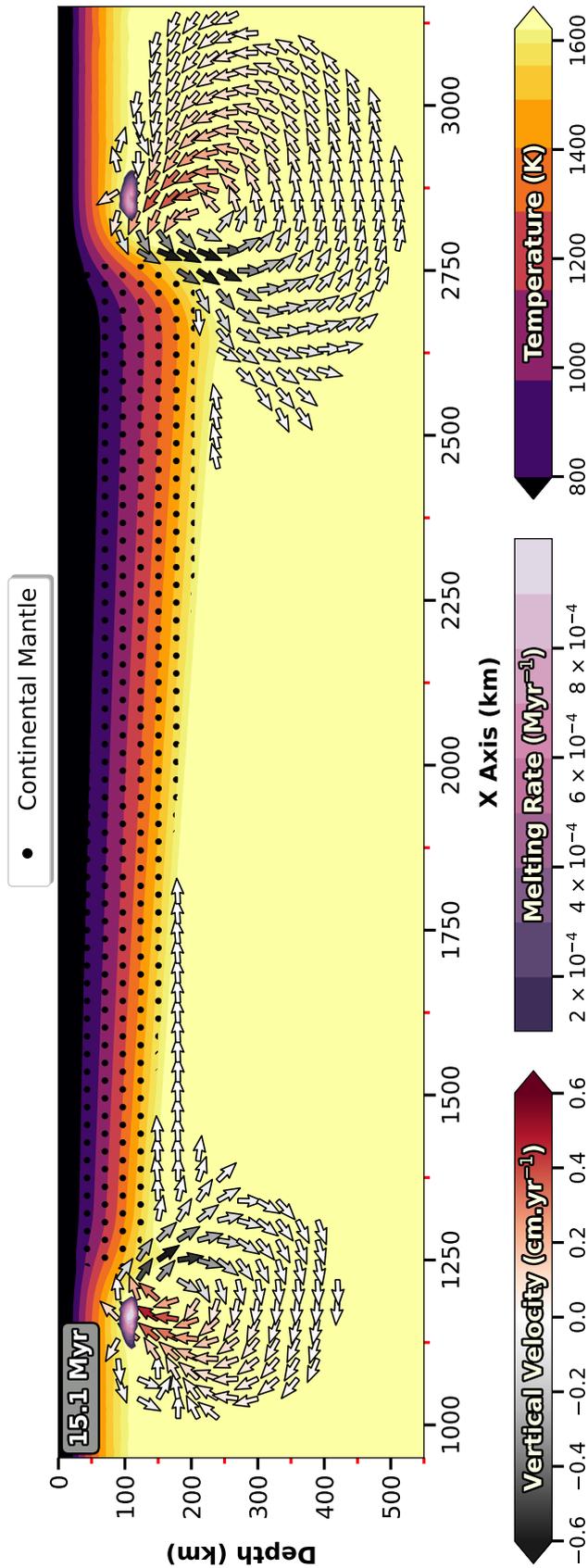


Figure S10. Effect of continental thickness on edge-driven cell development, as observed after 15 Myr for Case U400-Grad. Background colours represent temperature. Black dots depict the location of continental mantle. Arrow glyphs illustrate the velocity field and their colour indicates the strength of the flow. Particles that record active melting are represented by a superimposed surface, coloured by melting rate.

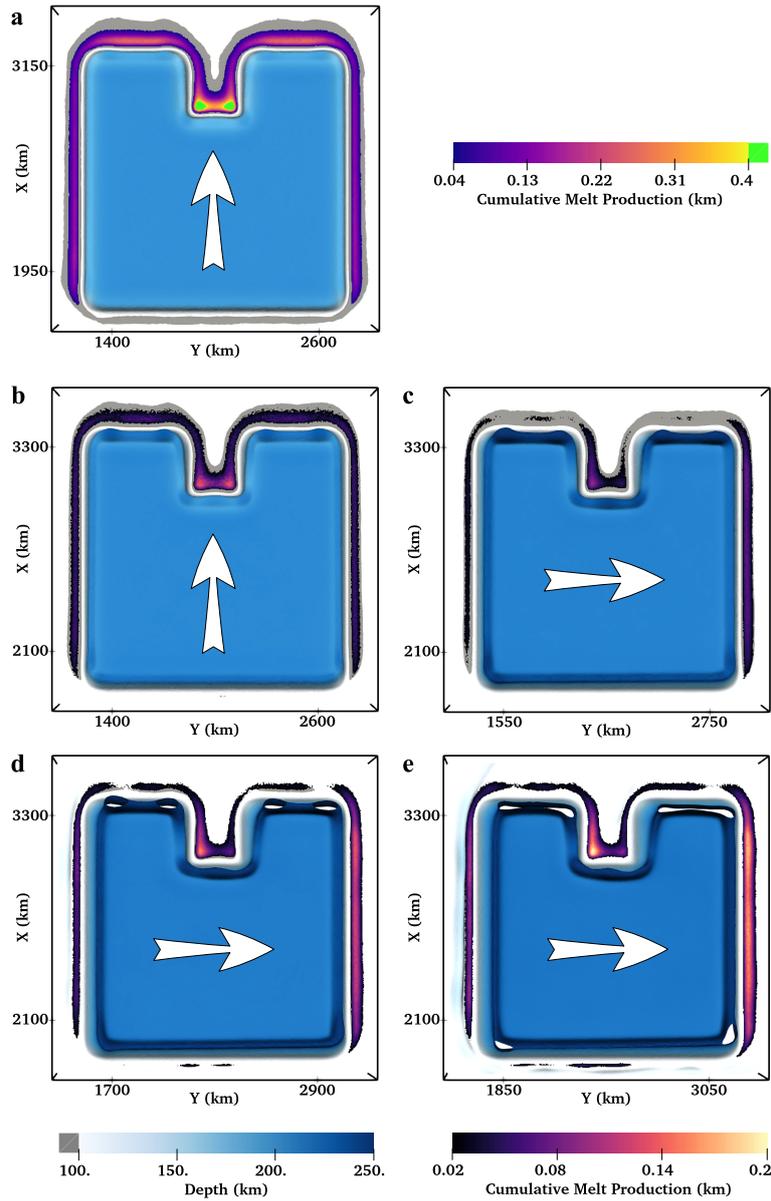


Figure S11. Melt production around the continent following a 90° change in prescribed plate motion and inflow direction at 16 Myr for the positive-x model. Large white arrows represent both the direction of plate motion and the direction of asthenospheric flow relative to the continent, and point from the continent's leading edge to its trailing edge. (a) Cumulative melt production after 12 Myr. (b) Cumulative melt production between 12 Myr and 16 Myr. (c) Cumulative melt production between 16 Myr and 20 Myr (i.e. immediately following the change in imposed flow direction). (d) Cumulative melt production between 16 Myr and 24 Myr. (e) Cumulative melt production between 16 Myr and 28 Myr.

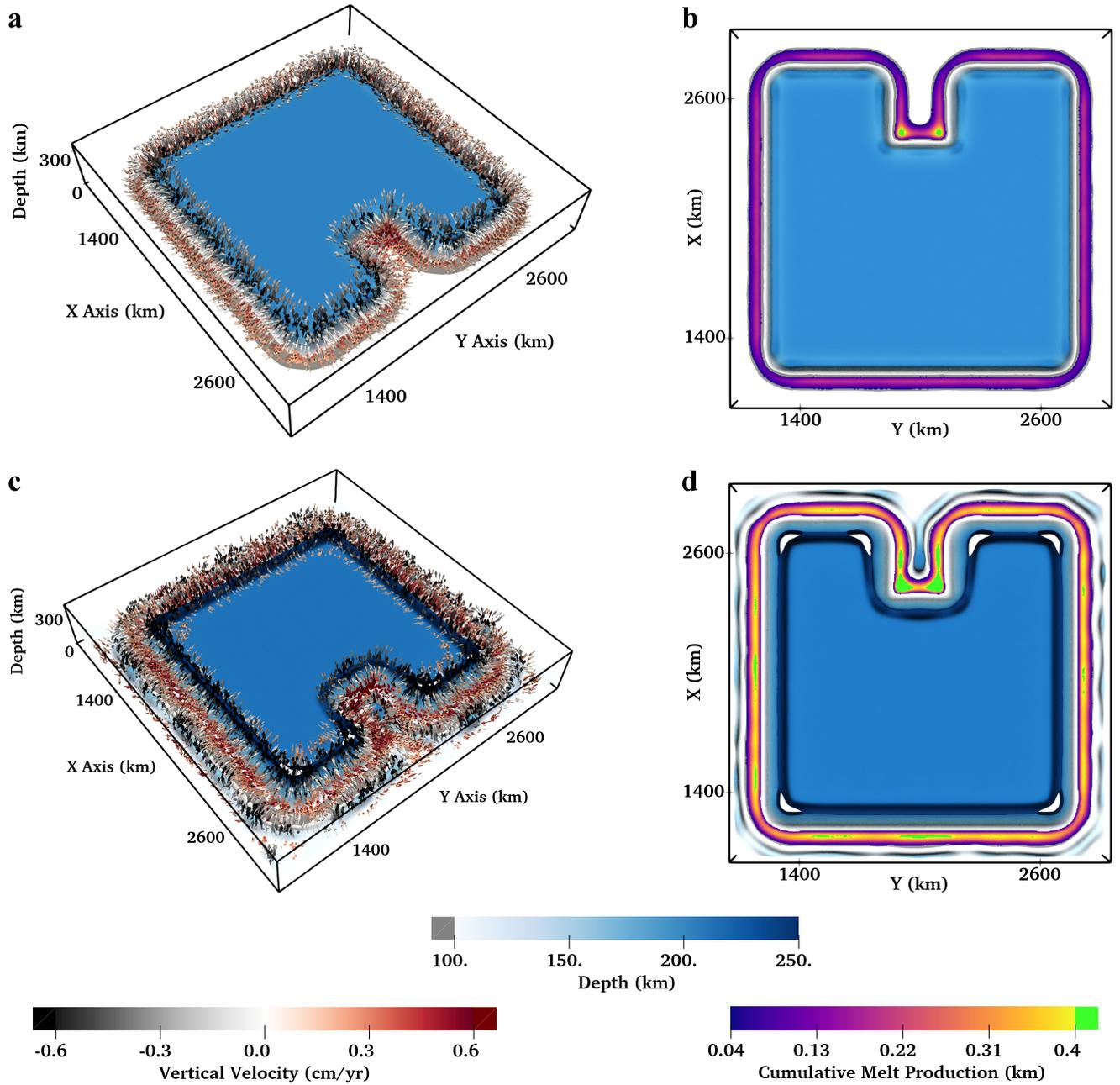


Figure S12. Comparison of the flow dynamics and melt production adjacent to the continent over time for Case U400. Graphic illustration is similar to Figures 7 and 8. (a) Velocity field after 15 Myr. (b) Cumulative melt production after 15 Myr. (c) Velocity field after 30 Myr. (d) Cumulative melt production after 30 Myr.