

Structural Nexus and Divide: the Western Tauern Window, Eastern Alps

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November 22, 2022

Abstract

The western Tauern Window of the Eastern Alps constitutes a mature transpressive wrench zone generated by Oligocene-Miocene convergence between the Dolomites Indenter and the European foreland. As a major structural divide, it translates convergence-parallel north-south shortening into convergence-perpendicular eastward lateral extrusion. About 7000 foliation, lineation, fold-axis, axial-plane, shear-zone, and shear-band measurements at ~1800 sites detail the structural geometry and evolution during indentation and transpression, modeled by numerical and analogue-material experiments. The results outline the western Tauern Window as an orogen-scale zone of localized deformation, consisting of tight, upright folds, reactivated by a sinistral shear-zone network. It connects the Giudicarie Belt southwest of the indenter salient with the Salzach-Ennstal-Mariazell-Puchberg Fault (SEMP) in the northeast. This transpressive zone has a sigmoidal vortex geometry, decoupling the Ötztal Basement in the west from the extruding wedges of the Eastern Alps in the east. Shortening was successively absorbed by nappe stacking, upright folding, and dome formation and then maintained by transpressional shearing that led to lateral extrusion, probably promoted by a change in the lithospheric configuration. The western part of the SEMP likely rotated [?]20deg clockwise around a pole approximately halfway along its entire length during the indentation.

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Key Points:

- The western Tauern Window forms a mature transpressive wrench zone with a sigmoidal vortex geometry
- The western Tauern Window links the Giudicarie Belt to the SEMP Fault, translating orogen-perpendicular shortening into -parallel extension
- The western Tauern Window decouples the Ötztal Basement in the west from the extruding wedges of the Eastern Alps in the east

Abstract

The western Tauern Window of the Eastern Alps constitutes a mature transpressive wrench zone generated by Oligocene-Miocene convergence between the Dolomites Indenter and the European foreland. As a major structural divide, it translates convergence-parallel north-south shortening into convergence-perpendicular eastward lateral extrusion. About 7000 foliation, lineation, fold-axis, axial-plane, shear-zone, and shear-band measurements at ~1800 sites detail the structural geometry and evolution during indentation and transpression, modeled by numerical and analogue-material experiments. The results outline the western Tauern Window as an orogen-scale zone of localized deformation, consisting of tight, upright folds, reactivated by a sinistral shear-zone network. It connects the Giudicarie Belt southwest of the indenter salient with the Salzach-Ennstal-Mariazell-Puchberg Fault (SEMP) in the northeast. This transpressive zone has a sigmoidal vortex geometry, decoupling the Ötztal Basement in the west from the extruding wedges of the Eastern Alps in the east.

Shortening was successively absorbed by nappe stacking, upright folding, and dome formation and then maintained by transpressional shearing that led to lateral extrusion, probably promoted by a change in the lithospheric configuration. The western part of the SEMP likely rotated 20° clockwise around a pole approximately halfway along its entire length during the indentation.

Plain Language Summary

The Alps constitute one of Earth’s best-studied continent-continent collision orogens. There, the Apulian plate, a continental sliver of the African plate, started to collide with the European plate ~ 66 million years ago. In the north, the Apulian plate has a triangular shape, the Dolomites Indenter. The Tauern Window at the tip of the Dolomites Indenter deformed stronger than its neighboring areas, exposing deeply-buried European-plate rocks that are surrounded by Apulian-plate upper crustal rocks. We studied the deformation within the western Tauern Window and found that it connects two major fault zones, i.e., the Giudicarie Belt in the southwest that accommodates orogen-perpendicular shortening, and the SEMP Fault in the northeast that accompanies orogen-parallel extension. Based on kinematic models and field data, the western SEMP Fault likely rotated clockwise 20° .

1 Introduction

Salients or oroclines (e.g., Bandar Abbas, Pamir-Hindu Kush, Hazare-Kashmir, Namche Barwa, Nanga Parbat), where promontories advance into weak crust, are studied to deduce the kinematics of indenter tectonics and the associated displacements in the lithosphere (e.g., Critelli & Garzanti, 1994; Kufner et al., 2016; Molinaro et al., 2004). Commonly observed processes are strain partitioning and localization, decoupling between tectonic blocks, deep-crustal exhumation, transpression, transtension, and slab breakoff (e.g., Chopin et al., 2012; Dewey et al., 1998; Fossen et al., 2013; Frehner, 2016; Kufner et al., 2016; Reiter et al., 2011; Reiter et al., 2018; Robin & Cruden, 1994). The structural evolution at indenter fronts has been modeled by numerical and analogue-material experiments, but controversies on the boundary conditions, reference systems and directions, and displacement amounts and rates in orogens hinder the transfer of their results to the natural systems (Burg & Podladchikov, 1999; Ratschbacher et al., 1991a, 1991b; Reiter et al., 2011; Rosenberg et al., 2004, 2007; Schueller & Davy, 2008). In addition, pre-existing anisotropies, common in orogens, may induce a structural evolution that deviates from the predicted one. Another difficulty is the quantification of shortening at the indenter fronts. Shortening in transpressional zones is often overestimated, as the wrench component of deformation remains underconsidered due to the lateral material movements out of the cross sections used to quantify the shortening (Tikoff & Peterson, 1998). To overcome this problem, we herein derive the kinematic vorticity number W_k to estimate the amounts of convergence-parallel shortening (contraction) and fold-hinge-parallel extension (stretching) based on the convergence angle, mea-

sured between the convergence direction and the active shear plane (Supporting Information Figure S1); this reflects the ratio between the simple and pure shear components of the bulk deformation (Fossen & Tikoff, 1993; Tikoff & Fossen, 1993).

We studied the western Tauern Window (TW) in front of the Dolomites Indenter in the European Alps (Figure 1a). The structural maps outline areas of dominate transpression and subordinate transtension, for example outlined by non-cylindrical folds and transecting foliations. In the field, we took foliation, lineation, fold axis, fold axial plane, shear zone, and shear band measurements. Based on their orientation, we defined five structural domains (A to E). We focus on the spatial distribution and relative temporal evolution of these structures and calculate the dihedral angles (section 4 Methods and section 5 Results) between the mean values of two distinct structures that formed in kinematic succession. We use the rotational direction of the dihedral angles (being clockwise or counterclockwise) and the kinematic vorticity number W_k to (1) deduce the kinematic connections between major fault systems, (2) discriminate between wrench-dominated and pure-shear-dominated transpressional domains, and (3) quantify the amounts of shortening and extension within the transpressional folds of the western TW. We review the existing hypotheses on the structural development of the TW and, based on our findings, modify them regarding the role of indentation, lateral extrusion, and fault linkage and rotation. Finally, we discuss the coupling between major fault zones, the decoupling of tectonic blocks, and complement the ongoing discussion about fault linkage and absolute displacements in the western TW by developing the Proto-SEMP hypothesis.

2 Geological Setting

The TW (Figure 1a) is the largest tectonic window of the Eastern Alps (Frisch, 1976), where lower plate rocks have been exhumed from >35-km-depth in the Cenozoic (e.g., Kurz et al., 2008; Selverstone & Spear, 1985; Spear & Franz, 1986). In this east-west elongate structural and metamorphic dome, the arcuate dome axis coincides with rocks recording the peak temperatures of high-grade Barrovian metamorphism (Grundmann & Morteani, 1985; Rosenberg et al., 2018; Selverstone, 1985; Schneider et al., 2015) and the youngest cooling ages (Bertrand et al., 2017; Luth & Willingshofer, 2008; Most, 2003; Rosenberg & Berger, 2009). We subdivided the TW into the eastern, central, and western sub-domes; the eastern and western sub-domes are characterized by elongate and concentric metamorphic isograd trajectories (Grundmann & Morteani, 1985; Scharf et al., 2013b) and intersecting and bordering shear zones (Figure 1a; e.g., Linzer et al., 2002; Neubauer et al., 1999; Rosenberg et al., 2004; Scharf et al., 2013a; Schneider et al., 2013). Framing shear zones are absent in the central dome; there, only structurally high nappes are exposed (e.g., Bousquet et al., 2012a; Schmid et al., 2013), partly folded into a map-scale sheet fold (Groß et al., 2020).

Two end-member models are debated for the formation of the TW. One empha-

sizes orogen-parallel, large-scale extension, exhuming the rocks of the TW along low-angle normal faults (e.g., Frisch et al., 2000; Neubauer et al., 1999), the other upright folding associated with erosional denudation (e.g., Cornelius, 1940; Laubscher, 1990). Yet, most authors agree on the activity of two kinematically-coupled processes, namely shortening due to the northward displacement of the Dolomites Indenter and eastward lateral material transport, associated with orogen-parallel extension; Ratschbacher et al. (1991a, 1991b) defined these as lateral extrusion, encompassing extension collapse, i.e., gravitational spreading of thickened and uplifted crust in an orogen, and tectonic escape. However, the amounts of shortening, displacement, and extension remain controversial (Frisch et al., 2000; Fügenschuh et al., 2012; Linzer et al., 2002; Luth et al., 2013; Neubauer et al., 1999; Pomella et al., 2011, 2012; Rosenberg & Berger, 2009; Rosenberg & Garcia, 2011, 2012; Scharf et al., 2013a; Schmid et al., 2013; Wolff et al., 2020). We contribute to this discussion with a compilation of structural measurements in the western TW to distinguish structural domains, and to assess the traces and interconnections of major shear zones.

2.1 Tectonostratigraphic Framework

Mesozoic ocean-derived and ophiolite-bearing units of the Glockner Nappe and Matreier Zone and siliciclastic rocks of the European distal margin were imbricated during European continental margin subduction (Figure 1a). The deepest structural units of the TW consist of Europe-derived, late-Variscan intrusions and their para-autochthonous, pre-Variscan host rocks covered by post-Variscan metasediments (Figure 1a), forming the Venediger Duplex, an antiformal stack generated by north-vergent nappe emplacement during the Adria-Europe collision. Above the intervening ocean-derived units of the Glockner Nappe and Matreier Zone, the hanging, Adria-derived Austroalpine nappes include the Meran-Mauls Basement, Ötztal Basement, Northern Calcareous Alps, Niedere Tauern, Gurktal Alps, and the DAV Basement (Figure 1a). All these units were thrust over the European continental-margin units with the units in the TW shortened due to nappe stacking (D_1) and upright folding (D_2) during the Alpine collision in the Eocene to Oligocene. This resulted in a thickened European crust (e.g., Frisch, 1976; Lammerer et al., 2008; Lammerer & Weger, 1998; Rosenberg et al., 2014, 2018; Schmid et al., 2013) with a declining thickness east of the TW (Spada et al., 2013). In the late stage of the orogenic evolution, in the Oligocene-Miocene, east-west extension and strike-slip motion (D_3) have accompanied shortening.

2.2 Structural Framework

The western TW consists of the (D_2) upright Ahorn-, Tuxer-, and Zillertaler antiforms that fold the Early Alpine (D_1) foliation of the Venediger Duplex (Figure 1a; Schmid et al., 2013; Lammerer & Weger, 1998). Estimates of the amount of shortening accommodated by these folds vary between ~60 km (Rosenberg et al., 2015), ~49 km (Rosenberg & Berger, 2009), and ~32 km (Schmid et al.,

2013), based on line-length balancing and assuming constant nappe thicknesses. The tight folds strike ENE, show sub-horizontal, doubly-plunging fold axes and sub-vertical axial planes; they are often associated with axial-plane foliations, and have up to ~17 km amplitudes (Figure 1b). In contrast, the upright folds in the central and eastern TW strike east to ESE, are open and flat-topped (box-type) with amplitudes of up to ~10 km, and lack axial-plane foliations (Figures 1c to 1d). These structural differences point to an abrupt along-strike change in the way shortening has been accommodated (Figure 2a).

The Brenner Fault at the western margin of the TW (Figure 1a) is subdivided in this study into the Brenner Mylonites (BM) and the Silltal Fault (SF, Figure 2b; Behrmann, 1988; Schmidegg, 1953; Selverstone, 1988). The top-west, normal-slip Brenner Fault detaches the Ötztal Basement from the underlying Glockner nappe. The steep limbs of the antiforms and the cores of the tight synforms in the westernmost TW are overprinted by sinistral shear zones, striking sub-parallel to their axial planes. From north to south, the map-scale sinistral shear zones are the Ahorn (ASZ), Greiner (GSZ), and Ahrntal (AhSZ) Shear Zones, each ~1 to 3-km-wide and tens of kilometers long (Figures 1a and 2b). In addition, several 10s to 100s of meters wide sinistral shear zones, e.g., the Tuxer (TSZ) and the Olperer (OSZ) Shear Zones, occur.

2.3 Surrounding Fault Zones

2.3.1 Giudicarie Belt The sinistral transpressive Giudicarie Belt (GB, Figure 1a) forms the western margin of the Dolomites Indenter, a ~77-km-long, N30°E-striking fault system, that offsets the ESE-striking Periadriatic Fault System. Displacement estimates along the GB vary between 15 to 30 km (e.g., Müller et al., 2001; Picotti et al., 1995; Viola et al., 2001) and ~70 km (e.g., Laubscher, 1988; Ratschbacher et al., 1991b; Werling, 1992) due to differing assumptions on its pre-indentation orientation and the amount of shortening accommodated at its southwestern tail. The former group of authors assumes an originally bent Periadriatic Fault System and therefore argues for moderate displacement along the GB, whereas the latter group assumes a straight, pre-indentation Periadriatic Fault System, requiring a larger displacement. Based on balanced cross-sections across the Southern Alps (Nussbaum, 2000; Schönborn, 1992), we favor an originally straight Periadriatic Fault System, hence a sinistral displacement of ~70 km along the GB. The GB includes the Pejo (PeF) and the Northern (NGF) and Southern Giudicarie Faults (SGF), and terminates in the north in the Jaufen (JF), Meran-Mauls (MMF), and Passeier Faults (PaF); the latter delimit, together with the southwestern corner of the TW, the N55°E-striking Meran-Mauls Basement (Figure 1a) (Pomella et al., 2011, 2012). The PaF cuts the JF and the MMF (Müller et al., 2001; Pomella et al., 2011). The thrust geometries inside the Dolomites Indenter exhibit an arcuate shape, indicating north-south ($\pm 10^\circ$) shortening when applying the bow-and-arrow rule (e.g., Elliot, 1976) to its major thrusts. GNSS measurements of the present-day Alpine kinematics indicate a counterclockwise rotation of Adria

against Europe (Caporali & Martin, 2000; Le Breton et al., 2017).

Seismic tomography outlined two lithospheric slabs whose lateral terminations spatially coincide with the GB. The eastern slab was interpreted as the Adriatic plate subducted northward down to 250 km depth; the western slab, likely part of the European plate, features incipient slab break-off (Kästle et al., 2020; Lippitsch et al., 2003; Mitterbauer et al., 2011; Zhao et al., 2016). This discontinuity in the lithospheric structure coincides with a change in seismic anisotropy (Bokelmann et al., 2013; Hetényi et al., 2018; Qorbani et al., 2015). Earthquakes with a magnitude M_L 5 (Richter scale) and hypocentral depths of ~ 20 km have strike-slip focal mechanisms along the GB (Reiter et al., 2018).

2.3.2 Salzach-Ennstal-Mariazell-Puchberg Fault The sinistral transpressive (west) to transtensive (east) Salzach-Ennstal-Mariazell-Puchberg Fault (SEMP, Figure 1a) strikes N70°E from Mittersill along the northern margin of the TW to the Vienna Basin (e.g., Cole et al., 2007; Frost et al., 2009; Linzer et al., 1995). Currently, the SEMP is a structural divide between the seismically active Northern Calcareous Alps in the north and the low-seismicity TW in the south (Reiter et al., 2018). Piercing points imply ~ 60 km displacement along the SEMP (Linzer et al., 2002), equivalent to ~ 56 km of east-west extension. Analogue-material models (Ratschbacher et al., 1991a; Rosenberg et al., 2004), simulating the indentation of the Dolomites Intender into the Eastern Alps, suggest that the sinistral faults along the northern boundary of the extruding wedges, e.g., the Proto-SEMP (chapter 6.5), initiated in the earliest stages of indentation and then rotated clockwise during progressive indentation. For the west-central SEMP, Wang and Neubauer (1998) inferred six evolution stages from paleostress analysis. Two involve predominantly strike-slip faulting and four are dominated by fault-normal compression; the maximum compressive stress axes rotated counterclockwise from NE to NW over time. Throughout the evolution of the SEMP, its northeastern tail has been confined to the southeastern salient of the European Platform, the southeastern tip of the Bohemian Massif (Ratschbacher et al., 1991b). At present, the southeastern tip of the Bohemian spur is located below the subparallel Mur-Mürz Fault (Figure 1a) at the Semmering Pass, close to Glognitz (16°00'East, 47°40'North; van Gelder et al., 2020). Geophysical data outline its subsurface extent (Grad et al., 2009; Baroň et al., 2019; Reinecker & Lenhardt, 1999) and suggest that the Bohemian spur is still acting as a buttress.

2.3.3 Pustertal-Gailtal Fault The dextral, N100°E-striking Pustertal-Gailtal Fault (PGF), a segment of the Periadriatic Fault System, divides the Eastern from the Southern Alps (Figure 1a, Polinski & Eisbacher, 1992) and defines the southern margin of the extruding wedges of the Eastern Alps (Ratschbacher et al., 1991b). Estimates of the Oligo-Miocene displacement along the PGF are indefinite. Frisch et al. (1998) and Laubscher (1988) argued for 100–150 km, pre-Miocene dextral displacement along the entire Periadriatic Fault System based on apparent map-view offsets and palinspastic

reconstructions. The dextral, NE-dipping Sprechenstein-Mauls Fault (SMF, Figure 2b), the youngest and westernmost, purely brittle segment of the PGF, offsets the western ductile tail of the PGF by ~ 2 km (Bistacchi et al., 2010). Earthquakes with focal mechanisms M_L 4 and hypocentral depths ~ 10 km indicate dextral strike-slip along the PGF (Reiter et al., 2018).

2.3.4 Brenner Mylonites and Silltal Fault First estimates of east-west extension across the west-dipping BM varied between ~ 9 and 14 km (Behrmann, 1988) and “several to tens” of kilometers (Selverstone, 1988). Recent estimates are ~ 70 km (Fügenschuh et al., 1997), 4 to 12 km (Rosenberg & Garcia, 2011, 2012), 35 ± 10 km (Wolff et al., 2020), and ~ 44 km (Fügenschuh et al., 2012). The throw across the BM varies continuously along strike (Rosenberg & Garcia, 2011, 2012), with a maximum of ~ 17 km in the area of the Brenner Pass along the hinge of the Tuxer Antiform (Figure 1a); there, the BM are thickest (Axen et al., 1995; Behrmann, 1988; Selverstone, 1988). Towards the northern and southern tails of the BM and SF, the throw decreases to ~ 5 km, which cannot be explained by folding of the footwall (Rosenberg & Garcia, 2011). Re-assessment (Fügenschuh et al., 2012; Rosenberg & Garcia, 2011, 2012) showed that extension was overestimated because exhumation was entirely attributed to normal faulting, ignoring the contributions of folding and erosion (Axen et al., 1995; Fügenschuh et al., 1997; Selverstone et al., 1995; Wolff et al., 2020). Following structural arguments (Rosenberg & Garcia, 2011, 2012) and using the average 29° dip of the BM obtained in this study (chapter 5.7.5 Extensional Shear Zones), we calculated ~ 10 km extension across the BM, in agreement with the first estimates (Behrmann, 1988; Selverstone, 1988).

The moderately west-dipping SF strikes ~ 30 km from Innsbruck to Sterzing (Figure 2b and 2c). North of Steinach (Figure 2c), syn- and antithetic normal faults occur in the hanging wall of the SF (Figures 1a and 2b; Reiser, 2010; Reiter et al., 2018). The seismically active Brenner-Inntal Transfer zone connects the SF with the Inntal Fault System (Figure 1a) with transtensive and transpressive faults in the hanging and footwall of the SF, respectively (Ortner et al., 2006). The hypocentral depths of the M_L 4 earthquakes are between 5 and 15 km (Reiter et al., 2018).

2.3.5 Tauern-Northern-Boundary Fault

The Tauern-Northern-Boundary Fault (TNBF) between the Glockner Nappe and the Lower Austroalpine nappes in the northwestern TW was interpreted to link the BM to the SEMP (Töchterle et al., 2011), to transform extensional into strike-slip displacements (Fügenschuh et al., 2012), and to have a throw of ~ 3 km, deduced from the TRANSALP seismic section (Lammerer et al., 2008). The TNBF is an outcrop-scale, 50 -m-thick, poorly exposed fault zone with varying shear sense indicators, perhaps with dominant top-north reverse and minor sinistral displacements (Bergmeister, 2010; Töchterle et al., 2011).

3 Deformation Fabrics

In the following, we present new and published structural data from the western TW (Figure 2) (Angel & Staber, 1950; Becker, 1993; Exner, 1956, 1962a, 1962b, 1979, 1980, 1983, 1989; Frank & Pestal, 2008; Frank et al., 1987; Giese, 2004; Höck et al., 1994; Karl et al., 1979; Lichtenheld, 2004; Moser, 2006; Rockenschaub & Nowotny, 2009, 2011). These data highlight a structural difference between the central and eastern and the western TW. Based on the mean orientation of the structures, we subdivided the western TW into five structural domains (Figure 2c, Domains A to E) and discriminated three deformation phases (D_1 to D_3), associated with foliations S_1 to S_3 .

S_1 foliations formed prior to the upright folds (D_2 ; Figure 2d). Although of possibly varying ages, S_1 are associated with D_1 nappe stacking and Eocene/Oligocene metamorphism (Bousquet et al., 2012b; Glodny et al., 2005; Nagel et al., 2013; Schmid et al., 2013). The widespread sub-vertical axial-plane foliations (S_{2a}) of the D_2 tight and upright folds strike ENE and cut the folded nappe contacts in the tight D_2 synforms of the western TW (Figure 2d and 2c). The micro- and meso-scale D_2 folds are disharmonic passive shear folds, with thickened hinges, thinned limbs (measured perpendicular to bedding), and Z- and S-shaped second-order folds. Along the margins of the western TW and in the Austroalpine nappes, flexural-slip folds dominate. Along the western margin of the TW, the anticline hinges plunge west, indicated by the circular strike of the nappe contacts with outward pointing bedding. There, the folded S_1 are cut by or form composite foliations with moderately west-dipping S_{2b} foliations, part of the normal-slip shear zones along the BF. S_{2a} and S_{2b} are spatially separated, occurring NE and NW of the indenter salient, respectively (S_{2a} and S_{2b} appear as solid and dashed trajectories in Figure 2d).

D_2 folds and S_2 foliations are overprinted by D_3 km- to meter-scale, subvertical strike-slip and extensional shear zones (Figure 2b). Major NNE- to ENE-striking, sinistral (C_{sin}) shear zones and minor ESE- to ENE-striking, dextral (C_{dex}) ones occur (Pennacchioni and Mancktelow, 2007; Bistacchi et al., 2010). The west-dipping extensional shear zones (C_{nor}) along the western margin of the TW (Figure 2b) formed contemporaneously with the strike-slip shear zones because of mutual overprinting relationships (Axen et al., 1995; Behrmann, 1988; Fügenschuh et al., 1997; Selverstone, 1988). All D_3 shear zones are mylonitic, often brittle-ductile, have higher mica content and smaller grain size than the host rocks, and show clear shear-sense indicators (e.g., Mancktelow & Pennacchioni, 2005; Pennacchioni & Mancktelow, 2007; Schneider et al., 2013; Selverstone, 1993).

4 Methods

We first summarize the geometry, kinematics, and metamorphism associated with the major shear zones of the western TW (Figure 2b). Most of these structures have been described (e.g., Behrmann, 1988; Behrmann & Frisch, 1990;

Lammerer and Weger 1998; Neubauer et al., 1999; Müller et al., 2001; Pomella et al., 2011; Reicherter et al., 1993; Schneider et al., 2013; Spiess, 1995; Steffen & Selverstone, 2006; Viola et al., 2001), but their extent and location differ in the literature. Therefore, we reassess the structures and the shear-zone pattern based on our new structural data and a literature compilation. Then, we present and discuss the field measurements and mean orientation values of specific structures shown in equal area, lower hemisphere stereoplots (created by Stereo32 version 0.9; Röllner & Trepmann, 2008). When the data show a preferred orientation and number >15 , we contoured them using a cosine exponential equation. If lineations and foliations are shown together, we contoured only the foliations. Mean values were deduced graphically from the data maxima. The individual field measurements of the Domains A to E are listed in the Supporting Information Dataset S1. Rotation of these structures during transpression led to deactivation and replacement by new structures representing the prevailing deformation field during the progressive deformation. The rotational sense of the successively formed structures is opposed to the material paths. We calculated dihedral angles between the mean values of structures, which formed in the prevailing deformational field, and that we infer to have formed in kinematic succession. This illustrates and quantifies their transpressional character and yielded different rotational senses for Domains A to E during transpression (Borradaile, 1987; Treagus and Treagus, 1981). The algebraic sign is positive (blue arrows) or negative (purple arrows) when the rotation from one mean value to the succeeding one is clockwise or counterclockwise, respectively (Figure S1).

5 Results and Interpretation

5.1 Ahorn Shear Zone

The ~2.5-km-wide and ~50-km-long, ~ENE-striking Ahorn Shear Zone (ASZ) is a transpressive mylonitic belt located along the northern limb of the western TW (Rosenberg & Schneider, 2008), extending the SEMP westward into deeper crustal levels (Figure 2b; Cole et al., 2007). The ASZ shows sinistral-oblique, south-side-up kinematics with a sub-vertical to steeply SSE-dipping mylonitic foliation and a shallowly west-plunging stretching lineation (Rosenberg & Schneider, 2008). The ASZ transitions into the SEMP in the area of Mittersill and Krimml where sinistral, brittle-ductile and ductile shear zones strike ~NNE and turn abruptly into the east-striking SEMP (Figure 2b and 2c; Cole et al., 2007; Reicherter et al., 1993). The metamorphic grade of the mylonites increases westward along-strike and southward perpendicular to the ASZ strike from 300°C to 400–500°C based on the quartz and feldspar recrystallization mechanisms and the stability of biotite (Schneider et al., 2013).

5.2 Tuxer Shear Zones

Lammerer & Weger (1998) described two sinistral shear zones of >40 km length within the Tuxer Antiform (Salzach-Riffler Fault), striking ESE from the Olperer

and Riffel summits in the west to Krimml in the east (Figure 2b and 2c). At Lammerer & Weger’s (1998) locations, we mapped an interconnected network of outcrop-scale, 1- to 10-m-thick, lower amphibolite-facies, sinistral shear zones, the Tuxer Shear Zones (TSZ, Figure 2b). The TSZ strike NE to east, dip sub-vertically to steeply south, and connect to the ASZ and the Greiner Shear Zone (see chapter 5.4) at their northeastern and southwestern tails, respectively (Figure 2b).

5.3 Olperer Shear Zones

We divided Lammerer & Weger’s (1998) shear zones in the Tuxer Antiform into the TSZ (section 5.2) and the Olperer Shear Zones (OSZ) because of their different orientations and kinematics. In agreement with Ebner et al. (2004), the OSZ constitute two shear zones of 10 to 15 km length, NE to north strike, and moderate to sub-vertical NW to west dip. Sinistral and top-NW normal shear occurred within these ~300-m-thick zones at their western tails. Feldspar ductility and biotite stability indicate syn-kinematic flow at amphibolite-facies conditions.

5.4 Greiner Shear Zone

The ~1-km-thick and ~50-km-long Greiner Shear Zone (GSZ) cuts all D_1 nappe contacts of the western TW and attains a maximum thickness in the Glockner Nappe (Figure 2b and 2e; Selverstone, 1993; Steffen et al., 2001). It strikes east to ENE, is sub-vertical, and has a sub-horizontal stretching lineation. Kinematic indicators imply sinistral (Behrmann & Frisch, 1990; De Vecchi & Baggio, 1982) and dextral (Barnes et al., 2004) shear. Metamorphism in the GSZ mylonites increases eastward along strike from greenschist to amphibolite facies, controlled by the west-plunging Greiner Synform (Figure 1a; e.g., Selverstone, 1985; Selverstone & Spear, 1985).

5.5 Ahrntal Shear Zone

The ~2-km-wide and ~70-km-long transpressive Ahrntal Shear Zone (AhSZ) at the southern limb of the western TW strikes NE to ENE, dips sub-vertically to steeply NNW, and shows sinistral and minor dextral and north-side-up shear (Figure 2b; Behrmann & Frisch, 1990; Reicherter et al., 1993; Schneider et al., 2009). The AhSZ cuts all D_1 nappe contacts and shows predominantly shallowly east-plunging stretching lineations. Metamorphism increases eastwards along strike from greenschist to lower amphibolite facies and northward, perpendicular to the strike, from 300°C to 400–500°C based on quartz and feldspar recrystallization mechanisms, biotite stability, and epidote composition (Kitzig, 2010; Reicherter et al., 1993; Wollnik, 2012). Hence, the metamorphic trends are complementary to the ASZ. Key outcrops in the Vals Valley, south of the Grabspitz summit (Figure 2c), show upright, open to tight folds in the north progressing into isoclinal and rootless folds with axial-plane foliations in the south, overprinted by sinistral shear zones (Figure 3a to 3d).

5.6 Jaufen Fault and Meran-Mauls Basement

The ~200- to 300-m-wide, >15-km-long JF strikes ~ENE; its ductile-brittle mylonites formed at lower greenschist-facies conditions (Müller et al., 2001; Spiess, 1995, 2001; Viola et al., 2001). The JF splits into two branches, one with top-west normal shear in the area of Gasteig (Viola et al., 2001), and one with sinistral-transpressive shear at the Penserjoch road NW of Elzenbaum (Figures 2b and 4; Müller et al., 2001). Our structural data, collected in the Meran-Mauls Basement and summarized in chapter 5.7 as Domain C, indicate that the upright folds of the western TW can be traced into the Austroalpine nappes (Figures 2c to 2d and 4).

5.7 Structural Elements of the Western Tauern Window

5.7.1 S_1 Foliation In Domains A to C (Figure 2c), the folded S_1 strike ENE and dip moderately to steeply NNW but locally SSE (Figure 3a and 3b), indicating an upright to slightly south-vergent sub-dome structure. The sub-vertical σ_1 -circle of S_1 in Domain A traces a sub-horizontal, WSW-trending fold axis, whereas the σ_1 -circles of S_1 in Domains B and C indicate gently ENE- and WSW-plunging fold axes, respectively (Figure 5a to 5c; σ_1 -circle: great circle that fits best the distribution of poles to a folded surface). S_1 and S_2 form a composite foliation along the steep limbs of the D_2 antiforms. A crenulation cleavage, comprising the folded S_1 cut by the axial-plane S_{2a} foliation (Figure 3a and 3b), dominates the fold hinges.

5.7.2 D_2 Fold Axes and Axial Planes The D_2 axial planes (AP_2) of Domains A and B strike ENE, whereas those of Domain C strike NE, sub-parallel to the northwestern margin of the Dolomites Indenter (Figure 5k to 5m). In a cylindrical fold, the σ_1 -circle and the mean axial plane should be orthogonal to each other and the σ_1 -axis should be the fold axis (Ramsay & Huber, 1987, p. 334). However, the values for α_1 (mean AP_2 – σ_1 -axis; i.e., angle between the strike of the mean D_2 axial planes and the pole to the σ_1 -circle) in Domains A and B show a -5° (counterclockwise) deviation from being orthogonal, whereas the α_1 value in Domain C indicates a $+11^\circ$ (clockwise) deviation (Figures 5a to 5c, 5k to 5m, and S1a to S1c, S1g in the supporting information). The D_2 fold axes (FA_2) of Domain A are sub-horizontal and trend ENE, whereas the fold axes in Domains B and C plunge moderately ENE and SW, respectively (Figure 5a to 5c and 5f to 5h). Further, the α_2 values (mean FA_2 – σ_1 -axis) indicate a deviation of -8° and -6° in Domains B and A, in contrast to a deviation of $+8^\circ$ in Domain C (Figures 5f to 5h, 5k to 5m, and S1). The orientation of successively formed structures (deformation fields) during the D_2 folding of S_1 , indicated by α_1 and α_2 , thus rotated counterclockwise in Domains A and B and clockwise in Domain C; the corresponding material paths rotated opposite to the deformation field, i.e., counterclockwise in Domain C and clockwise in Domains A and B (chapter 6.4).

The FA_2 – σ_1 -axis deviations (α_1 and α_2) in Domains A, B, and C indicate non-

cylindrical folding in the western TW, which is diagnostic for transpressional or transtensional folding (Dewey et al., 1998; Ramsay & Huber, 1987; Tikoff & Peterson, 1998; Treagus & Treagus, 1981). The opposite rotations in Domains A and B respectively Domain C (Figures 5a to 5c, 5k to 5m, and S1) reflect the different strikes of the indenter margins causing dextral transpressive folds in domain C and sinistral ones in domains A and B (Figure S1). The different strikes are governed by the orientation of indenter margins and their angle to the convergence direction.

5.7.3 S_2 Foliation and L_2 Stretching Lineation In Domain A, the sub-vertical S_{2a} axial-plane foliations strike ENE, whereas in Domains B and C, they strike ENE–NE, i.e., slightly more to the north, and dip oppositely, SE and NW, respectively (Figure 6a to 6c). The angle β_3 (mean AP_2 –mean S_{2a}) describes the transection of the axial planes (AP_2) by the axial plane foliation (S_{2a}); S_{2a} deviates counterclockwise from AP_2 in Domains A and B and clockwise in Domain C (Figures 5k to 5m, 6a to 6c, and S1). Equally, the β_4 values (mean FA_2 –mean S_{2a}) in Domains A to C deviate clockwise in Domain C and counterclockwise in Domains A and B. According to Borradaile (1978), the β_3 and β_4 values obtained from cleavage-transected folds indicate dextral transpressive shear for Domains A and B, and sinistral one for Domain C. However, Treagus and Treagus (1981) showed that the relationship between cleavage-transected folds and transpressive shear sense rather depends on the initial orientation of the convergence direction to the shear zone boundary. Accordingly, the dihedral angles β_1 to β_4 indicate clockwise rotation of the deformation field in Domain C west of the indenter salient and counterclockwise rotation in Domains A and B east of the indenter salient during the same transpressive event. The dihedral angles β_5 (-axis– S_{2a}) of Domains A to C are -6° , -4° , and -5° . The L_2 stretching lineations are sub-horizontal in Domain B (Figure 6b), sub-horizontal to gently WSW-, rarely ENE-plunging in Domain A, and mostly shallowly WSW-plunging in Domain C, with an increasing WSW-plunge along-strike from Domain B to C (Figure 6a to 6c).

5.7.4 Transcurrent Shear Zones In Domains A, B, and C, the values for β_6 (mean S_{2a} –mean C_{sin}) are -7° , -15° , and -18° , respectively; these are typical but especially for Domain A relatively small angles for sinistral S-C fabrics (Figures 6a to 6c, 6f to 6h, and S1; Passchier & Trouw, 2005). The values for β_7 (mean C_{sin} –mean C'_{sin}) are -20° , -16° , and -18° , indicating typical C-C' angular relationships in all Domains (Figures 6f to 6h, 6k to 6m, and S1). The relatively small β_6 angle in Domain A and the typical β_7 angles suggest a mature shear zone system formed by prolonged activity. In Domain A, the sinistral shear zones (C_{sin}) are sub-vertical and strike ~ENE; in Domain B and C, they strike NE with opposing dips, steeply SE and NW, respectively (Figure 6g to 6h). Stretching lineations (L_{sin}) are sub-horizontal in Domain B, plunge shallowly SW in Domain A, and moderately SW to WNW in Domain C (Figure 6f to 6h). In Domains A, C, and D, conjugate dextral shear zones (C_{dex}) are associated

with variably-oriented stretching lineations (L_{dex} , Figure 7a, 7e, and 7i). The mean strike of C_{dex} changes from ENE to E to SE across the Domains C, A, and D, forming an arc around the indenter salient.

5.7.5 Extensional Shear Zones Extensional shear zones (C_{nor}) in Domains A and E show a large orientation scatter, but are, in general, sub-parallel to the S_{2b} foliation in Domain E (Figure 7c, 7m, and 7o). Based on the spatial distribution of S_{2b} (Figure 2d), the west-plunging FA_2 (Figures 2c and 5j), and the westward increasing plunge of L_2 (Figure 6e), we infer that the C_{nor} nucleated along the hinges and limbs of the west-plunging D_2 folds, ultimately forming the BM. In the areas of the OSZ and the JF (Figure 2b), outcrop-scale shear zones show sinistral-oblique, top-west normal kinematics, i.e., transtension, connecting the BM to the sinistral shear zones of the western TW. The extensional shear zones dip moderately NW in Domain A and gently NE in Domain C, where they are associated with shallowly NW-plunging stretching lineations (Figure 7c and 7g), parallel the Sprechenstein-Mauls Fault (Bistacchi et al., 2010).

5.7.6 Shear Bands Sinistral shear bands (C'_{sin}) in all five Domains (A to E) have a similar appearance, strike in average $N34^\circ E$, and dip steeply to sub-vertically, indicating a homogeneous deformation field in and around the western TW (Figure 6k to 6o). Assuming that shear bands form at angles of 15 – 35° to the shear-zone boundary (Passchier and Trouw, 2005), the MMF ($N55^\circ E$) with an angle of 21° to the average C'_{sin} strike may constitute the structure that is closest to the shear zone boundary during the C'_{sin} formation. The dextral shear bands (C'_{dex}) in Domains A, C, and D strike east; in Domain E, they strike ESE (Figure 7b, 7f, 7j, and 7l). Moderately west-dipping extensional shear bands (C'_{nor}) are common in Domains E and C, where they parallel the BM (Axen et al., 1995); they are rare in Domain A (Figure 7d, 7h, and 7n).

5.7.7 Structural elements in Domain D: Incipient Extruding Wedge

Structural elements like the S_2 foliation (S_{2a} and S_{2b}) and the D_3 shear zones are less developed in Domain D than in Domains A to C. The folded S_1 predominantly dip gently to steeply south, i.e., opposite to those in Domains A to C (Figure 5a to 5d). The sub-horizontal FA_2 trend east (Figure 5d and 5i) and the sub-vertical AP_2 strike east (Figure 5n). Towards the west, the D_2 folds tighten and axial-plane foliations become frequent. The rarely observed, sub-vertical S_{2a} strikes east and the related L_2 lineation plunges gently east (Figure 6d), i.e., opposite to Domain C (Figure 6c). The sub-vertical sinistral shear zones (C_{sin}) strike ENE, show gently west-plunging L_{sin} (Figure 6i); the sub-vertical dextral shear zones (C_{dex}) strike east (Figure 7j). Both the C_{sin} and C_{dex} are more eastward oriented than those in Domains A to C.

5.7.8 Structural elements in Domain E: Western Margin of the Tauern Window

The major difference between Domain E and the other Domains is

that none of its structural elements is sub-vertical. The folded S_1 dip mainly NNE, indicating south-verging folds (Brandner et al., 2008; Rosenberg & Garcia, 2011); the FA_2 plunge gently west, and the AP_2 dip moderately north (Figure 5e, 5j, and 5o), similar to the D_2 folds in Domain D (Figure 5i and 5n). The S_{2a} axial-plane foliations strike ENE and mainly dip moderately NNW; the associated stretching lineations plunge gently west (Figure 6e). In Domain E and along its transition to Domain A, the shallowly WNW-dipping S_{2b} dominate the structural grain (Figures 5e and 7m o), following the west-plunging hinge of the Tuxer Antiform. We observed only few NE-striking sinistral and ESE-striking dextral shear zones, but numerous, top-west normal shear zones, paralleling the BM, with down-dip stretching lineations (Figures 6j, 7k, and 7m) (e.g., Axen et al., 1995). In our field study, we could not find convincing evidence for the existence of the TNBF (Bergmeister, 2010; Fügenschuh et al., 2012; Töchterle et al., 2011).

A key outcrop in St. Jodok (Figure 2c) exhibits NNW-dipping normal shear zones (C_{nor}) associated with D_3 folds with gently NNW-dipping axial planes (AP_3) (Figure 8a to 8c). The D_3 folds refold the tight, south-verging D_2 folds and are accompanied by subvertical, NE-striking tension gashes (Figure 8d). These relationships indicate that the normal shear zones along the western margin of the TW post-date the D_2 folds. Additionally, the C_{nor} and AP_3 follow the arcuate strike of the folded S_1 along the northern limb of the Tuxer Antiform, delimiting the BM to the north, and connecting them to the ENE-striking sinistral-transpressive OSZ. To the south, the BM are delimited by the sinistral-transpressive JF.

5.8 Estimates of the Amounts of Shortening, Stretching, and Sinistral Strike-Slip

A critical parameter for estimating the amounts of shortening, stretching, and sinistral strike-slip is the movement direction of the Dolomites Indenter; the latter has been assumed to be NNW to N (e.g., Laubscher, 1988; Scharf et al., 2013; Schmid et al., 2013). Based on the analogue-material modeling results of Rosenberg et al., (2007) and the interpretation of the PaF, NGF, and SGF as strike-slip faults formed in a wrench-dominated transpressional regime, we argue for a convergence direction of N20°E; we include a $\pm 10^\circ$ uncertainty in our calculations (Figure S3). In section 6.3 (Transpressional Hypothesis), we detail the geometry of the western TW as transpressive zone and anticipate the structural orientation of its center, Domain A, as being representative for this zone. The angle between the mean strike (N60°E) of the sinistral shear zones (C_{sin}) in domain A and the inferred N20°E convergence direction is 40°. This indicates pure-shear-dominated transpression with a kinematic vorticity number W_k of 0.22, estimated using the graph proposed by Tikoff & Peterson (1998, Figure S3). Hence, 22% of the N30°E-displacement of ~70 km along the GF, which caused the shortening in the TW in front of the Dolomites Indenter (amount of contraction) (Laubscher, 1988), can be attributed to the hinge

parallel stretch and 78% to folding (true amount of contraction). According to Tikoff & Peterson (1998) and using the $\pm 10^\circ$ uncertainty in the convergence direction, we calculated $55 \pm 6/-9$ km of shortening accommodated by folds and $15 \pm 9/-6$ km hinge parallel stretch (Figure S3). Our result for shortening is larger than the estimate of ~ 32 km (Schmid et al., 2013) but similar to the estimates of ~ 49 km (Rosenberg and Berger, 2009) and ~ 60 km (Rosenberg et al., 2015) based on balanced cross sections. According to Tikoff & Peterson (1998), the amount of hinge parallel stretch equals the wrench component in transpressive systems. Therefore, sinistral strike-slip together with the hinge parallel stretch in the western TW is $15 \pm 9/-6$ km, together contributing $13 \pm 8/-5$ km to E-W extension.

6 Discussion

In the following, we discuss three hypotheses for the localized exhumation in the western TW. We also discuss the rotation of the Proto-SEMP during transpression, and wrench zone formation across the Eastern Alps.

6.1 Transtension Hypothesis

The TW was interpreted as a pull-apart structure in a transtensional setting (e.g., Genser & Neubauer, 1989; Neubauer et al., 1999). Strain modeling shows that upright open folds can form during transtension (Fossen et al., 2013). Such experiments indicate that the axial planes of transtensional folds strike perpendicular or at a high angle to the extension direction (Rey et al., 2011), and rotate toward the divergence vector (), that is the vector sum of the simple and pure shear components in transtensive (and transpressive) strain fields (Fossen et al., 2013). In sinistral transtension, the orientation of the divergence vector, approximated by the transtensional fold axes, has a clockwise deviation from the shear zone boundary (Fossen et al., 2013, their Figure 2a).

We used the mean strike ($N60^\circ E$) of C_{sin} in Domain A as approximating the shear zone boundary during the D_2 and D_3 deformation. The mean trend ($N57^\circ E$) of the FA_2 fold axes is sub-parallel to the shear zone boundary in Domain C (Figure 5h), and deviates 14° and 8° clockwise in Domains A and B, respectively (Figures 5f and 5g). These fold axes-shear zone boundary relationships exclude the formation of D_2 folds as transtensional folds (Fossen et al., 2013). In addition, the geometry of transtensional folds is different from those observed in the western TW, where D_2 fold hinges are sub-parallel, not sub-perpendicular to the extension direction. The axial planes of D_2 folds in the western TW strike at high angles to the BM and are therefore kinematically unsuitable to accommodate large amounts of east-west extension. Only small-scale D_3 folds in Domain E have an appropriate orientation to accommodate east-west extension and could be interpreted as collapse folds (Froitzheim, 1992; Fossen et al., 2013).

6.2 Extensional Unroofing Hypothesis

Exhumation of the western TW by extensional unroofing requires that extension along the BM and SF are transferred to transcurrent sinistral and dextral strike-slip faults at the northern and southern tails of the Brenner Fault, respectively (Fügenshuh et al., 1997; Scharf et al., 2013a; Schmid et al., 2013). Our fieldwork shows that neither a sinistral strike-slip fault at the northern boundary of the western TW nor a km-scale, dextral strike-slip fault at the southern tail of the BM exists. The dextral PGF nucleates at the salient of the Dolomites Indenter that is located ~10 km ESE of the Brenner Fault. We traced the westernmost occurrence of the dextral PGF to the Valler Jöchl that is ~13 km away from the Brenner Fault. In spite of the widespread occurrence of sinistral shear zones throughout the western TW and the Meran-Mauls Basement (Figures 2b and 6f to 6i), Domain E lacks such structures (Figures 2b and 6j). The TNBF is a small-scale structure (section 2.3.5). The northwestern margin of the TW is characterized by south-verging, asymmetric F_2 folds (Figures 2c, 5e, 5j, and 5o) and the folded S_1 of the northern limbs are reactivated/overprinted by S_{2a} and S_{2b} (Figures 6e and 7o). The brittle SMF that possibly connects to the BM at the southwestern margin of the TW (Bistacchi et al., 2010), has no ductile precursor. Hence, it never was part of the pre-indentation Periadriatic Fault System. We predominantly found sinistral and normal-sense shear indicators in the field. Dextral shear indicators along the Meran-Mauls Fault document the pre-existence of dextral strike-slip along the Periadriatic Fault System.

6.3 Transpression Hypothesis

We interpret the large sinistral shear zone network within the western TW as a first-order structure linking the GB to the SEMP, transferring indentation into lateral extrusion. The mean orientation of the structural elements within Domains A to C show four along-strike trends from SW to NE in the western TW (Figures 2b to 2d). First, the S_{2a} foliations and C_{sin} strike NE at the lateral terminations of the western TW (Domains B and C) and ENE in its center (Domain A, Figures 6a to 6c, 6f to 6h, and 9a). Second, these foliations and shear zones show a steepening of the average dip from the lateral terminations (Domains B and C) to the center (Domain A), and third, an along-strike flip in dip direction (Figures 6a to 6c, 6f to 6h, and 9a). Fourth, the fold axes are doubly plunging towards the lateral terminations of the western TW (Domains B and C) and sub-horizontal in its center (Domain A, Figures 5a to 5c, and 5f to 5h). This sigmoidal foliation pattern resembles that of a transpression zone in a sinistral strike-slip system, e.g., a restraining bend or a strike-slip duplex, in which Domain A is the transpression zone and Domains B and C approximate the bordering wrench zones (Dewey et al., 1998; Sanderson & Marchini, 1984; Woodcock & Fischer, 1986). The vortex of the foliation is located in the central Domain A (Figure 9b), as described for transpressive systems (Robin & Cruden, 1994).

Generally, the stretching lineations are shallowly plunging but scatter between

sub-horizontal and steeply westward plunging along the axis of the western TW. The variable bearing and plunge agree with numerical model results of stretching lineations formed in transpression (Robin & Cruden, 1994). Further, the fold amplitudes decrease and the fold wavelengths narrows from the central Domain A towards the outer Domains B and C, indicating non-cylindrical (conical) folds; such style is predicted by numerical models of transpressional folds (Frehner, 2016).

The dihedral angles α_1 to α_4 in Domains A to C, which mainly describe the geometric evolution of the D_2 folds, indicate a deviation of the mean strike/trend of the different structures formed in kinematic succession that is consistently clockwise in Domain C and counterclockwise in Domains A and B (Figures S1a to c, S1g). This indicates counterclockwise material-plane rotations in Domain C and clockwise rotations in Domains A and B and can be explained by the orientations of the two margins of the Dolomites Indenter, parallel to the MMF and PGF, causing different deformation fields east and west of the indenter salient, e.g., bending the preexisting S_1 foliations. The dihedral angles α_5 to α_7 , which mainly describe the geometric evolution of the D_2 shear zones, indicate exclusively counterclockwise deviations during sinistral shearing in all three Domains (A to C; Figures S1d to f, and S1g). The mean strike of the C'_{sin} , sub-parallel to the PaF, NGF and SGF, is constant in all domains, indicating a similar, late-stage deformation field related to the Dolomites Indenter (Figures 6k to 6o). As the sinistral shear zones (C_{sin}) in Domains A to C reactivate the AP_2 axial plane foliation, we argue that they are kinematically linked to the D_2 folds and can be interpreted as part of the transpressive zone (Woodcock & Fischer, 1986; Dewey et al., 1998). This transpressive zone initiated during non-cylindrical folding during indentation and progressed by the reactivation of the $S2_2$ as slip planes during sinistral transpression. The switch in the rotational sense of the structures from opposing directions during non-cylindric folding in Domain C compared to Domains A and B into a uniform rotation sense during shearing in all three Domains supports the two-stage evolution within a constant deformation field.

6.4 Corner Effect, Partitioning, and Decoupling

The sinistral transpressive zone of the western TW established a structural connection between the GB and the SEMP with a kinematic continuity between NNE-ward indentation and eastward extrusion. Indentation induced a transpressive zone with upright folding and hinge-parallel stretching that transitioned into deformation governed by strike-slip shear zones. Outside the transpressive zone, conjugate sinistral and dextral strike-slip faults formed in Domain D along the NNE-facing indenter margin, and extensional shear zones formed in Domain E. Partitioning of NNE-SSW shortening caused a divergence of material flow away from the indenter salient within Domains D and E (cf. Ježek et al., 2002; Reiter et al., 2011).

Kinematically, the BM, JF, and OSZ (Figure 2b) decouple the Ötztal Basement

from the western TW by transtensional to extensional deformation west of the transpressive zone. East of the indenter salient conjugate shear zones, i.e., the sinistral AhSZ, DAV, SpSZ and the dextral PGF, Iseltal, and Mölltal faults (Figure 1a) and other small-scale, conjugate faults in Domain D decouple the eastward extruding wedge from the transpressive zone. Hence, the transpressive zone is not part of the eastward extruding wedge, instead it comprises a restraining-bend structural junction between the GB and the SEMP (Figure 9b).

Analog-material and numerical experiments showed that within sinistral transpressive zones, transpressive fold axes initiate parallel to the maximum instantaneous stretching axis and with increasing strain, rotate clockwise and stay parallel to the long axis of the strain ellipse (Frehner, 2016; Ratschbacher et al., 1991a, 1991b; Rosenberg et al., 2004, 2007). The mean orientation of fold axes in the western TW, especially in Domain A, form an angle of $\sim 44^\circ$ to the GB, suggesting—at first glance—a rather juvenile transpressive structure, where transpressional folds only initiated and started to rotate clockwise towards the indenter margin (Fossen et al., 2013; Frehner, 2016; James & Watkinson, 1994; Tikoff & Peterson, 1998; Treagus & Treagus, 1981). However, the western TW combines transpression due to the connection of two fault zones (GB and SEMP) and the indentation imposed by the Dolomites Indenter. Numerical indentation models (Ježek et al., 2002) show that the deformation pattern in front of an indenter changes little through time, supporting the interpretation of the western TW as a rather mature sinistral transpressive zone that has clear borders in Domains D and E and connects the GB to the SEMP (Ježek et al., 2002).

6.4.1 Decoupling to the West Rocks north of the GB (Figure 1a; Ötztal Basement) were shortened little because of two geometric aspects. First, the angle of 10 to 25° between the $N20^\circ E$ convergence direction and the $N30^\circ E$ strike of the PaF, SGF, and NGF caused a rather oblique deformation field west of the indenter margin compared to the nearly orthogonal shortening in the northern margin of the indenter (the PGF; Figure 9b). Second, the Dolomites Indenter experienced a net eastward movement, which promoted extension in front of the indenter salient. The FA_2 and AP_2 in Domain C strike NE, subparallel to the northwestern margin of the Dolomites Indenter, and rotated counterclockwise during ongoing shortening, indicated by consistently positive dihedral angles α_1 to α_4 (Figure S1). The FA_2 and AP_2 in Domains A and B strike ENE and rotated clockwise during ongoing shortening indicated by exclusively negative dihedral angles α_1 to α_4 (Figure S1). We argue that this opposing rotation of the material planes/lines NW and NE of the indenter salient caused additional, about convergence-perpendicular extension, necking the D_2 folds (Figure 9b, stereoplots of the D_2 folds). The S_{2b} foliation is restricted to the west-plunging dome axis and the BM (Domain E). Together with the westward increasing steepness of the L_2 stretching lineation within the transpressive zone, it likely is a structural expression of this local extension. The S_{2b} foliation pre-dates the top-west extensional shear zones/bands (C_{nor} , C'_{nor}), that detach and decouple

the Ötztal Basement from the transpressive zone. The OSZ (Ebner et al., 2004; Lammerer & Weger, 1998), structures observed at St. Jodok (Figure 8), and partly the JF (Müller et al., 2001; Viola et al., 2001), are transtensive, transferring sinistral displacement of the western TW into east-west extension along the BM (Figure 2b). Extensional shear zones within the TW in the area of Steinach (Figures 2b and 2c) dip NNW (Figure 8a), tracing the BM in a convex arc northeast-ward (Fügenschuh et al., 1997; Töchterle et al., 2011). Therefore, the ENE-striking normal shear zones in the area of St. Jodok separate the thick BM in the south from the brittle SF in the north (Behrmann, 1988; Fügenschuh et al., 1997; Reiser, 2010; Reiter et al., 2018; Schmidegg, 1953). Finally, the NNE-SSW shortening caused a component of eastward motion of the indenter, promoting maximum east-west extension in front of the indenter tip (Rosenberg et al., 2004, 2007). Hence, Domain E marks a decoupling zone between the shortened western TW and the Ötztal Basement (Figure 9b). The BM are coupled with and the SF together with syn- and antithetic faults in its hanging wall are decoupled from the transpressive zone of the western TW (Figure 9b). Thus, how to explain the extension along the SF? We speculate that it is part of a late-stage releasing band connecting the sinistral shear along the IF in the north with that along JF and PaF in the south; these would involve up to a few kms of late brittle normal faulting along the BF.

6.4.2 Decoupling to the East The AhSZ bounds the central TW in the west that lacks high-amplitude folds, subvertical foliations, and transcurrent shear zones (Figures 2a to 2e). Accordingly, the exhumation level is less deep than in the western TW and large areas expose rocks of the structurally high units. North of the PGF (Figure 1a), the convergence in Domain D was mainly accommodated by upright D_2 folds; their axial planes (AP_2) and the rarely developed S_{2a} have an angle of $\sim 20^\circ$ to the PGF and the latter fade out eastward (Figure 5n). The folds are overprinted by conjugate sinistral and dextral shear/fault zones implying NNE-SSW shortening and eastward material transfer away from the indenter salient (Figure 9b). Domain D, bound by the AhSZ in the north and the PGF in the south, forms the western tip of an eastward extruding wedge (Ratschbacher et al., 1991b).

The ENE-striking transpressive zone of the western TW (Domain A) turns into a NE-strike in Domain B. There, the number of D_2 folds is reduced to two major antiforms, indicating less localized shortening. Several NE-striking sinistral shear zones delimit the transpressive zone to the east from the central TW, where it enters the SEMP with a sudden change in strike (Figures 2b, 2d, 2e; Cole et al., 2007; Rosenberg & Schneider, 2008). We argue that Domain B marks the area where the distributed transpressive deformation expressed by non-cylindric folding and sinistral shearing of the western TW was transferred into more localized sinistral shear zones south of Mittersill (e.g., RSZ, Figure 2b; Cole et al., 2007) and ultimately to the brittle-ductile SEMP (Frost et al., 2011). The fault/shear zones south and east of the western TW that connect to the SEMP and the PGF decouple the extruding central and eastern TW

from the stationary western TW (Linzer et al., 2002; Peresson & Decker, 1997). Based on the following observations, we interpret that shortening inside the western TW is at maximum and gradual decreases eastward, and strike-slip motion and extension is minimum in the western TW and gradually increases eastward. First, the location of the western TW—at the tip of the indenter—accommodated maximum shortening and minimum lateral translation. Second, east of the western TW, shortening is localized along the SEMP and PGF, given the large displacements of both faults east of the western TW. Third, the SEMP and numerous conjugate strike-slip faults south and east of the TW nucleate east of the western TW. Forth, the SEMP shows a succession from transpression in the west to transtension in the east along strike.

6.5 Proto-SEMP Hypothesis

In accordance with the results of the analogue-material models (Ratschbacher et al., 1991a, 1991b; Rosenberg et al., 2007), we propose that the N70°E-striking SEMP had a more northerly initial strike and nucleated northeast of the indenter tip, i.e., it never was connected to the GB in the first place (Figures 9b and S4). We present two approaches to restore its orientation to the time of early indentation (Proto-SEMP). The first approach (Proto-SEMP₁) is a counterclockwise back-rotation of the present-day western SEMP around a vertical rotation pole close to Liezen (Figure 1a), using the 55-km NNE-SSW shortening and 13-km eastward extension suggested in this study for the western TW. In this restoration, the Proto-SEMP₁ had an initial N50°E strike, subparallel to the present-day strike of the Meran-Mauls Basement, and rotated 20° clockwise together with the sub-parallel IF and MMzF (Figures 1a and S4). Palinspastic restorations of Fodor (1995) and Linzer et al. (1995) also imply a N50°E strike of the Proto-SEMP. The Northern Calcareous Alps in between rotated counterclockwise along antithetic Riedel faults, deduced from paleomagnetic analyses of intramontane basins interpreted as domino-block rotation (Haubold et al., 1999; Márton et al., 2000).

The second approach uses the results of paleostress analysis along the western SEMP; these yielded six deformational events, two (D₃ and D₅) involved mostly strike-slip deformation, four mainly thrusting (Wang & Neubauer, 1999). Against the authors’ interpretation, we kept the orientation of the principal stress axes constant and rotated the present-day SEMP 55° counterclockwise towards a Proto-SEMP₂ orientation of N15°E (Figure 9b), using the rotations derived by Wang & Neubauer (1999); we consider this rotation value an extreme. Both approaches support our hypothesis of a clockwise rotating SEMP during indentation under a stable convergence direction (Figures 9c and S4).

6.6 Wrench Zone Hypothesis

The TW consists of upright folds, delimited by conjugate transpressive shear zones (Ratschbacher et al., 1991a, b; Rosenberg et al., 2004; 2007), forming an arcuate culmination in front of the Dolomites Indenter. This arcuate dome of the

TW with a triangular crustal block south of it (Figure 1a) is consistent with the majority of indentation models (Schueller & Davy, 2008, for a review), which show localized shortening and conjugate shear in front of a triangle pointing away from the indenter margin. However, the western TW accumulated more deformation as the central and eastern TW, indicating a different evolution in the late stage. We defined the Domains A to C as a mature sinistral transpressive zone, connecting the initially separated GB and the SEMP via a restraining bend (Figure 9b). The western TW forms the western margin of the stable triangle in front of the Dolomites Indenter. In an early stage of indentation, the western TW developed as a right step-over between the independently existing GB and the Proto-SEMP with localized high-strain shortening accommodated by upright folds (Figure S4); it evolved over time into a zone dominated by sinistral wrenching. We argue that this transpressive zone together with the GB and the SEMP constitutes a sinistral wrench zone translating Dolomites indentation into lateral extrusion. By that, it decouples the Ötztal Basement in the west, experiencing normal shear/faulting along the Brenner Fault and sinistral transtension along the OSZ and the JF, and the central and eastern TW in the east, experiencing eastward extrusion along conjugate shear zones, e.g., the PGF, SEMP and minor strike-slip faults in between (Ratschbacher et al., 1991a, 1991b; Rosenberg et al., 2007).

7 Conclusions

The western Tauern Window shows a structural evolution distinct from the central and eastern Tauern Window. Tight, upright folds of high-amplitude, subvertical axial plane foliations, and sinistral shear zones indicate absorption of orogen-perpendicular shortening. The western Tauern Window constitutes a right step-over connecting the sinistral transpressive Giudicarie Belt, subparallel to the indentation direction of the Dolomites Indenter, with the sinistral SEMP Fault, a major fault zone related to the eastward lateral extrusion of the central and eastern Eastern Alps. The ~ 70 km indentation by the Dolomites Indenter has been manifested within the western Tauern Window by upright folds and sinistral shear zones, accommodating $55 \pm 6/-9$ km of shortening, and $15 \pm 9/-6$ km hinge parallel stretch and likewise $15 \pm 9/-6$ km sinistral shear zones, resulting in $13 \pm 7/-5$ km of east-west extension. Farther east, the SEMP Fault has accommodated ~ 56 km of eastward lateral extrusion. At the salient of the Dolomites Indenter, the western Tauern Window forms a relatively stationary structural divide, decoupling the western Eastern Alps along the top-west, normal-slip Brenner Fault from the central and eastern Eastern Alps that extrude eastward. In the central Tauern Window, north-south shortening decreases in comparison to the western Tauern Window, as seen from the preservation of higher tectonostratigraphic units, the lower amplitude of folds, and the lack of axial plane foliations. In turn, the amount of lateral extrusion increases, as indicated by the increasing abundance of conjugated strike-slip shear/fault zones within the Austroalpine nappes south and east of the Tauern Window. The structures and the inferred displacements within the western Tauern Win-

dow are consistent with exhumation dominated by erosional denudation during transpressive folding. We interpret the western Tauern Window as a transpressive, right step-over between the sinistral Giudicarie Belt and a sub-parallel Proto-SEMP, which was pinned by the West-European Platform at the southern salient of the Bohemian massif. During indentation, the western Proto-SEMP progressively rotated clockwise around a vertical axis close to Liezen, attaining its present day orientation.

8 Acknowledgments and Data

This study was funded by the DFG grant Ro2177/4. We acknowledge family Schwärzer, especially M. Schwärzer, G. Fankhauser and R. Emberger for field support and accommodation. For helpful discussion, we thank A. Bertrand, S. Favaro, S. Garcia, D. Rutte, and R. Schuster. For critical and constructive reviews of the manuscript in an early stage, we thank M. R. Handy, H. Pomella, and S. M. Schmid. Reviews by C. Teyssier and three anonymous reviewers caused a substantial refocusing of the manuscript.

This data set contains 6965 structural data from 1774 outcrops in the western Tauern Window, collected during July to August, 2007, June to September, 2008, June to September, 2009, July to October, 2010, using a Breithaupt "GEKOM" Stratum Compass, provided by the Freie Universität Berlin, Germany. The raw data, plotted in the lower hemisphere and equal area plots of Figures 5a to 5o, 6a to 6o, and 7a to 7o are given in the Supporting Information Dataset S1. The Supplementary Information Figures 1a to g, 2, and 3 contains the different dihedral angles between the mean values of the respective structural elements of the Domains A to C. The georeferenced raw data are available in the open access research data base OpARA of the Technische Universität Dresden and Technische Universität Bergakademie Freiberg.

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10 Figure Captions

Figure 1a. Simplified tectonostratigraphic map of the Tauern Window and surrounding units modified after (Bousquet et al., 2012b). **b. to d.** Structural sections of the western, central, and eastern sub-dome of the Tauern Window simplified after Brander (2013) and Schmid et al. (2013).

Figure 2a. Foliation map of the Tauern Window shows the main foliation (undifferentiated). Compiled literature and new data (see paragraph 2 for references). **b. to e.** Close ups of the western Tauern Window based on (Bigi et al., 1994) showing **b.** Traces of the macro-scale sinistral shear zones; **c.** Outcrops of this study, definition of the five structural Domains (A to E), and traces of the structural sections (Figure 4); **d.** Interpreted traces of the S_{2a} axial-plane (solid lines) and the S_{2b} foliations (dashed lines); **e.** Interpreted traces of the F_2 upright folds and the tectonostratigraphic units.

Figure 3. Field photographs along the Vals valley from north to south. **a.** Folded S_1 upright, tight folds, Width of the photo is approximately 4 m; **b.** Rootless S_1 folds and newly formed sub-vertical S_{2a} axial-plane foliation; **c.** S_{2a} axial-plane foliation and localized sinistral shear zones (C_{sin}), having an additional north-side-up component; **d.** Top view on sub-vertical S_{2a} axial-plane foliation and localized sinistral shear bands C'_{sin} .

Figure 4. SE-trending structural cross section running from Rosskopf to Onserberg (see Figure 2a for trace). Lithological units based on the Geologische Karte 1:50.000, Blatt 175 Sterzing.

Figure 5. Stereoplots of contoured data in ten contouring intervals, number of data, maximum, minimum, mean densities (ρ), cosine exponent, and mean values are given in the bottom-left columns. **a.** to **e.** S_1 foliation, great circles indicate S_1 -circles. **f.** to **j.** D_2 fold axes (FA_2). **k.** to **o.** D_2 axial planes (AP_2).

Figure 6. Stereoplots of contoured data in ten contouring intervals, number of data, maximum, minimum, mean densities (ρ), cosine exponent, and mean values are given in the bottom-left columns and the lower right corner. **a.** to **e.** S_{2a} axial-plane foliations and L_2 lineations, great circles indicate S_{2a} mean values. **f.** to **j.** Sinistral shear zones (C_{sin}) and stretching lineations (L_{sin}), great circles indicate C_{sin} mean values. **k.** to **o.** Sinistral shear bands (C'_{sin}), great circles indicate C'_{sin} mean values.

Figure 7. Stereoplots of contoured data in ten contouring intervals, number of data, maximum, minimum, mean densities (ρ), cosine exponent, and mean values are given in the bottom-left columns and the lower right corners. **a.**, **e.**, **k.**, **j.** Dextral shear zones (C_{dex}) and stretching lineations (L_{dex}), great circles indicate C_{dex} mean values. **b.**, **f.**, **l.**, **i.** Dextral shear bands (C'_{dex}), great circles indicate C'_{dex} mean values. **c.**, **g.**, **m.** Extensional shear zones (C_{nor}) and stretching lineations (L_{nor}), great circles indicate C_{nor} mean values. **d.**, **h.**, **n.** Extensional shear bands (C'_{nor}), great circles indicate C'_{nor} mean values. **o.** Composite foliations (S_{2b}), great circles indicate S_{2b} mean value.

Figure 8. **a.** Sketch of a key outcrop near St. Jodok (outcrop length ~100 m) and stereoplots; from left to right: S_1 foliations, AP_2 axial planes, C_{nor} extensional shear zones, and AP_3 collapse folds. **b.** to **d.** South-verging, tight D_2 folds (F_2) are sheared by normal-sense shear zones along their limbs. Collapse folds (F_3) and tension gashes overprint steep F_2 folds.

Figure 9. **a.** Block model of the western Tauern Window. Structural map and sections are based on Brandner (2013) and Schmid et al. (2013). Map is displaced and view is parallel to the wrench zone (~NE) to illustrate the along strike variation of the sinistral shear zones (red lines). **b.** Structural summary of the wrench zone highlighted in red. Mean great circles and mean vectors based on data shown in Figures 5, 6, and 7. Sectors with upper-right-to-lower-left stripes indicate the assumed $N20^\circ E$ ($\pm 10^\circ$) convergence direction of the Dolomites Indenter with respect to the major faults forming the wrench zone (GF, MMF, and Proto-SEMP). Sectors with upper-left-to-lower-right stripes indicate the conver-

gence vector of the respective shear zone boundary (-20°), in which transpression is wrench-dominated. For the MMF and the western TW, the convergence angles are 35° and 40° , respectively, indicating pure-shear-dominated transpression (Tikoff and Peterson, 1998). For the GF, the Proto-SEMP₁, and the Proto-SEMP₂, the convergence vectors are towards N10°E, N30°E and N15°E, respectively, indicating mostly wrench-dominated transpression (Tikoff and Peterson, 1998). **c.** Structural reinterpretation of the deformation stages of Wang and Neubauer (1998), left: Wang and Neubauer's (1998) interpretation of counterclockwise rotation of principle stress axes around a fixed SEMP, right: reinterpretation in this study assumes a fixed ($\sim$ N) direction of principle stresses and a $\sim 55^\circ$ clockwise rotation of the SEMP into the Proto-SEMP orientation.

Supporting Table 1: raw data of structural measurements

Domain A			Domain B			Domain C			Domain D			Domain E		
338	64	S ₁	350	30	S ₁	161	58	S ₁	350	42	S ₁	49	55	S ₀
165	75	S ₁	352	36	S ₁	132	70	S ₁	357	43	S ₁	62	64	S ₀
249	46	S ₁	303	54	S ₁	153	60	S ₁	342	44	S ₁	43	51	S ₀
315	65	S ₁	304	57	S ₁	163	65	S ₁	326	24	S ₁	186	88	S ₁
0	53	S ₁	330	60	S ₁	337	81	S ₁	120	78	S ₁	238	22	S ₁
353	30	S ₁	322	54	S ₁	343	70	S ₁	124	81	S ₁	243	37	S ₁
346	35	S ₁	39	34	S ₁	345	70	S ₁	144	54	S ₁	326	45	S ₁
325	36	S ₁	173	20	S ₁	347	35	S ₁	142	45	S ₁	174	19	S ₁
350	42	S ₁	338	13	S ₁	323	60	S ₁	142	44	S ₁	357	45	S ₁
11	48	S ₁	336	41	S ₁	319	60	S ₁	151	60	S ₁	180	48	S ₁
359	58	S ₁	188	39	S ₁	335	63	S ₁	143	64	S ₁	169	63	S ₁
0	54	S ₁	21	56	S ₁	327	62	S ₁	150	84	S ₁	169	58	S ₁
347	64	S ₁	16	55	S ₁	311	54	S ₁	124	38	S ₁	192	74	S ₁
169	35	S ₁	25	38	S ₁	306	69	S ₁	119	36	S ₁	181	60	S ₁
162	84	S ₁	20	42	S ₁	329	57	S ₁	229	35	S ₁	349	74	S ₁
143	39	S ₁	24	54	S ₁	355	52	S ₁	116	33	S ₁	351	79	S ₁
107	14	S ₁	22	52	S ₁	343	47	S ₁	127	57	S ₁	191	40	S ₁
241	70	S ₁	146	66	S ₁	359	39	S ₁	357	49	S ₁	186	44	S ₁
183	78	S ₁	124	61	S ₁	359	39	S ₁	152	10	S ₁	320	47	S ₁
181	62	S ₁	133	24	S ₁	346	53	S ₁	147	39	S ₁	315	64	S ₁
178	57	S ₁	183	24	S ₁	242	54	S ₁	68	44	S ₁	315	40	S ₁
352	88	S ₁	192	26	S ₁	317	68	S ₁	75	44	S ₁	344	57	S ₁
151	75	S ₁	173	88	S ₁	315	64	S ₁	32	48	S ₁	330	45	S ₁
171	69	S ₁	351	87	S ₁	336	64	S ₁	38	42	S ₁	334	71	S ₁
182	65	S ₁	157	72	S ₁	331	46	S ₁	115	9	S ₁	330	64	S ₁
181	71	S ₁	136	36	S ₁	148	64	S ₁	116	4	S ₁	324	67	S ₁
170	71	S ₁	154	30	S ₁	141	51	S ₁	45	72	S ₁	50	6	S ₁
339	67	S ₁	134	84	S ₁	129	50	S ₁	63	48	S ₁	355	79	S ₁
327	52	S ₁	152	55	S ₁	139	50	S ₁	34	66	S ₁	45	30	S ₁
168	79	S ₁	313	66	S ₁	288	50	S ₁	3	38	S ₁	277	47	S ₁
193	35	S ₁	19	74	S ₁	281	59	S ₁	9	23	S ₁	336	38	S ₁
352	62	S ₁	21	74	S ₁	275	74	S ₁	256	76	S ₁	338	49	S ₁
330	70	S ₁	198	78	S ₁	355	30	S ₁	288	77	S ₁	332	25	S ₁
340	60	S ₁	38	87	S ₁	331	27	S ₁	281	67	S ₁	315	33	S ₁
351	89	S ₁	33	53	S ₁	105	75	S ₁	284	60	S ₁	316	30	S ₁
177	87	S ₁	4	58	S ₁	332	74	S ₁	130	56	S ₁	335	64	S ₁
325	73	S ₁	21	75	S ₁	326	48	S ₁	112	57	S ₁	335	63	S ₁
347	87	S ₁	17	74	S ₁	302	38	S ₁	115	57	S ₁	337	76	S ₁
343	79	S ₁	349	69	S ₁	265	21	S ₁	144	63	S ₁	328	68	S ₁
318	65	S ₁	11	73	S ₁	260	21	S ₁	124	35	S ₁	336	32	S ₁
310	61	S ₁	29	28	S ₁	268	67	S ₁	163	41	S ₁	335	35	S ₁
165	78	S ₁	1	36	S ₁	305	35	S ₁	139	37	S ₁	300	19	S ₁
331	45	S ₁	24	45	S ₁	297	43	S ₁	130	76	S ₁	57	9	S ₁
148	57	S ₁	25	43	S ₁	323	68	S ₁	144	44	S ₁	359	20	S ₁
321	55	S ₁	20	70	S ₁	320	68	S ₁	142	48	S ₁	355	54	S ₁

Supporting Table 1: raw data of structural measurements

Domain A			Domain B			Domain C			Domain D			Domain E		
325	37	S ₁	8	48	S ₁	325	70	S ₁	153	44	S ₁	330	56	S ₁
320	56	S ₁	341	74	S ₁	136	52	S ₁	148	48	S ₁	334	60	S ₁
337	80	S ₁	22	40	S ₁	123	63	S ₁	98	36	S ₁	328	52	S ₁
330	40	S ₁	10	51	S ₁	322	58	S ₁	163	25	S ₁	332	48	S ₁
355	61	S ₁	30	40	S ₁	322	55	S ₁	139	64	S ₁	333	49	S ₁
339	34	S ₁	24	51	S ₁	321	46	S ₁	85	32	S ₁	280	33	S ₁
351	74	S ₁	21	45	S ₁	322	53	S ₁	129	85	S ₁	284	33	S ₁
172	65	S ₁	11	55	S ₁	342	34	S ₁	356	42	S ₁	315	46	S ₁
2	75	S ₁	181	33	S ₁	2	32	S ₁	3	45	S ₁	309	41	S ₁
158	72	S ₁	194	45	S ₁	356	34	S ₁	168	54	S ₁	297	35	S ₁
166	76	S ₁	209	45	S ₁	324	72	S ₁	185	64	S ₁	257	33	S ₁
155	57	S ₁	196	42	S ₁	338	60	S ₁	187	51	S ₁	290	35	S ₁
154	50	S ₁	142	52	S ₁	312	47	S ₁	181	59	S ₁	288	35	S ₁
316	62	S ₁	353	62	S ₁	313	41	S ₁	184	65	S ₁	56	48	S ₁
153	73	S ₁	168	68	S ₁	328	49	S ₁	156	65	S ₁	62	57	S ₁
334	65	S ₁	131	72	S ₁	321	54	S ₁	163	60	S ₁	57	49	S ₁
315	72	S ₁	340	32	S ₁	328	44	S ₁	160	45	S ₁	79	49	S ₁
331	64	S ₁	114	15	S ₁	316	38	S ₁	181	40	S ₁	72	53	S ₁
34	36	S ₁	11	13	S ₁	342	53	S ₁	171	85	S ₁	106	62	S ₁
11	44	S ₁	304	30	S ₁	334	57	S ₁	185	76	S ₁	120	67	S ₁
4	50	S ₁	329	22	S ₁	359	28	S ₁	181	71	S ₁	58	60	S ₁
159	81	S ₁	331	54	S ₁	359	25	S ₁	156	86	S ₁	85	61	S ₁
158	71	S ₁	2	65	S ₁	325	65	S ₁	347	88	S ₁	101	68	S ₁
168	67	S ₁	143	68	S ₁	332	49	S ₁	170	79	S ₁	97	68	S ₁
167	68	S ₁	129	67	S ₁	296	39	S ₁	27	65	S ₁	157	75	S ₁
351	86	S ₁	153	55	S ₁	316	33	S ₁	22	65	S ₁	157	62	S ₁
175	79	S ₁	157	56	S ₁	82	20	S ₁	14	76	S ₁	120	24	S ₁
175	81	S ₁	137	79	S ₁	194	28	S ₁	0	56	S ₁	149	75	S ₁
172	90	S ₁	132	80	S ₁	223	28	S ₁	2	74	S ₁	170	52	S ₁
346	79	S ₁	129	76	S ₁	348	35	S ₁	9	74	S ₁	162	86	S ₁
325	69	S ₁	130	77	S ₁	346	38	S ₁	165	78	S ₁	264	59	S ₁
341	80	S ₁	129	69	S ₁	344	48	S ₁	165	85	S ₁	247	75	S ₁
180	40	S ₁	30	19	S ₁	5	30	S ₁	140	82	S ₁	191	88	S ₁
168	83	S ₁	42	30	S ₁	345	35	S ₁	135	79	S ₁	218	43	S ₁
168	60	S ₁	30	22	S ₁	335	32	S ₁	154	84	S ₁	283	45	S ₁
175	41	S ₁	48	23	S ₁	348	35	S ₁	163	83	S ₁	176	85	S ₁
170	71	S ₁	31	40	S ₁	340	44	S ₁	350	83	S ₁	211	36	S ₁
170	65	S ₁	33	36	S ₁	338	61	S ₁	350	81	S ₁	198	73	S ₁
160	35	S ₁	59	37	S ₁	167	64	S ₁	334	65	S ₁	235	49	S ₁
148	35	S ₁	58	34	S ₁	177	40	S ₁	334	73	S ₁	184	79	S ₁
145	55	S ₁	48	29	S ₁	191	28	S ₁	320	54	S ₁	168	76	S ₁
230	34	S ₁	52	35	S ₁	211	27	S ₁	355	45	S ₁	164	41	S ₁
150	38	S ₁	64	48	S ₁	264	33	S ₁	315	49	S ₁	175	55	S ₁
150	56	S ₁	59	29	S ₁	303	68	S ₁	352	39	S ₁	198	41	S ₁
175	67	S ₁	85	23	S ₁	288	87	S ₁	10	49	S ₁	188	35	S ₁

Supporting Table 1: raw data of structural measurements

Domain A			Domain B			Domain C			Domain D			Domain E		
73	35	S ₁	73	27	S ₁	277	74	S ₁	358	45	S ₁	104	87	S ₁
252	62	S ₁	96	26	S ₁	324	50	S ₁	353	42	S ₁	9	63	S ₁
315	34	S ₁	28	43	S ₁	21	25	S ₁	334	52	S ₁	19	70	S ₁
346	59	S ₁	71	39	S ₁	19	23	S ₁	354	79	S ₁	350	52	S ₁
322	48	S ₁	288	68	S ₁	25	25	S ₁	355	78	S ₁	17	58	S ₁
325	60	S ₁	300	48	S ₁	58	15	S ₁	16	48	S ₁	281	32	S ₁
342	75	S ₁	148	26	S ₁	267	4	S ₁	342	44	S ₁	317	42	S ₁
351	40	S ₁	338	81	S ₁	292	35	S ₁	11	66	S ₁	309	33	S ₁
358	58	S ₁	39	35	S ₁	273	42	S ₁	338	56	S ₁	175	82	S ₁
328	62	S ₁	20	38	S ₁	7	20	S ₁	349	70	S ₁	173	88	S ₁
332	55	S ₁	142	26	S ₁	97	53	S ₁	351	81	S ₁	173	79	S ₁
340	60	S ₁	339	21	S ₁	289	38	S ₁	11	83	S ₁	176	37	S ₁
340	72	S ₁	316	24	S ₁	247	47	S ₁	359	84	S ₁	348	24	S ₁
340	84	S ₁	106	55	S ₁	277	47	S ₁	338	63	S ₁	347	31	S ₁
342	70	S ₁	108	61	S ₁	310	63	S ₁	320	70	S ₁	206	60	S ₁
170	89	S ₁	64	35	S ₁	272	52	S ₁	9	35	S ₁	240	35	S ₁
254	32	S ₁	75	39	S ₁	251	64	S ₁	62	45	S ₁	228	38	S ₁
336	38	S ₁	329	82	S ₂	270	19	S ₁	46	39	S ₁	339	60	S ₁
342	38	S ₁	330	67	S ₂	113	87	S ₁	33	34	S ₁	351	86	S ₁
159	75	S ₁	178	62	S ₂	272	67	S ₁	47	32	S ₁	191	69	S ₁
150	60	S ₁	216	65	S ₂	279	37	S ₁	24	43	S ₁	325	31	S ₁
335	38	S ₁	185	75	S ₂	291	69	S ₁	45	37	S ₁	167	72	S ₁
328	37	S ₁	192	33	S ₂	268	45	S ₁	44	34	S ₁	338	22	S ₁
1	58	S ₁	180	56	S ₂	266	45	S ₁	5	42	S ₁	350	47	S ₁
357	54	S ₁	184	77	S ₂	304	58	S ₁	69	34	S ₁	170	85	S ₁
346	53	S ₁	189	80	S ₂	282	40	S ₁	24	43	S ₁	336	55	S ₁
326	45	S ₁	216	56	S ₂	306	52	S ₁	179	49	S ₁	198	42	S ₁
340	35	S ₁	3	82	S ₂	312	53	S ₁	165	50	S ₁	190	88	S ₁
339	69	S ₁	10	84	S ₂	337	65	S ₁	225	66	S ₁	0	52	S ₁
331	35	S ₁	220	80	S ₂	311	82	S ₁	168	66	S ₁	215	45	S ₁
147	42	S ₁	211	86	S ₂	286	79	S ₁	164	30	S ₁	216	49	S ₁
165	59	S ₁	135	86	S ₂	321	65	S ₁	135	24	S ₁	246	25	S ₁
165	59	S ₁	325	68	S ₂	326	85	S ₁	175	48	S ₁	203	33	S ₁
322	48	S ₁	312	69	S ₂	321	56	S ₁	189	27	S ₁	202	39	S ₁
328	46	S ₁	359	79	S ₂	0	55	S ₁	177	42	S ₁	204	29	S ₁
340	46	S ₁	186	88	S ₂	321	41	S ₁	20	8	S ₁	247	22	S ₁
350	49	S ₁	346	85	S ₂	328	48	S ₁	208	33	S ₁	250	28	S ₁
325	68	S ₁	346	86	S ₂	348	57	S ₁	225	32	S ₁	197	14	S ₁
18	89	S ₁	351	85	S ₂	348	66	S ₁	346	18	S ₁	202	26	S ₁
10	61	S ₁	151	60	S ₂	331	82	S ₁	354	38	S ₁	246	18	S ₁
171	85	S ₁	159	63	S ₂	65	53	S ₁	220	36	S ₁	232	28	S ₁
162	83	S ₁	148	62	S ₂	354	64	S ₁	194	52	S ₁	235	29	S ₁
10	61	S ₁	155	67	S ₂	349	54	S ₁	177	28	S ₁	251	22	S ₁
11	41	S ₁	157	65	S ₂	348	49	S ₁	207	43	S ₁	263	28	S ₁
5	48	S ₁	153	67	S ₂	14	47	S ₁	214	27	S ₁	257	41	S ₁

Supporting Table 1: raw data of structural measurements

Domain A			Domain B			Domain C			Domain D			Domain E		
31	17	S ₁	355	74	S ₂	342	80	S ₁	192	77	S ₁	240	35	S ₁
344	57	S ₁	360	73	S ₂	347	65	S ₁	207	77	S ₁	253	49	S ₁
355	69	S ₁	138	80	S ₂	162	59	S ₁	3	74	S ₁	266	59	S ₁
332	67	S ₁	150	72	S ₂	162	49	S ₁	167	44	S ₁	310	48	S ₁
336	79	S ₁	135	73	S ₂	308	48	S ₁	193	60	S ₁	316	52	S ₁
335	88	S ₁	168	78	S ₂	304	45	S ₁	159	52	S ₁	293	47	S ₁
157	64	S ₁	157	84	S ₂	34	28	S ₁	168	64	S ₁	265	35	S ₁
155	62	S ₁	329	83	S ₂	48	30	S ₁	171	66	S ₁	317	30	S ₁
155	62	S ₁	329	89	S ₂	123	66	S ₁	351	53	S ₁	335	33	S ₁
162	46	S ₁	317	84	S ₂	137	67	S ₁	305	55	S ₁	274	25	S ₁
166	52	S ₁	318	82	S ₂	120	11	S ₁	311	20	S ₁	267	27	S ₁
170	52	S ₁	122	79	S ₂	356	28	S ₁	340	42	S ₁	239	15	S ₁
120	49	S ₁	131	70	S ₂	179	10	S ₁	347	45	S ₁	205	24	S ₁
144	35	S ₁	131	72	S ₂	348	45	S ₁	188	86	S ₁	191	28	S ₁
131	43	S ₁	145	62	S ₂	11	26	S ₁	3	88	S ₁	191	21	S ₁
165	82	S ₁	346	74	S ₂	32	25	S ₁	0	84	S ₁	208	9	S ₁
45	19	S ₁	348	71	S ₂	341	40	S ₁	342	43	S ₁	172	25	S ₁
35	23	S ₁	344	71	S ₂	345	35	S ₁	359	81	S ₁	202	19	S ₁
340	35	S ₁	342	75	S ₂	353	45	S ₁	174	65	S ₁	229	21	S ₁
176	82	S ₁	339	65	S ₂	356	38	S ₁	183	75	S ₁	219	30	S ₁
115	82	S ₁	339	72	S ₂	351	30	S ₁	151	34	S ₁	335	20	S ₁
191	5	S ₁	353	68	S ₂	324	28	S ₁	172	58	S ₁	326	32	S ₁
240	10	S ₁	355	68	S ₂	302	35	S ₁	158	30	S ₁	329	18	S ₁
342	72	S ₁	358	68	S ₂	106	25	S ₁	174	46	S ₁	195	63	S ₁
348	78	S ₁	6	72	S ₂	120	51	S ₁	169	70	S ₁	184	81	S ₁
166	78	S ₁	1	77	S ₂	233	83	S ₁	168	67	S ₁	329	34	S ₁
324	83	S ₁	346	85	S ₂	264	28	S ₁	174	64	S ₁	186	27	S ₁
177	64	S ₁	342	81	S ₂	325	30	S ₁	178	80	S ₁	13	89	S ₁
152	69	S ₁	350	84	S ₂	344	22	S ₁	170	64	S ₁	22	46	S ₁
185	87	S ₁	160	65	S ₂	296	31	S ₁	170	67	S ₁	4	64	S ₁
264	34	S ₁	322	83	S ₂	334	81	S ₁	165	43	S ₁	33	43	S ₁
284	45	S ₁	151	68	S ₂	246	77	S ₁	154	55	S ₁	9	67	S ₁
153	75	S ₁	336	64	S ₂	263	63	S ₁	162	57	S ₁	182	72	S ₁
152	88	S ₁	174	48	S ₂	277	82	S ₁	168	55	S ₁	178	46	S ₁
350	87	S ₁	168	50	S ₂	278	81	S ₁	171	61	S ₁	186	72	S ₁
336	90	S ₁	188	58	S ₂	186	28	S ₁	166	67	S ₁	330	55	S ₁
336	90	S ₁	181	47	S ₂	154	62	S ₁	180	56	S ₁	337	47	S ₁
355	38	S ₁	112	60	S ₂	172	47	S ₁	172	70	S ₁	169	39	S ₁
347	60	S ₁	114	57	S ₂	322	52	S ₁	142	15	S ₁	220	34	S ₁
349	87	S ₁	94	30	S ₂	324	50	S ₁	175	65	S ₁	344	36	S ₁
355	85	S ₁	97	63	S ₂	304	440	S ₁	161	41	S ₁	320	22	S ₁
6	56	S ₁	105	70	S ₂	336	87	S ₁	172	40	S ₁	15	25	S ₁
2	55	S ₁	259	37	S ₂	353	85	S ₁	155	24	S ₁	354	35	S ₁
355	76	S ₁	285	51	S ₂	315	48	S ₁	135	19	S ₁	337	44	S ₁
5	84	S ₁	125	46	S ₂	334	62	S ₁	175	35	S ₁	24	28	S ₁

Supporting Table 1: raw data of structural measurements

Domain A			Domain B			Domain C			Domain D			Domain E		
172	87	S ₁	91	45	S ₂	297	34	S ₁	170	38	S ₁	5	40	S ₁
145	62	S ₁	316	65	S ₂	304	25	S ₁	165	68	S ₁	334	59	S ₁
116	46	S ₁	109	63	S ₂	329	48	S ₁	164	67	S ₁	330	21	S ₁
349	58	S ₁	119	63	S ₂	356	45	S ₁	164	63	S ₁	334	28	S ₁
33	27	S ₁	119	67	S ₂	345	47	S ₁	167	72	S ₁	355	81	S ₂
112	24	S ₁	128	80	S ₂	323	60	S ₁	172	78	S ₁	343	90	S ₂
21	29	S ₁	132	71	S ₂	321	48	S ₁	205	33	S ₁	342	88	S ₂
340	70	S ₁	131	80	S ₂	328	62	S ₁	206	30	S ₁	342	87	S ₂
332	70	S ₁	139	72	S ₂	303	60	S ₁	190	37	S ₁	357	78	S ₂
354	86	S ₁	133	72	S ₂	308	56	S ₁	190	45	S ₁	353	75	S ₂
357	72	S ₁	132	69	S ₂	300	85	S ₁	161	34	S ₁	359	60	S ₂
349	88	S ₁	137	84	S ₂	309	70	S ₁	174	45	S ₁	345	46	S ₂
346	65	S ₁	136	86	S ₂	269	58	S ₁	166	35	S ₁	144	80	S ₂
8	57	S ₁	138	74	S ₂	328	60	S ₁	173	35	S ₁	155	72	S ₂
324	43	S ₁	133	80	S ₂	314	59	S ₁	188	40	S ₁	325	86	S ₂
329	9	S ₁	150	90	S ₂	309	26	S ₁	196	37	S ₁	309	73	S ₂
312	42	S ₁	158	87	S ₂	325	37	S ₁	19	24	S ₁	333	85	S ₂
145	81	S ₁	148	76	S ₂	332	48	S ₁	14	30	S ₁	318	83	S ₂
153	88	S ₁	142	78	S ₂	331	49	S ₁	10	20	S ₁	16	69	S ₂
5	86	S ₁	148	78	S ₂	272	22	S ₁	106	27	S ₁	15	79	S ₂
165	35	S ₁	158	68	S ₂	247	21	S ₁	13	67	S ₁	21	80	S ₂
146	27	S ₁	150	82	S ₂	303	51	S ₁	357	59	S ₁	22	76	S ₂
146	20	S ₁	146	84	S ₂	316	54	S ₁	18	80	S ₁	348	63	S ₂
347	53	S ₁	150	82	S ₂	331	39	S ₁	11	81	S ₁	349	74	S ₂
335	69	S ₁	142	82	S ₂	327	38	S ₁	167	36	S ₁	358	67	S ₂
329	65	S ₁	288	58	S ₂	339	55	S ₁	162	22	S ₁	344	46	S ₂
338	57	S ₁	290	73	S ₂	340	54	S ₁	180	54	S ₁	351	59	S ₂
335	50	S ₁	134	71	S ₂	292	75	S ₁	199	56	S ₁	353	70	S ₂
280	32	S ₁	293	76	S ₂	304	86	S ₁	210	45	S ₁	332	79	S ₂
344	54	S ₁	121	90	S ₂	251	37	S ₁	191	45	S ₁	345	71	S ₂
351	64	S ₁	310	67	S ₂	259	39	S ₁	224	38	S ₁	330	45	S ₂
334	55	S ₁	133	80	S ₂	152	26	S ₁	134	23	S ₁	334	71	S ₂
340	60	S ₁	129	63	S ₂	161	24	S ₁	121	24	S ₁	330	64	S ₂
342	72	S ₁	120	64	S ₂	98	35	S ₁	194	38	S ₁	324	67	S ₂
332	65	S ₁	162	82	S ₂	93	31	S ₁	203	53	S ₁	330	64	S ₂
341	72	S ₁	153	75	S ₂	130	83	S ₁	200	58	S ₁	330	64	S ₂
12	55	S ₁	162	82	S ₂	134	64	S ₁	136	78	S ₁	319	67	S ₂
10	58	S ₁	153	75	S ₂	291	48	S ₁	150	58	S ₁	330	69	S ₂
5	64	S ₁	356	39	S ₂	291	40	S ₁	147	63	S ₁	323	63	S ₂
253	8	S ₁	334	62	S ₂	301	46	S ₁	144	69	S ₁	319	81	S ₂
215	18	S ₁	45	30	S ₂	240	34	S ₁	160	67	S ₁	342	40	S ₂
160	65	S ₁	33	33	S ₂	256	35	S ₁	203	55	S ₁	332	35	S ₂
170	90	S ₁	347	46	S ₂	155	72	S ₁	192	64	S ₁	332	49	S ₂
156	60	S ₁	333	37	S ₂	141	45	S ₁	216	35	S ₁	333	53	S ₂
150	80	S ₁	150	80	S ₂	157	54	S ₁	170	65	S ₁	352	37	S ₂

Supporting Table 1: raw data of structural measurements

Domain A			Domain B			Domain C			Domain D			Domain E		
334	74	S ₁	161	85	S ₂	308	50	S ₁	186	55	S ₁	342	48	S ₂
173	25	S ₁	145	88	S ₂	306	54	S ₁	196	37	S ₁	345	49	S ₂
115	3	S ₁	161	78	S ₂	306	46	S ₁	296	39	S ₁	352	52	S ₂
80	42	S ₁	149	62	S ₂	341	67	S ₁	186	73	S ₁	354	52	S ₂
350	84	S ₁	332	82	S ₂	331	58	S ₁	214	51	S ₁	359	52	S ₂
145	45	S ₁	326	86	S ₂	333	61	S ₁	198	13	S ₁	6	45	S ₂
120	52	S ₁	345	77	S ₂	331	50	S ₁	196	14	S ₁	328	52	S ₂
348	57	S ₁	28	73	S ₂	322	72	S ₁	2	40	S ₁	340	73	S ₂
194	83	S ₁	30	88	S ₂	318	48	S ₁	58	45	S ₁	44	54	S ₂
40	72	S ₁	271	20	S ₂	176	65	S ₁	290	15	S ₁	355	46	S ₂
7	61	S ₁	159	30	S ₂	188	69	S ₁	113	18	S ₁	343	48	S ₂
347	67	S ₁	135	36	S ₂	299	56	S ₁	172	63	S ₁	331	50	S ₂
347	37	S ₁	258	85	C _{dex}	304	56	S ₁	179	43	S ₁	358	51	S ₂
356	39	S ₁	38	77	C _{dex}	302	60	S ₁	182	80	S ₁	325	40	S ₂
172	55	S ₁	22	72	C _{dex}	338	47	S ₁	168	46	S ₁	5	61	S ₂
184	57	S ₁	356	39	C _{rev}	333	45	S ₁	174	53	S ₁	324	65	S ₂
358	70	S ₁	352	45	C _{rev}	310	41	S ₁	172	65	S ₁	10	43	S ₂
344	65	S ₁	11	66	C _{rev}	228	21	S ₁	186	71	S ₁	342	84	S ₂
350	55	S ₁	194	74	C _{rev}	300	6	S ₁	189	80	S ₁	333	57	S ₂
355	68	S ₁	131	73	C _{sin}	301	50	S ₁	343	46	S ₁	152	70	S ₂
6	45	S ₁	124	72	C _{sin}	288	58	S ₁	0	52	S ₁	168	71	S ₂
2	37	S ₁	140	70	C _{sin}	280	43	S ₁	145	35	S ₁	332	85	S ₂
332	34	S ₁	296	75	C _{sin}	174	21	S ₁	32	22	S ₁	143	80	S ₂
337	37	S ₁	304	85	C _{sin}	325	25	S ₁	172	33	S ₁	308	88	S ₂
346	67	S ₁	112	82	C _{sin}	269	18	S ₁	121	42	S ₁	343	66	S ₂
334	54	S ₁	210	78	C _{sin}	177	23	S ₁	139	28	S ₁	343	52	S ₂
172	84	S ₁	11	63	C _{sin}	291	37	S ₁	182	24	S ₁	244	90	S ₂
355	86	S ₁	39	78	C _{sin}	200	24	S ₁	146	36	S ₁	244	90	S ₂
334	35	S ₁	5	65	C _{sin}	281	49	S ₁	172	54	S ₁	337	72	S ₂
341	54	S ₁	186	80	C _{sin}	273	48	S ₁	178	43	S ₁	348	87	S ₂
342	50	S ₁	17	86	C _{sin}	333	54	S ₁	149	38	S ₁	331	70	S ₂
352	60	S ₁	139	79	C _{sin}	325	42	S ₁	206	46	S ₁	334	86	S ₂
356	72	S ₁	135	85	C _{sin}	303	33	S ₁	178	87	S ₁	329	42	S ₂
348	70	S ₁	129	72	C _{sin}	16	29	S ₁	187	82	S ₁	327	54	S ₂
324	27	S ₁	323	86	C _{sin}	309	49	S ₁	9	68	S ₁	343	53	S ₂
329	26	S ₁	125	60	C _{sin}	19	90	S ₁	359	62	S ₁	340	57	S ₂
331	44	S ₁	152	61	C _{sin}	2	70	S ₁	342	72	S ₁	318	51	S ₂
349	59	S ₁	162	70	C _{sin}	318	52	S ₁	341	42	S ₁	176	40	S ₂
342	70	S ₁	126	74	C _{sin}	343	74	S ₁	327	60	S ₁	156	68	S ₂
345	55	S ₁	128	79	C _{sin}	314	56	S ₁	280	34	S ₁	170	47	S ₂
340	56	S ₁	126	82	C _{sin}	344	38	S ₁	10	66	S ₁	292	90	S ₂
346	35	S ₁	137	90	C _{sin}	276	48	S ₁	37	30	S ₁	140	80	S ₂
344	50	S ₁	135	84	C _{sin}	326	46	S ₁	353	78	S ₁	134	80	S ₂
345	23	S ₁	137	75	C _{sin}	317	48	S ₁	339	84	S ₁	300	82	S ₂
149	37	S ₁	122	78	C _{sin}	334	81	S ₁	338	49	S ₁	334	36	S ₂

Supporting Table 1: raw data of structural measurements

Domain A			Domain B			Domain C			Domain D			Domain E		
5	71	S ₁	118	70	C _{sin}	353	81	S ₁	118	18	S ₁	339	21	S ₂
338	40	S ₁	122	70	C _{sin}	5	67	S ₁	146	54	S ₁	264	79	S ₂
310	62	S ₁	330	85	C _{sin}	24	77	S ₁	158	82	S ₁	273	76	S ₂
345	60	S ₁	335	88	C _{sin}	343	54	S ₁	152	65	S ₁	167	85	S ₂
331	73	S ₁	350	87	C _{sin}	189	46	S ₁	163	68	S ₁	166	78	S ₂
320	75	S ₁	348	85	C _{sin}	289	29	S ₁	328	86	S ₁	357	67	S ₂
350	81	S ₁	126	60	C _{sin}	202	58	S ₁	156	80	S ₁	11	64	S ₂
295	45	S ₁	311	78	C _{sin}	231	32	S ₁	156	32	S ₁	285	10	S ₃
338	55	S ₁	296	75	C _{sin}	207	20	S ₁	158	30	S ₁	220	28	S ₃
353	80	S ₁	304	85	C _{sin}	258	52	S ₁	140	24	S ₁	306	7	S ₃
153	76	S ₁	112	82	C _{sin}	340	52	S ₁	121	20	S ₁	353	19	S ₃
130	68	S ₁	291	65	C _{sin}	2	44	S ₁	144	23	S ₁	100	36	S ₃
143	62	S ₁	164	66	C _{sin}	173	5	S ₁	188	23	S ₁	319	16	S ₃
136	70	S ₁	298	68	C _{sin}	67	29	S ₁	337	85	S ₁	289	45	S ₃
144	75	S ₁	320	85	C _{sin}	305	21	S ₁	357	82	S ₁	248	46	S ₃
138	66	S ₁	178	82	C _{sin}	173	15	S ₁	1	84	S ₁	277	53	S ₃
140	74	S ₁	191	78	C _{sin}	81	54	S ₁	168	30	S ₁	197	30	S ₃
142	79	S ₁	181	74	C _{sin}	214	35	S ₁	137	28	S ₁	308	59	S ₃
137	40	S ₁	192	84	C _{sin}	44	20	S ₁	168	35	S ₁	226	19	S ₃
161	51	S ₁	30	53	C _{sin}	24	16	S ₁	178	42	S ₁	253	32	S ₃
154	69	S ₁	321	78	C _{sin}	4	20	S ₁	190	56	S ₁	263	30	S ₃
316	33	S ₁	317	90	C _{sin}	26	56	S ₁	175	62	S ₁	315	28	S ₃
144	84	S ₁	322	82	C _{sin}	48	31	S ₁	174	30	S ₁	300	30	S ₃
140	75	S ₁	157	51	C' _{dex}	78	79	S ₁	112	36	S ₁	339	60	S ₃
141	56	S ₁	4	79	C' _{dex}	65	79	S ₁	66	45	S ₁	335	50	S ₃
176	48	S ₁	174	73	C' _{dex}	52	37	S ₁	30	39	S ₁	266	18	S ₃
170	67	S ₁	96	46	C' _{nor}	33	46	S ₁	118	25	S ₁	284	27	S ₃
299	50	S ₁	133	43	C' _{nor}	15	39	S ₁	170	65	S ₁	338	18	S ₃
289	52	S ₁	102	49	C' _{nor}	340	53	S ₁	357	68	S ₁	344	16	S ₃
262	24	S ₁	83	55	C' _{nor}	257	39	S ₁	152	63	S ₁	118	20	S ₃
238	15	S ₁	66	51	C' _{nor}	337	44	S ₁	17	72	S ₁	286	24	S ₃
183	39	S ₁	68	25	C' _{nor}	347	42	S ₁	174	85	S ₁	286	26	S ₃
312	67	S ₁	60	54	C' _{nor}	341	50	S ₁	148	78	S ₁	333	39	S ₃
310	67	S ₁	80	45	C' _{nor}	335	65	S ₁	170	66	S ₁	357	65	S ₃
324	80	S ₁	91	71	C' _{nor}	331	58	S ₁	338	84	S ₁	341	56	S ₃
326	78	S ₁	141	67	C' _{nor}	326	67	S ₁	176	84	S ₁	259	59	S ₃
288	59	S ₁	99	74	C' _{nor}	331	45	S ₁	333	79	S ₁	294	54	S ₃
308	66	S ₁	64	50	C' _{nor}	321	40	S ₁	178	22	S ₁	280	47	S ₃
176	56	S ₁	139	45	C' _{sin}	338	40	S ₁	320	24	S ₁	285	57	S ₃
164	62	S ₁	119	86	C' _{sin}	356	45	S ₁	114	40	S ₁	305	55	S ₃
145	66	S ₁	113	75	C' _{sin}	320	43	S ₁	113	24	S ₁	110	25	S ₃
153	66	S ₁	97	81	C' _{sin}	353	51	S ₁	6	14	S ₁	87	32	S ₃
170	53	S ₁	129	74	C' _{sin}	338	41	S ₁	143	37	S ₁	292	38	S ₃
169	57	S ₁	132	90	C' _{sin}	308	34	S ₁	307	36	S ₁	100	23	S ₃
140	62	S ₁	316	82	C' _{sin}	329	33	S ₁	148	73	S ₁	305	30	S ₃

Supporting Table 1: raw data of structural measurements

Domain A			Domain B			Domain C			Domain D			Domain E		
140	67	S_1	320	88	C'_{sin}	358	36	S_1	138	68	S_1	311	28	S_3
183	63	S_1	141	78	C'_{sin}	11	26	S_1	336	68	S_1	336	38	S_3
301	87	S_1	149	80	C'_{sin}	16	36	S_1	333	71	S_1	316	36	S_3
321	61	S_1	101	76	C'_{sin}	329	9	S_1	328	61	S_1	336	31	S_3
166	39	S_1	102	80	C'_{sin}	307	14	S_1	81	10	S_1	262	28	S_3
164	70	S_1	104	80	C'_{sin}	65	24	S_1	321	32	S_1	216	35	S_3
153	70	S_1	124	83	C'_{sin}	350	28	S_1	174	20	S_1	14	25	S_3
168	56	S_1	108	82	C'_{sin}	288	25	S_1	307	38	S_1	326	36	S_3
244	22	S_1	296	84	C'_{sin}	294	39	S_1	311	47	S_1	326	46	S_3
150	77	S_1	110	85	C'_{sin}	338	40	S_1	353	69	S_1	314	40	S_3
287	23	S_1	106	81	C'_{sin}	335	39	S_1	216	58	S_1	285	32	S_3
164	24	S_1	33	17	AP_1	328	30	S_1	298	30	S_1	287	28	S_3
58	33	S_1	6	30	AP_1	18	30	S_1	181	26	S_1	293	41	S_3
319	44	S_1	31	41	AP_1	21	20	S_1	174	41	S_1	283	44	S_3
326	51	S_1	31	40	AP_1	324	27	S_1	166	50	S_1	282	38	S_3
354	21	S_1	33	36	AP_1	341	33	S_1	109	28	S_1	292	39	S_3
225	14	S_1	59	37	AP_1	332	50	S_1	136	31	S_1	282	37	S_3
57	21	S_1	58	34	AP_1	339	39	S_1	77	22	S_1	286	32	S_3
289	17	S_1	48	29	AP_1	296	41	S_1	154	47	S_1	309	30	S_3
130	27	S_1	52	35	AP_1	312	40	S_1	185	48	S_1	325	30	S_3
193	18	S_1	64	48	AP_1	315	37	S_1	121	55	S_1	298	26	S_3
154	4	S_1	59	29	AP_1	323	33	S_1	128	34	S_1	301	27	S_3
255	20	S_1	85	23	AP_1	304	40	S_1	112	32	S_1	285	29	S_3
226	19	S_1	73	27	AP_1	313	38	S_1	125	30	S_1	204	14	S_3
339	19	S_1	96	26	AP_1	322	58	S_1	140	41	S_1	214	7	S_3
215	21	S_1	28	43	AP_1	315	70	S_1	166	22	S_1	259	12	S_3
337	42	S_1	71	39	AP_1	316	59	S_1	163	34	S_1	317	11	S_3
305	15	S_1	320	76	AP_2	308	40	S_1	218	32	S_1	160	17	S_3
294	10	S_1	30	53	AP_2	301	56	S_1	188	26	S_1	230	45	S_3
311	31	S_1	209	72	AP_2	304	49	S_1	172	35	S_1	6	41	S_3
172	23	S_1	205	61	AP_2	306	55	S_1	166	62	S_1	262	13	S_3
181	35	S_1	214	66	AP_2	329	68	S_1	218	30	S_1	209	34	S_3
335	50	S_1	216	56	AP_2	331	58	S_1	206	25	S_1	0	0	S_3
44	21	S_1	202	62	AP_2	325	59	S_1	192	10	S_1	270	27	S_3
326	36	S_1	234	36	AP_2	313	77	S_1	357	43	S_1	269	24	S_3
168	38	S_1	259	78	AP_2	335	52	S_1	276	35	S_1	254	11	S_3
208	11	S_1	268	82	AP_2	323	63	S_1	285	38	S_1	256	6	S_3
244	11	S_1	191	82	AP_2	325	71	S_1	301	55	S_1	323	21	S_3
336	26	S_1	356	82	AP_2	328	79	S_1	222	66	S_1	236	20	S_3
321	44	S_1	171	85	AP_2	333	68	S_1	198	75	S_1	292	34	S_3
289	23	S_1	180	90	AP_2	347	48	S_1	359	61	S_1	300	33	S_3
127	25	S_1	166	82	AP_2	347	48	S_1	348	36	S_1	309	48	S_3
131	16	S_1	344	80	AP_2	334	71	S_1	352	67	S_1	53	11	S_3
190	3	S_1	167	86	AP_2	337	60	S_1	357	42	S_1	299	25	S_3
146	39	S_1	167	87	AP_2	341	64	S_1	348	63	S_1	96	15	S_3

Supporting Table 1: raw data of structural measurements

Domain A			Domain B			Domain C			Domain D			Domain E		
201	10	S ₁	352	47	AP ₂	335	77	S ₁	354	60	S ₁	300	30	S ₃
188	44	S ₁	355	48	AP ₂	344	69	S ₁	350	57	S ₁	286	34	S ₃
166	58	S ₁	346	76	AP ₂	326	57	S ₁	159	24	S ₁	281	40	S ₃
183	42	S ₁	11	45	AP ₂	153	62	S ₁	168	18	S ₁	267	47	S ₃
178	79	S ₁	349	66	AP ₂	154	42	S ₁	164	23	S ₁	273	34	S ₃
158	51	S ₁	92	74	AP ₂	161	39	S ₁	148	25	S ₁	300	37	S ₃
209	34	S ₁	83	70	AP ₂	150	62	S ₁	176	25	S ₁	302	40	S ₃
186	42	S ₁	315	75	AP ₂	357	88	S ₁	166	9	S ₁	320	58	S ₃
165	55	S ₁	296	58	AP ₂	199	60	S ₁	170	37	S ₁	320	52	S ₃
152	79	S ₁	272	22	AP ₂	196	53	S ₁	130	11	S ₁	323	56	S ₃
147	82	S ₁	204	30	AP ₂	198	66	S ₁	254	15	S ₁	299	40	S ₃
149	58	S ₁	153	50	AP ₂	169	90	S ₁	258	6	S ₁	320	40	S ₃
174	48	S ₁	125	16	AP ₂	325	47	S ₁	136	45	S ₁	306	29	S ₃
151	45	S ₁	251	50	AP ₂	307	51	S ₁	120	36	S ₁	251	41	S ₃
173	53	S ₁	234	58	AP ₂	303	47	S ₁	116	28	S ₁	222	62	S ₃
152	59	S ₁	109	81	AP ₂	28	15	S ₁	172	56	S ₁	286	27	S ₃
172	37	S ₁	225	80	AP ₂	296	29	S ₁	156	75	S ₁	314	14	S ₃
147	26	S ₁	345	35	AP ₂	156	51	S ₁	170	65	S ₁	255	26	S ₃
165	38	S ₁	227	47	AP ₂	126	45	S ₁	153	57	S ₁	2	26	S ₃
269	19	S ₁	291	48	AP ₂	139	44	S ₁	172	49	S ₁	338	39	S ₃
131	17	S ₁	311	62	AP ₂	103	40	S ₁	188	52	S ₁	330	21	S ₃
311	16	S ₁	249	43	AP ₂	327	67	S ₁	148	26	S ₁	296	50	S ₃
212	45	S ₁	312	70	AP ₂	116	72	S ₁	162	25	S ₁	268	35	S ₃
194	63	S ₁	185	25	AP ₂	91	38	S ₁	173	49	S ₁	254	7	S ₃
333	74	S ₁	280	15	AP ₂	110	25	S ₁	183	63	S ₁	307	23	S ₃
338	66	S ₁	148	24	AP ₂	141	35	S ₁	190	42	S ₁	281	23	S ₃
331	15	S ₁	160	90	AP ₂	153	45	S ₁	157	55	S ₁	265	23	S ₃
0	0	S ₁	350	80	AP ₂	148	51	S ₁	172	50	S ₁	78	8	S ₃
349	37	S ₁	162	82	AP ₂	325	78	S ₁	171	60	S ₁	66	10	S ₃
342	24	S ₁	271	20	AP ₂	180	58	S ₁	166	39	S ₁	91	2	S ₃
263	16	S ₁	159	30	AP ₂	137	54	S ₁	178	40	S ₁	231	19	S ₃
332	62	S ₁	135	36	AP ₂	128	58	S ₁	174	38	S ₁	285	12	S ₃
347	45	S ₁	28	73	AP ₂	129	33	S ₁	211	27	S ₁	288	22	S ₃
317	30	S ₁	30	88	AP ₂	101	41	S ₁	185	19	S ₁	2	67	AP ₁
312	63	S ₁	152	68	AP ₂	250	27	S ₁	203	44	S ₁	6	64	AP ₁
316	63	S ₁	163	82	AP ₂	247	16	S ₁	183	63	S ₁	17	67	AP ₁
302	57	S ₁	159	51	AP ₂	50	52	S ₁	200	67	S ₁	62	22	AP ₁
117	30	S ₁	332	82	AP ₂	72	55	S ₁	194	22	S ₁	188	40	AP ₁
156	55	S ₁	326	86	AP ₂	331	15	S ₁	323	33	S ₁	220	14	AP ₁
146	65	S ₁	345	77	AP ₂	266	24	S ₁	302	21	S ₁	244	18	AP ₁
194	25	S ₁	100	9	FA ₁	265	35	S ₁	273	23	S ₁	256	25	AP ₁
300	29	S ₁	132	3	FA ₁	355	25	S ₁	158	30	S ₁	280	28	AP ₁
324	42	S ₁	328	22	FA ₁	47	26	S ₁	168	27	S ₁	291	24	AP ₁
244	8	S ₁	124	4	FA ₁	69	22	S ₁	243	21	S ₁	300	30	AP ₁
324	58	S ₁	312	3	FA ₁	52	24	S ₁	165	44	S ₁	320	45	AP ₁

Supporting Table 1: raw data of structural measurements

Domain A			Domain B			Domain C			Domain D			Domain E		
323	54	S ₁	310	3	FA ₁	69	32	S ₁	203	17	S ₁	321	57	AP ₁
289	40	S ₁	272	42	FA ₂	63	13	S ₁	230	13	S ₁	332	40	AP ₁
304	45	S ₁	262	24	FA ₂	359	49	S ₁	212	58	S ₁	335	38	AP ₁
334	80	S ₁	280	23	FA ₂	328	54	S ₁	207	68	S ₁	336	34	AP ₁
342	82	S ₁	278	22	FA ₂	337	54	S ₁	200	83	S ₁	337	45	AP ₁
319	72	S ₁	288	12	FA ₂	340	46	S ₁	238	64	S ₁	354	40	AP ₁
342	35	S ₁	288	8	FA ₂	341	38	S ₁	234	62	S ₁	357	67	AP ₁
327	50	S ₁	320	30	FA ₂	341	58	S ₁	211	70	S ₁	357	59	AP ₁
315	36	S ₁	283	2	FA ₂	336	64	S ₁	216	76	S ₁	341	78	AP ₂
340	52	S ₁	72	40	FA ₂	328	68	S ₁	200	81	S ₁	342	84	AP ₂
332	56	S ₁	85	19	FA ₂	99	66	S ₁	210	70	S ₁	0	25	AP ₂
334	46	S ₁	83	22	FA ₂	101	67	S ₁	222	68	S ₁	0	63	AP ₂
190	21	S ₁	53	42	FA ₂	115	66	S ₁	217	68	S ₁	2	76	AP ₂
307	37	S ₁	83	47	FA ₂	54	87	S ₁	222	76	S ₁	2	88	AP ₂
328	48	S ₁	73	32	FA ₂	232	75	S ₁	210	65	S ₁	2	79	AP ₂
352	62	S ₁	53	24	FA ₂	11	67	S ₁	198	66	S ₁	2	67	AP ₂
349	60	S ₁	67	40	FA ₂	32	69	S ₁	168	50	S ₁	2	67	AP ₂
354	61	S ₁	74	42	FA ₂	23	65	S ₁	167	71	S ₁	3	67	AP ₂
346	56	S ₁	55	45	FA ₂	16	62	S ₁	172	84	S ₁	3	50	AP ₂
346	60	S ₁	349	43	FA ₂	44	60	S ₁	169	62	S ₁	5	55	AP ₂
193	14	S ₁	359	37	FA ₂	34	65	S ₁	188	73	S ₁	5	77	AP ₂
188	16	S ₁	36	33	FA ₂	37	58	S ₁	180	78	S ₁	5	44	AP ₂
191	13	S ₁	21	39	FA ₂	297	72	S ₁	171	66	S ₁	6	44	AP ₂
335	67	S ₁	114	20	FA ₂	344	66	S ₁	202	75	S ₁	6	56	AP ₂
335	77	S ₁	121	20	FA ₂	322	82	S ₁	188	64	S ₁	7	87	AP ₂
330	88	S ₁	125	16	FA ₂	288	42	S ₁	189	54	S ₁	7	58	AP ₂
2	33	S ₁	44	44	FA ₂	309	47	S ₁	192	64	S ₁	8	59	AP ₂
32	17	S ₁	22	0	FA ₂	304	74	S ₁	204	80	S ₁	8	18	AP ₂
30	14	S ₁	235	60	FA ₂	310	45	S ₁	217	81	S ₁	10	54	AP ₂
6	44	S ₁	225	15	FA ₂	319	50	S ₁	16	78	S ₁	10	64	AP ₂
256	36	S ₁	202	10	FA ₂	334	50	S ₁	45	72	S ₁	11	53	AP ₂
12	45	S ₁	208	5	FA ₂	326	47	S ₁	158	14	S ₁	12	34	AP ₂
11	66	S ₁	256	17	FA ₂	348	60	S ₁	162	57	S ₁	12	33	AP ₂
9	48	S ₁	71	70	FA ₂	314	58	S ₁	173	62	S ₁	12	65	AP ₂
316	40	S ₁	210	48	FA ₂	337	68	S ₁	182	59	S ₁	13	48	AP ₂
313	38	S ₁	240	20	FA ₂	150	82	S ₁	121	88	S ₁	14	45	AP ₂
321	26	S ₁	98	26	FA ₂	198	42	S ₁	62	58	S ₁	16	57	AP ₂
325	36	S ₁	110	21	FA ₂	111	72	S ₁	60	63	S ₁	16	50	AP ₂
158	72	S ₁	300	10	L ₁	150	60	S ₁	61	57	S ₁	17	50	AP ₂
156	79	S ₁	297	22	L ₁	144	70	S ₁	89	65	S ₁	18	65	AP ₂
137	27	S ₁	253	17	L ₁	308	72	S ₁	61	723	S ₁	19	52	AP ₂
216	34	S ₁	231	16	L ₂	162	82	S ₁	100	73	S ₁	21	57	AP ₂
353	25	S ₁	108	6	L ₂	188	77	S ₁	103	64	S ₁	21	17	AP ₂
357	28	S ₁	284	34	L ₂	171	58	S ₁	100	74	S ₁	21	87	AP ₂
344	62	S ₁	114	13	L ₂	157	41	S ₁	155	80	S ₁	22	76	AP ₂

Supporting Table 1: raw data of structural measurements

Domain A			Domain B			Domain C			Domain D			Domain E		
358	63	S ₁	282	40	L ₂	152	46	S ₁	5	45	S ₁	26	80	AP ₂
178	38	S ₁	278	4	L ₂	160	47	S ₁	346	31	S ₁	28	67	AP ₂
181	46	S ₁	226	4	L ₂	156	38	S ₁	353	54	S ₁	29	54	AP ₂
154	15	S ₁	232	8	L ₂	135	40	S ₁	357	45	S ₁	30	46	AP ₂
183	37	S ₁	268	8	L ₂	195	24	S ₁	342	54	S ₁	32	62	AP ₂
183	34	S ₁	277	7	L ₂	185	15	S ₁	9	18	S ₁	34	42	AP ₂
168	33	S ₁	275	11	L ₂	195	18	S ₁	0	42	S ₁	34	50	AP ₂
161	32	S ₁	253	27	L ₂	315	45	S ₁	336	17	S ₁	41	47	AP ₂
121	21	S ₁	246	2	L ₂	333	52	S ₁	4	35	S ₁	42	87	AP ₂
147	14	S ₁	226	29	L ₂	308	78	S ₁	344	22	S ₁	61	88	AP ₂
165	16	S ₁	228	21	L ₂	318	78	S ₁	358	34	S ₁	70	64	AP ₂
146	22	S ₁	255	13	L ₂	320	72	S ₁	346	48	S ₁	74	83	AP ₂
164	33	S ₁	235	23	L ₂	17	31	S ₁	337	14	S ₁	92	53	AP ₂
352	54	S ₁	238	22	L ₂	34	42	S ₁	325	55	S ₁	95	74	AP ₂
350	73	S ₁	270	13	L ₂	57	35	S ₁	312	53	S ₁	154	58	AP ₂
354	72	S ₁	268	10	L ₂	80	60	S ₁	336	72	S ₁	160	71	AP ₂
358	54	S ₁	32	24	L ₂	6	28	S ₁	322	64	S ₁	175	82	AP ₂
11	48	S ₁	20	22	L ₂	335	38	S ₁	39	80	S ₁	187	75	AP ₂
338	68	S ₁	36	17	L ₂	112	38	S ₁	72	65	S ₁	190	52	AP ₂
348	36	S ₁	61	11	L ₂	150	50	S ₁	42	75	S ₁	219	70	AP ₂
351	73	S ₁	235	7	L ₂	22	49	S ₁	296	80	S ₁	221	40	AP ₂
351	63	S ₁	58	2	L ₂	22	62	S ₁	148	82	S ₁	229	49	AP ₂
337	63	S ₁	43	8	L ₂	44	40	S ₁	137	79	S ₁	239	85	AP ₂
347	54	S ₁	48	9	L ₂	349	12	S ₁	138	86	S ₁	246	78	AP ₂
350	57	S ₁	47	13	L ₂	291	35	S ₁	288	80	S ₁	257	68	AP ₂
355	62	S ₁	46	12	L ₂	193	24	S ₁	332	86	S ₁	258	68	AP ₂
351	62	S ₁	53	13	L ₂	198	24	S ₁	103	84	S ₁	289	19	AP ₂
349	70	S ₁	72	3	L ₂	185	21	S ₁	137	90	S ₁	304	22	AP ₂
349	67	S ₁	58	30	L ₂	160	28	S ₁	150	80	S ₁	309	14	AP ₂
349	71	S ₁	40	0	L _{sin}	192	16	S ₁	100	81	S ₁	313	44	AP ₂
359	75	S ₁	38	3	L _{sin}	164	39	S ₁	102	81	S ₁	317	90	AP ₂
0	83	S ₁	210	4	L _{sin}	160	26	S ₁	158	82	S ₁	318	56	AP ₂
355	90	S ₁	36	5	L _{sin}	228	10	S ₁	119	73	S ₁	327	46	AP ₂
350	60	S ₁	34	7	L _{sin}	245	9	S ₁	128	66	S ₁	333	23	AP ₂
350	61	S ₁	35	0	L _{sin}	266	13	S ₁	109	65	S ₁	334	90	AP ₂
359	69	S ₁	59	4	L _{sin}	281	31	S ₁	138	61	S ₁	335	38	AP ₂
349	60	S ₁	249	2	L _{sin}	256	36	S ₁	91	87	S ₁	337	20	AP ₂
350	50	S ₁	58	15	L _{sin}	348	54	S ₁	276	80	S ₁	338	35	AP ₂
219	9	S ₁	58	15	L _{nor}	342	36	S ₁	138	82	S ₁	339	90	AP ₂
226	26	S ₁	220	23	L _{dex}	322	36	S ₁	257	85	S ₁	340	35	AP ₂
195	30	S ₁	227	12	L _{dex}	294	55	S ₁	233	81	S ₁	342	60	AP ₂
194	53	S ₁				296	50	S ₁	147	82	S ₁	342	47	AP ₂
198	48	S ₁				291	56	S ₁	113	81	S ₁	342	28	AP ₂
194	51	S ₁				316	41	S ₁	134	80	S ₁	343	65	AP ₂
192	53	S ₁				298	41	S ₁	190	80	S ₁	344	83	AP ₂

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
56	61	S ₁	139	65	S ₂	313	39	S ₁	186	78	S ₁	344	25	AP ₂
56	64	S ₁	346	65	S ₂	331	37	S ₁	142	68	S ₁	345	55	AP ₂
60	84	S ₁	342	68	S ₂	326	33	S ₁	130	78	S ₁	345	49	AP ₂
277	39	S ₁	8	74	S ₂	325	37	S ₁	115	49	S ₁	345	19	AP ₂
351	77	S ₁	317	75	S ₂	312	55	S ₁	6	41	S ₁	346	86	AP ₂
351	78	S ₁	320	72	S ₂	303	54	S ₁	0	45	S ₁	346	60	AP ₂
359	72	S ₁	102	52	S ₂	309	45	S ₁	330	38	S ₁	346	58	AP ₂
8	74	S ₁	128	75	S ₂	312	53	S ₁	328	38	S ₁	346	38	AP ₂
6	67	S ₁	319	82	S ₂	318	58	S ₁	10	33	S ₁	347	61	AP ₂
0	70	S ₁	342	90	S ₂	312	48	S ₁	3	26	S ₁	347	52	AP ₂
2	71	S ₁	342	72	S ₂	310	86	S ₁	1	41	S ₁	348	64	AP ₂
186	72	S ₁	357	78	S ₂	139	84	S ₁	342	45	S ₁	349	84	AP ₂
351	80	S ₁	189	63	S ₂	144	87	S ₁	2	58	S ₁	350	50	AP ₂
357	78	S ₁	173	53	S ₂	324	90	S ₁	356	52	S ₁	351	61	AP ₂
156	42	S ₁	199	52	S ₂	148	88	S ₁	334	30	S ₁	351	76	AP ₂
159	37	S ₁	9	73	S ₂	200	23	S ₁	353	30	S ₁	352	47	AP ₂
156	78	S ₁	352	71	S ₂	172	28	S ₁	105	38	S ₁	352	66	AP ₂
159	76	S ₁	351	57	S ₂	181	24	S ₁	121	45	S ₁	353	50	AP ₂
152	45	S ₁	354	61	S ₂	189	18	S ₁	116	33	S ₁	353	70	AP ₂
146	30	S ₁	345	80	S ₂	184	12	S ₁	359	53	S ₁	353	79	AP ₂
150	32	S ₁	324	83	S ₂	205	60	S ₁	16	56	S ₁	353	19	AP ₂
156	82	S ₁	139	82	S ₂	202	61	S ₁	8	62	S ₁	353	53	AP ₂
153	83	S ₁	156	60	S ₂	196	65	S ₁	2	73	S ₁	353	51	AP ₂
142	38	S ₁	159	80	S ₂	197	50	S ₁	2	62	S ₁	355	57	AP ₂
152	45	S ₁	13	50	S ₂	184	72	S ₁	353	47	S ₁	355	58	AP ₂
146	60	S ₁	22	52	S ₂	210	68	S ₁	355	50	S ₁	356	65	AP ₂
142	58	S ₁	11	43	S ₂	204	50	S ₁	345	51	S ₁	357	60	AP ₂
139	51	S ₁	351	50	S ₂	218	42	S ₁	353	48	S ₁	358	26	AP ₂
150	69	S ₁	331	48	S ₂	206	65	S ₁	354	46	S ₁	359	87	AP ₂
181	35	S ₁	342	58	S ₂	195	50	S ₁	163	90	S ₁	359	65	AP ₂
162	82	S ₁	347	58	S ₂	202	51	S ₁	166	75	S ₁	359	38	AP ₂
157	82	S ₁	345	45	S ₂	196	55	S ₁	165	67	S ₁	348	61	AP ₂
162	76	S ₁	34	63	S ₂	196	45	S ₁	157	60	S ₁	351	78	AP ₂
345	84	S ₁	342	80	S ₂	20	88	S ₁	142	67	S ₁	355	72	AP ₂
321	78	S ₁	356	87	S ₂	197	88	S ₁	143	72	S ₁	359	49	AP ₂
336	72	S ₁	176	85	S ₂	183	51	S ₁	2	61	S ₂	350	32	AP ₃
352	66	S ₁	174	81	S ₂	210	65	S ₁	23	79	S ₂	343	40	AP ₃
16	57	S ₁	168	81	S ₂	198	72	S ₁	22	82	S ₂	3	20	AP ₃
9	58	S ₁	176	84	S ₂	327	23	S ₁	124	68	S ₂	3	21	AP ₃
152	60	S ₁	6	83	S ₂	17	33	S ₁	311	86	S ₂	4	64	AP ₃
169	55	S ₁	355	86	S ₂	149	60	S ₁	133	88	S ₂	6	30	AP ₃
352	56	S ₁	359	86	S ₂	301	31	S ₁	136	60	S ₂	10	64	AP ₃
350	50	S ₁	178	88	S ₂	159	90	S ₁	356	88	S ₂	15	78	AP ₃
351	74	S ₁	170	84	S ₂	167	56	S ₁	331	89	S ₂	17	87	AP ₃
345	75	S ₁	176	86	S ₂	194	39	S ₁	166	52	S ₂	21	20	AP ₃

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
347	67	S ₁	182	77	S ₂	198	54	S ₁	177	70	S ₂	28	38	AP ₃
338	54	S ₁	180	77	S ₂	202	23	S ₁	173	59	S ₂	34	85	AP ₃
341	65	S ₁	178	69	S ₂	192	35	S ₁	178	62	S ₂	34	31	AP ₃
341	52	S ₁	173	88	S ₂	308	30	S ₁	194	70	S ₂	56	23	AP ₃
340	55	S ₁	347	87	S ₂	341	46	S ₁	192	77	S ₂	70	90	AP ₃
331	74	S ₁	350	90	S ₂	343	45	S ₁	196	80	S ₂	164	53	AP ₃
345	85	S ₁	13	87	S ₂	342	45	S ₁	194	84	S ₂	166	75	AP ₃
352	66	S ₁	359	87	S ₂	157	45	S ₁	188	83	S ₂	172	67	AP ₃
336	62	S ₁	180	89	S ₂	347	60	S ₁	188	85	S ₂	179	72	AP ₃
342	50	S ₁	1	86	S ₂	348	60	S ₁	186	89	S ₂	191	70	AP ₃
233	36	S ₁	179	89	S ₂	351	54	S ₁	188	82	S ₂	195	8	AP ₃
154	65	S ₁	5	87	S ₂	219	40	S ₁	180	74	S ₂	196	82	AP ₃
153	50	S ₁	190	88	S ₂	235	33	S ₁	172	78	S ₂	200	80	AP ₃
56	25	S ₁	7	87	S ₂	220	46	S ₁	170	75	S ₂	207	71	AP ₃
74	45	S ₁	359	86	S ₂	239	18	S ₁	174	80	S ₂	213	4	AP ₃
30	34	S ₁	5	86	S ₂	208	30	S ₁	191	64	S ₂	218	57	AP ₃
98	25	S ₁	3	88	S ₂	234	11	S ₁	207	66	S ₂	222	62	AP ₃
88	41	S ₁	0	83	S ₂	218	18	S ₁	202	63	S ₂	229	28	AP ₃
312	35	S ₁	186	83	S ₂	27	60	S ₁	212	72	S ₂	236	76	AP ₃
316	41	S ₁	181	86	S ₂	219	37	S ₁	176	60	S ₂	251	18	AP ₃
329	75	S ₁	352	86	S ₂	191	18	S ₁	205	55	S ₂	256	88	AP ₃
324	69	S ₁	355	83	S ₂	153	25	S ₁	194	62	S ₂	257	72	AP ₃
212	24	S ₁	1	85	S ₂	198	23	S ₁	185	54	S ₂	264	24	AP ₃
165	38	S ₁	358	82	S ₂	181	26	S ₁	188	63	S ₂	281	25	AP ₃
328	54	S ₁	356	87	S ₂	309	25	S ₁	161	73	S ₂	284	26	AP ₃
332	54	S ₁	5	88	S ₂	288	74	S ₁	175	82	S ₂	303	20	AP ₃
329	76	S ₁	173	88	S ₂	268	78	S ₁	170	84	S ₂	313	23	AP ₃
334	64	S ₁	180	90	S ₂	108	82	S ₁	343	85	S ₂	337	34	AP ₃
330	61	S ₁	2	87	S ₂	280	71	S ₁	149	88	S ₂	351	54	AP ₃
351	50	S ₁	151	85	S ₂	122	86	S ₁	157	83	S ₂	353	13	AP ₃
355	51	S ₁	149	86	S ₂	109	75	S ₁	328	86	S ₂	1	57	AP ₃
331	59	S ₁	151	88	S ₂	113	72	S ₁	340	82	S ₂	351	55	AP ₃
328	56	S ₁	142	75	S ₂	114	69	S ₁	159	81	S ₂	353	49	AP ₃
328	70	S ₁	148	64	S ₂	261	41	S ₁	162	71	S ₂	355	56	AP ₃
341	45	S ₁	150	70	S ₂	240	20	S ₁	147	90	S ₂	207	16	AP ₃
342	49	S ₁	1	78	S ₂	254	31	S ₁	145	80	S ₂	345	64	AP ₃
316	80	S ₁	159	82	S ₂	298	17	S ₁	149	75	S ₂	15	90	C _{dex}
326	74	S ₁	160	75	S ₂	357	36	S ₁	5	62	S ₂	10	88	C _{dex}
321	81	S ₁	168	65	S ₂	307	12	S ₁	38	48	S ₂	38	54	C _{dex}
197	41	S ₁	134	73	S ₂	3	19	S ₁	15	52	S ₂	45	59	C _{dex}
195	30	S ₁	152	90	S ₂	22	21	S ₁	38	46	S ₂	32	65	C _{dex}
169	24	S ₁	338	80	S ₂	10	26	S ₁	9	39	S ₂	357	69	C _{dex}
171	27	S ₁	165	84	S ₂	19	21	S ₁	16	46	S ₂	25	75	C _{dex}
151	75	S ₁	311	13	S ₃	41	29	S ₁	338	39	S ₂	176	82	C _{dex}
151	73	S ₁	339	59	S ₃	346	32	S ₁	18	62	S ₂	240	29	C _{nor}

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
170	90	S ₁	339	59	S ₃	330	24	S ₁	344	51	S ₂	236	34	C _{nor}
169	89	S ₁	324	28	S ₃	334	32	S ₁	345	56	S ₂	299	58	C _{nor}
157	63	S ₁	322	30	S ₃	304	66	S ₁	14	52	S ₂	290	55	C _{nor}
149	75	S ₁	347	48	S ₃	94	78	S ₁	19	49	S ₂	313	55	C _{nor}
177	34	S ₁	357	67	C _{dex}	301	65	S ₁	49	30	S ₂	304	56	C _{nor}
157	60	S ₁	333	85	C _{dex}	297	67	S ₁	325	53	S ₂	283	49	C _{nor}
169	38	S ₁	350	85	C _{dex}	319	59	S ₁	10	57	S ₂	276	44	C _{nor}
179	39	S ₁	183	88	C _{dex}	316	64	S ₁	330	45	S ₂	211	32	C _{nor}
168	64	S ₁	130	90	C _{dex}	316	65	S ₁	10	46	S ₂	221	36	C _{nor}
164	65	S ₁	341	85	C _{dex}	294	45	S ₁	30	51	S ₂	205	48	C _{nor}
166	69	S ₁	161	81	C _{dex}	285	47	S ₁	330	69	S ₂	235	38	C _{nor}
292	27	S ₁	161	78	C _{dex}	275	52	S ₁	353	75	S ₂	207	22	C _{nor}
315	42	S ₁	188	58	C _{dex}	281	48	S ₁	25	50	S ₂	213	25	C _{nor}
317	37	S ₁	196	63	C _{dex}	291	62	S ₁	326	55	S ₂	169	43	C _{nor}
326	42	S ₁	8	76	C _{dex}	332	61	S ₁	339	81	S ₂	192	24	C _{nor}
328	67	S ₁	12	60	C _{dex}	332	68	S ₁	30	69	S ₂	177	38	C _{nor}
336	64	S ₁	11	83	C _{dex}	328	67	S ₁	16	63	S ₂	57	29	C _{nor}
137	48	S ₁	7	78	C _{dex}	310	65	S ₁	27	70	S ₂	82	48	C _{nor}
119	64	S ₁	22	88	C _{dex}	311	42	S ₁	179	78	S ₂	244	18	C _{nor}
140	62	S ₁	185	87	C _{dex}	310	54	S ₁	19	70	S ₂	1	53	C _{nor}
174	75	S ₁	188	65	C _{dex}	314	65	S ₁	4	75	S ₂	25	16	C _{nor}
166	84	S ₁	195	73	C _{dex}	337	77	S ₁	186	86	S ₂	348	38	C _{nor}
136	58	S ₁	199	69	C _{dex}	299	61	S ₁	355	79	S ₂	81	36	C _{nor}
196	84	S ₁	182	63	C _{dex}	316	78	S ₁	352	90	S ₂	108	27	C _{nor}
27	89	S ₁	333	76	C _{dex}	322	55	S ₁	180	87	S ₂	84	30	C _{nor}
151	69	S ₁	174	67	C _{dex}	324	61	S ₁	18	76	S ₂	98	42	C _{nor}
134	66	S ₁	5	74	C _{dex}	308	54	S ₁	159	35	S ₂	140	32	C _{nor}
177	50	S ₁	102	58	C _{dex}	313	37	S ₁	170	49	S ₂	176	22	C _{nor}
169	67	S ₁	1	78	C _{dex}	321	62	S ₁	177	35	S ₂	188	17	C _{nor}
164	47	S ₁	1	83	C _{dex}	311	56	S ₁	158	38	S ₂	56	19	C _{nor}
159	61	S ₁	341	79	C _{dex}	321	59	S ₁	134	24	S ₂	291	42	C _{nor}
356	80	S ₁	4	88	C _{dex}	307	62	S ₁	128	38	S ₂	290	40	C _{nor}
23	44	S ₁	355	87	C _{dex}	315	40	S ₁	43	43	S ₂	171	13	C _{nor}
40	46	S ₁	7	77	C _{dex}	303	39	S ₁	36	36	S ₂	300	34	C _{nor}
321	66	S ₁	183	87	C _{dex}	291	49	S ₁	38	35	S ₂	259	34	C _{nor}
329	70	S ₁	339	63	C _{dex}	307	59	S ₁	23	44	S ₂	296	52	C _{nor}
273	22	S ₁	343	55	C _{dex}	299	52	S ₁	189	54	C _{dex}	271	61	C _{nor}
302	20	S ₁	162	82	C _{dex}	306	72	S ₁	185	43	C _{dex}	307	42	C _{nor}
188	39	S ₁	354	83	C _{dex}	307	70	S ₁	182	48	C _{dex}	354	68	C _{nor}
196	40	S ₁	321	57	C _{dex}	318	43	S ₁	185	63	C _{dex}	325	72	C _{nor}
198	40	S ₁	329	69	C _{dex}	337	47	S ₁	183	65	C _{dex}	290	58	C _{nor}
195	48	S ₁	9	67	C _{dex}	308	41	S ₁	356	88	C _{dex}	319	26	C _{nor}
222	26	S ₁	356	72	C _{dex}	315	48	S ₁	174	90	C _{dex}	331	20	C _{nor}
195	36	S ₁	182	80	C _{dex}	281	64	S ₁	349	88	C _{dex}	265	58	C _{nor}
168	38	S ₁	192	72	C _{dex}	54	64	S ₁	0	84	C _{dex}	264	65	C _{nor}

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
330	47	S ₁	182	85	C _{dex}	319	54	S ₁	171	58	C _{dex}	283	31	C _{nor}
332	54	S ₁	330	68	C _{dex}	317	50	S ₁	152	40	C _{dex}	294	48	C _{nor}
332	50	S ₁	5	76	C _{dex}	329	45	S ₁	31	58	C _{nor}	226	27	C _{nor}
356	40	S ₁	182	83	C _{dex}	315	53	S ₁	20	58	C _{nor}	217	38	C _{nor}
8	40	S ₁	305	69	C _{dex}	313	55	S ₁	7	35	C _{nor}	226	33	C _{nor}
330	57	S ₁	136	88	C _{dex}	334	65	S ₁	286	65	C _{nor}	226	28	C _{nor}
345	54	S ₁	131	87	C _{dex}	332	41	S ₁	321	42	C _{rev}	209	38	C _{nor}
11	42	S ₁	247	52	C _{dex}	326	53	S ₁	331	33	C _{rev}	274	52	C _{nor}
329	30	S ₁	4	34	C _{dex}	334	36	S ₁	38	46	C _{rev}	278	16	C _{nor}
344	39	S ₁	314	65	C _{dex}	239	11	S ₁	358	71	C _{sin}	320	50	C _{nor}
4	32	S ₁	321	62	C _{dex}	1	26	S ₁	163	77	C _{sin}	337	43	C _{nor}
355	32	S ₁	339	76	C _{dex}	353	15	S ₁	161	90	C _{sin}	231	28	C _{nor}
12	24	S ₁	337	57	C _{dex}	274	29	S ₁	169	80	C _{sin}	34	48	C _{nor}
342	49	S ₁	4	66	C _{dex}	290	61	S ₁	160	80	C _{sin}	330	21	C _{nor}
0	77	S ₁	12	62	C _{dex}	296	55	S ₁	335	83	C _{sin}	269	14	C _{nor}
351	70	S ₁	32	30	C _{dex}	220	70	S ₁	157	75	C _{sin}	343	74	C _{sin}
353	82	S ₁	112	40	C _{dex}	229	68	S ₁	145	82	C _{sin}	339	79	C _{sin}
0	75	S ₁	357	86	C _{dex}	226	60	S ₁	327	82	C _{sin}	346	74	C _{sin}
9	52	S ₁	167	83	C _{dex}	316	37	S ₁	328	80	C _{sin}	337	88	C _{sin}
346	67	S ₁	8	76	C _{dex}	315	36	S ₁	318	73	C _{sin}	8	48	C _{sin}
333	86	S ₁	350	82	C _{dex}	321	81	S ₁	319	66	C _{sin}	3	40	C _{sin}
334	54	S ₁	334	77	C _{dex}	314	81	S ₁	329	77	C _{sin}	10	56	C _{sin}
353	75	S ₁	345	79	C _{dex}	321	89	S ₁	327	67	C _{sin}	353	50	C _{sin}
333	47	S ₁	340	84	C _{dex}	156	85	S ₁	328	83	C _{sin}	353	48	C _{sin}
329	54	S ₁	355	83	C _{dex}	119	68	S ₁	164	76	C _{sin}	356	64	C _{sin}
147	31	S ₁	350	85	C _{dex}	115	65	S ₁	351	88	C _{sin}	330	60	C _{sin}
3	77	S ₁	142	90	C _{dex}	107	74	S ₁	333	77	C _{sin}	322	32	C _{sin}
145	75	S ₁	172	88	C _{dex}	138	67	S ₁	346	85	C _{sin}	325	41	C _{sin}
180	72	S ₁	359	74	C _{dex}	119	62	S ₁	130	89	C _{sin}	347	38	C _{sin}
161	73	S ₁	324	71	C _{dex}	160	70	S ₁	55	27	C _{sin}	278	75	C _{sin}
121	73	S ₁	326	75	C _{dex}	195	10	S ₁	340	34	C _{sin}	201	42	C _{sin}
340	60	S ₁	165	88	C _{dex}	164	17	S ₁	324	48	C _{sin}	199	45	C _{sin}
129	68	S ₁	174	80	C _{dex}	224	14	S ₁	335	50	C _{sin}	308	45	C _{sin}
129	67	S ₁	180	88	C _{dex}	184	86	S ₁	340	54	C _{sin}	297	58	C _{sin}
322	54	S ₁	178	82	C _{dex}	15	72	S ₁	352	34	C _{sin}	317	77	C _{sin}
322	44	S ₁	338	90	C _{dex}	162	45	S ₁	13	26	C _{sin}	301	55	C _{sin}
336	75	S ₁	340	88	C _{dex}	331	57	S ₁	26	32	C _{sin}	349	46	C _{sin}
330	86	S ₁	215	74	C _{dex}	324	51	S ₁	356	67	C _{sin}	100	36	C _{sin}
345	43	S ₁	216	81	C _{dex}	204	87	S ₁	351	58	C _{sin}	111	52	C _{sin}
351	60	S ₁	215	52	C _{dex}	203	83	S ₁	2	57	C _{sin}	90	61	C _{sin}
150	75	S ₁	180	50	C _{dex}	201	88	S ₁	352	84	C _{sin}	281	61	C _{sin}
152	75	S ₁	133	24	C _{dex}	170	88	S ₁	174	88	C _{sin}	46	43	C' _{dex}
152	74	S ₁	126	30	C _{dex}	160	80	S ₁	350	87	C _{sin}	36	46	C' _{dex}
299	50	S ₁	132	32	C _{dex}	149	83	S ₁	336	87	C _{sin}	23	60	C' _{dex}
280	44	S ₁	229	68	C _{dex}	359	76	S ₂	162	87	C _{sin}	52	43	C' _{dex}

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
295	40	S ₁	214	82	C _{dex}	345	70	S ₂	358	45	C _{sin}	18	44	C' _{dex}
307	42	S ₁	302	73	C _{dex}	349	87	S ₂	12	50	C _{sin}	352	68	C' _{dex}
200	62	S ₁	337	74	C _{dex}	352	72	S ₂	336	68	C _{sin}	337	45	C' _{dex}
213	61	S ₁	168	86	C _{dex}	352	58	S ₂	333	65	C _{sin}	329	45	C' _{dex}
201	55	S ₁	5	75	C _{dex}	335	55	S ₂	340	75	C _{sin}	357	50	C' _{dex}
206	58	S ₁	5	83	C _{dex}	257	70	S ₂	340	68	C _{sin}	349	61	C' _{dex}
355	88	S ₁	10	87	C _{dex}	233	78	S ₂	38	46	C _{sin}	131	75	C' _{dex}
202	70	S ₁	335	90	C _{dex}	228	78	S ₂	166	77	C _{sin}	21	52	C' _{dex}
208	64	S ₁	27	72	C _{dex}	211	84	S ₂	175	77	C _{sin}	21	47	C' _{dex}
330	33	S ₁	32	66	C _{dex}	208	86	S ₂	42	68	C' _{dex}	17	42	C' _{dex}
144	64	S ₁	158	78	C _{dex}	184	86	S ₂	36	28	C' _{dex}	15	54	C' _{dex}
168	69	S ₁	159	76	C _{dex}	77	72	S ₂	22	65	C' _{dex}	10	64	C' _{dex}
218	41	S ₁	14	75	C _{dex}	49	55	S ₂	333	88	C' _{dex}	2	60	C' _{dex}
133	74	S ₁	184	78	C _{dex}	47	54	S ₂	173	77	C' _{dex}	352	68	C' _{rev}
21	34	S ₁	35	89	C _{dex}	23	86	S ₂	154	86	C' _{dex}	337	45	C' _{rev}
31	40	S ₁	225	87	C _{dex}	16	87	S ₂	336	85	C' _{dex}	329	45	C' _{rev}
159	39	S ₁	225	84	C _{dex}	15	58	S ₂	337	79	C' _{dex}	305	80	C' _{nor}
161	38	S ₁	7	73	C _{dex}	15	70	S ₂	165	85	C' _{dex}	293	31	C' _{nor}
11	72	S ₁	18	80	C _{dex}	15	80	S ₂	175	67	C' _{dex}	359	60	C' _{nor}
358	76	S ₁	346	84	C _{dex}	14	50	S ₂	191	69	C' _{dex}	356	58	C' _{nor}
156	58	S ₁	198	90	C _{dex}	13	75	S ₂	5	90	C' _{dex}	338	57	C' _{nor}
332	90	S ₁	336	81	C _{dex}	12	65	S ₂	352	72	C' _{dex}	337	55	C' _{nor}
4	65	S ₁	336	86	C _{dex}	10	54	S ₂	12	54	C' _{dex}	333	55	C' _{nor}
191	51	S ₁	172	71	C _{dex}	10	81	S ₂	148	64	C' _{dex}	314	57	C' _{nor}
62	3	S ₁	161	72	C _{dex}	6	66	S ₂	157	54	C' _{dex}	303	68	C' _{nor}
350	75	S ₁	17	46	C _{dex}	2	86	S ₂	149	54	C' _{dex}	281	71	C' _{nor}
8	54	S ₁	357	58	C _{dex}	165	52	S ₂	41	84	C' _{dex}	278	75	C' _{nor}
1	54	S ₁	5	89	C _{dex}	165	88	S ₂	28	84	C' _{dex}	344	61	C' _{nor}
16	77	S ₁	184	84	C _{dex}	167	76	S ₂	80	45	C' _{dex}	312	83	C' _{nor}
165	90	S ₁	329	69	C _{dex}	170	77	S ₂	20	52	C' _{dex}	305	54	C' _{nor}
342	67	S ₁	339	65	C _{dex}	176	83	S ₂	50	67	C' _{dex}	304	49	C' _{nor}
330	83	S ₁	356	80	C _{dex}	246	25	S ₂	46	53	C' _{dex}	299	70	C' _{nor}
163	81	S ₁	341	85	C _{dex}	239	29	S ₂	70	84	C' _{dex}	298	58	C' _{nor}
176	87	S ₁	20	75	C _{dex}	226	24	S ₂	50	75	C' _{dex}	291	45	C' _{nor}
183	83	S ₁	20	56	C _{dex}	226	25	S ₂	163	88	C' _{dex}	283	55	C' _{nor}
187	87	S ₁	14	68	C _{dex}	210	20	S ₂	165	84	C' _{dex}	276	43	C' _{nor}
342	67	S ₁	208	89	C _{dex}	203	29	S ₂	188	85	C' _{dex}	273	40	C' _{nor}
333	78	S ₁	208	80	C _{dex}	199	42	S ₂	163	89	C' _{dex}	267	44	C' _{nor}
325	42	S ₁	210	88	C _{dex}	193	29	S ₂	172	87	C' _{dex}	233	23	C' _{nor}
163	63	S ₁	358	72	C _{dex}	191	49	S ₂	174	64	C' _{dex}	322	50	C' _{nor}
172	85	S ₁	358	80	C _{dex}	11	48	S ₂	178	60	C' _{dex}	318	32	C' _{nor}
176	84	S ₁	7	89	C _{dex}	317	46	S ₂	177	56	C' _{dex}	317	29	C' _{nor}
351	85	S ₁	212	80	C _{dex}	297	46	S ₂	175	64	C' _{dex}	311	64	C' _{nor}
349	82	S ₁	171	76	C _{dex}	295	40	S ₂	185	67	C' _{dex}	299	55	C' _{nor}
165	87	S ₁	175	55	C _{dex}	302	38	S ₂	195	70	C' _{dex}	295	46	C' _{nor}

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
325	84	S ₁	29	56	C _{dex}	349	59	S ₂	202	68	C' _{dex}	289	68	C' _{nor}
166	64	S ₁	45	69	C _{dex}	349	65	S ₂	39	69	C' _{dex}	284	75	C' _{nor}
145	80	S ₁	27	87	C _{dex}	341	67	S ₂	40	77	C' _{dex}	284	55	C' _{nor}
318	75	S ₂	212	63	C _{dex}	338	66	S ₂	24	72	C' _{dex}	282	41	C' _{nor}
330	76	S ₂	234	72	C _{dex}	334	64	S ₂	212	86	C' _{dex}	282	61	C' _{nor}
357	87	S ₂	207	60	C _{dex}	333	50	S ₂	187	90	C' _{dex}	280	65	C' _{nor}
359	90	S ₂	229	83	C _{dex}	332	54	S ₂	6	81	C' _{dex}	276	64	C' _{nor}
170	88	S ₂	234	79	C _{dex}	331	60	S ₂	16	75	C' _{dex}	274	78	C' _{nor}
331	68	S ₂	193	78	C _{dex}	321	55	S ₂	29	84	C' _{dex}	270	64	C' _{nor}
356	79	S ₂	185	76	C _{dex}	294	76	S ₂	31	74	C' _{dex}	268	58	C' _{nor}
356	82	S ₂	342	68	C _{dex}	292	21	S ₂	192	43	C' _{dex}	266	38	C' _{nor}
330	84	S ₂	343	86	C _{dex}	291	51	S ₂	196	49	C' _{dex}	266	46	C' _{nor}
343	76	S ₂	172	76	C _{dex}	290	48	S ₂	234	33	C' _{dex}	265	38	C' _{nor}
188	82	S ₂	187	86	C _{dex}	290	75	S ₂	247	33	C' _{dex}	264	46	C' _{nor}
344	84	S ₂	357	80	C _{dex}	289	55	S ₂	263	25	C' _{dex}	264	29	C' _{nor}
337	72	S ₂	348	80	C _{dex}	289	64	S ₂	210	39	C' _{dex}	264	65	C' _{nor}
340	86	S ₂	343	81	C _{dex}	289	24	S ₂	198	25	C' _{dex}	263	44	C' _{nor}
345	90	S ₂	220	78	C _{dex}	288	23	S ₂	187	20	C' _{dex}	260	42	C' _{nor}
168	84	S ₂	13	74	C _{dex}	287	72	S ₂	189	54	C' _{dex}	260	68	C' _{nor}
172	88	S ₂	14	70	C _{dex}	280	75	S ₂	185	43	C' _{dex}	259	61	C' _{nor}
333	87	S ₂	141	84	C _{dex}	276	63	S ₂	182	48	C' _{dex}	259	82	C' _{nor}
324	86	S ₂	172	88	C _{dex}	276	77	S ₂	185	63	C' _{dex}	256	28	C' _{nor}
335	89	S ₂	8	55	C _{dex}	276	64	S ₂	183	65	C' _{dex}	250	38	C' _{nor}
351	76	S ₂	9	67	C _{dex}	275	68	S ₂	24	80	C' _{dex}	250	43	C' _{nor}
350	74	S ₂	18	63	C _{dex}	274	53	S ₂	32	85	C' _{dex}	250	42	C' _{nor}
337	75	S ₂	12	90	C _{dex}	274	64	S ₂	32	80	C' _{dex}	250	46	C' _{nor}
310	78	S ₂	180	77	C _{dex}	268	23	S ₂	31	81	C' _{dex}	246	41	C' _{nor}
354	84	S ₂	4	81	C _{dex}	266	38	S ₂	32	70	C' _{dex}	244	55	C' _{nor}
325	81	S ₂	343	85	C _{dex}	266	24	S ₂	220	81	C' _{dex}	238	35	C' _{nor}
327	88	S ₂	2	86	C _{dex}	264	34	S ₂	237	89	C' _{dex}	235	54	C' _{nor}
338	84	S ₂	198	76	C _{dex}	250	39	S ₂	40	66	C' _{dex}	216	48	C' _{nor}
340	80	S ₂	2	82	C _{dex}	246	44	S ₂	179	38	C' _{nor}	212	44	C' _{nor}
344	85	S ₂	205	84	C _{dex}	245	30	S ₂	178	36	C' _{nor}	211	58	C' _{nor}
166	82	S ₂	41	81	C _{dex}	89	84	S ₂	124	24	C' _{nor}	201	64	C' _{nor}
165	85	S ₂	29	74	C _{dex}	98	84	S ₂	254	42	C' _{nor}	116	24	C' _{nor}
358	78	S ₂	31	70	C _{dex}	103	44	S ₂	244	54	C' _{nor}	267	58	C' _{nor}
338	85	S ₂	3	78	C _{dex}	107	87	S ₂	224	52	C' _{nor}	259	64	C' _{nor}
0	80	S ₂	358	70	C _{dex}	108	49	S ₂	223	69	C' _{nor}	247	38	C' _{nor}
345	79	S ₂	326	42	C _{nor}	109	85	S ₂	96	65	C' _{nor}	239	59	C' _{nor}
335	84	S ₂	308	34	C _{nor}	112	72	S ₂	349	74	C' _{rev}	232	39	C' _{nor}
340	86	S ₂	307	41	C _{nor}	114	71	S ₂	348	77	C' _{rev}	184	64	C' _{nor}
350	80	S ₂	305	37	C _{nor}	115	75	S ₂	44	68	C' _{rev}	220	27	C' _{nor}
345	76	S ₂	161	61	C _{nor}	118	68	S ₂	51	74	C' _{rev}	201	26	C' _{nor}
335	82	S ₂	161	65	C _{nor}	119	85	S ₂	41	69	C' _{rev}	323	39	C' _{nor}
344	87	S ₂	105	88	C _{nor}	120	82	S ₂	40	67	C' _{rev}	319	37	C' _{nor}

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
0	84	S ₂	322	72	C _{nor}	124	55	S ₂	0	46	C' _{sin}	318	54	C' _{nor}
358	79	S ₂	100	81	C _{nor}	126	86	S ₂	7	58	C' _{sin}	314	60	C' _{nor}
163	86	S ₂	155	49	C _{nor}	128	90	S ₂	301	65	C' _{sin}	304	59	C' _{nor}
169	84	S ₂	245	14	C _{nor}	129	55	S ₂	106	87	C' _{sin}	283	38	C' _{nor}
167	82	S ₂	224	35	C _{nor}	135	89	S ₂	107	77	C' _{sin}	42	44	C' _{nor}
352	88	S ₂	294	64	C _{nor}	140	78	S ₂	28	50	C' _{sin}	37	48	C' _{nor}
340	77	S ₂	268	41	C _{nor}	141	75	S ₂	101	68	C' _{sin}	40	40	C' _{nor}
355	84	S ₂	70	49	C _{nor}	142	85	S ₂	107	67	C' _{sin}	24	51	C' _{nor}
358	75	S ₂	44	55	C _{nor}	146	88	S ₂	337	85	C' _{sin}	19	54	C' _{nor}
155	86	S ₂	276	72	C _{nor}	150	86	S ₂	346	90	C' _{sin}	94	37	C' _{nor}
344	85	S ₂	296	57	C _{nor}	151	72	S ₂	74	52	C' _{sin}	76	45	C' _{nor}
160	89	S ₂	279	53	C _{nor}	152	79	S ₂	141	76	C' _{sin}	45	45	C' _{nor}
6	74	S ₂	263	53	C _{nor}	155	87	S ₂	129	78	C' _{sin}	46	43	C' _{nor}
175	88	S ₂	254	65	C _{nor}	162	87	S ₂	137	89	C' _{sin}	36	46	C' _{nor}
337	88	S ₂	140	15	C _{nor}	163	86	S ₂	300	74	C' _{sin}	23	60	C' _{nor}
167	82	S ₂	152	19	C _{nor}	265	88	S ₂	132	87	C' _{sin}	52	43	C' _{nor}
355	73	S ₂	164	31	C _{nor}	272	72	S ₂	128	80	C' _{sin}	18	44	C' _{nor}
338	75	S ₂	310	42	C _{nor}	295	40	S ₂	291	82	C' _{sin}	157	48	C' _{rev}
336	86	S ₂	354	46	C _{nor}	297	76	S ₂	298	75	C' _{sin}	83	43	C' _{rev}
345	81	S ₂	333	61	C _{nor}	297	46	S ₂	283	53	C' _{sin}	332	76	C' _{sin}
2	82	S ₂	6	79	C _{nor}	299	85	S ₂	284	64	C' _{sin}	327	72	C' _{sin}
335	72	S ₂	160	55	C _{nor}	300	64	S ₂	308	90	C' _{sin}	327	63	C' _{sin}
342	65	S ₂	140	58	C _{nor}	302	38	S ₂	309	87	C' _{sin}	321	67	C' _{sin}
341	82	S ₂	346	66	C _{nor}	306	83	S ₂	127	88	C' _{sin}	317	64	C' _{sin}
351	81	S ₂	175	85	C _{nor}	306	80	S ₂	131	89	C' _{sin}	316	90	C' _{sin}
349	66	S ₂	345	76	C _{nor}	308	73	S ₂	133	86	C' _{sin}	314	70	C' _{sin}
346	77	S ₂	349	80	C _{nor}	308	34	S ₂	302	78	C' _{sin}	314	66	C' _{sin}
358	88	S ₂	353	84	C _{nor}	308	81	S ₂	303	90	C' _{sin}	312	75	C' _{sin}
342	80	S ₂	292	33	C _{nor}	308	70	S ₂	342	85	C' _{sin}	308	74	C' _{sin}
134	86	S ₂	304	27	C _{nor}	308	80	S ₂	2	86	C' _{sin}	304	68	C' _{sin}
0	82	S ₂	294	28	C _{nor}	309	88	S ₂	346	79	C' _{sin}	304	67	C' _{sin}
347	89	S ₂	288	32	C _{nor}	310	66	S ₂	148	89	C' _{sin}	301	85	C' _{sin}
355	83	S ₂	288	21	C _{nor}	310	86	S ₂	76	43	C' _{sin}	300	70	C' _{sin}
3	90	S ₂	327	25	C _{nor}	310	78	S ₂	317	55	C' _{sin}	298	75	C' _{sin}
334	84	S ₂	288	30	C _{nor}	311	88	S ₂	327	81	C' _{sin}	288	80	C' _{sin}
341	76	S ₂	302	20	C _{nor}	312	72	S ₂	341	82	C' _{sin}	286	85	C' _{sin}
315	65	S ₂	323	35	C _{nor}	312	86	S ₂	326	76	C' _{sin}	286	81	C' _{sin}
357	72	S ₂	248	24	C _{nor}	313	72	S ₂	305	72	C' _{sin}	178	52	C' _{sin}
335	82	S ₂	181	50	C _{nor}	317	52	S ₂	298	87	C' _{sin}	175	57	C' _{sin}
166	86	S ₂	343	34	C _{rev}	317	46	S ₂	144	87	C' _{sin}	174	82	C' _{sin}
167	89	S ₂	347	47	C _{rev}	318	62	S ₂	148	90	C' _{sin}	165	55	C' _{sin}
351	82	S ₂	357	38	C _{rev}	318	74	S ₂	139	74	C' _{sin}	147	87	C' _{sin}
175	89	S ₂	326	87	C _{rev}	321	71	S ₂	288	90	C' _{sin}	139	72	C' _{sin}
162	85	S ₂	337	85	C _{rev}	321	80	S ₂	125	80	C' _{sin}	139	70	C' _{sin}
337	90	S ₂	335	81	C _{rev}	322	73	S ₂	103	90	C' _{sin}	135	57	C' _{sin}

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
166	87	S ₂	138	98	C _{rev}	323	78	S ₂	136	72	C' _{sin}	118	78	C' _{sin}
336	75	S ₂	142	81	C _{rev}	325	78	S ₂	137	68	C' _{sin}	114	81	C' _{sin}
162	82	S ₂	320	85	C _{rev}	325	78	S ₂	126	78	C' _{sin}	105	75	C' _{sin}
170	82	S ₂	349	85	C _{rev}	325	71	S ₂	305	83	C' _{sin}	96	84	C' _{sin}
355	75	S ₂	351	85	C _{rev}	326	77	S ₂	307	88	C' _{sin}	87	77	C' _{sin}
358	77	S ₂	346	71	C _{rev}	326	86	S ₂	304	84	C' _{sin}	40	82	C' _{sin}
342	82	S ₂	334	65	C _{rev}	326	88	S ₂	326	62	C' _{sin}	32	75	C' _{sin}
324	86	S ₂	135	48	C _{rev}	326	75	S ₂	318	56	C' _{sin}	5	63	C' _{sin}
337	83	S ₂	153	36	C _{rev}	326	86	S ₂	302	75	C' _{sin}	2	67	C' _{sin}
156	83	S ₂	326	81	C _{rev}	328	80	S ₂	310	77	C' _{sin}	273	17	L ₁
166	87	S ₂	355	85	C _{rev}	329	85	S ₂	288	75	C' _{sin}	93	6	L ₁
342	89	S ₂	353	72	C _{rev}	329	54	S ₂	307	70	C' _{sin}	236	9	L ₁
345	80	S ₂	337	72	C _{rev}	330	90	S ₂	274	38	C' _{sin}	62	5	L ₁
343	75	S ₂	335	75	C _{rev}	330	86	S ₂	295	31	C' _{sin}	50	3	L ₁
350	90	S ₂	304	67	C _{rev}	330	84	S ₂	292	31	C' _{sin}	73	35	L ₁
348	84	S ₂	311	45	C _{rev}	330	89	S ₂	291	34	C' _{sin}	222	32	L ₁
162	85	S ₂	314	45	C _{rev}	332	69	S ₂	286	25	C' _{sin}	235	43	L ₁
334	78	S ₂	334	51	C _{rev}	332	84	S ₂	294	30	C' _{sin}	254	35	L ₁
155	83	S ₂	334	52	C _{rev}	334	69	S ₂	296	32	C' _{sin}	253	37	L ₁
350	88	S ₂	302	55	C _{rev}	334	82	S ₂	320	57	C' _{sin}	233	47	L ₁
175	84	S ₂	303	52	C _{rev}	335	82	S ₂	312	57	C' _{sin}	230	46	L ₁
165	83	S ₂	9	67	C _{rev}	335	79	S ₂	330	73	C' _{sin}	289	3	L ₁
341	90	S ₂	12	63	C _{rev}	337	74	S ₂	139	89	C' _{sin}	264	24	L ₁
343	75	S ₂	18	53	C _{rev}	342	74	S ₂	309	80	C' _{sin}	253	34	L ₁
155	85	S ₂	157	70	C _{sin}	342	87	S ₂	328	86	C' _{sin}	254	45	L ₁
0	90	S ₂	167	63	C _{sin}	150	75	C _{dex}	309	88	C' _{sin}	236	18	L ₁
151	88	S ₂	343	82	C _{sin}	153	71	C _{dex}	308	90	C' _{sin}	245	24	L ₁
152	85	S ₂	345	88	C _{sin}	178	68	C _{dex}	344	77	AP ₁	239	15	L ₁
358	86	S ₂	342	72	C _{sin}	156	68	C _{dex}	12	55	AP ₁	229	21	L ₁
358	90	S ₂	354	84	C _{sin}	355	70	C _{dex}	39	45	AP ₁	219	30	L ₁
0	79	S ₂	188	88	C _{sin}	338	68	C _{dex}	32	22	AP ₁	279	7	L ₁
330	84	S ₂	2	90	C _{sin}	131	67	C _{dex}	245	46	AP ₁	109	7	L ₁
334	81	S ₂	139	89	C _{sin}	123	52	C _{dex}	222	50	AP ₁	285	47	L ₁
334	81	S ₂	338	89	C _{sin}	138	30	C _{dex}	322	28	AP ₁	97	24	L ₁
350	83	S ₂	332	89	C _{sin}	141	28	C _{dex}	27	15	AP ₁	282	11	L ₁
354	89	S ₂	333	82	C _{sin}	135	34	C _{dex}	39	22	AP ₁	262	12	L ₁
150	79	S ₂	333	79	C _{sin}	105	76	C _{dex}	42	25	AP ₁	252	19	L ₁
325	90	S ₂	335	81	C _{sin}	288	86	C _{dex}	164	30	AP ₁	263	6	L ₁
170	84	S ₂	145	87	C _{sin}	324	68	C _{dex}	134	39	AP ₁	277	39	L ₁
154	88	S ₂	144	88	C _{sin}	326	60	C _{dex}	341	29	AP ₁	274	19	L ₁
342	75	S ₂	172	79	C _{sin}	319	58	C _{dex}	32	75	AP ₂	271	23	L ₁
325	88	S ₂	152	74	C _{sin}	345	70	C _{dex}	38	73	AP ₂	268	10	L ₁
170	71	S ₂	152	77	C _{sin}	353	73	C _{dex}	175	82	AP ₂	285	25	L ₁
349	87	S ₂	154	84	C _{sin}	36	36	C _{dex}	356	82	AP ₂	329	27	L ₁
178	77	S ₂	148	85	C _{sin}	76	25	C _{dex}	132	78	AP ₂	87	1	L ₁

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
157	87	S ₂	151	85	C _{sin}	5	65	C _{dex}	148	60	AP ₂	252	25	L ₂
349	80	S ₂	137	71	C _{sin}	16	53	C _{dex}	298	70	AP ₂	269	7	L ₂
342	88	S ₂	139	75	C _{sin}	50	42	C _{dex}	319	32	AP ₂	102	20	L ₂
346	84	S ₂	149	80	C _{sin}	34	48	C _{dex}	106	88	AP ₂	72	4	L ₂
166	84	S ₂	148	74	C _{sin}	289	70	C _{nor}	105	81	AP ₂	84	7	L ₂
158	85	S ₂	168	86	C _{sin}	1	64	C _{nor}	124	84	AP ₂	276	23	L ₂
175	84	S ₂	325	81	C _{sin}	359	69	C _{nor}	309	87	AP ₂	271	34	L ₂
175	56	S ₂	329	81	C _{sin}	22	55	C _{nor}	146	77	AP ₂	201	53	L ₂
333	84	S ₂	324	83	C _{sin}	18	45	C _{nor}	145	42	AP ₂	184	59	L ₂
2	83	S ₂	155	77	C _{sin}	19	54	C _{nor}	319	78	AP ₂	203	59	L ₂
353	80	S ₂	170	84	C _{sin}	22	66	C _{nor}	7	47	AP ₂	235	22	L ₂
315	66	S ₂	148	86	C _{sin}	329	75	C _{nor}	15	27	AP ₂	238	29	L ₂
348	78	S ₂	339	84	C _{sin}	317	86	C _{nor}	347	64	AP ₂	78	18	L ₂
320	71	S ₂	340	80	C _{sin}	30	53	C _{nor}	168	85	AP ₂	274	1	L ₂
356	89	S ₂	340	84	C _{sin}	20	45	C _{nor}	166	62	AP ₂	260	48	L ₂
358	85	S ₂	338	64	C _{sin}	305	45	C _{nor}	328	70	AP ₂	254	36	L ₂
315	64	S ₂	339	74	C _{sin}	267	72	C _{nor}	335	78	AP ₂	262	18	L _{sin}
8	89	S ₂	338	76	C _{sin}	265	75	C _{nor}	157	89	AP ₂	254	19	L _{sin}
350	74	S ₂	328	62	C _{sin}	13	48	C _{nor}	343	83	AP ₂	260	30	L _{sin}
164	85	S ₂	345	85	C _{sin}	347	37	C _{nor}	7	84	AP ₂	252	44	L _{sin}
337	89	S ₂	18	85	C _{sin}	348	65	C _{nor}	171	76	AP ₂	212	32	L _{sin}
5	89	S ₂	11	85	C _{sin}	350	55	C _{nor}	344	90	AP ₂	261	7	L _{nor}
359	80	S ₂	9	83	C _{sin}	138	83	C _{rev}	346	81	AP ₂	247	16	L _{nor}
180	80	S ₂	4	82	C _{sin}	355	77	C _{rev}	194	76	AP ₂	240	13	L _{nor}
348	83	S ₂	8	79	C _{sin}	108	88	C _{rev}	11	89	AP ₂	247	16	L _{nor}
345	80	S ₂	6	87	C _{sin}	296	86	C _{rev}	219	85	AP ₂	238	10	L _{nor}
165	80	S ₂	7	58	C _{sin}	223	73	C _{rev}	203	73	AP ₂	268	5	L _{nor}
335	80	S ₂	357	43	C _{sin}	308	85	C _{rev}	199	74	AP ₂	273	4	L _{nor}
186	78	S ₂	26	40	C _{sin}	333	89	C _{rev}	211	74	AP ₂	355	32	L _{nor}
350	88	S ₂	345	55	C _{sin}	119	77	C _{rev}	189	85	AP ₂	261	3	FA ₁
355	85	S ₂	338	46	C _{sin}	117	80	C _{rev}	330	78	AP ₂	276	2	FA ₁
344	90	S ₂	339	69	C _{sin}	305	87	C _{rev}	169	74	AP ₂	270	3	FA ₁
335	89	S ₂	323	68	C _{sin}	135	82	C _{rev}	343	79	AP ₂	270	2	FA ₁
161	89	S ₂	326	42	C _{sin}	318	88	C _{rev}	352	82	AP ₂	276	29	FA ₁
350	86	S ₂	308	34	C _{sin}	324	86	C _{rev}	6	60	AP ₂	284	9	FA ₁
167	79	S ₂	307	41	C _{sin}	211	90	C _{rev}	13	38	AP ₂	254	3	FA ₁
149	80	S ₂	305	37	C _{sin}	186	70	C _{rev}	352	46	AP ₂	86	17	FA ₁
146	88	S ₂	152	80	C _{sin}	183	66	C _{rev}	358	51	AP ₂	269	6	FA ₁
158	75	S ₂	156	80	C _{sin}	348	75	C _{rev}	182	86	AP ₂	255	19	FA ₁
144	67	S ₂	322	90	C _{sin}	181	85	C _{rev}	164	87	AP ₂	257	19	FA ₁
355	88	S ₂	148	84	C _{sin}	123	68	C _{rev}	179	86	AP ₂	267	44	FA ₁
159	88	S ₂	158	81	C _{sin}	111	84	C _{rev}	61	89	AP ₂	272	27	FA ₁
152	82	S ₂	140	80	C _{sin}	295	15	C _{rev}	208	82	AP ₂	260	11	FA ₁
165	71	S ₂	150	70	C _{sin}	303	31	C _{rev}	196	74	AP ₂	247	18	FA ₁
336	81	S ₂	330	88	C _{sin}	292	81	C _{sin}	170	88	AP ₂	285	14	FA ₁

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
176	87	S ₂	338	70	C _{sin}	304	86	C _{sin}	180	90	AP ₂	260	11	FA ₁
347	73	S ₂	340	90	C _{sin}	296	79	C _{sin}	10	84	AP ₂	247	18	FA ₁
151	80	S ₂	340	75	C _{sin}	335	48	C _{sin}	178	80	AP ₂	253	19	FA ₂
180	72	S ₂	161	82	C _{sin}	318	50	C _{sin}	170	78	AP ₂	265	8	FA ₂
174	87	S ₂	148	87	C _{sin}	327	50	C _{sin}	175	73	AP ₂	291	14	FA ₂
162	88	S ₂	311	73	C _{sin}	334	90	C _{sin}	180	75	AP ₂	277	15	FA ₂
354	71	S ₂	168	68	C _{sin}	315	75	C _{sin}	355	88	AP ₂	254	22	FA ₂
180	72	S ₂	154	67	C _{sin}	157	80	C _{sin}	171	80	AP ₂	278	3	FA ₂
344	70	S ₂	154	72	C _{sin}	164	89	C _{sin}	342	88	AP ₂	276	4	FA ₂
153	70	S ₂	155	73	C _{sin}	140	85	C _{sin}	175	90	AP ₂	252	38	FA ₂
152	67	S ₂	154	78	C _{sin}	274	51	C _{sin}	47	64	AP ₂	84	14	FA ₂
168	69	S ₂	144	80	C _{sin}	250	30	C _{sin}	162	80	AP ₂	266	7	FA ₂
168	82	S ₂	134	88	C _{sin}	279	71	C _{sin}	190	90	AP ₂	85	2	FA ₂
335	86	S ₂	139	87	C _{sin}	306	39	C _{sin}	10	90	AP ₂	270	11	FA ₂
337	85	S ₂	133	77	C _{sin}	293	45	C _{sin}	330	90	AP ₂	270	7	FA ₂
344	79	S ₂	176	77	C _{sin}	287	50	C _{sin}	148	84	AP ₂	265	7	FA ₂
346	78	S ₂	169	82	C _{sin}	251	60	C _{sin}	323	90	AP ₂	276	4	FA ₂
342	80	S ₂	164	75	C _{sin}	88	90	C _{sin}	183	45	AP ₂	72	5	FA ₂
342	82	S ₂	156	73	C _{sin}	260	79	C _{sin}	191	89	AP ₂	94	4	FA ₂
340	87	S ₂	322	86	C _{sin}	266	85	C _{sin}	220	88	AP ₂	80	6	FA ₂
355	88	S ₂	172	90	C _{sin}	264	73	C _{sin}	252	76	AP ₂	117	7	FA ₂
178	87	S ₂	140	81	C _{sin}	268	78	C _{sin}	263	52	AP ₂	278	10	FA ₂
312	85	S ₂	132	80	C _{sin}	262	74	C _{sin}	261	64	AP ₂	276	23	FA ₂
156	85	S ₂	165	85	C _{sin}	132	48	C _{sin}	14	79	AP ₂	86	7	FA ₂
320	60	S ₂	137	75	C _{sin}	133	54	C _{sin}	357	55	AP ₂	110	8	FA ₂
350	81	S ₂	311	85	C _{sin}	146	60	C _{sin}	346	58	AP ₂	115	12	FA ₂
345	84	S ₂	137	68	C _{sin}	119	51	C _{sin}	232	32	AP ₂	87	18	FA ₂
338	86	S ₂	149	72	C _{sin}	121	49	C _{sin}	242	48	AP ₂	105	19	FA ₂
323	87	S ₂	138	73	C _{sin}	334	82	C _{sin}	268	55	AP ₂	95	14	FA ₂
340	86	S ₂	153	62	C _{sin}	325	90	C _{sin}	86	78	AP ₄	299	24	FA ₂
164	80	S ₂	150	49	C _{sin}	337	55	C _{sin}	91	69	AP ₄	122	21	FA ₂
142	75	S ₂	140	76	C _{sin}	346	76	C _{sin}	281	90	AP ₄	301	27	FA ₂
165	90	S ₂	131	77	C _{sin}	331	72	C _{sin}	94	82	AP ₄	91	2	FA ₂
358	83	S ₂	142	84	C _{sin}	342	76	C _{sin}	92	79	AP ₄	262	11	FA ₂
302	75	S ₂	142	77	C _{sin}	334	80	C _{sin}	308	84	AP ₄	267	12	FA ₂
160	90	S ₂	142	75	C _{sin}	158	88	C _{sin}	132	82	AP ₄	277	13	FA ₂
331	70	S ₂	154	83	C _{sin}	311	86	C _{sin}	158	77	AP ₄	274	18	FA ₂
338	80	S ₂	148	83	C _{sin}	326	73	C _{sin}	231	58	AP ₄	266	18	FA ₂
341	85	S ₂	135	72	C _{sin}	314	72	C _{sin}	108	74	AP ₄	272	7	FA ₂
333	55	S ₂	135	65	C _{sin}	318	58	C _{sin}	79	82	AP ₄	108	13	FA ₂
332	50	S ₂	147	90	C _{sin}	155	77	C _{sin}	252	74	AP ₄	101	23	FA ₂
337	65	S ₂	331	88	C _{sin}	130	72	C _{sin}	111	78	AP ₄	245	35	FA ₂
357	88	S ₂	335	70	C _{sin}	142	69	C _{sin}	93	85	AP ₄	97	9	FA ₂
158	90	S ₂	339	74	C _{sin}	266	74	C _{sin}	112	90	AP ₄	94	6	FA ₂
334	89	S ₂	326	80	C _{sin}	260	75	C _{sin}	126	83	AP ₄	323	30	FA ₂

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
338	83	S ₂	148	85	C _{sin}	274	80	C _{sin}	116	88	AP ₄	321	25	FA ₂
0	85	S ₂	336	87	C _{sin}	114	71	C _{sin}	133	88	AP ₄	78	23	FA ₂
155	86	S ₂	159	77	C _{sin}	125	78	C _{sin}	142	84	AP ₄	113	17	FA ₂
152	87	S ₂	174	74	C _{sin}	117	84	C _{sin}	324	65	AP ₄	250	5	FA ₂
154	90	S ₂	159	72	C _{sin}	100	86	C _{sin}	103	82	AP ₄	260	28	FA ₂
171	69	S ₂	354	74	C _{sin}	79	89	C _{sin}	130	32	FA ₁	320	52	FA ₂
167	65	S ₂	345	75	C _{sin}	303	62	C _{sin}	103	32	FA ₁	279	22	FA ₂
136	81	S ₂	185	85	C _{sin}	298	68	C _{sin}	335	38	FA ₁	2	9	FA ₂
332	86	S ₂	0	74	C _{sin}	312	77	C _{sin}	349	36	FA ₁	279	21	FA ₂
337	87	S ₂	2	72	C _{sin}	312	77	C _{sin}	71	14	FA ₁	280	21	FA ₂
344	68	S ₂	4	82	C _{sin}	298	82	C _{sin}	65	11	FA ₁	307	43	FA ₂
171	56	S ₂	164	87	C _{sin}	332	59	C _{sin}	74	20	FA ₁	307	18	FA ₂
160	61	S ₂	151	87	C _{sin}	322	38	C _{sin}	100	20	FA ₁	301	26	FA ₂
172	69	S ₂	149	73	C _{sin}	293	70	C _{sin}	124	1	FA ₂	306	33	FA ₂
328	82	S ₂	151	90	C _{sin}	303	77	C _{sin}	303	7	FA ₂	300	38	FA ₂
333	82	S ₂	144	86	C _{sin}	324	76	C _{sin}	91	46	FA ₂	292	16	FA ₂
340	82	S ₂	325	82	C _{sin}	320	75	C _{sin}	88	50	FA ₂	294	30	FA ₂
180	90	S ₂	330	85	C _{sin}	316	84	C _{sin}	226	1	FA ₂	285	17	FA ₂
135	88	S ₂	331	85	C _{sin}	300	85	C _{sin}	225	2	FA ₂	296	17	FA ₂
142	56	S ₂	349	81	C _{sin}	272	84	C _{sin}	48	25	FA ₂	307	22	FA ₂
139	74	S ₂	324	85	C _{sin}	318	83	C _{sin}	110	29	FA ₂	298	26	FA ₂
161	76	S ₂	342	70	C _{sin}	316	85	C _{sin}	56	18	FA ₂	357	28	FA ₂
155	71	S ₂	341	77	C _{sin}	108	90	C _{sin}	38	21	FA ₂	4	9	FA ₂
153	62	S ₂	336	76	C _{sin}	296	86	C _{sin}	74	28	FA ₂	278	17	FA ₂
168	68	S ₂	343	84	C _{sin}	5	52	C' _{dex}	264	5	FA ₂	269	24	FA ₂
153	83	S ₂	165	86	C _{sin}	29	45	C' _{dex}	254	3	FA ₂	271	18	FA ₂
349	72	S ₂	331	82	C _{sin}	37	60	C' _{dex}	252	7	FA ₂	233	44	FA ₂
169	82	S ₂	322	74	C _{sin}	57	53	C' _{dex}	79	8	FA ₂	274	42	FA ₂
358	90	S ₂	320	72	C _{sin}	226	77	C' _{dex}	167	22	FA ₂	269	53	FA ₂
1	88	S ₂	345	72	C _{sin}	17	83	C' _{dex}	62	73	FA ₂	256	9	FA ₂
155	89	S ₂	344	77	C _{sin}	216	63	C' _{dex}	84	74	FA ₂	256	33	FA ₂
351	87	S ₂	157	83	C _{sin}	195	64	C' _{dex}	281	37	FA ₂	240	47	FA ₂
347	79	S ₂	153	90	C _{sin}	0	80	C' _{dex}	270	38	FA ₂	254	35	FA ₂
351	83	S ₂	334	83	C _{sin}	357	85	C' _{dex}	135	74	FA ₂	244	39	FA ₂
350	80	S ₂	155	83	C _{sin}	349	48	C' _{dex}	146	66	FA ₂	206	43	FA ₂
355	85	S ₂	152	90	C _{sin}	41	55	C' _{dex}	132	74	FA ₂	85	12	FA ₂
188	58	S ₂	156	77	C _{sin}	22	55	C' _{dex}	188	77	FA ₂	286	4	FA ₂
346	87	S ₂	153	78	C _{sin}	258	48	C' _{dex}	260	7	FA ₂	294	27	FA ₂
355	75	S ₂	168	87	C _{sin}	183	78	C' _{dex}	86	10	FA ₂	304	22	FA ₂
353	79	S ₂	158	68	C _{sin}	176	76	C' _{dex}	287	14	FA ₂	267	41	FA ₂
352	80	S ₂	161	67	C _{sin}	208	68	C' _{dex}	118	0	FA ₂	263	28	FA ₂
3	69	S ₂	139	76	C _{sin}	191	70	C' _{dex}	270	10	FA ₂	272	13	FA ₂
357	75	S ₂	131	79	C _{sin}	14	65	C' _{dex}	275	7	FA ₂	280	6	FA ₂
4	67	S ₂	134	65	C _{sin}	7	72	C' _{dex}	265	30	FA ₂	287	11	FA ₂
3	74	S ₂	340	86	C _{sin}	139	74	C' _{dex}	262	27	FA ₂	269	5	FA ₂

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
6	81	S ₂	155	87	C _{sin}	146	81	C' _{dex}	267	20	FA ₂	288	32	FA ₂
357	71	S ₂	335	75	C _{sin}	294	53	C' _{dex}	223	31	FA ₂	276	13	FA ₂
357	77	S ₂	333	76	C _{sin}	292	47	C' _{dex}	247	10	FA ₂	270	19	FA ₂
353	77	S ₂	339	67	C _{sin}	299	45	C' _{dex}	240	15	FA ₂	286	6	FA ₂
355	80	S ₂	333	75	C _{sin}	25	15	C' _{dex}	145	8	FA ₂	288	19	FA ₂
3	78	S ₂	340	80	C _{sin}	345	45	C' _{dex}	244	32	FA ₂	276	8	FA ₂
356	77	S ₂	334	86	C _{sin}	167	69	C' _{dex}	106	16	FA ₂	290	5	FA ₂
6	64	S ₂	155	20	C _{sin}	99	54	C' _{dex}	93	0	FA ₂	228	20	FA ₂
7	90	S ₂	312	82	C _{sin}	151	55	C' _{dex}	100	20	FA ₂	283	22	FA ₂
7	81	S ₂	163	64	C _{sin}	170	53	C' _{dex}	287	14	FA ₂	319	55	FA ₂
166	88	S ₂	333	70	C _{sin}	181	34	C' _{dex}	127	74	FA ₂	94	6	FA ₂
357	88	S ₂	332	61	C _{sin}	182	32	C' _{dex}	132	54	FA ₂	269	30	FA ₂
358	88	S ₂	324	55	C _{sin}	139	68	C' _{dex}	144	64	FA ₂	282	25	FA ₂
178	84	S ₂	326	65	C _{sin}	6	64	C' _{dex}	153	48	FA ₂	277	24	FA ₂
3	89	S ₂	124	66	C _{sin}	350	75	C' _{dex}	96	42	FA ₂	244	3	FA ₃
161	75	S ₂	298	84	C _{sin}	329	77	C' _{dex}	275	22	FA ₂	325	10	FA ₃
182	84	S ₂	294	88	C _{sin}	340	72	C' _{dex}	272	12	FA ₂	80	3	FA ₃
191	78	S ₂	284	76	C _{sin}	4	82	C' _{dex}	262	29	FA ₂	259	15	FA ₃
176	69	S ₂	108	71	C _{sin}	7	88	C' _{dex}	275	10	FA ₂	284	7	FA ₃
343	74	S ₂	88	84	C _{sin}	172	76	C' _{dex}	285	14	FA ₂	267	4	FA ₃
188	85	S ₂	104	74	C _{sin}	350	89	C' _{dex}	87	12	FA ₂	244	22	FA ₃
194	88	S ₂	134	86	C _{sin}	0	65	C' _{dex}	112	7	FA ₂	114	14	FA ₃
199	72	S ₂	281	69	C _{sin}	21	69	C' _{dex}	94	18	FA ₂	285	24	FA ₃
336	87	S ₂	289	69	C _{sin}	354	73	C' _{dex}	99	15	FA ₂	274	5	FA ₃
152	84	S ₂	291	53	C _{sin}	3	67	C' _{dex}	88	10	FA ₂	274	13	FA ₃
150	80	S ₂	340	64	C _{sin}	356	64	C' _{dex}	279	28	FA ₂	272	13	FA ₃
332	89	S ₂	311	45	C _{sin}	347	88	C' _{dex}	250	20	FA ₂	282	17	FA ₃
140	84	S ₂	160	88	C _{sin}	343	78	C' _{dex}	75	25	FA ₂	122	12	FA ₃
314	80	S ₂	134	72	C _{sin}	319	55	C' _{dex}	266	9	FA ₂	270	8	FA ₃
331	87	S ₂	122	65	C _{sin}	320	61	C' _{dex}	285	27	FA ₂	260	1	FA ₃
142	84	S ₂	318	87	C _{sin}	24	27	C' _{dex}	242	51	FA ₂	273	24	FA ₃
321	78	S ₂	308	84	C _{sin}	31	36	C' _{dex}	151	60	FA ₄	263	31	FA ₃
351	85	S ₂	328	90	C _{sin}	45	36	C' _{dex}	69	56	FA ₄	267	23	FA ₃
353	82	S ₂	142	87	C _{sin}	222	58	C' _{dex}	260	87	FA ₄	341	28	FA ₃
173	89	S ₂	315	77	C _{sin}	203	71	C' _{dex}	80	81	FA ₄	285	32	FA ₃
358	84	S ₂	154	63	C _{sin}	325	43	C' _{dex}	76	76	FA ₄	319	31	FA ₃
355	85	S ₂	142	83	C _{sin}	256	44	C' _{dex}	240	54	FA ₄	299	30	FA ₃
161	86	S ₂	159	59	C _{sin}	230	50	C' _{dex}	72	76	FA ₄	290	20	FA ₃
6	85	S ₂	146	68	C _{sin}	200	37	C' _{dex}	214	77	FA ₄	321	15	FA ₃
6	84	S ₂	147	69	C _{sin}	260	55	C' _{dex}	156	85	FA ₄	325	13	FA ₃
349	84	S ₂	94	84	C _{sin}	264	52	C' _{dex}	113	69	FA ₄	282	15	FA ₃
340	87	S ₂	76	65	C _{sin}	255	39	C' _{dex}	155	64	FA ₄	280	12	FA ₃
160	79	S ₂	246	79	C _{sin}	288	79	C' _{dex}	320	60	FA ₄	277	7	FA ₃
162	76	S ₂	286	56	C _{sin}	284	77	C' _{dex}	212	40	FA ₄	290	10	FA ₃
331	60	S ₂	147	72	C _{sin}	274	88	C' _{dex}	62	85	FA ₄	279	21	FA ₃

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain E		
335	57	S ₂	333	83	C _{sin}	357	87	C' _{dex}	259	88	FA ₄	291	32	FA ₃
341	70	S ₂	326	81	C _{sin}	185	86	C' _{dex}	126	83	FA ₄	278	12	FA ₃
152	86	S ₂	307	85	C _{sin}	353	84	C' _{dex}	194	42	FA ₄	274	16	FA ₃
332	90	S ₂	347	43	C _{sin}	164	64	C' _{dex}	286	53	FA ₄	294	0	FA ₃
144	89	S ₂	351	85	C _{sin}	157	72	C' _{dex}	39	14	L ₁	300	4	FA ₃
140	89	S ₂	271	49	C _{sin}	347	86	C' _{dex}	29	6	L ₁	286	11	FA ₃
147	70	S ₂	303	56	C _{sin}	339	87	C' _{dex}	271	8	L ₁	286	10	FA ₃
0	69	S ₂	280	88	C _{sin}	158	82	C' _{dex}	272	9	L ₁			
333	80	S ₂	101	77	C _{sin}	164	68	C' _{dex}	272	4	L ₁			
343	75	S ₂	116	80	C _{sin}	171	80	C' _{dex}	111	35	L ₁			
333	90	S ₂	18	82	C _{sin}	330	84	C' _{dex}	105	37	L ₁			
338	81	S ₂	17	74	C _{sin}	0	75	C' _{dex}	267	22	L ₁			
165	90	S ₂	337	47	C _{sin}	17	83	C' _{dex}	246	29	L ₁			
162	87	S ₂	331	52	C _{sin}	186	89	C' _{dex}	254	14	L ₁			
142	74	S ₂	314	49	C _{sin}	354	82	C' _{dex}	257	37	L ₁			
138	80	S ₂	321	36	C _{sin}	8	80	C' _{dex}	247	11	L ₁			
326	90	S ₂	300	50	C _{sin}	9	70	C' _{dex}	246	20	L ₁			
339	89	S ₂	295	66	C _{sin}	294	42	C' _{dex}	250	22	L ₁			
328	80	S ₂	287	68	C _{sin}	311	36	C' _{dex}	257	37	L ₁			
160	89	S ₂	298	72	C _{sin}	333	55	C' _{dex}	264	28	L ₁			
321	87	S ₂	288	70	C _{sin}	334	50	C' _{dex}	74	49	L ₁			
325	85	S ₂	278	69	C _{sin}	27	65	C' _{dex}	106	51	L ₁			
335	88	S ₂	280	58	C _{sin}	20	70	C' _{dex}	98	39	L ₁			
157	80	S ₂	307	77	C _{sin}	24	66	C' _{dex}	274	36	L ₁			
153	81	S ₂	294	74	C _{sin}	5	90	C' _{dex}	74	27	L ₁			
330	90	S ₂	299	73	C _{sin}	258	58	C' _{dex}	82	11	L ₁			
325	77	S ₂	299	72	C _{sin}	306	45	C' _{nor}	66	27	L ₁			
138	85	S ₂	286	78	C _{sin}	317	55	C' _{nor}	73	28	L ₁			
336	85	S ₂	278	67	C _{sin}	224	52	C' _{nor}	76	18	L ₁			
341	80	S ₂	110	67	C _{sin}	230	48	C' _{nor}	148	40	L ₁			
326	83	S ₂	118	67	C _{sin}	295	78	C' _{nor}	90	34	L ₁			
326	86	S ₂	84	75	C _{sin}	268	70	C' _{nor}	69	24	L ₁			
330	83	S ₂	133	90	C _{sin}	264	16	C' _{nor}	72	9	L ₁			
324	82	S ₂	149	82	C _{sin}	321	16	C' _{nor}	73	74	L ₁			
324	81	S ₂	153	73	C _{sin}	297	36	C' _{nor}	58	74	L ₁			
154	82	S ₂	155	82	C _{sin}	247	21	C' _{nor}	75	61	L ₁			
162	88	S ₂	154	76	C _{sin}	151	55	C' _{nor}	284	7	L ₁			
351	75	S ₂	148	80	C _{sin}	170	53	C' _{nor}	108	2	L ₁			
353	71	S ₂	110	77	C _{sin}	181	34	C' _{nor}	272	8	L ₁			
328	65	S ₂	126	84	C _{sin}	182	32	C' _{nor}	97	26	L ₂			
348	85	S ₂	312	85	C _{sin}	139	68	C' _{nor}	103	23	L ₂			
163	72	S ₂	304	83	C _{sin}	332	52	C' _{nor}	101	23	L ₂			
356	63	S ₂	141	75	C _{sin}	329	64	C' _{nor}	92	25	L ₂			
181	40	S ₂	141	76	C _{sin}	198	43	C' _{nor}	94	28	L ₂			
183	43	S ₂	149	84	C _{sin}	216	36	C' _{nor}	103	32	L ₂			

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain D			Domain A		
161	88	S ₂	263	53	C _{sin}	4	21	C' _{nor}	94	18	L ₂	318	32	AP ₃
175	73	S ₂	254	65	C _{sin}	293	53	C' _{nor}	107	37	L ₂	300	22	AP ₃
171	79	S ₂	304	80	C _{sin}	273	43	C' _{nor}	110	11	L ₂	314	29	AP ₃
163	45	S ₂	149	82	C _{sin}	276	45	C' _{nor}	126	12	L ₂	285	45	AP ₃
335	80	S ₂	121	83	C _{sin}	226	22	C' _{nor}	132	34	L ₂	288	33	AP ₃
152	50	S ₂	129	73	C _{sin}	244	28	C' _{nor}	135	28	L ₂	246	52	AP ₃
150	89	S ₂	307	77	C _{sin}	252	43	C' _{nor}	3	45	L ₂	272	45	AP ₃
147	77	S ₂	287	89	C _{sin}	334	80	C' _{nor}	281	19	L _{sin}	283	41	AP ₃
150	86	S ₂	304	40	C _{sin}	332	78	C' _{nor}	284	60	L _{sin}	92	60	AP ₃
146	71	S ₂	304	69	C _{sin}	270	57	C' _{nor}	235	34	L _{sin}	268	69	AP ₃
350	75	S ₂	271	76	C _{sin}	260	70	C' _{nor}	256	28	L _{sin}	253	65	AP ₃
337	63	S ₂	308	54	C _{sin}	208	40	C' _{nor}	251	34	L _{sin}	274	72	AP ₃
341	62	S ₂	306	59	C _{sin}	219	53	C' _{nor}				89	87	AP ₃
189	79	S ₂	302	76	C _{sin}	228	53	C' _{nor}				310	24	AP ₃
349	81	S ₂	295	65	C _{sin}	344	70	C' _{nor}				312	24	AP ₃
337	61	S ₂	304	54	C _{sin}	333	66	C' _{nor}				241	28	AP ₃
353	68	S ₂	320	66	C _{sin}	283	64	C' _{nor}				236	44	AP ₃
329	50	S ₂	295	65	C _{sin}	263	38	C' _{nor}				222	49	AP ₃
322	68	S ₂	311	64	C _{sin}	248	54	C' _{nor}				321	17	AP ₃
351	49	S ₂	328	62	C _{sin}	250	63	C' _{nor}				314	15	AP ₃
335	55	S ₂	345	85	C _{sin}	271	38	C' _{nor}				342	25	AP ₃
322	45	S ₂	156	81	C _{sin}	239	45	C' _{nor}				338	35	AP ₃
326	70	S ₂	140	76	C _{sin}	264	74	C' _{nor}				302	10	AP ₃
134	87	S ₂	348	52	C _{sin}	9	70	C' _{nor}				37	30	FA ₁
326	83	S ₂	348	42	C _{sin}	305	65	C' _{nor}				51	22	FA ₁
333	74	S ₂	297	80	C _{sin}	239	75	C' _{nor}				78	37	FA ₁
154	88	S ₂	132	83	C _{sin}	247	63	C' _{nor}				86	24	FA ₁
144	67	S ₂	143	80	C _{sin}	267	67	C' _{nor}				242	7	FA ₁
329	70	S ₂	309	87	C _{sin}	266	61	C' _{nor}				224	31	FA ₁
331	85	S ₂	324	85	C _{sin}	257	61	C' _{nor}				242	28	FA ₁
162	85	S ₂	153	89	C _{sin}	24	66	C' _{nor}				224	31	FA ₁
330	80	S ₂	156	90	C _{sin}	5	90	C' _{nor}				250	10	FA ₁
344	66	S ₂	146	85	C _{sin}	258	58	C' _{nor}				254	14	FA ₁
331	90	S ₂	149	84	C _{sin}	117	72	C' _{rev}				274	2	FA ₁
338	86	S ₂	340	81	C _{sin}	118	69	C' _{rev}				277	11	FA ₁
149	84	S ₂	328	82	C _{sin}	72	42	C' _{rev}				71	4	FA ₁
334	89	S ₂	336	86	C _{sin}	67	42	C' _{rev}				245	5	FA ₁
160	85	S ₂	342	85	C _{sin}	301	60	C' _{rev}				85	7	FA ₁
150	81	S ₂	113	70	C _{sin}	307	57	C' _{rev}				74	4	FA ₁
332	69	S ₂	100	80	C _{sin}	303	50	C' _{rev}				96	7	FA ₁
349	84	S ₂	333	85	C _{sin}	320	30	C' _{rev}				92	5	FA ₁
347	82	S ₂	327	88	C _{sin}	325	75	C' _{rev}				254	7	FA ₁
166	85	S ₂	286	55	C _{sin}	304	70	C' _{rev}				259	0	FA ₁
173	83	S ₂	328	82	C _{sin}	292	65	C' _{rev}				110	24	FA ₁
351	68	S ₂	331	90	C _{sin}	271	51	C' _{rev}				102	18	FA ₁

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain A			Domain A		
166	86	S ₂	154	73	C _{sin}	68	77	C' _{rev}	71	59	L ₂	100	15	FA ₁
350	88	S ₂	142	72	C _{sin}	58	64	C' _{rev}	74	69	L ₂	69	7	FA ₂
355	80	S ₂	332	76	C _{sin}	201	69	C' _{rev}	73	67	L ₂	251	3	FA ₂
329	71	S ₂	312	82	C _{sin}	224	77	C' _{rev}	70	24	L ₂	227	26	FA ₂
329	61	S ₂	313	84	C _{sin}	205	70	C' _{rev}	64	48	L ₂	240	14	FA ₂
328	72	S ₂	148	65	C _{sin}	184	73	C' _{rev}	72	41	L ₂	255	4	FA ₂
357	73	S ₂	139	58	C _{sin}	240	90	C' _{rev}	68	46	L ₂	249	2	FA ₂
355	77	S ₂	163	72	C _{sin}	306	88	C' _{rev}	84	45	L ₂	72	16	FA ₂
344	62	S ₂	166	65	C _{sin}	305	75	C' _{rev}	90	36	L ₂	84	24	FA ₂
340	78	S ₂	343	86	C _{sin}	294	42	C' _{rev}	90	34	L ₂	250	5	FA ₂
175	75	S ₂	158	80	C _{sin}	311	36	C' _{rev}	93	51	L ₂	78	6	FA ₂
183	85	S ₂	346	89	C _{sin}	333	55	C' _{rev}	79	55	L ₂	228	8	FA ₂
7	67	S ₂	167	88	C _{sin}	334	50	C' _{rev}	98	57	L ₂	81	12	FA ₂
2	59	S ₂	339	86	C _{sin}	27	65	C' _{rev}	275	45	L ₂	264	24	FA ₂
334	60	S ₂	345	86	C _{sin}	20	70	C' _{rev}	270	35	L ₂	254	30	FA ₂
348	64	S ₂	139	80	C _{sin}	18	67	C' _{sin}	256	23	L ₂	254	16	FA ₂
0	59	S ₂	148	70	C _{sin}	119	72	C' _{sin}	254	46	L ₂	256	19	FA ₂
332	87	S ₂	130	67	C _{sin}	114	71	C' _{sin}	262	62	L ₂	255	16	FA ₂
341	81	S ₂	146	55	C _{sin}	126	85	C' _{sin}	96	34	L ₂	93	29	FA ₂
332	80	S ₂	152	75	C _{sin}	113	77	C' _{sin}	68	39	L ₂	93	30	FA ₂
332	85	S ₂	155	87	C _{sin}	277	89	C' _{sin}	89	45	L ₂	251	5	FA ₂
0	70	S ₂	147	74	C _{sin}	298	85	C' _{sin}	96	47	L ₂	71	1	FA ₂
359	71	S ₂	313	77	C _{sin}	316	55	C' _{sin}	50	45	L ₂	63	10	FA ₂
344	52	S ₂	310	74	C _{sin}	122	75	C' _{sin}	52	43	L ₂	72	20	FA ₂
347	56	S ₂	314	72	C _{sin}	306	78	C' _{sin}	58	40	L ₂	74	20	FA ₂
1	70	S ₂	304	90	C _{sin}	324	70	C' _{sin}	54	30	L ₂	65	26	FA ₂
358	65	S ₂	301	80	C _{sin}	254	82	C' _{sin}	78	35	L ₂	72	20	FA ₂
181	84	S ₂	289	89	C _{sin}	270	69	C' _{sin}	64	29	L ₂	69	28	FA ₂
337	86	S ₂	111	88	C _{sin}	257	70	C' _{sin}	60	52	L ₂	14	66	FA ₂
343	65	S ₂	334	81	C _{sin}	292	77	C' _{sin}	72	5	L ₂	16	50	FA ₂
184	71	S ₂	331	77	C _{sin}	124	70	C' _{sin}	12	64	L ₂	66	20	FA ₂
1	89	S ₂	161	86	C _{sin}	117	76	C' _{sin}	251	47	L ₂	85	13	FA ₂
167	82	S ₂	316	90	C _{sin}	302	90	C' _{sin}	237	39	L ₂	272	32	FA ₂
169	88	S ₂	315	84	C _{sin}	300	72	C' _{sin}	225	37	L ₂	253	5	FA ₂
9	90	S ₂	321	66	C _{sin}	274	77	C' _{sin}	233	38	L ₂	245	12	FA ₂
171	75	S ₂	122	78	C _{sin}	77	88	C' _{sin}	249	25	L ₂	245	15	FA ₂
178	82	S ₂	315	86	C _{sin}	261	87	C' _{sin}	247	25	L ₂	79	5	FA ₂
191	86	S ₂	150	90	C _{sin}	126	80	C' _{sin}	242	19	L ₂	69	4	FA ₂
8	84	S ₂	140	84	C _{sin}	123	84	C' _{sin}	243	22	L ₂	76	0	FA ₂
188	83	S ₂	321	83	C _{sin}	136	81	C' _{sin}	244	24	L ₂	234	10	FA ₂
345	69	S ₂	305	78	C _{sin}	121	79	C' _{sin}	247	24	L ₂	242	9	FA ₂
341	75	S ₂	304	77	C _{sin}	283	83	C' _{sin}	31	43	L ₂	269	24	FA ₂
178	79	S ₂	349	67	C _{sin}	284	57	C' _{sin}	51	29	L ₂	244	22	FA ₂
178	83	S ₂	352	62	C _{sin}	260	77	C' _{sin}	50	16	L ₂	244	11	FA ₂
336	64	S ₂	145	75	C _{sin}	265	77	C' _{sin}	242	26	L ₂	222	59	FA ₂

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain A			Domain A		
334	72	S_2	140	77	C_{sin}	110	45	C'_{sin}	243	25	L_2	240	80	FA_2
342	82	S_2	310	42	C_{sin}	112	44	C'_{sin}	247	52	L_2	257	1	FA_2
357	58	S_2	295	72	C_{sin}	106	89	C'_{sin}	248	47	L_2	256	2	FA_2
351	81	S_2	139	84	C_{sin}	105	90	C'_{sin}	93	28	L_2	244	3	FA_2
346	77	S_2	329	84	C_{sin}	237	83	C'_{sin}	97	27	L_2	90	11	FA_2
346	67	S_2	332	85	C_{sin}	149	74	C'_{sin}	98	38	L_2	240	9	FA_2
335	90	S_2	332	89	C_{sin}	105	76	C'_{sin}	234	38	L_2	55	3	FA_2
334	90	S_2	246	78	C_{sin}	108	75	C'_{sin}	231	46	L_2	62	1	FA_2
334	78	S_2	264	85	C_{sin}	107	74	C'_{sin}	237	18	L_2	40	14	FA_2
333	76	S_2	312	62	C_{sin}	100	86	C'_{sin}	234	20	L_2	219	11	FA_2
339	80	S_2	347	66	C_{sin}	301	84	C'_{sin}	235	17	L_2	218	19	FA_2
349	73	S_2	349	63	C_{sin}	277	65	C'_{sin}	39	15	L_2	225	26	FA_2
342	55	S_2	110	74	C_{sin}	275	72	C'_{sin}	55	10	L_2	70	15	FA_2
349	80	S_2	307	88	C_{sin}	90	85	C'_{sin}	62	3	L_2	70	21	FA_2
334	50	S_2	303	78	C_{sin}	86	73	C'_{sin}	61	9	L_2	239	22	FA_2
345	69	S_2	91	72	C_{sin}	306	68	C'_{sin}	81	34	L_2	75	16	FA_2
324	78	S_2	320	75	C_{sin}	306	80	C'_{sin}	67	22	L_2	56	1	FA_2
161	78	S_2	305	90	C_{sin}	233	90	C'_{sin}	74	22	L_2	237	5	FA_2
335	88	S_2	308	87	C_{sin}	42	89	C'_{sin}	88	23	L_2	265	20	FA_2
159	82	S_2	342	68	C_{sin}	246	85	C'_{sin}	94	38	L_2	254	5	FA_2
159	74	S_2	141	88	C_{sin}	225	78	C'_{sin}	152	74	L_2	266	2	FA_2
339	87	S_2	332	84	C_{sin}	306	82	C'_{sin}	86	59	L_2	265	4	FA_2
333	80	S_2	167	88	C_{sin}	309	90	C'_{sin}	55	27	L_2	257	17	FA_2
342	72	S_2	329	84	C_{sin}	129	86	C'_{sin}	87	27	L_2	264	21	FA_2
339	71	S_2	335	82	C_{sin}	280	58	C'_{sin}	56	36	L_2	260	7	FA_2
344	79	S_2	129	83	C_{sin}	271	68	C'_{sin}	62	32	L_2	263	11	FA_2
349	89	S_2	134	85	C_{sin}	106	81	C'_{sin}	88	25	L_2	281	54	FA_2
334	69	S_2	167	86	C_{sin}	116	84	C'_{sin}	84	28	L_2	285	3	FA_2
338	74	S_2	171	86	C_{sin}	114	81	C'_{sin}	83	48	L_2	84	26	FA_2
336	85	S_2	134	40	C_{sin}	99	75	C'_{sin}	77	33	L_2	95	17	FA_2
329	80	S_2	132	60	C_{sin}	115	77	C'_{sin}	85	12	L_2	88	32	FA_2
330	85	S_2	155	75	C_{sin}	298	88	C'_{sin}	82	8	L_2	89	31	FA_2
299	69	S_2	325	79	C_{sin}	310	80	C'_{sin}	168	77	L_2	90	35	FA_2
332	76	S_2	149	83	C_{sin}	118	85	C'_{sin}	222	58	L_2	90	12	FA_2
332	77	S_2	328	86	C_{sin}	305	87	C'_{sin}	232	42	L_2	89	18	FA_2
346	88	S_2	149	86	C_{sin}	141	78	C'_{sin}	107	63	L_2	263	33	FA_2
336	88	S_2	313	81	C_{sin}	82	68	C'_{sin}	73	53	L_2	245	20	FA_2
152	70	S_2	165	82	C_{sin}	93	80	C'_{sin}	81	31	L_2	112	5	FA_2
153	81	S_2	356	88	C_{sin}	289	70	C'_{sin}	83	28	L_2	111	1	FA_2
160	81	S_2	166	70	C_{sin}	98	86	C'_{sin}	84	46	L_2	102	32	FA_2
150	83	S_2	165	71	C_{sin}	90	89	C'_{sin}	89	44	L_2	94	23	FA_2
156	80	S_2	345	82	C_{sin}	96	80	C'_{sin}	246	42	L_2	84	18	FA_2
156	81	S_2	346	78	C_{sin}	291	81	C'_{sin}	243	58	L_2	86	22	FA_2
146	82	S_2	350	87	C_{sin}	286	87	C'_{sin}	240	52	L_2	281	5	FA_2
322	88	S_2	343	73	C_{sin}	315	77	C'_{sin}	246	56	L_2	340	14	FA_2

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain A			Domain A		
333	80	S_2	353	80	C_{sin}	308	82	C'_{sin}	235	52	L_2	330	24	FA_2
3387	80	S_2	0	80	C_{sin}	319	87	C'_{sin}	250	49	L_2	329	32	FA_2
159	75	S_2	181	89	C_{sin}	274	77	C'_{sin}	252	55	L_2	285	10	FA_2
160	74	S_2	170	86	C_{sin}	283	79	C'_{sin}	263	56	L_2	270	1	FA_2
325	84	S_2	161	68	C_{sin}	247	63	C'_{sin}	253	56	L_2	71	10	FA_2
326	87	S_2	116	64	C_{sin}	267	67	C'_{sin}	262	55	L_2	70	16	FA_2
157	79	S_2	127	78	C_{sin}	266	61	C'_{sin}	237	55	L_2	94	23	FA_2
157	66	S_2	119	52	C_{sin}	257	61	C'_{sin}	239	54	L_2	89	29	FA_2
295	65	S_2	285	82	C_{sin}	306	88	C'_{sin}	247	36	L_2	77	34	FA_2
298	67	S_2	125	62	C_{sin}	305	75	C'_{sin}	242	47	L_2	287	8	FA_2
144	83	S_2	112	65	C_{sin}	147	20	AP_1	269	75	L_2	284	2	FA_2
331	90	S_2	314	80	C_{sin}	195	56	AP_1	248	63	L_2	91	5	FA_2
335	90	S_2	318	67	C_{sin}	204	54	AP_1	241	61	L_2	96	15	FA_2
144	69	S_2	306	66	C_{sin}	286	44	AP_1	75	37	L_2	78	4	FA_2
146	76	S_2	331	71	C_{sin}	305	34	AP_1	91	42	L_2	79	9	FA_2
327	87	S_2	333	84	C_{sin}	306	38	AP_1	75	52	L_2	268	6	FA_2
149	88	S_2	343	88	C_{sin}	37	67	AP_1	75	28	L_2	92	32	FA_2
142	88	S_2	324	84	C_{sin}	123	27	AP_1	252	4	L_2	45	45	FA_2
153	89	S_2	336	83	C_{sin}	172	45	AP_1	251	19	L_2	89	22	FA_2
144	90	S_2	324	80	C_{sin}	210	29	AP_1	250	27	L_2	65	34	FA_2
148	90	S_2	330	60	C_{sin}	153	30	AP_1	68	13	L_2	230	39	FA_2
151	90	S_2	310	90	C_{sin}	140	63	AP_1	65	15	L_2	236	18	FA_2
142	90	S_2	286	89	C_{sin}	97	14	AP_1	53	9	L_2	275	62	FA_2
330	85	S_2	138	88	C_{sin}	73	52	AP_1	59	20	L_2	64	17	FA_2
336	80	S_2	330	52	C_{sin}	70	50	AP_1	59	11	L_2	72	8	FA_2
154	86	S_2	316	56	C_{sin}	291	16	AP_1	47	20	L_2	53	12	FA_2
141	84	S_2	313	67	C_{sin}	265	18	AP_1	15	38	L_2	52	29	FA_2
155	87	S_2	123	55	C_{sin}	303	10	AP_1	40	27	L_2	95	12	FA_2
330	70	S_2	267	83	C_{sin}	216	23	AP_1	34	28	L_2	99	22	FA_2
332	78	S_2	295	81	C_{sin}	197	45	AP_1	81	28	L_2	59	32	FA_2
153	80	S_2	330	51	C_{sin}	89	0	AP_1	81	20	L_2	92	4	FA_2
149	85	S_2	332	84	C_{sin}	228	14	AP_1	89	10	L_2	248	13	FA_3
336	83	S_2	330	82	C_{sin}	279	28	AP_1	68	24	L_2	250	13	FA_3
334	75	S_2	308	60	C_{sin}	274	54	AP_1	78	14	L_2	253	2	FA_3
333	75	S_2	309	66	C_{sin}	22	26	AP_1	75	25	L_2	243	54	FA_3
333	75	S_2	314	51	C_{sin}	33	29	AP_1	85	24	L_2	251	32	FA_3
335	84	S_2	335	62	C_{sin}	334	36	AP_1	77	19	L_2	256	42	FA_3
336	75	S_2	318	58	C_{sin}	239	11	AP_1	68	24	L_2	252	12	FA_3
336	85	S_2	326	64	C_{sin}	1	26	AP_1	71	20	L_2	85	36	FA_3
156	87	S_2	358	46	C_{sin}	353	15	AP_1	69	27	L_2	266	35	FA_3
161	89	S_2	334	39	C_{sin}	274	29	AP_1	71	29	L_2	264	28	FA_3
157	87	S_2	319	81	C_{sin}	308	85	AP_2	80	23	L_2	242	43	FA_3
331	90	S_2	297	69	C_{sin}	300	86	AP_2	67	32	L_2	235	31	FA_3
334	86	S_2	142	78	C_{sin}	351	48	AP_2	78	18	L_2	25	35	FA_3
335	86	S_2	132	86	C_{sin}	24	64	AP_2	76	33	L_2	82	47	FA_3

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain A			Domain A		
333	88	S ₂	154	78	C _{sin}	323	67	AP ₂	76	22	L ₂	212	52	FA ₃
336	89	S ₂	151	77	C _{sin}	341	82	AP ₂	256	15	L ₂	217	60	FA ₃
325	70	S ₂	128	72	C _{sin}	144	52	AP ₂	257	8	L ₂	231	59	FA ₃
339	82	S ₂	132	76	C _{sin}	130	57	AP ₂	248	4	L ₂	153	85	FA ₃
339	82	S ₂	139	72	C _{sin}	90	90	AP ₂	256	21	L ₂	271	17	FA ₃
161	88	S ₂	124	60	C _{sin}	329	65	AP ₂	266	22	L ₂	274	15	FA ₃
357	79	S ₂	121	79	C _{sin}	326	84	AP ₂	252	39	L ₂	298	18	FA ₃
126	47	S ₂	115	80	C _{sin}	312	73	AP ₂	253	14	L ₂	252	4	FA ₃
135	58	S ₂	127	77	C _{sin}	302	72	AP ₂	261	33	L ₂	258	11	FA ₃
160	69	S ₂	118	70	C _{sin}	309	65	AP ₂	253	11	L ₂	267	8	FA ₃
156	73	S ₂	303	85	C _{sin}	204	73	AP ₂	254	18	L ₂	82	11	L ₁
135	50	S ₂	307	90	C _{sin}	166	69	AP ₂	242	8	L ₂	285	7	L ₁
150	57	S ₂	312	90	C _{sin}	171	69	AP ₂	263	5	L ₂	272	3	L ₁
137	78	S ₂	309	78	C _{sin}	17	9	AP ₂	220	30	L ₂	258	18	L ₁
139	76	S ₂	313	83	C _{sin}	330	15	AP ₂	232	10	L ₂	259	20	L ₁
144	64	S ₂	337	67	C _{sin}	95	37	AP ₂	237	20	L ₂	265	13	L ₁
145	57	S ₂	344	70	C _{sin}	68	22	AP ₂	249	27	L ₂	263	20	L ₁
132	51	S ₂	356	74	C _{sin}	110	74	AP ₂	234	4	L ₂	65	4	L ₁
142	55	S ₂	107	61	C _{sin}	93	85	AP ₂	229	15	L ₂	252	8	L ₁
133	68	S ₂	300	78	C _{sin}	280	75	AP ₂	230	20	L ₂	261	11	L ₁
137	64	S ₂	304	85	C _{sin}	258	86	AP ₂	241	8	L ₂	239	34	L ₁
157	77	S ₂	332	67	C _{sin}	266	83	AP ₂	243	5	L ₂	255	21	L ₁
156	72	S ₂	322	67	C _{sin}	294	79	AP ₂	250	21	L ₂	255	32	L ₁
344	58	S ₂	319	55	C _{sin}	299	72	AP ₂	236	17	L ₂	260	32	L ₁
328	52	S ₂	321	71	C _{sin}	284	64	AP ₂	229	29	L ₂	248	21	L ₁
160	88	S ₂	323	67	C _{sin}	282	67	AP ₂	42	18	L ₂	262	19	L ₁
336	88	S ₂	168	72	C _{sin}	277	45	AP ₂	52	10	L ₂	261	6	L ₁
332	86	S ₂	324	48	C _{sin}	317	50	AP ₂	232	10	L ₂	249	21	L ₁
148	86	S ₂	309	35	C _{sin}	320	70	AP ₂	224	8	L ₂	246	2	L ₁
0	72	S ₂	336	60	C _{sin}	333	52	AP ₂	60	7	L ₂	254	15	L ₁
345	85	S ₂	338	65	C _{sin}	333	69	AP ₂	51	5	L ₂	249	46	L ₁
352	64	S ₂	342	45	C _{sin}	325	82	AP ₂	250	14	L ₂	235	41	L ₁
21	65	S ₂	355	78	C _{sin}	343	90	AP ₂	242	9	L ₂	221	24	L ₁
10	68	S ₂	349	82	C _{sin}	131	37	AP ₂	236	12	L ₂	55	8	L ₁
172	60	S ₂	353	85	C _{sin}	133	34	AP ₂	228	4	L ₂	60	4	L ₁
173	60	S ₂	349	84	C _{sin}	117	60	AP ₂	238	6	L ₂	254	4	L ₁
315	80	S ₂	339	86	C _{sin}	243	72	AP ₂	90	13	L ₂	235	18	L ₁
323	73	S ₂	353	85	C _{sin}	270	88	AP ₂	275	5	L ₂	232	11	L ₁
326	90	S ₂	354	87	C _{sin}	276	76	AP ₂	82	16	L ₂	83	20	L ₁
137	90	S ₂	343	84	C _{sin}	90	70	AP ₂	82	5	L ₂	88	21	L ₁
158	84	S ₂	342	77	C _{sin}	80	70	AP ₂	246	46	L ₃	245	6	L ₁
160	82	S ₂	325	63	C _{sin}	91	70	AP ₂	242	44	L ₃	255	14	L ₁
157	82	S ₂	326	57	C _{sin}	345	73	AP ₂	242	39	L ₃	257	12	L ₁
162	87	S ₂	339	50	C _{sin}	345	73	AP ₂	235	44	L ₃	232	2	L ₁
159	82	S ₂	342	77	C _{sin}	326	87	AP ₂	273	3	L ₃	208	52	L ₁

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain A			Domain A		
185	83	S ₂	329	66	C _{sin}	324	82	AP ₂	250	23	L _{dex}	226	25	L ₁
340	90	S ₂	294	80	C _{sin}	329	80	AP ₂	271	16	L _{dex}	232	24	L ₁
349	86	S ₂	300	68	C _{sin}	146	84	AP ₂	261	58	L _{dex}	236	24	L ₁
339	86	S ₂	286	62	C _{sin}	330	78	AP ₂	109	30	L _{dex}	236	28	L ₁
340	87	S ₂	292	60	C _{sin}	93	80	AP ₂	242	24	L _{dex}	264	19	L ₁
344	89	S ₂	320	87	C _{sin}	321	88	AP ₂	216	15	L _{dex}	264	22	L ₁
159	83	S ₂	145	86	C _{sin}	145	89	AP ₂	238	39	L _{dex}	273	32	L ₁
340	82	S ₂	346	84	C _{sin}	146	87	AP ₂	78	45	L _{dex}	251	19	L ₁
337	84	S ₂	308	86	C _{sin}	37	76	AP ₂	78	20	L _{dex}	255	17	L ₁
171	80	S ₂	351	82	C _{sin}	312	45	AP ₂	105	26	L _{dex}	62	4	L ₁
169	86	S ₂	156	90	C _{sin}	345	52	AP ₂	273	11	L _{dex}	241	17	L ₁
169	88	S ₂	321	86	C _{sin}	260	86	AP ₂	21	54	L _{dex}	250	14	L ₁
172	85	S ₂	331	89	C _{sin}	311	74	AP ₂	23	59	L _{dex}	246	10	L ₁
164	87	S ₂	312	83	C _{sin}	312	72	AP ₂	262	30	L _{rev}	248	19	L ₁
166	86	S ₂	310	80	C _{sin}	308	70	AP ₂	268	35	L _{rev}	57	4	L ₁
335	84	S ₂	316	83	C _{sin}	316	75	AP ₂	66	6	L _{rev}	262	20	L ₁
338	65	S ₂	301	77	C _{sin}	356	86	AP ₂	230	25	L _{rev}	89	20	L ₁
335	58	S ₂	306	79	C _{sin}	180	34	AP ₂	49	5	L _{rev}	218	10	L ₁
317	63	S ₂	317	77	C _{sin}	167	26	AP ₂	48	14	L _{rev}	85	28	L ₁
326	70	S ₂	309	85	C _{sin}	305	78	AP ₂	245	10	L _{rev}	265	23	L ₁
343	82	S ₂	317	86	C _{sin}	321	85	AP ₂	265	19	L _{sin}	109	11	L ₁
335	80	S ₂	313	80	C _{sin}	357	76	AP ₂	259	14	L _{sin}	271	5	L ₁
332	79	S ₂	317	76	C _{sin}	352	62	AP ₂	264	17	L _{sin}	76	5	L ₁
324	78	S ₂	318	70	C _{sin}	218	58	AP ₂	260	28	L _{sin}	251	9	L ₁
168	66	S ₂	288	88	C _{sin}	252	82	AP ₂	265	20	L _{sin}	82	8	L ₁
161	63	S ₂	303	86	C _{sin}	269	73	AP ₂	163	64	L _{sin}	264	1	L ₁
154	70	S ₂	306	88	C _{sin}	267	72	AP ₂	247	32	L _{sin}	272	5	L ₁
145	65	S ₂	304	86	C _{sin}	246	88	AP ₂	243	32	L _{sin}	106	3	L ₁
180	70	S ₂	301	85	C _{sin}	245	90	AP ₂	234	17	L _{sin}	72	4	L ₁
176	78	S ₂	301	90	C _{sin}	75	83	AP ₂	236	8	L _{sin}	82	5	L ₁
162	86	S ₂	125	85	C _{sin}	83	68	AP ₂	226	10	L _{sin}	261	7	L ₁
323	83	S ₂	114	88	C _{sin}	72	73	AP ₂	223	3	L _{sin}	258	8	L ₁
345	87	S ₂	321	90	C _{sin}	284	36	AP ₂	252	17	L _{sin}	76	4	L ₁
140	87	S ₂	140	78	C _{sin}	293	44	AP ₂	251	21	L _{sin}	243	3	L ₁
133	88	S ₂	106	80	C _{sin}	290	40	AP ₂	228	18	L _{sin}	70	1	L ₁
131	84	S ₂	114	69	C _{sin}	353	70	AP ₂	231	15	L _{sin}	72	4	L ₁
0	82	S ₂	124	90	C _{sin}	150	76	AP ₂	228	27	L _{sin}	261	21	L ₁
153	74	S ₂	136	87	C _{sin}	357	68	AP ₂	228	22	L _{sin}	267	24	L ₁
152	67	S ₂	305	78	C _{sin}	12	53	AP ₂	230	21	L _{sin}	243	8	L ₁
355	80	S ₂	317	75	C _{sin}	282	50	AP ₂	222	22	L _{sin}	224	14	L ₁
331	86	S ₂	149	84	C _{sin}	273	46	AP ₂	236	12	L _{sin}	59	8	L ₁
340	80	S ₂	150	84	C _{sin}	213	60	AP ₂	233	37	L _{sin}	38	24	L ₁
350	80	S ₂	145	80	C _{sin}	208	56	AP ₂	234	37	L _{sin}	232	1	L ₁
159	90	S ₂	144	78	C _{sin}	337	28	AP ₂	244	12	L _{sin}	248	5	L ₁
148	89	S ₂	130	61	C _{sin}	23	46	AP ₂	243	17	L _{sin}	270	14	L ₁

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain A			Domain A		
335	81	S ₂	94	64	C _{sin}	2	85	AP ₂	240	18	L _{sin}	218	38	L ₁
343	74	S ₂	114	72	C _{sin}	346	77	AP ₂	232	8	L _{sin}	160	67	L ₁
336	89	S ₂	117	70	C _{sin}	111	33	AP ₂	232	8	L _{sin}	220	49	L ₁
339	78	S ₂	129	68	C _{sin}	233	56	AP ₂	233	9	L _{sin}	215	13	L ₁
152	84	S ₂	108	54	C _{sin}	223	78	AP ₂	230	10	L _{sin}	219	21	L ₁
173	78	S ₂	115	64	C _{sin}	194	71	AP ₂	235	14	L _{sin}	233	20	L ₁
142	83	S ₂	136	82	C _{sin}	298	84	AP ₂	226	12	L _{sin}	234	12	L ₁
314	85	S ₂	130	75	C _{sin}	139	78	AP ₂	251	7	L _{sin}	250	38	L ₁
330	69	S ₂	140	80	C _{sin}	299	75	AP ₂	260	24	L _{sin}	256	12	L ₁
341	37	S ₂	148	90	C _{sin}	129	65	AP ₂	77	14	L _{sin}	76	11	L ₁
331	67	S ₂	135	79	C _{sin}	117	75	AP ₂	42	1	L _{sin}	250	9	L ₁
339	62	S ₂	133	75	C _{sin}	104	72	AP ₂	42	15	L _{sin}	222	3	L ₁
341	54	S ₂	325	89	C _{sin}	171	42	AP ₂	229	29	L _{sin}	266	7	L ₁
298	65	S ₂	330	87	C _{sin}	343	51	AP ₂	222	24	L _{sin}	260	6	L ₁
346	62	S ₂	150	89	C _{sin}	338	49	AP ₂	239	16	L _{sin}	248	18	L ₁
323	74	S ₂	338	64	C _{sin}	32	55	AP ₂	217	26	L _{sin}	226	4	L ₁
320	77	S ₂	277	90	C _{sin}	45	61	AP ₂	203	7	L _{sin}	269	14	L ₁
312	81	S ₂	122	82	C _{sin}	279	10	AP ₂	262	28	L _{sin}	248	17	L ₁
323	85	S ₂	292	83	C _{sin}	279	32	AP ₂	244	24	L _{sin}	329	22	L ₁
319	70	S ₂	282	72	C _{sin}	338	28	AP ₂	262	21	L _{sin}	240	22	L ₁
324	73	S ₂	276	67	C _{sin}	332	32	AP ₂	42	37	L _{sin}	330	24	L ₁
321	60	S ₂	275	70	C _{sin}	340	22	AP ₂	249	12	L _{sin}	264	10	L ₁
323	78	S ₂	130	72	C _{sin}	326	40	AP ₂	253	5	L _{sin}	261	3	L ₁
169	72	S ₂	135	70	C _{sin}	131	78	AP ₂	256	11	L _{sin}	82	2	L ₁
141	90	S ₂	132	85	C _{sin}	111	75	AP ₂	58	2	L _{sin}	81	24	L ₁
149	84	S ₂	297	83	C _{sin}	133	74	AP ₂	79	19	L _{sin}	96	28	L ₁
141	89	S ₂	299	80	C _{sin}	116	67	AP ₂	82	22	L _{sin}	85	32	L ₁
313	74	S ₂	304	82	C _{sin}	101	90	AP ₂	261	15	L _{sin}	76	36	L ₁
327	63	S ₂	113	80	C _{sin}	310	90	AP ₂	256	17	L _{sin}	43	20	L ₁
332	63	S ₂	133	71	C _{sin}	319	90	AP ₂	66	6	L _{sin}	44	17	L ₁
325	68	S ₂	306	74	C _{sin}	151	68	AP ₂	230	25	L _{sin}	64	7	L ₁
319	65	S ₂	104	87	C _{sin}	150	76	AP ₂	49	5	L _{sin}	58	4	L ₁
306	61	S ₂	289	74	C _{sin}	326	46	AP ₂	48	14	L _{sin}	252	24	L ₁
267	74	S ₂	296	84	C _{sin}	349	39	AP ₂	245	10	L _{sin}	248	22	L ₁
295	65	S ₂	297	68	C _{sin}	175	45	AP ₂	69	32	L _{sin}	252	12	L ₁
302	67	S ₂	319	85	C _{sin}	181	61	AP ₂	86	30	L _{sin}	275	22	L ₁
294	66	S ₂	139	82	C _{sin}	175	59	AP ₂	83	31	L _{sin}	275	26	L ₁
305	53	S ₂	305	72	C _{sin}	202	84	AP ₂	254	24	L _{sin}	264	17	L ₁
314	73	S ₂	127	81	C _{sin}	340	82	AP ₂	46	38	L _{sin}	256	4	L ₁
288	50	S ₂	294	89	C _{sin}	359	70	AP ₂	29	58	L _{sin}	260	3	L ₁
310	62	S ₂	241	71	C _{sin}	5	87	AP ₂	247	37	L _{sin}	259	8	L ₁
137	62	S ₂	106	69	C _{sin}	5	72	AP ₂	242	37	L _{sin}	256	12	L ₁
143	63	S ₂	150	83	C _{sin}	348	69	AP ₂	93	29	L _{sin}	240	45	L ₁
137	54	S ₂	144	90	C _{sin}	200	32	AP ₂	234	12	L _{sin}	238	32	L ₁
141	55	S ₂	118	72	C _{sin}	220	32	AP ₂	26	44	L _{sin}	222	52	L ₁

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain A			Domain A		
143	50	S ₂	135	83	C _{sin}	210	88	AP ₂	37	36	L _{sin}	242	40	L ₁
149	74	S ₂	136	82	C _{sin}	197	5	AP ₂	41	35	L _{sin}	228	38	L ₁
141	68	S ₂	314	88	C _{sin}	11	64	AP ₂	40	25	L _{sin}	241	20	L ₁
121	90	S ₂	143	78	C _{sin}	13	66	AP ₂	33	37	L _{sin}	239	21	L ₁
149	61	S ₂	143	89	C _{sin}	24	48	AP ₂	71	34	L _{sin}	240	28	L ₁
138	70	S ₂	308	84	C _{sin}	21	65	AP ₂	72	56	L _{sin}	107	11	L ₁
155	67	S ₂	137	82	C _{sin}	29	86	AP ₂	75	14	L _{sin}	267	13	L ₁
151	75	S ₂	78	37	AP ₁	323	87	AP ₂	77	31	L _{sin}	267	7	L ₁
142	75	S ₂	359	64	AP ₁	340	84	AP ₂	264	13	L _{sin}	100	29	L ₁
145	80	S ₂	22	70	AP ₁	304	40	AP ₂	277	3	L _{sin}	105	8	L ₁
142	80	S ₂	131	36	AP ₁	77	75	AP ₃	287	33	L _{sin}	0	76	L ₁
150	54	S ₂	45	26	AP ₁	88	81	AP ₃				72	7	L ₁
129	53	S ₂	104	42	AP ₁	86	77	AP ₃				232	18	L ₁
81	50	S ₂	155	43	AP ₁	90	90	AP ₃				4	90	L ₁
337	75	S ₂	146	34	AP ₁	80	79	AP ₃				209	40	L ₁
347	88	S ₂	73	56	AP ₁	95	78	AP ₃				257	10	L ₁
342	82	S ₂	83	29	AP ₁	251	49	L ₁				255	24	L ₂
353	86	S ₂	10	54	AP ₁	263	48	L ₁				252	16	L ₂
341	88	S ₂	353	61	AP ₁	290	41	L ₁				254	12	L ₂
347	87	S ₂	277	32	AP ₁	345	17	L ₁				259	6	L ₂
321	84	S ₂	198	58	AP ₁	341	39	L ₁				214	15	L ₂
172	90	S ₂	177	44	AP ₁	8	47	L ₁				239	12	L ₂
333	75	S ₂	173	82	AP ₁	357	43	L ₁				265	3	L ₂
3	82	S ₂	166	72	AP ₁	320	58	L ₁				260	7	L ₂
336	84	S ₂	351	56	AP ₁	232	24	L ₁				255	13	L ₂
357	80	S ₂	328	24	AP ₁	42	1	L ₁				260	6	L ₂
339	84	S ₂	327	28	AP ₁	25	17	L ₁				262	3	L ₂
171	84	S ₂	298	24	AP ₁	29	32	L ₁				80	18	L ₂
171	87	S ₂	166	15	AP ₁	36	27	L ₁				254	4	L ₂
167	86	S ₂	12	33	AP ₁	10	16	L ₁				265	1	L ₂
354	86	S ₂	321	45	AP ₁	240	6	L ₁				260	26	L ₂
170	86	S ₂	335	45	AP ₁	56	20	L ₁				254	23	L ₂
155	81	S ₂	146	9	AP ₁	58	13	L ₁				276	24	L ₂
161	75	S ₂	173	33	AP ₁	63	2	L ₁				251	14	L ₂
162	75	S ₂	165	43	AP ₁	62	13	L ₁				251	16	L ₂
150	73	S ₂	188	38	AP ₁	112	40	L ₁				64	6	L ₂
151	73	S ₂	169	28	AP ₁	109	14	L ₁				264	21	L ₂
159	76	S ₂	153	60	AP ₁	108	24	L ₁				241	13	L ₂
163	82	S ₂	168	64	AP ₁	268	35	L ₁				256	5	L ₂
149	74	S ₂	170	37	AP ₁	279	24	L ₁				258	1	L ₂
152	72	S ₂	22	71	AP ₁	289	28	L ₁				262	17	L ₂
165	84	S ₂	133	18	AP ₁	195	36	L ₁				102	6	L ₂
162	83	S ₂	338	72	AP ₂	196	31	L ₁				258	23	L ₂
171	79	S ₂	332	74	AP ₂	3	9	L ₁				240	16	L ₂
163	81	S ₂	344	80	AP ₂	18	25	L ₁				258	19	L ₂

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain A		
158	81	S ₂	335	89	AP ₂	355	9	L ₁	256	17	L ₂
176	85	S ₂	346	83	AP ₂	248	22	L ₂	260	7	L ₂
168	83	S ₂	169	89	AP ₂	248	10	L ₂	251	8	L ₂
180	81	S ₂	11	69	AP ₂	243	37	L ₂	60	11	L ₂
178	79	S ₂	11	60	AP ₂	252	32	L ₂	276	6	L ₂
191	75	S ₂	153	80	AP ₂	251	5	L ₂	269	3	L ₂
310	75	S ₂	160	82	AP ₂	245	21	L ₂	231	17	L ₂
320	81	S ₂	331	70	AP ₂	250	22	L ₂	254	29	L ₂
320	76	S ₂	338	65	AP ₂	244	25	L ₂	252	14	L ₂
176	67	S ₂	344	80	AP ₂	255	23	L ₂	262	10	L ₂
170	87	S ₂	335	79	AP ₂	231	23	L ₂	240	6	L ₂
168	86	S ₂	6	77	AP ₂	241	24	L ₂	261	5	L ₂
156	90	S ₂	354	83	AP ₂	299	72	L ₂	252	4	L ₂
152	83	S ₂	160	88	AP ₂	292	72	L ₂	75	2	L ₂
152	87	S ₂	342	65	AP ₂	240	25	L ₂	253	24	L ₂
156	81	S ₂	157	68	AP ₂	244	22	L ₂	258	24	L ₂
158	82	S ₂	165	72	AP ₂	238	45	L ₂	81	24	L ₂
144	87	S ₂	345	84	AP ₂	260	64	L ₂	249	9	L ₂
152	71	S ₂	340	75	AP ₂	266	58	L ₂	238	16	L ₂
159	74	S ₂	325	86	AP ₂	260	61	L ₂	258	13	L ₂
149	72	S ₂	339	77	AP ₂	266	56	L ₂	250	8	L ₂
336	84	S ₂	332	71	AP ₂	304	60	L ₂	264	22	L ₂
335	88	S ₂	190	71	AP ₂	300	64	L ₂	264	16	L ₂
169	83	S ₂	335	90	AP ₂	306	64	L ₂	253	11	L ₂
159	83	S ₂	156	75	AP ₂	262	50	L ₂	75	1	L ₂
149	88	S ₂	164	78	AP ₂	262	24	L ₂	79	14	L ₂
346	85	S ₂	337	81	AP ₂	250	28	L ₂	64	12	L ₂
328	85	S ₂	187	50	AP ₂	253	29	L ₂	272	55	L ₂
156	81	S ₂	167	82	AP ₂	262	26	L ₂	252	25	L ₂
148	85	S ₂	339	80	AP ₂	249	25	L ₂	253	30	L ₂
340	75	S ₂	131	88	AP ₂	257	31	L ₂	260	41	L ₂
340	78	S ₂	135	80	AP ₂	232	36	L ₂	266	43	L ₂
326	84	S ₂	159	81	AP ₂	274	17	L ₂	226	35	L ₂
315	80	S ₂	342	62	AP ₂	262	3	L ₂	244	20	L ₂
351	72	S ₂	4	62	AP ₂	250	7	L ₂	253	16	L ₂
343	84	S ₂	176	74	AP ₂	34	39	L ₂	228	22	L ₂
146	84	S ₂	5	81	AP ₂	13	45	L ₂	253	28	L ₂
150	87	S ₂	342	73	AP ₂	31	46	L ₂	51	9	L ₂
323	85	S ₂	344	43	AP ₂	46	44	L ₂	256	9	L ₂
168	76	S ₂	341	41	AP ₂	37	49	L ₂	251	6	L ₂
158	80	S ₂	170	53	AP ₂	247	3	L ₂	245	5	L ₂
163	77	S ₂	145	82	AP ₂	253	16	L ₂	246	2	L ₂
170	80	S ₂	298	78	AP ₂	263	9	L ₂	242	0	L ₂
152	78	S ₂	147	48	AP ₂	292	18	L ₂	247	4	L ₂
148	75	S ₂	163	71	AP ₂	288	9	L ₂	249	19	L ₂

Supporting Table 1: raw data of structural measurements

Domain A			Domain A			Domain C			Domain A		
152	75	S ₂	155	80	AP ₂	289	11	L ₂	255	20	L ₂
140	90	S ₂	329	77	AP ₂	249	19	L _{dex}	248	6	L ₂
148	90	S ₂	333	63	AP ₂	266	0	L _{dex}	254	14	L ₂
146	90	S ₂	317	80	AP ₂	313	7	L _{nor}	260	18	L ₂
314	49	S ₂	135	75	AP ₂	315	12	L _{nor}	252	14	L ₂
328	47	S ₂	136	84	AP ₂	314	8	L _{nor}	246	8	L ₂
330	46	S ₂	327	73	AP ₂	316	20	L _{nor}	243	7	L ₂
340	84	S ₂	156	87	AP ₂	310	16	L _{nor}	242	11	L ₂
161	90	S ₂	159	90	AP ₂	240	30	L _{sin}	233	37	L ₂
337	65	S ₂	332	84	AP ₂	246	26	L _{sin}	258	4	L ₂
344	73	S ₂	332	54	AP ₂	306	45	L _{sin}	261	11	L ₂
129	76	S ₂	349	56	AP ₂	292	44	L _{sin}	90	29	L ₂
145	78	S ₂	13	46	AP ₂	310	48	L _{sin}	92	22	L ₂
177	81	S ₂	140	75	AP ₂	283	46	L _{sin}	279	2	L ₂
151	71	S ₂	144	66	AP ₂	225	26	L _{sin}	87	11	L ₂
160	69	S ₂	356	51	AP ₂	287	39	L _{sin}	266	4	L ₂
163	80	S ₂	343	63	AP ₂	285	52	L _{sin}	175	2	L ₂
152	75	S ₂	343	53	AP ₂	305	52	L _{sin}	85	3	L ₂
165	84	S ₂	352	35	AP ₂	271	65	L _{sin}	94	0	L ₂
163	81	S ₂	348	55	AP ₂	269	39	L _{sin}	269	4	L ₂
153	77	S ₂	358	62	AP ₂	259	27	L _{sin}	275	6	L ₂
160	86	S ₂	342	54	AP ₂	266	3	FA ₁	270	4	L ₂
157	85	S ₂	348	52	AP ₂	275	19	FA ₁	266	5	L ₂
150	75	S ₂	346	59	AP ₂	343	10	FA ₁	268	4	L ₂
348	74	S ₂	19	76	AP ₂	33	16	FA ₁	265	4	L ₂
343	67	S ₂	10	76	AP ₂	37	11	FA ₁	88	28	L ₂
346	69	S ₂	10	80	AP ₂	130	12	FA ₁	90	44	L ₂
339	79	S ₂	9	89	AP ₂	108	22	FA ₁	91	32	L ₂
343	76	S ₂	11	90	AP ₂	107	26	FA ₁	91	25	L ₂
341	80	S ₂	181	81	AP ₂	195	23	FA ₁	83	22	L ₂
350	75	S ₂	181	82	AP ₂	68	24	FA ₁	94	34	L ₂
356	77	S ₂	163	81	AP ₂	125	54	FA ₁	100	27	L ₂
354	75	S ₂	178	74	AP ₂	175	7	FA ₁	92	21	L ₂
348	90	S ₂	348	89	AP ₂	293	8	FA ₁	67	27	L ₂
353	90	S ₂	348	90	AP ₂	250	10	FA ₁	278	6	L ₂
349	87	S ₂	26	25	AP ₂	274	15	FA ₁	62	12	L ₂
349	85	S ₂	80	38	AP ₂	91	4	FA ₁	69	12	L ₂
344	87	S ₂	46	39	AP ₂	158	15	FA ₁	75	20	L ₂
352	84	S ₂	12	86	AP ₂	254	6	FA ₁	64	2	L ₂
343	85	S ₂	6	82	AP ₂	203	4	FA ₁	45	7	L ₂
342	72	S ₂	1	67	AP ₂	285	22	FA ₁	61	17	L ₂
350	74	S ₂	357	73	AP ₂	96	15	FA ₁	74	5	L ₂
174	83	S ₂	336	65	AP ₂	267	20	FA ₁	62	28	L ₂
308	78	S ₂	349	86	AP ₂	265	12	FA ₁	234	3	L ₂
348	86	S ₂	349	62	AP ₂	261	24	FA ₁	93	28	L ₂

Supporting Table 1: raw data of structural measurements

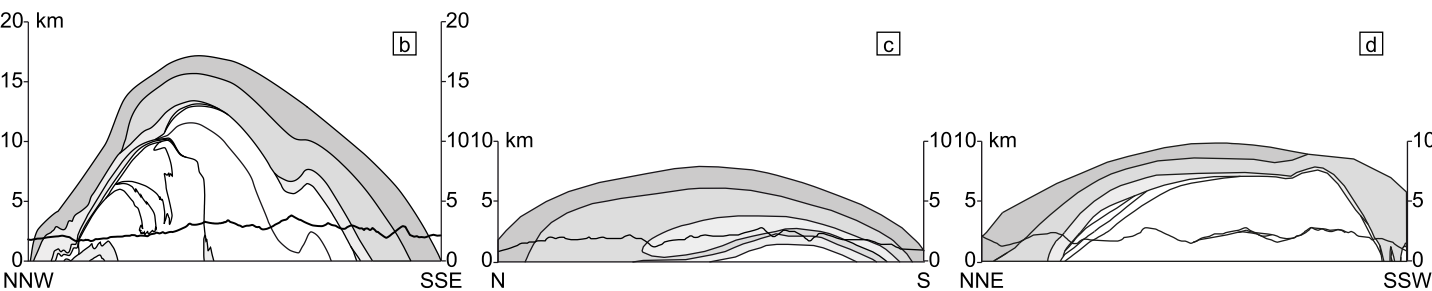
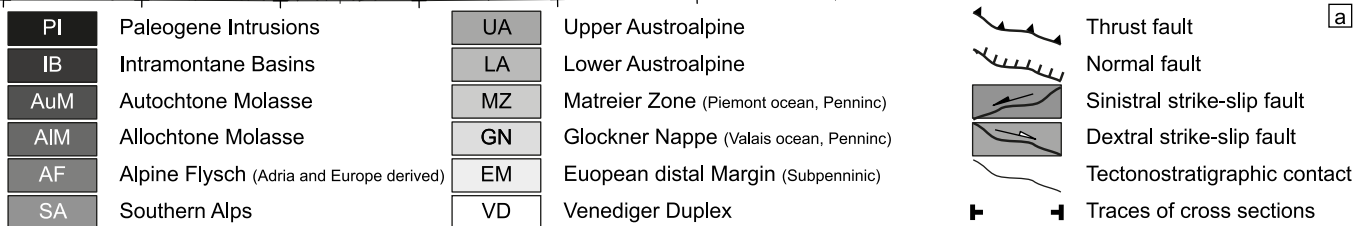
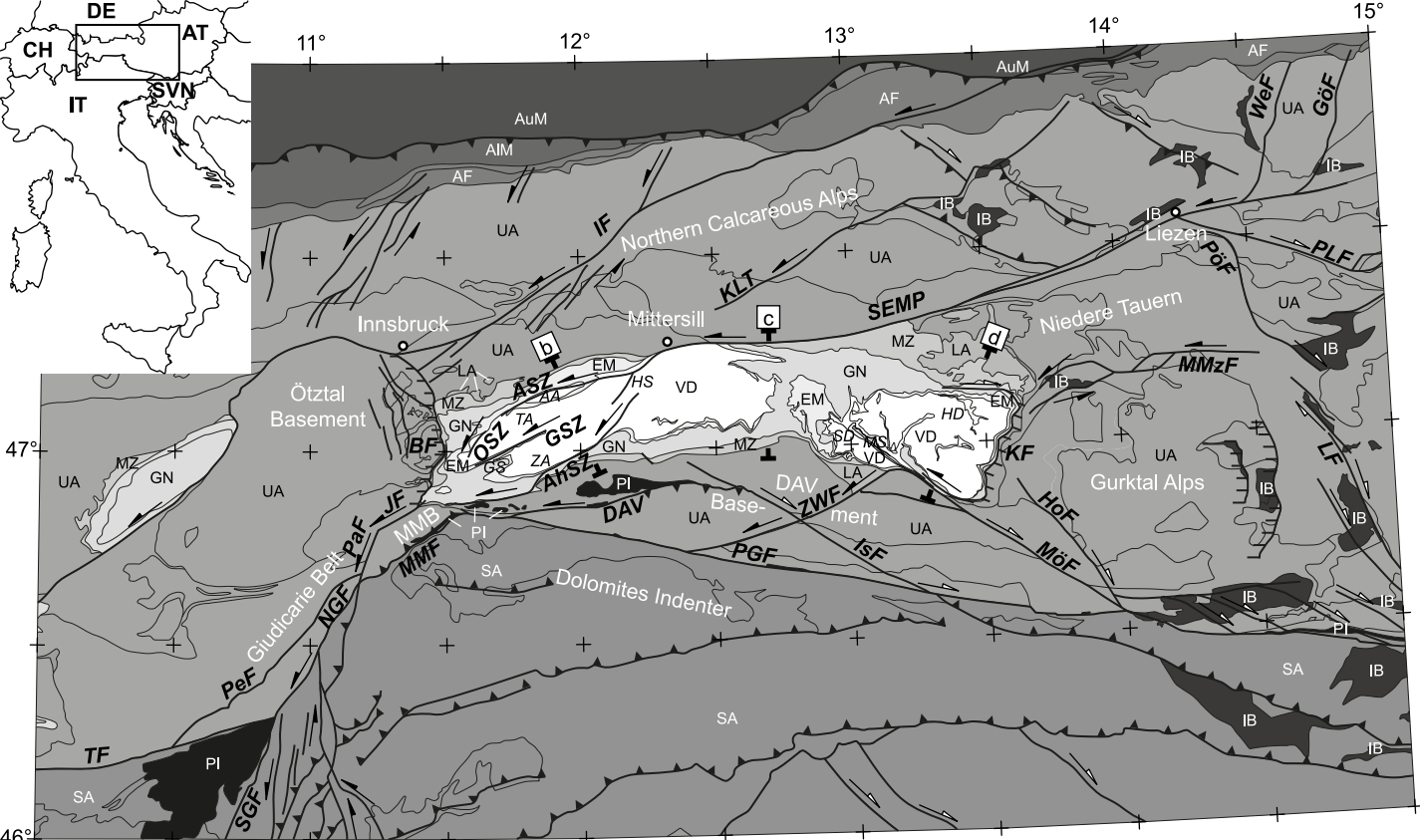
Domain A			Domain A			Domain C			Domain A		
324	59	S ₂	159	82	AP ₂	258	13	FA ₁	76	35	L ₂
330	72	S ₂	163	78	AP ₂	9	65	FA ₂	70	26	L ₂
334	65	S ₂	342	84	AP ₂	30	60	FA ₂	90	25	L ₂
345	64	S ₂	154	76	AP ₂	225	26	FA ₂	262	28	L ₂
351	60	S ₂	340	88	AP ₂	214	23	FA ₂	258	25	L ₂
306	87	S ₂	328	67	AP ₂	226	41	FA ₂	232	12	L ₂
127	67	S ₂	344	84	AP ₂	205	13	FA ₂	49	11	L ₂
332	70	S ₂	186	84	AP ₂	51	4	FA ₂	226	24	L ₂
339	76	S ₂	182	78	AP ₂	264	13	FA ₂	235	10	L ₂
322	83	S ₂	149	80	AP ₂	76	2	FA ₂	251	30	L ₂
323	90	S ₂	167	82	AP ₂	77	7	FA ₂	176	68	L ₂
320	90	S ₂	348	86	AP ₂	29	0	FA ₂	244	16	L ₂
153	84	S ₂	346	80	AP ₂	34	14	FA ₂	242	37	L ₂
151	78	S ₂	354	79	AP ₂	40	23	FA ₂	236	30	L ₂
328	72	S ₂	8	81	AP ₂	26	18	FA ₂	237	48	L ₂
324	78	S ₂	13	86	AP ₂	26	10	FA ₂	241	30	L ₂
328	75	S ₂	13	85	AP ₂	28	32	FA ₂	252	14	L ₂
311	81	S ₂	9	66	AP ₂	13	33	FA ₂	254	12	L ₂
127	53	S ₂	344	72	AP ₂	357	12	FA ₂	254	14	L ₂
129	62	S ₂	181	86	AP ₂	2	13	FA ₂	261	20	L ₂
147	75	S ₂	352	86	AP ₂	189	13	FA ₂	242	12	L ₂
144	82	S ₂	355	83	AP ₂	190	20	FA ₂	242	4	L ₂
155	61	S ₂	1	85	AP ₂	13	17	FA ₂	274	2	L ₂
153	61	S ₂	5	88	AP ₂	12	14	FA ₂	94	14	L ₂
316	87	S ₂	173	88	AP ₂	237	4	FA ₂	58	53	L ₂
134	85	S ₂	180	90	AP ₂	258	40	FA ₂	250	7	L ₂
316	87	S ₂	2	87	AP ₂	80	15	FA ₂	252	13	L ₂
134	85	S ₂	134	73	AP ₂	227	16	FA ₂	242	8	L ₂
126	69	S ₂	356	87	AP ₂	238	20	FA ₂	254	9	L ₂
127	69	S ₂	176	85	AP ₂	190	20	FA ₂	254	0	L ₂
133	80	S ₂	174	81	AP ₂	194	15	FA ₂	250	0	L ₂
135	62	S ₂	168	81	AP ₂	164	8	FA ₂	245	1	L ₂
132	58	S ₂	176	84	AP ₂	164	8	FA ₂	76	15	L ₂
149	77	S ₂	6	83	AP ₂	56	8	FA ₂	82	18	L ₂
150	80	S ₂	355	86	AP ₂	242	29	FA ₂	280	6	L ₂
324	75	S ₂	170	84	AP ₂	241	40	FA ₂	78	39	L ₂
332	75	S ₂	176	86	AP ₂	241	30	FA ₂	51	41	L ₂
314	79	S ₂	359	70	AP ₂	243	13	FA ₂	98	26	L ₂
313	84	S ₂	4	76	AP ₂	72	29	FA ₂	91	27	L ₂
154	88	S ₂	313	13	AP ₂	318	40	FA ₂	88	25	L ₂
335	67	S ₂				243	13	FA ₂	83	23	L ₂
338	75	S ₂				333	36	FA ₂	272	2	L ₂
329	69	S ₂				230	9	FA ₂	83	34	L ₂
176	67	S ₂				243	9	FA ₂	87	30	L ₂
321	87	S ₂				230	60	FA ₂	96	26	L ₂

Supporting Table 1: raw data of structural measurements

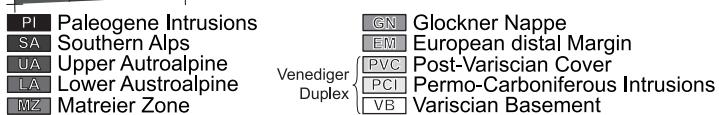
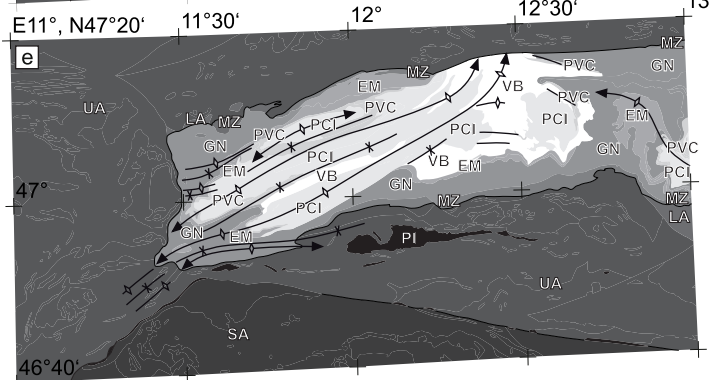
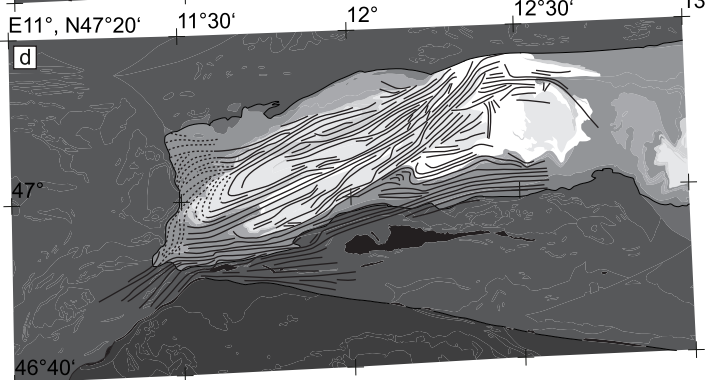
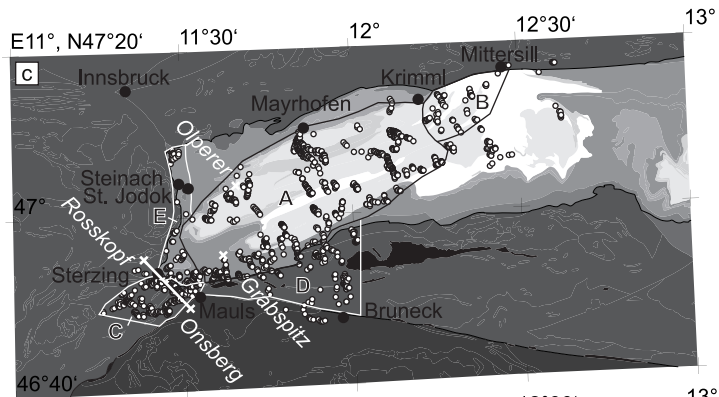
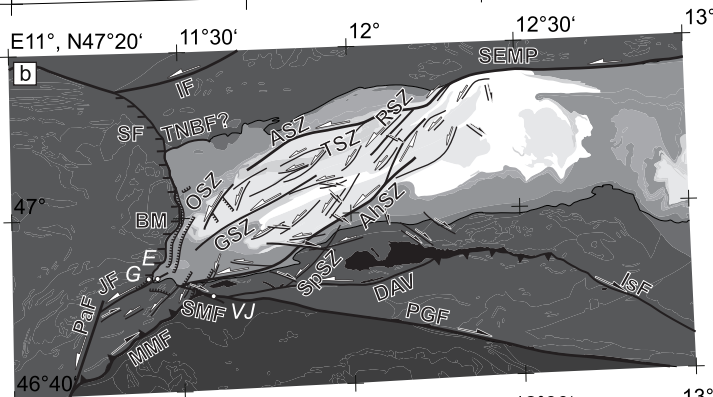
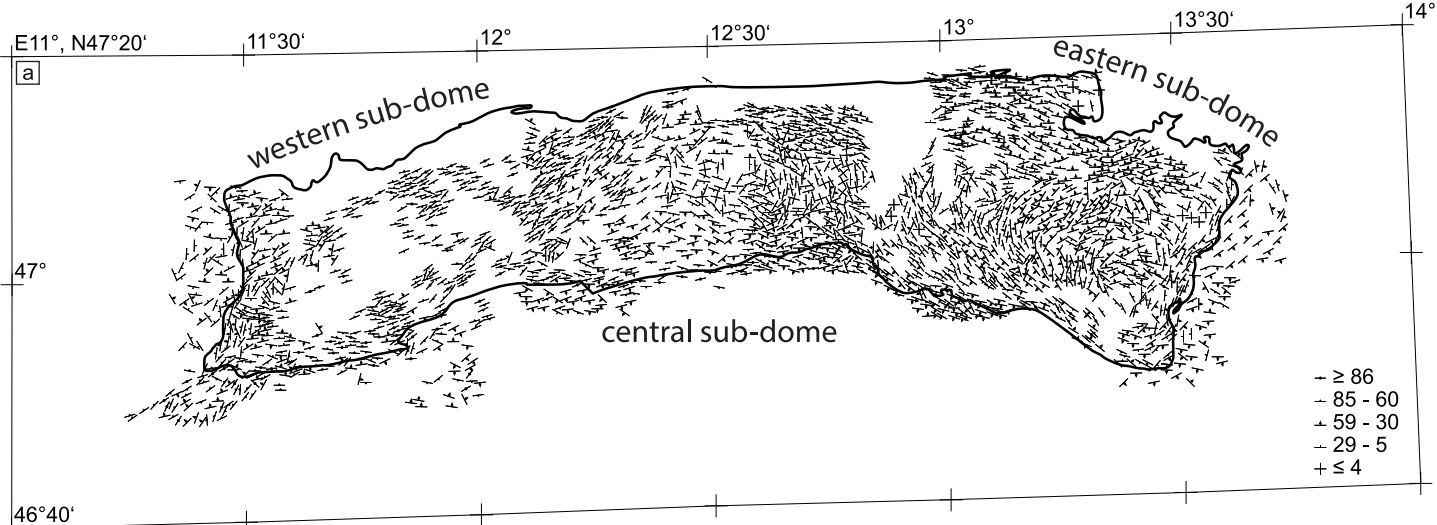
Domain A		
329	85	S ₂
300	57	S ₂
328	77	S ₂
328	85	S ₂
322	86	S ₂
316	84	S ₂
318	68	S ₂
324	73	S ₂
325	85	S ₂
328	89	S ₂
152	87	S ₂
306	81	S ₂
323	81	S ₂
166	78	S ₂
171	75	S ₂
346	80	S ₂
176	77	S ₂
160	73	S ₂
149	88	S ₂
148	87	S ₂
164	86	S ₂
191	78	S ₂
170	79	S ₂
178	76	S ₂
182	74	S ₂
185	72	S ₂
180	76	S ₂
191	72	S ₂
177	87	S ₂
346	86	S ₂
340	86	S ₂
318	70	S ₂
308	67	S ₂
292	65	S ₂
292	64	S ₂
279	65	S ₂
317	74	S ₂
348	84	S ₂
311	63	S ₂
319	58	S ₂
333	75	S ₂
330	68	S ₂
164	90	S ₂
338	77	S ₂
138	62	S ₂

Domain C		
240	45	FA ₂
225	18	FA ₂
240	14	FA ₂
293	42	FA ₂
339	28	FA ₂
351	20	FA ₂
329	5	FA ₂
346	21	FA ₂
77	34	FA ₂
269	68	FA ₂
267	60	FA ₂
295	14	FA ₂
101	8	FA ₂
290	53	FA ₂
101	43	FA ₂
238	30	FA ₂
47	17	FA ₂
194	8	FA ₂
194	59	FA ₂
197	27	FA ₂
237	21	FA ₂
122	18	FA ₂
124	23	FA ₂
19	12	FA ₂
13	26	FA ₂
20	4	FA ₂
19	28	FA ₂
8	31	FA ₂
47	14	FA ₂
59	18	FA ₂
35	25	FA ₂
57	4	FA ₂
126	2	FA ₂
248	7	FA ₂
11	24	FA ₂
90	71	FA ₃
129	74	FA ₃
87	70	FA ₃
86	85	FA ₃
120	75	FA ₃
93	78	FA ₃

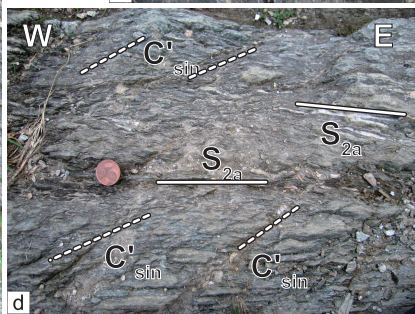
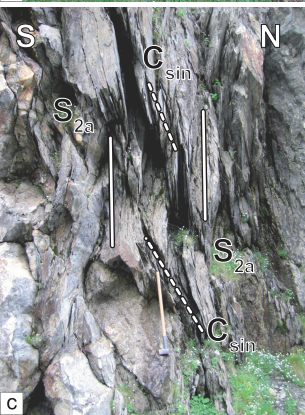
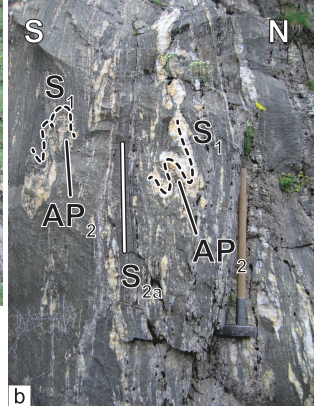
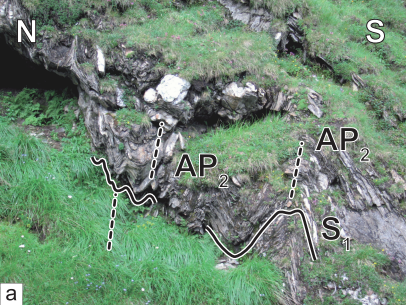
Domain A		
98	27	L ₂
92	35	L ₂
69	87	L ₂
94	25	L ₂
90	34	L ₂
94	24	L ₂
96	9	L ₂
101	14	L ₂
92	30	L ₂
87	14	L ₂
119	34	L ₂
81	24	L ₂
87	7	L ₂
94	35	L ₂
92	17	L ₂
92	35	L ₂
95	17	L ₂
94	41	L ₂
91	17	L ₂
92	26	L ₂
96	3	L ₂
112	29	L ₂
86	16	L ₂
86	26	L ₂
88	12	L ₂
87	12	L ₂
250	21	L ₂
251	21	L ₂
240	40	L ₂
234	35	L ₂
237	41	L ₂
243	38	L ₂
41	18	L ₂
40	11	L ₂
235	28	L ₂
234	35	L ₂
45	8	L ₂
90	47	L ₂
84	55	L ₂
82	40	L ₂
251	16	L ₂
88	65	L ₂
67	31	L ₂
68	29	L ₂
267	5	L ₂

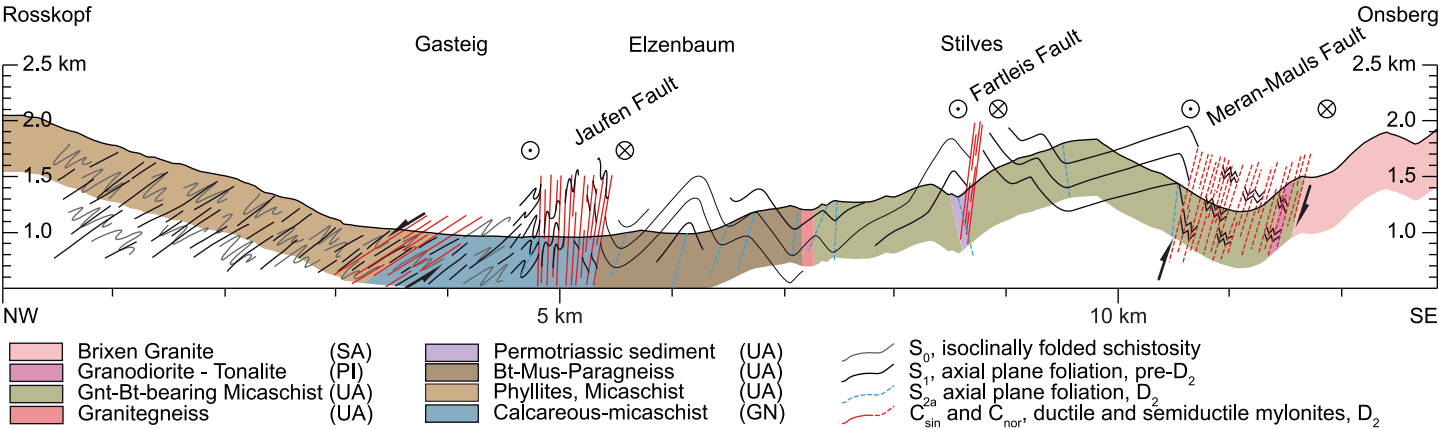


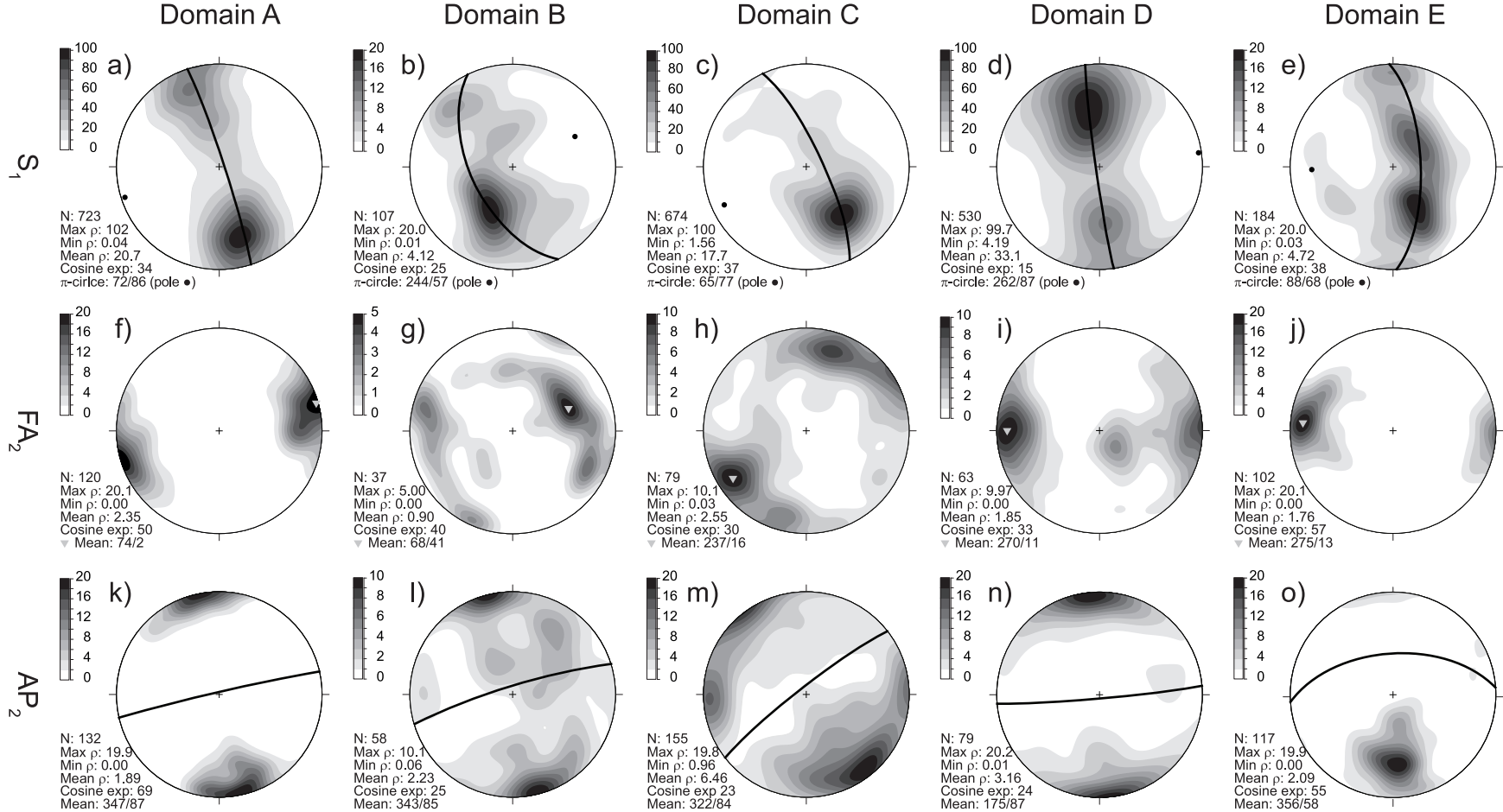
AhSZ: Ahnrtal Shear Zone, ASZ: Ahorn Shear Zone, BF: Brenner Fault, DAV: Deferegggen-Antholz-Vals Fault, GÖF: Görttschitztal Fault, GSZ: Greiner Shear Zone, HoF: Hochstuhl Fault, IF: Innental Fault, IS: Iseltal Fault, JF: Jaufen Fault, KLT: Königssee-Lammertal-Traunsee Fault, KF: Katschberg Fault, LF: Lavanttal Fault, MMB: Meran-Mauls Basement, MMF: Meran-Mauls Fault, MMZF: Mur-Mürz Fault, MÖF: Mölltal Fault, NGF: Northern Giudicarie Fault, OSZ: Olperer Shear Zone, PaF: Passeier Fault, PeF: Pejo Fault, PLF: Palten-Liesing-Fault, PöF: Pöls Fault, PGF: Pustertal-Gailtal Fault, SEMP: Salzach-Ennstal-Mariazell-Puchberg Fault, SGF: Southern Giudicarie Fault, TF: Tonale Fault, WeF: Wyer Fault, ZWF: Zwischenberge-Wöllentratzen Fault, AA: Ahorn Antiform, GS: Greiner Synform, HD: Hochalm Dome, HS: Habach Synform, MS: Mallnitz Synform, SD: Sonnblick Dome, TA: Tuxer Antiform, ZA: Zillertaler Antiform

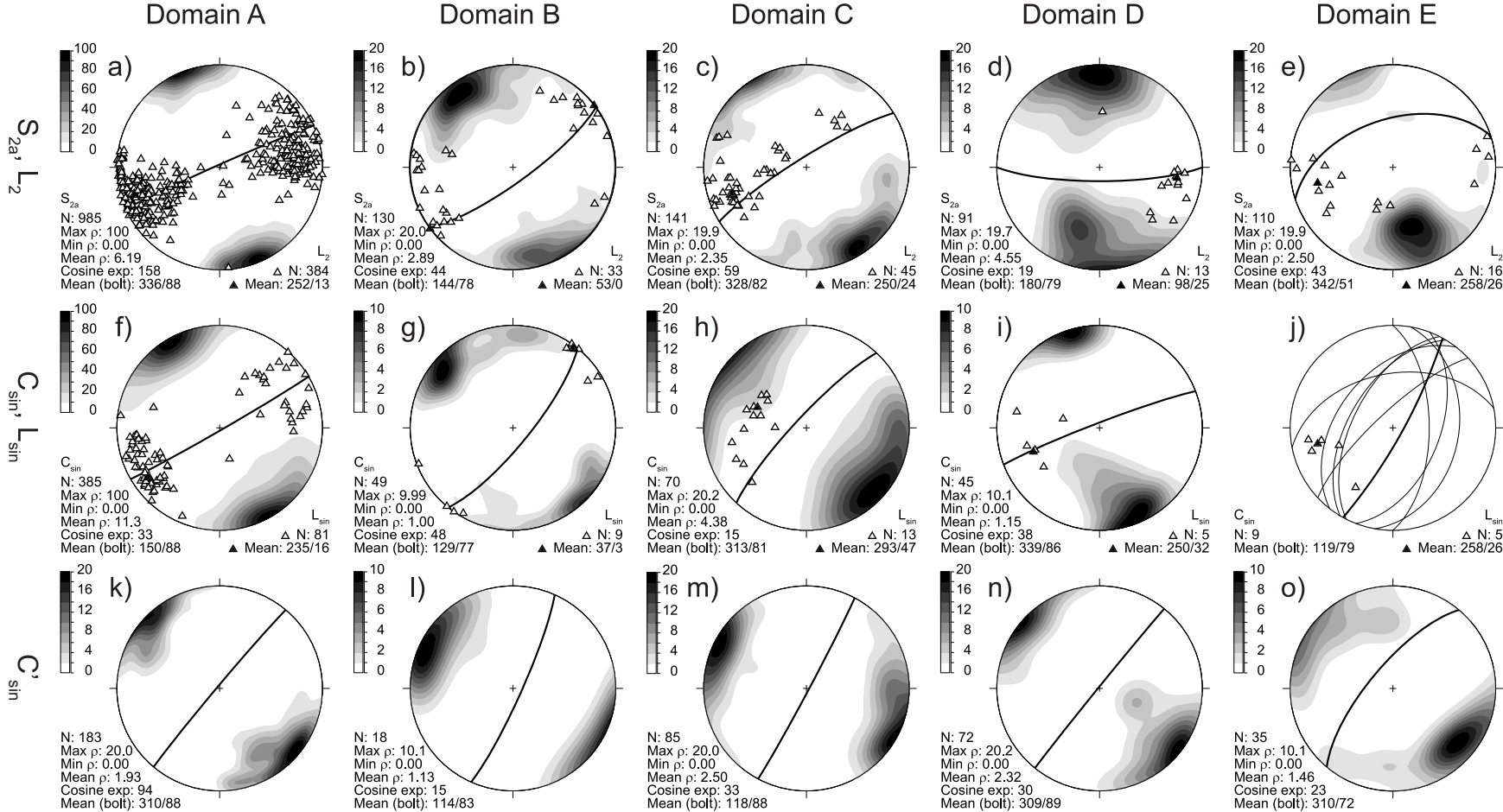


AHSZ: Ahrntal Shear Zone, ASZ: Ahorn Shear Zone, BM: Brenner Mylonites, DAV: Deferggen-Antholz-Vals Fault, E: Elzenbaum, G: Gasteig, GSZ: Greiner Shear Zone, IF: Innental Fault, IsF: Iseltal Fault, JF: Jaufen Fault, MMF: Meran-Maules Fault, OSZ: Olperer Shear Zone, PaF: Passeier Fault, PGF: Pustertal Fault, RSZ: Rinderkar Shear Zone, SEMP: Salzach-Ennstal-Puchberg-Mariazell Fault, SF: Silltal Fault, SMF: Sprechstein-Maules Fault, SpSZ: Speikboden Shear Zone, TNBF: Tauern Northern Boundary Fault, TSZ: Tuxer shear zones, VJ: Valler Jöchl

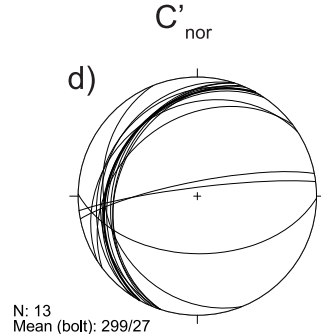
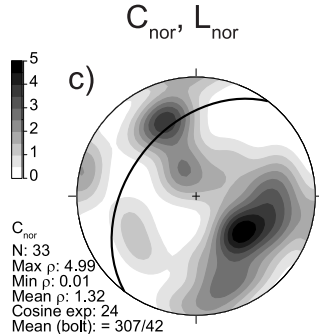
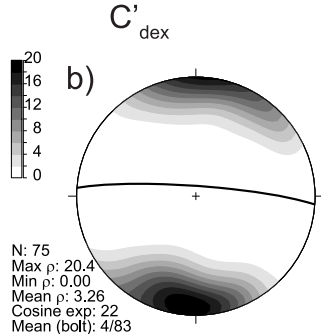
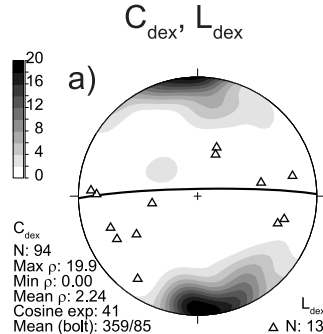




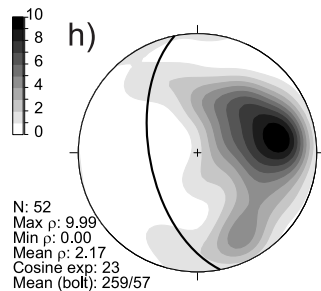
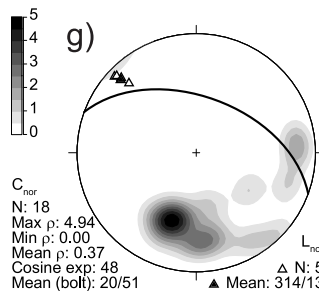
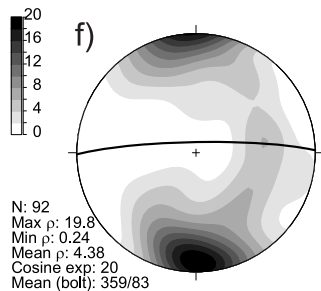
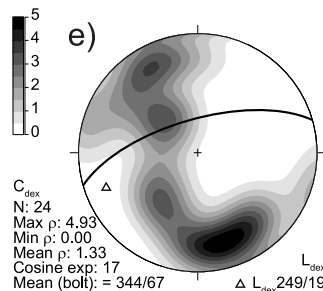




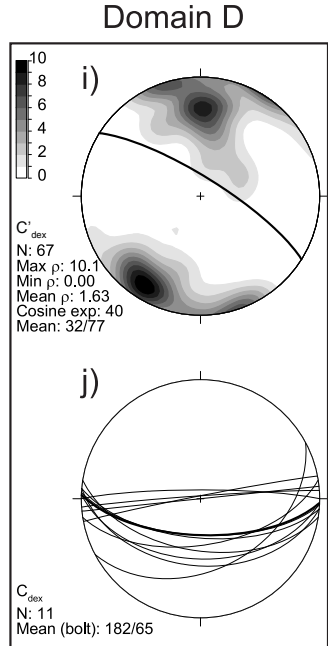
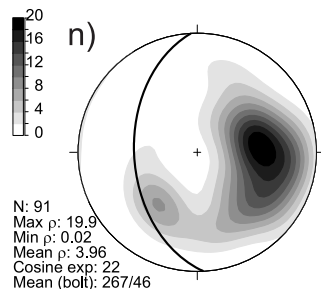
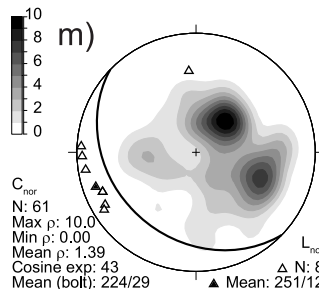
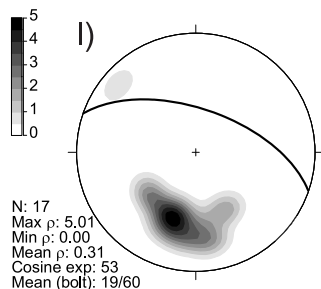
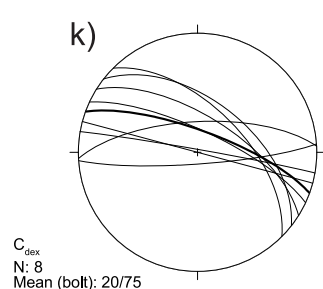
Domain A

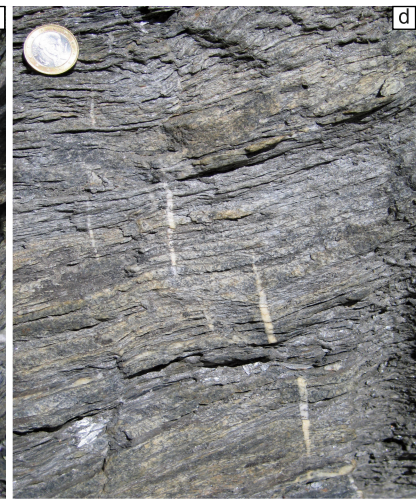
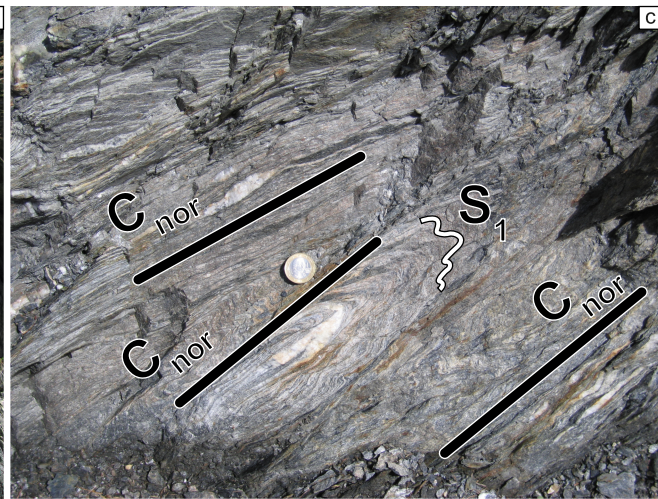
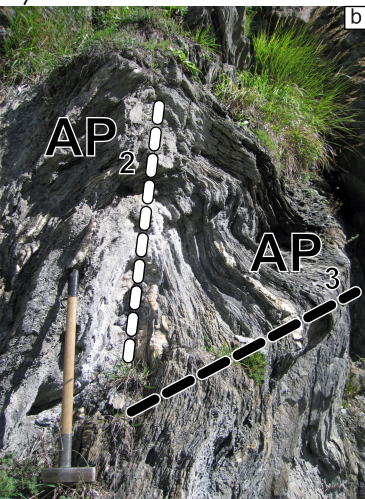
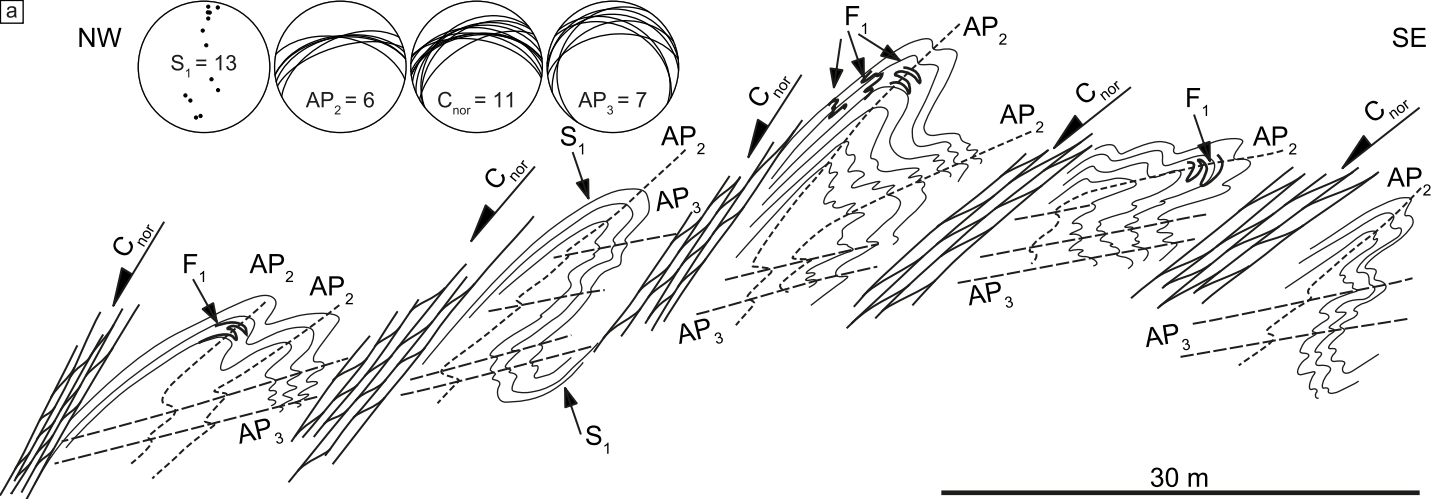


Domain C

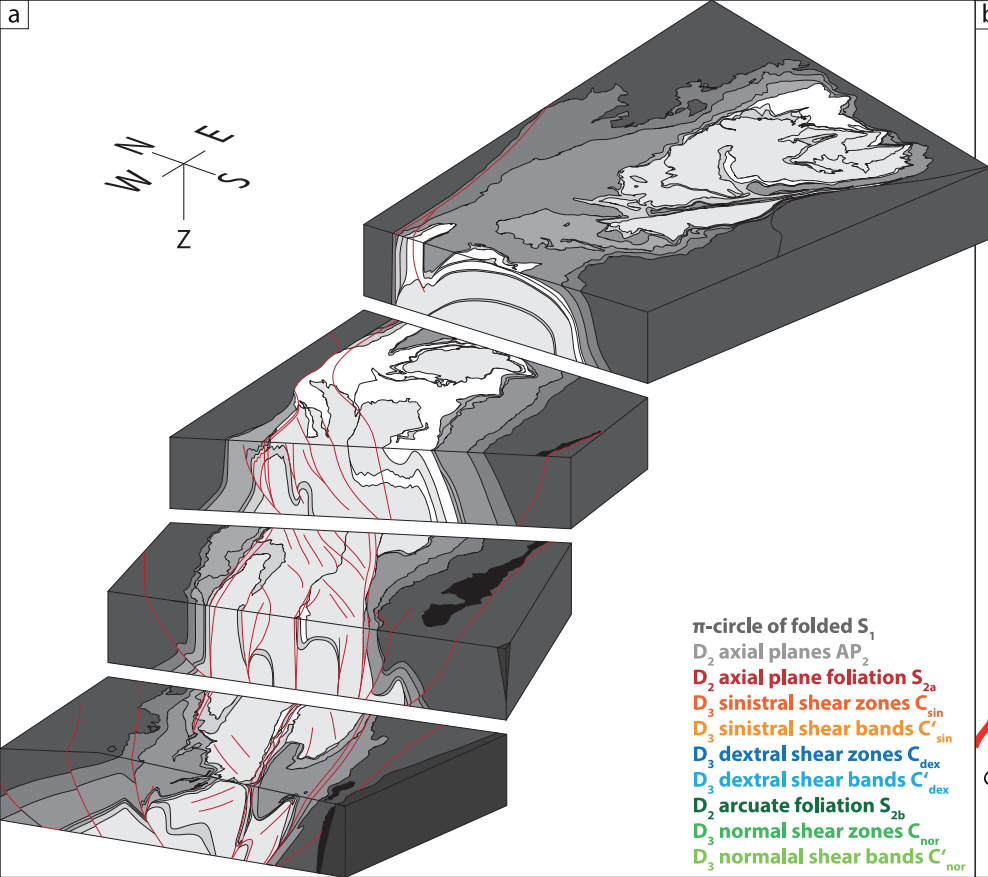


Domain E

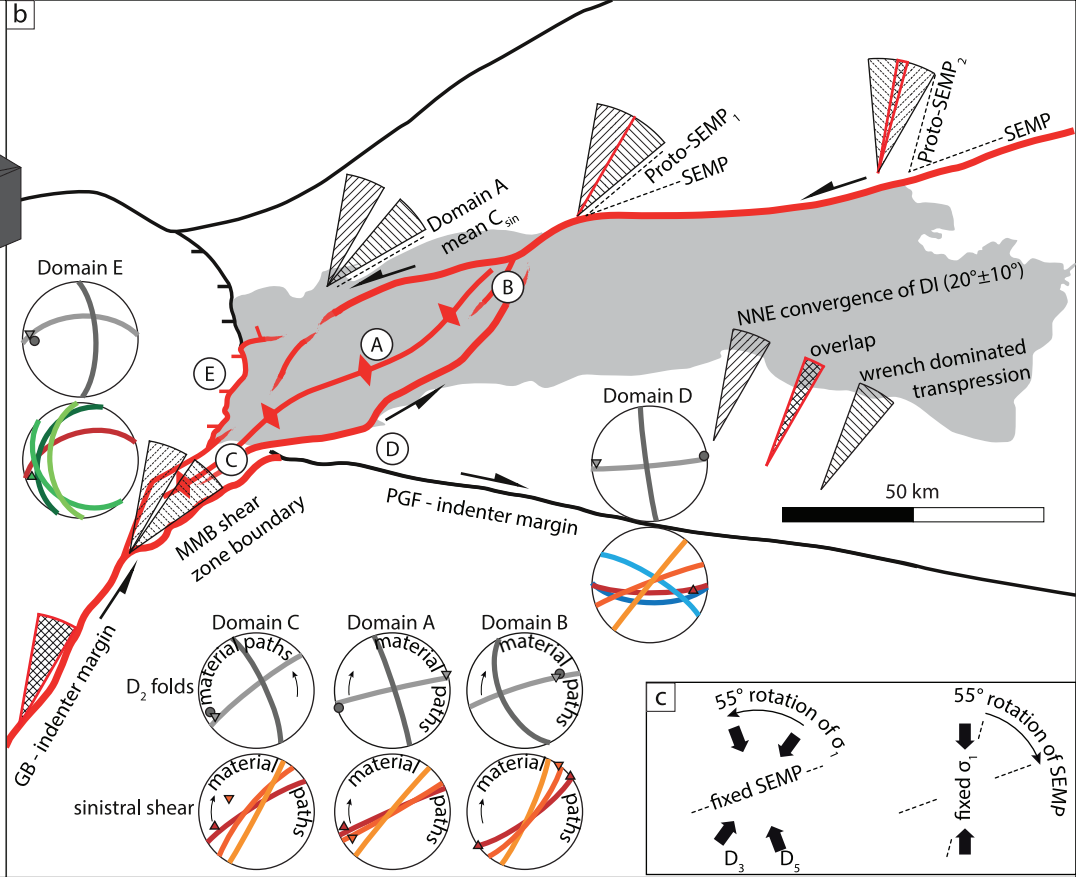




a



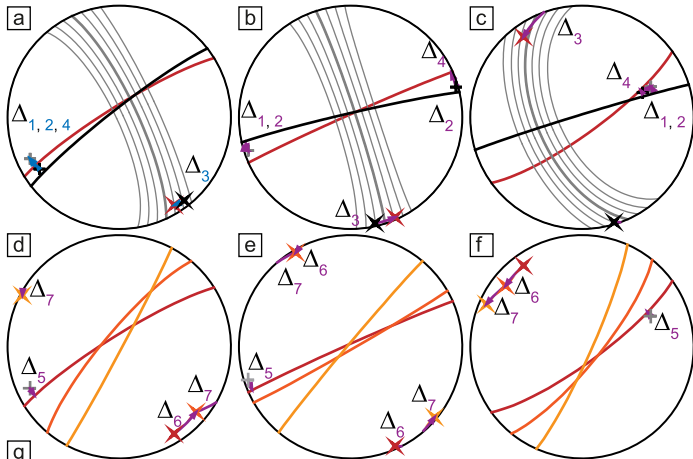
b



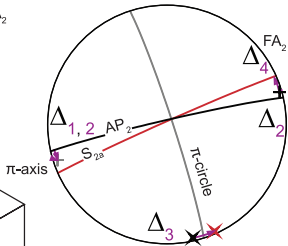
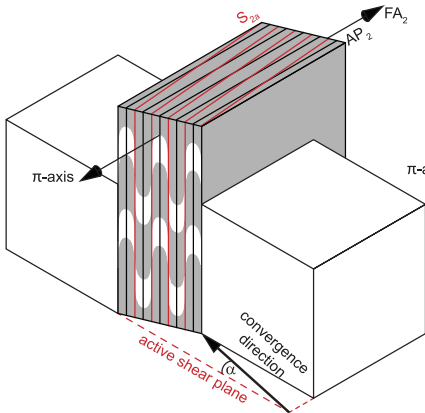
Domain C

Domain A

Domain B



Dihedral angles (in degree °)		Domain C	Domain A	Domain B
$\Delta_1 = (\text{AP}_2 - \pi\text{-axis})$	(/ , +)	11	-5	-5
$\Delta_2 = (\text{FA}_2 - \pi\text{-axis})$	(+ , +)	8	-6	-8
$\Delta_3 = (\text{AP}_2 - \text{S}_{2a})$	(✕ , ✕)	6	-11	-25
$\Delta_4 = (\text{FA}_2 - \text{S}_{2a})$	(+ , /)	3	-9	-3
$\Delta_5 = (\pi\text{-axis} - \text{S}_{2a})$	(+ , /)	-5	-6	-4
$\Delta_6 = (\text{S}_{2a} - \text{C}_{\sin})$	(✕ , ✕)	-18	-7	-15
$\Delta_7 = (\text{C}_{\sin} - \text{C}'_{\sin})$	(✕ , ✕)	-18	-20	-16



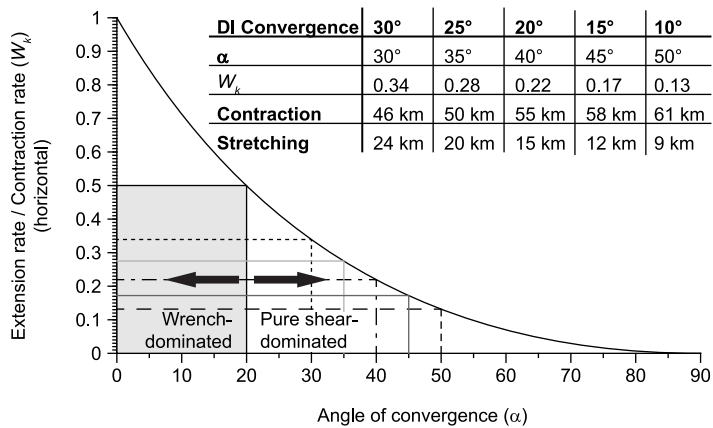
Dihedral angles (D_2 folding)

$$\Delta_1 = (AP_2 - \pi\text{-axis}) \quad (\nearrow, +)$$

$$\Delta_2 = (FA_2 - \pi\text{-axis}) \quad (+, +)$$

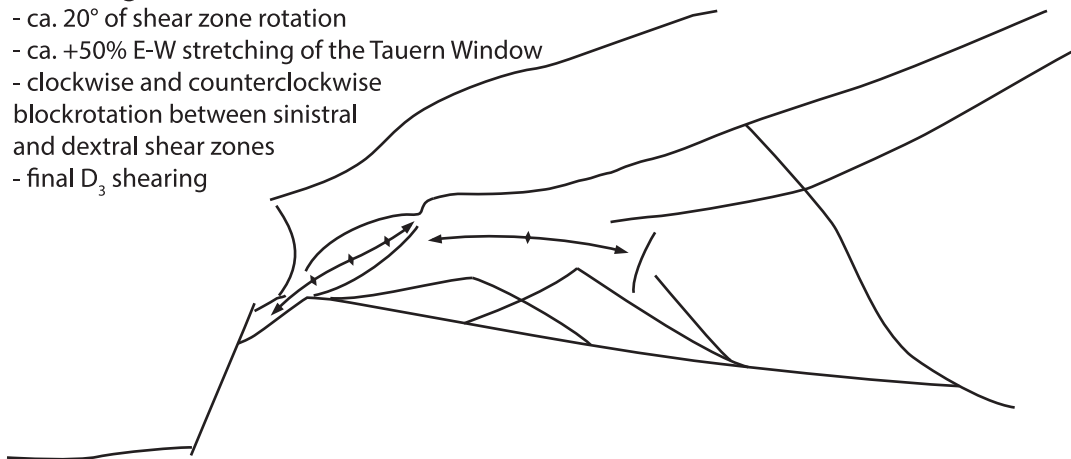
$$\Delta_3 = (AP_2 - S_{2a}) \quad (\times, \times)$$

$$\Delta_4 = (FA_2 - S_{2a}) \quad (+, \nearrow)$$



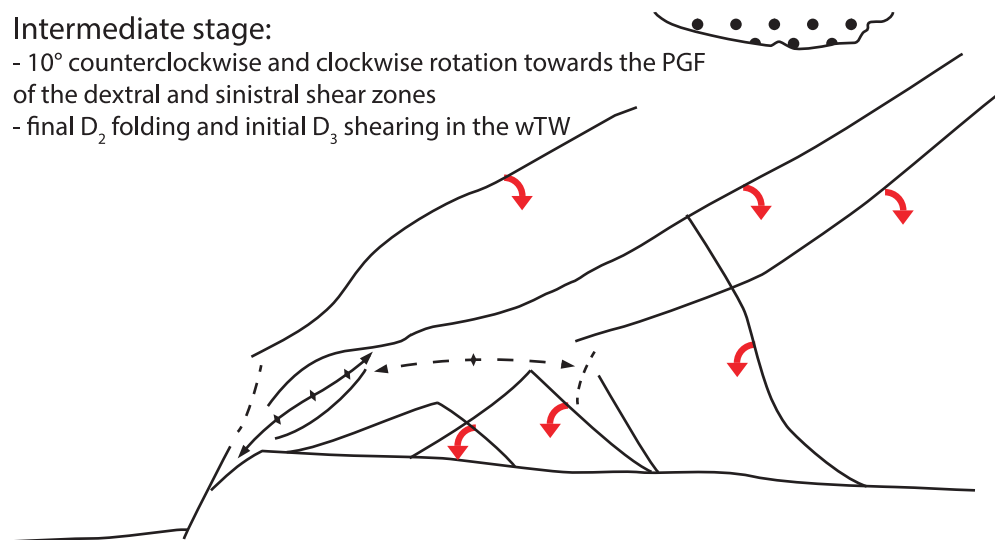
Final stage:

- ca. 20° of shear zone rotation
- ca. +50% E-W stretching of the Tauern Window
- clockwise and counterclockwise blockrotation between sinistral and dextral shear zones
- final D_3 shearing



Intermediate stage:

- 10° counterclockwise and clockwise rotation towards the PGF of the dextral and sinistral shear zones
- final D_2 folding and initial D_3 shearing in the wTW



Initial stage:

- N-S to NNE-SSW directed shortening
- angles between the conjugated shear zones are larger in the west than in the east
- initial D_2 folding in the western TW

