# Multivariable Integrated Evaluation of Hydrodynamic Modeling: A Comparison of Performance considering different Baseline Topography Data

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#### Abstract

Continental-scale river hydrodynamic modeling is useful for understanding the global hydrological cycle, and model evaluation is essential for robust calibration and assessing model performance. Although many models have been robustly evaluated using several variables separately, methods for the integrated multivariable evaluation of models have yet to be established. Here, we propose an evaluation method using the overall basin skill score (OSK), based on considering the spatial distribution of different variables via a sub-basin approach. The OSK approach integrates multiple variables to overcome observation-related limitations, such as the distinct temporal and spatial dimensions and unit of measurement unique to each variable, thus judging model performance objectively at the sub-basin and basin scales. As a case study, the global river model, CaMa-Flood, was evaluated using three variables discharge, water surface elevation, and flooded areadfor the Amazon Basin, focusing on the impact of using different types of baseline topography data (SRTM and MERIT digital elevation models [DEMs]). CaMa-Flood with the MERIT DEM performed robustly well over a wide range of river depth parameters with a maximum OSK of 0.51 against 0.46 for the SRTM DEM. Single-variable evaluation for all three variables proved inadequate due to low sensitivity for river bathymetry, with good performance outcomes potentially arising for the wrong reasons. This study confirmed that model evaluation using this method enables a balanced evaluation of different variables and a robust estimation of the best parameter set. The proposed method proved useful for flexible, integrated multivariable model evaluation, with modifications allowed per the user's requirements.

1	Multivariable Integrated Evaluation of Hydrodynamic Modeling: A
2	Comparison of Performance considering different Baseline
3	Topography Data
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8	Key Points:
9 10	• Integrated Multivariable Evaluation of Hydrodynamic Model using subbasin approach.
11 12	• Performance metric combining variables with distinct temporal and spatial dimensions and measurement units.
13 14 15	• Multivariable evaluation suggested MERIT DEM performs consistently better in hydrodynamic modelling
16	Abstract
17	Continental-scale river hydrodynamic modeling is useful for understanding the global
18	hydrological cycle, and model evaluation is essential for robust calibration and
19	assessing model performance. Although many models have been robustly evaluated
20	using several variables separately, methods for the integrated multivariable evaluation
21	of models have yet to be established. Here, we propose an evaluation method using the
22	overall basin skill score (OSK), based on considering the spatial distribution of different
23	variables via a sub-basin approach. The OSK approach integrates multiple variables to
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performance objectively at the sub-basin and basin scales. As a case study, the global 26 27 river model, CaMa-Flood, was evaluated using three variables-discharge, water surface elevation, and flooded area-for the Amazon Basin, focusing on the impact of 28 using different types of baseline topography data (SRTM and MERIT digital elevation 29 models [DEMs]). CaMa-Flood with the MERIT DEM performed robustly well over a 30 wide range of river depth parameters with a maximum OSK of 0.51 against 0.46 for the 31 SRTM DEM. Single-variable evaluation for all three variables proved inadequate due to 32 low sensitivity for river bathymetry, with good performance outcomes potentially 33 arising for the wrong reasons. This study confirmed that model evaluation using this 34 method enables a balanced evaluation of different variables and a robust estimation of 35 the best parameter set. The proposed method proved useful for flexible, integrated 36 multivariable model evaluation, with modifications allowed per the user's requirements. 37

38

## Plain Language Summary

The hydrodynamic model is an import tool to understand the many natural phenomena 39 related to the water cycle. Its accuracy depends on the many input data, like runoff and 40 41 topography. Accurate representation of the natural system using the hydrodynamic model can be judged based on the models' performance. The model's performance 42 43 depends on the accurate estimation of variables and judged based on the evaluation 44 metric's score. Earlier, many studies focused on either a single variable or multiple 45 variables considering separately for model evaluation. Here we proposed a method, integrating multiple variables by combining each variable's performance into a single 46 47 overall basin skill score for comparing two topography data. The proposed method is the first of its kind, integrating variables with different temporal and spatial dimensions 48

and measurement units for performance evaluation. The method has a significant
advantage of combining different variables for robust evaluation.

51

#### 52 **1** Introduction

53 Continental-scale river hydrodynamic modeling is essential for understanding the 54 global hydrological cycle and supporting flood monitoring as well as water resource management with regard to water security and natural hazards (Siqueira et al., 2018). 55 Hydrodynamic modeling processes depend on topographic data to replicate 56 57 characteristics and processes within a landscape (Callow et al., 2007; Jarihani et al., 2015). Data from a digital elevation model (DEM) representing topography comprise 58 one of the critical datasets required in many types of studies, such as those of runoff 59 generation, lake water storage changes, river routing, and flood inundation modeling 60 (Hawker, Bates, et al., 2018; Jung & Jasinski, 2015; Sampson et al., 2016; Yamazaki et 61 62 al., 2014, 2017). DEMs provide key data that govern the accuracy of hydrological and hydrodynamic models (Bates et al., 1998; Bates et al., 2005; Baugh et al., 2013; Jarihani 63 et al., 2015; Sanders, 2007). Highly accurate DEMs are needed for the better 64 65 representation of river hydrodynamics and flood modeling.

Many regions of the world rely on spaceborne DEMs due to the lack of availability of highly accurate airborne DEMs. Advances in remote-sensing techniques helped with achieving more accurate spaceborne DEMs (Yamazaki et al., 2017). The Shuttle Radar Topography Mission (SRTM) DEM and Advance Spaceborne Thermal Emission and Reflection Radiometer Global DEM, which provide data covering the whole world, are examples of DEMs developed due to improvements in remote-sensing techniques (Jung

72	& Jasinski, 2015; Yamazaki et al., 2017). Spaceborne DEMs contain various non-
73	negligible errors affecting vertical accuracy. Efforts have been made to correct these
74	errors, such as the steps taken in producing the Multi-Error-Removed Improved-Terrain
75	(MERIT) DEM (Yamazaki et al., 2017) and TanDEM-X 90 DEM (Rizzoli et al., 2017).
76	The MERIT DEM is a highly accurate spaceborne DEM that removes major error
77	components from existing DEMs. It was developed by removing the absolute bias,
78	stripe noise, speckle noise, and tree height bias using multiple satellite datasets and
79	filtering techniques (Yamazaki et al., 2017).
80	Many studies have demonstrated the advantages of the MERIT DEM over the SRTM
80	Many studies have demonstrated the advantages of the MERT DEM over the SKTM
81	and other DEMs (Hawker, Bates, et al., 2018; Hawker, Rougier, et al., 2018; Hawker et
82	al., 2019; Liu et al., 2019; Yamazaki et al., 2017). The comparisons were mostly
83	restricted to vertical accuracy or spatial error assessment using reference altimetry data.
84	There has been little research on evaluating the MERIT DEM using river hydrodynamic
85	model simulations. A few studies have examined the effects of DEMs, including
86	MERIT, in flood inundation modeling (Archer et al., 2018; Hawker, Bates, et al., 2018;
87	Hawker, Rougier, et al., 2018), but the evaluations were limited to flood extent or the
88	water surface elevation (WSE). The hydrodynamic performance can be affected by
89	uncertainty in the runoff or other model parameters, such as Manning's coefficient, river
90	channel bathymetry, and channel width. In accordance with the theory of equifinality,
91	models based on many parameter sets can perform acceptably well, but they "might be
92	right for the wrong reasons" (Beven, 2006; Kirchner, 2006). The acceptable
93	performance of a hydrodynamic model is more likely for single-variable rather than
94	multivariable evaluation. In addition, evaluation based on fewer variables makes it
95	difficult to trace errors (García-Díez et al., 2015). There are many possible solutions to

96 improve the process representation and reduce uncertainty in model predictions (Meyer
97 Oliveira et al., 2021). One of the easiest and most efficient solutions is the use of a
98 complementary dataset to evaluate the model. Insight regarding the performance of
99 different DEMs from considering multiple uncertainties while using river hydrodynamic
100 models can help to reduce the errors for better prediction of flood events.

101 The robustness and proper representation of the natural system can be confirmed by 102 evaluating the model across various simulated hydrological variables (Stisen et al., 103 2018). The availability of remote-sensing data with fair temporal and spatial resolution 104 is advantageous for hydrodynamic model evaluation using multiple variables. Many studies (Meyer Oliveira et al., 2021; Paiva et al., 2013; Patro et al., 2009) performed 105 robust evaluation of hydrological-hydrodynamic and hydrodynamic models using 106 multiple variables. The techniques involved the use of many possible objective 107 108 functions, including the root mean square error (RMSE), Nash-Sutcliffe efficiency coefficient (NSE), and coefficient of determination ( $\mathbb{R}^2$ ). The use of multiple objective 109 functions makes the evaluation cumbersome, and it is difficult to describe the overall 110 111 combined performance due to all variables. Selection of the best model parameters using these techniques is complex, making objective model evaluation difficult. The 112 integration of these metrics for evaluating river hydrodynamic models is impossible due 113 to different measurement units and ranges. For example, the NSE is unitless and ranges 114 from  $-\infty$  to 1, whereas the RMSE has the same unit as the variable of interest and 115 ranges from 0 to  $\infty$ . In addition, the spatial dimension and measurement units of 116 observed variables, such as discharge (Q), Water Surface Elevation (WSE), and flood 117 118 extent, vary. Q and WSE are recorded as point observations with measurement units of  $m^{3}$ /s and m, respectively, whereas flood extent involves two-dimensional observations 119

120	with a measurement unit of $m^2$ . A methodology for evaluating river hydrodynamic
121	models that includes integrating various observations with different temporal and spatial
122	dimensions has not been established.

123 This study proposes an integrated multivariable evaluation of river hydrodynamic 124 models for subjective assessment. The proposed multivariable integrated evaluation 125 technique was applied for catchment-based macro-scale floodplain (CaMa-Flood) river hydrodynamic model (Yamazaki et al., 2011) simulations considering two different 126 127 DEMs, the MERIT DEM and SRTM DEM, as a case study. The evaluation was performed using a range of parameters to cover the various possible uncertainties and 128 errors. An integrated metric approach considering observations of multiple variables (Q, 129 WSE, and flooded area) at the sub-basin scale was adopted. The overall basin skill score 130 (OSK) was calculated using the sub-basin skill score to represent the performance of 131 132 CaMa-Flood with the two DEMs. The OSK helps to rank the simulations to compare the best set of parameters for the CaMa-Flood river hydrodynamic model considering 133 multiple variables. The proposed evaluation technique will help with determining the 134 135 improvement in predictions of river hydrodynamics by a representative model due to improvement of a DEM, e.g., the MERIT DEM. 136

137 2 Methodology and Data Description

138 2.1 Study Framework

139 Simulations with a global river hydrodynamic model, CaMa-Flood, at a resolution of

- $140 \quad 0.1^{\circ}$  (~10 km at the equator) were performed using the SRTM DEM and MERIT DEM,
- 141 and model performance for multiple variables was evaluated. The framework of the
- 142 study is presented in Error! Reference source not found.. The CaMa-Flood model (see

143 Section 2.3) used runoff forcing data (see Section 2.5) as the input for the simulations. Simulations were performed using two different DEMs, the SRTM DEM and MERIT 144 145 DEM (see Section 2.4), for various parameters (see Section 2.7), and uncertainties were included. The sub-basin approach was adopted for skill score computation using three 146 different variables. Q, WSE, and the flooded area (FA) (see Section 2.6) were taken as 147 observations for each sub-basin for metric computation (see Section 2.8). The overall 148 model performance was evaluated based on the OSK, which was calculated by 149 150 averaging the sub-basin skill scores for a DEM that were estimated for a parameter using an evaluation metric. The best parameter set, as assessed by comparing the OSK, 151 was used to compare the model performance of CaMa-Flood between the SRTM and 152 153 MERIT DEMs (see Section 3). The integrated multivariable evaluation technique was 154 applied to Amazon River Basin data to compare the performance of the CaMa-Flood river hydrodynamic model with two different DEMs. The average normalized NSE 155 156 (NNSE) value was calculated for Q, WSE, and FA observations for each sub-basin, considering mainstream observations for Q and WSE and a 50-km buffer around the 157 main stream for FA. The OSK was calculated by averaging the sub-basin skill scores, 158 representing the performance of CaMa-Flood for a given DEM and river depth 159 160 parameter.



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Figure 1: Study framework showing the flowchart of calculation of the OSK from sub-basin skill scores calculated using the NNSE values associated with Q, WSE, and FA.

164 **2.2 Study Area** 

The Amazon Basin (Figure 4**Error! Reference source not found.**) was selected as the study region to evaluate the MERIT and SRTM DEMs using CaMa-Flood. The Amazon Basin has the largest drainage basin in the world, covering an area of approximately  $7,050,000 \text{ km}^2$ , with the largest river discharge (annual average of 200,000 m<sup>3</sup>/s at the river mouth), and accounts for 20% (one-fifth) of the total runoff discharge into the world's oceans (Richey et al., 1989).

cause backwater effects to control part of the river (Meade et al., 1991; Paiva et al., 172 173 2013). The vast floodplains along the Amazon main stem significantly impact the hydrodynamics of the middle and lower reaches. Seasonally flooded areas are found on 174 the Amazon plains (Hess et al., 2003; Papa et al., 2010). The main river channel 175 exchanges a 5%–30% annual discharge with the surrounding areas (Alsdorf et al., 2010; 176 Richey et al., 1989). These characteristics make the Amazon Basin a good case study 177 178 for hydrodynamic model evaluation. Quantification of hydrological model events for a large basin is often difficult due to a 179 180 lack of adequate data (Chen et al., 2010). However, large numbers of observations are 181 available for the Amazon region. Many *in situ* gauges are installed along the main stem and major tributaries (Yamazaki et al., 2012), and satellite observation data are useful 182 for monitoring large-scale floods and droughts (Chen et al., 2010). 183

The Amazon region is characterized by complex river hydraulics. The low river slopes

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## 2.3 Hydrodynamic Model

185 In this study, we used CaMa-Flood (Yamazaki et al., 2011, 2012, 2013), which is a river routing model with a global distribution. It uses the one-dimensional St. Venant local 186 inertial equation (Bates et al., 2010), making simulations of continental-scale river 187 hydrodynamics computationally efficient. The model simulates river and floodplain 188 hydrodynamics (e.g., river Q, WSE, inundated area, and surface water storage) by 189 routing the input runoff generated by a land surface model to a predefined river network 190 191 map. The river networks and sub-grid parameters were created by applying the FLOW upscaling method (Yamazaki et al., 2009) at 0.1° (~10 km) resolution, using a flow 192 direction map and DEMs. The SRTM DEM combined with HydroSHEDS (Lehner et al., 193

2008) flow directions and MERIT Hydro (Yamazaki et al., 2019) combined with a 194 hydrologically adjusted version of the MERIT DEM were used as input to apply the 195 196 FLOW upscaling method. River networks were discretized into unit catchments with sub-grid topographic parameters for river channels and floodplains. The water balance 197 equation determines the water storage in each catchment as a prognostic variable, where 198 the catchment is delineated by a DEM. The local inertial equation is used to calculate 199 river Q, whereas the water level and FA are identified using water storage levels in each 200 201 unit catchment based on sub-grid topographic information.

202 **2.4 D** 

## **Digital Elevation Models**

203 The DEM is one of the most important inputs for physical-based models. In this study,

the SRTM and MERIT DEMs were compared using a river hydrodynamic model.

SRTM is an international research effort in which DEMs are obtained on a near-global

scale from 56°S to 60°N to generate the most complete high-resolution digital

topographic database of the Earth. The SRTM DEM (Farr et al., 2007) uses synthetic

208 aperture radar interferometry data to produce the highest resolution digital topographic

map of the Earth. It has a resolution of 1 arc-second (i.e., 30 m at the equator) with 15 m
of vertical accuracy.

The MERIT DEM (Yamazaki et al., 2017) is a highly accurate global DEM with a 3 arc-second resolution (~90 m). The SRTM3 DEM (Farr et al., 2007) and AW3D-30 m DEM (Tadono et al., 2015) were used as baseline DEMs to produce the MERIT DEM after the removal of multiple error components (absolute bias, stripe noise, speckle noise, and tree height bias) from existing spaceborne DEMs. Improved DEMs (without biases and errors) can represent the altitude and slope more accurately, as illustrated in

217	Figure 2(b) and (c). For a river channel delineated using a DEM, any error in altitude in
218	the DEM will directly affect the channel depth; hence, accurate WSE values may not be
219	obtained even if Q can be estimated correctly. As shown in Figure 2, a biased DEM
220	cannot provide accurate results, even if Q values are correct, and the WSE data will be
221	affected due to errors in elevation and slope or vice versa. The MERIT DEM is
222	expected to analyze multiple variables simultaneously in an improved manner, thus
223	enhancing the overall performance of the river hydrodynamic model.



(a) Top view of the River Channel with Flood Plain

(b) River Channel with Flood Plain (True State and Biased DEM)



(c) River Channel with Flood Plain (True State and Unbiased DEM)



Figure 2: Biased and corrected DEM showing the effects of trees bias on Q, WSE, and

FA estimations.

## 227 2.5 Runoff Forcing Data

- 228 CaMa-Flood uses runoff as an input for simulations. We used eartH2Observe (Dutra et
- al., 2017) runoff data produced by the land surface hydrological model Hydrology Tiled
- 230 ECMWF Scheme for Surface Exchanges over Land (HTESSEL) forced with the

WATCH Forcing Data methodology applied to ERA-Interim dataset (WFDEI; Weedon
et al., 2014) on weather boundary conditions (Balsamo et al., 2009). The combination of
HTESSEL runoff data and CaMa-Flood produced better results (Zhou et al., 2020). The
runoff data resolution is 0.25°, distributed to each unit catchment according to the areal
proportion of the unit catchment in the corresponding grid.

#### 236 2.6 Observation Data

## 237 **2.6.1 Discharge**

Daily Q data for the observation locations shown in Figure 4 were used to evaluate the
Q simulations. The Brazilian Agency for Water Resources (ANA), Peruvian and
Bolivian National Meteorology and Hydrology Services (Servicio Nacional de
Meteorología e Hidrología), and Hydrology, Biogeochemistry and Geodynamic of the
Amazon Basin (HYBAM) program (http://www.ore-hybam.org) provided daily-scale
data for the 1999–2009 period. The data for 2001–2009 were considered for integrated
multivariable evaluation.

#### 245 **2.6.2 Water Surface Elevation**

ENVISAT satellite altimetry data (Santos da Silva et al., 2010, <u>http://hydroweb.theia-</u> <u>land.fr/</u>) were used to evaluate the WSE. The ENVISAT satellite has a 35-day repeat orbit and an intertrack distance of 80 km. Data from 2002 to 2010 were used for metric calculation. The ENVISAT altimetry data referenced EGM 2008. Preprocessing was performed using the program provided by the National Geospatial-Intelligence Agency (http://earth-info.nga.mil) to convert the data to EGM96 geoid format. The processed EGM96 geoid-referenced data were compared with the CaMa-Flood simulations.

#### 253 **2.6.3 Flood Extent**

254 A multi-satellite monthly global inundation extent dataset with a spatial resolution of approximately 25 km × 25 km, available from 1993 to 2004 (Papa et al., 2010), was 255 used for flood extent comparison. These data were derived from multiple satellite 256 observations comprising passive (Special Sensor Microwave Imager) and active (ERS 257 scatterometer) microwaves along with visible and near-infrared imagery (Advanced 258 Very High-resolution Radiometer). Multi-satellite data can capture inundation under the 259 vegetation canopy and were therefore used to evaluate CaMa-Flood simulations of the 260 Amazon Basin. Data were provided for an equal-area grid of  $0.25^{\circ} \times 0.25^{\circ}$  at the 261 equator, where each pixel has a surface area of 773  $\text{km}^2$ . They were converted into the 262 Cartesian coordinate system for comparison with CaMa-Flood simulations. The data 263 with the modified coordinate system were downscaled from  $0.25^{\circ}$  (~25 km) to  $0.05^{\circ}$  (~5 264 km) by dividing the values equally over 25 pixels. Later, they were upscaled from  $0.05^{\circ}$ 265 (~5 km) to  $0.1^{\circ}$  (~10 km) by summing the values over 2 × 2 pixels. The final  $0.1^{\circ}$ 266 downscaled observation data were used for comparison with the CaMa-Flood 267 simulations. 268

## 269 2.7 Model Parameterization

River hydrodynamic models have many sources of uncertainty. These model
uncertainties were taken into consideration in the model evaluation by assessing a range
of parameters. The CaMa-Flood model has three river channel parameters: channel
width, channel depth, and Manning's roughness coefficient. A constant value of 0.03 is
given as Manning's coefficient in the model. Channel width was derived using satellite

data (Yamazaki et al., 2014), whereas river depth was estimated using the power law
equation as follows:

$$H = aQ^b \tag{1}$$

278 Where *H* is the river depth, *Q* is annual average discharge, *a* is coefficient *b* exponent 279 of the power law given by constant value

280 River depth is the most uncertain of the three parameters as the uncertainty in the Manning's coefficient is small, with the usual range for rivers lying between 0.02 and 281 0.04 (Brêda et al., 2019; Chow, 1959), whereas an empirical equation is used to 282 calculate depth. Depth is perturbed to obtain a range of parameters for each simulation 283 to encompass the model's uncertainties. There are many possible ways to change river 284 285 depth by changing the value of the constant in the power law equation. Here, the river depth was varied by varying the depth at the river mouth and changing the gradient 286 across the basin, as illustrated in Figure 3. The exponent "b" varied from 0.35 to 0.85 287 with an interval of 0.05 and the coefficient "a" of the power law equation to achieve a 288 fixed depth value at the river mouth. 289



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Figure 3: River depth vs. Q plot representing the power law equation ( $H = aQ^b$ ). Lines were drawn considering the depth at the river mouth (the same color represents the same depth at the river mouth), and the gradient along the river was changed by adjusting the range of exponent "b" and coefficient "a" accordingly.

295 2.8 Sub-basin Skill Evaluation

The three variables used in the model evaluation study were Q, WSE, and FA. All three variables have different dimensions, i.e., Q and WSE are recorded as point observations, whereas FA is recorded as areal observations. In addition, these variables were not observed at the same location, as shown in Figure 4(a)-(b). The sub-basin approach was

300 adopted to overcome the difficulties related to observation locations and dimensions.

The basin was decomposed into similar sub-basins, and the skill score was calculated 301 considering all three variables for each sub-basin. In this study, the Amazon Basin was 302 decomposed into 25 sub-basins as shown in Figure 4Error! Reference source not found.(c). 303 The sub-basins were produced using a sub-basin minimum area threshold value of  $1.5 \times$ 304  $10^{11}$  m<sup>2</sup> and a minimum percentage of each sub-basin's contribution to the confluence 305 point of 1%. Tributaries with contribution areas to the main stream between two sub-306 basins (i.e., interbasin) larger than a threshold value of  $1.5 \times 10^{11}$  m<sup>2</sup> were also treated 307 as separate sub-basins. River pixels having an upstream area larger than the input 308 threshold of  $1.5 \times 10^{11}$  m<sup>2</sup> treated as the main stream river for each subbasin. 309

310

## (a) Amazon Basin with Observations



(c) Decomposed Subbasins



312	Figure 4: (a) Map of the Amazon Basin with Q, WSE, FA observation locations
313	indicated (gray circles, triangles, and green shaded areas, respectively), (b) The
314	zoomed-in area shows sub-basin 13, with red circles and yellow triangles indicating the
315	considered observations of Q and WSE, respectively, along the sub-basin main river
316	channel and the pink shaded area indicating the FA considered (50 km on each side of
317	the main river). (c) Decomposed sub-basins with identification numbers.
318	The skill score of each sub-basin was calculated considering the Q and WSE point
319	observations for the main stream of the sub-basin to exclude impacts from minor
320	streams and take large-scale hydrodynamics into consideration, as shown in Figure 4(b)
321	For FA, permanent water bodies were excluded from the analysis by considering a 100-

322 km-wide buffer zone (50-km buffer on each side) along the main river channel (orange-

red thin line), as shown in Figure 4(a)-(b). The floodplain width of Amazon is

approximately 30 times of main river channel width (Paiva et al., 2011), and hence 50-

km buffer on each side of the river channel selected to represent the farthest flood

region influenced by the main river. The buffer region helps with determining the

327 impacts of main stream parameters on flood extent while neglecting flooding from

328 small streams and permanent water bodies in the model evaluation.

Most model evaluations using multiple variables are performed with multiple objective functions, which usually have different scales and units. This makes multivariable evaluation burdensome and inappropriate for large basins. A simple model evaluation metric for measuring the quality of a simulation using multiple variables was developed, namely, performance was evaluated in terms of the OSK, a single value with no units. This metric was developed using the NNSE, as calculated in Eq. 2, and derived using
the NSE (Nossent & Bauwens, 2012), as shown in Eq. 3.

$$NNSE = \frac{1}{2 - NSE}$$
(2)

337 
$$NSE = 1 - \frac{\sum_{i=1}^{n} (O_i - P_i)^2}{\sum_{i=1}^{n} (O_i - \bar{O})^2}$$
(3)

where  $O_i$  and  $P_i$  are the observed and modeled values at time *i*, respectively, and  $\overline{O}$  is the mean of observations.

As the model was evaluated for different variables with different dimensional units, the 340 341 NNSE makes it easier to assess the overall performance across all variables. This 342 evaluation method is not overly sensitive to a model consistently deviating from mean observation values, and the metric ranges from 0 to 1. The metric does not have any 343 units and can be compared or combined for many different variables, as well as 344 arithmetically averaged to obtain a unique value for spatially distributed values. The 345 sub-basin skill score was calculated for the Amazon sub-basins for which observations 346 were available for all three variables. A sub-basin without observations for any of the 347 three variables, Q, WSE, and FA, was excluded from the calculation of OSK. The OSK 348 349 was calculated as follows:

350 
$$F_{OSK} = \frac{1}{K} \sum_{i=1}^{K} \left( W_Q \times \frac{1}{m} \sum_{j=1}^{m} NNSE_Q + W_{WSE} \times \frac{1}{n} \sum_{j=1}^{n} NNSE_{WSE} + W_{FA} \times NNSE_{FA} \right)$$
351 (4)

where m and n are the number of observations for Q and WSE, respectively, in each sub-basin for the main stream.  $W_Q$ ,  $W_{WSE}$ , and  $W_{FA}$  are the weights given to each variable, where  $W_Q + W_{WSE} + W_{FA} = 1$  and K is the number of sub-basins (here, it is 25) used in the OSK calculations. For the current assessment, we weighted each variable equally, i.e.,  $W_Q = W_{WSE} = W_{FA} = 1/3$ .

#### 357 **3 Results**

Integrated multivariable evaluation of Amazon Basin modeling was applied. Figure 5 358 shows the contour plot of OSKs for different parameters defined using the coefficient "a" 359 and exponent "b" from Eq. 1. The OSK (Figure 5) indicates the performance of the 360 CaMa-Flood model for the respective parameter and DEMs with equal weighting for 361 each variable for each sub-basin. As observed for most parameters, the CaMa-Flood 362 hydrodynamic model performed better with the MERIT DEM than with the SRTM 363 DEM. The maximum OSK values of 0.46 and 0.51 for the SRTM and MERIT DEMs 364 365 indicated the best set of parameters for multivariable evaluation. Here, CaMa-Flood performed best with the SRTM DEM for a = 0.349 and b = 0.35, and with the MERIT 366 DEM for a = 0.144 and b = 0.45. In the simulations performed with wide ranges of 367 parameter values, the robust performance of CaMa-Flood was confirmed, and the model 368 was more accurate with the MERIT DEM than with the SRTM DEM (Figure 5). 369



370

Figure 5: OSK contour plot with equal weighting of all three variables (Q, WSE, and
FA) for (a) the SRTM DEM and (b) the MERIT DEM.



373

Figure 6: Sub-basin skill scores for (a) Q, (b) WSE, and (c) FA (or flood extent) with the SRTM DEM and for (d) Q, (e) WSE, and (f) FA with the MERIT DEM, and skill scores representing combined multiple variables with the (g) SRTM and (h) MERIT DEMs for the best set of parameters.

The sub-basin skill scores for each variable are shown separately in Figure 6(a)-(f) for 378 the SRTM DEM with a = 0.349 and b = 0.35, corresponding to a depth at the river 379 mouth of 25 m, and for the MERIT DEM with a = 0.45 and b = 0.144, corresponding to 380 a depth at the river mouth of 35 m. Here, a and b represent the coefficient and exponent 381 of Eq. 1, respectively, and the parameters corresponding to the best OSK in Figure 5. 382 The OSK for the Amazon Basin was obtained by taking the arithmetic average of the 383 skill score of each sub-basin. Considerable improvement was observed for WSE 384 385 predictions as it is directly affected by topography. The gray color (Figure 6) indicates sub-basins for which observations of the variables of interest were unavailable. Among 386 the three variables, the FA predictive performance was poorer than that for the other 387 388 two variables with both the MERIT and SRTM DEMs. This may be due to many reasons, including poor spatial (~25 km) and temporal resolution (monthly average) of 389 the FA observation data, and the indirect estimations of flood extent (i.e., FA) in the 390 391 Global Inundation Extent from Multi-Satellites dataset are associated with more uncertainty compared to the directly measured Q and WSE observations. The simplicity 392 of the downscaling method adopted (see Section Error! Reference source not found.) may 393 not represent the complexity of the true values, and uncertainties may be present. The 394 395 sub-basin skill scores and OSKs for combined multiple variables are shown in Figure 396 6(g)–(h). A significant improvement was observed with the MERIT DEM compared to the SRTM DEM. In addition, a major improvement occurred for upstream sub-basins 397 with the MERIT DEM compared to the SRTM DEM. This suggests that the MERIT 398 DEM can more accurately represent small streams and topography than can the SRTM 399 DEM, especially for upstream basins. 400

401	Plots of simulated and observed Q over time for sub-basin 18 and sub-basin 3 are shown
402	in Figure 7(a) and (b) (see Figure 4(c)) for the best set of parameters. These sub-basins
403	were selected to represent basins located at upstream and downstream, respectively,
404	with good and poor predictive performance based on the sub-basin skill score value
405	(calculated using the NNSE value for Q, WSE, and FA). Sub-basin 18 had sub-basin
406	skill scores of 0.47 and 0.57, whereas sub-basin 3 has sub-basin skill scores of 0.21 and
407	0.24 for the SRTM and MERIT DEM, respectively. As shown in Figure 7(a) and Figure
408	7(b), which represent sub-basin 18 and sub-basin 3 (see Figure 4 (c)), respectively, Q was
409	not sensitive to which DEM was used. The relative RMSEs (RRMSEs) for sub-basin 18
410	were 13.07% and 13.59%, and those for sub-basin 3 were 149.86% and 145.17% for
411	SRTM and MERIT, respectively, confirming that the model exhibited similar
412	performance with both DEMs. Figure 7(c) and Figure 7(d) show the time-varying
413	simulated and observed WSE (ENVISAT) for sub-basins 18 and 3 (see Figure 4(c)) for
414	some of the virtual stations. The RRMSE values for sub-basin 18 observations were
415	12.41% and 2.5%, and those for sub-basin 3 observations were 3.34% and 1.22% for
416	SRTM and MERIT, respectively. These observations demonstrated significant
417	improvement in the WSE simulations for MERIT compared to SRTM. This
418	improvement was likely mainly due to the removal of tree biases (tree height) in the
419	Amazon region, which decreases the WSE. Although SRTM performed better than
420	MERIT (refer to Figure 7(e),(f)) in terms of predicting FA in sub-basin 18, with
421	RRMSEs of 31.49% and 64.51% for SRTM and MERIT, respectively, the high peaks
422	for sub-basin 3 were better represented by MERIT than by SRTM. RRMSE values of
423	31.21% and 28.92% for SRTM and MERIT, respectively, showed that the MERIT



Figure 7: Time-series plots of simulated and observed Q for (a) sub-basin 18 (see
Figure 4(c)) and (b) sub-basin 3 (see Figure 4(c)), simulated and observed WSE for (c)
sub-basin 18 (see Figure 4(c)) and (d) sub-basin 3 (see Figure 4(c)), and simulated and
observed FA for (e) sub-basin 18 (see Figure 4(c)) and (f) sub-basin 3 (see Figure 4(c)).



maximum OSK, i.e., those for the best parameters based on the integrated multivariable
evaluation of the CaMa-Flood river hydrodynamic model considering a particular DEM.
The interquartile range for the best parameter set was small compared to most of the
other parameters, suggesting that the best parameters performed almost equally well for
most of the sub-basins.



Figure 8: Sub-basin skill scores for the parameters considered by the SRTM and
MERIT DEMs for depth at the river mouth of (a) 25 m, (b) 35 m, (c) 45 m, and (d) 55
m.

## 444 **4 Discussion**

440

To confirm the robustness of integrated multivariable evaluation, we performed a

446 comparison against single-variable evaluation. Here, we evaluated a model of interest

447 using average NNSE values for Q, WSE, and FA separately. Figure 9 shows the contour

448	plot of OSKs, i.e., average basin NNSE values considering Q, WSE, and FA
449	individually, for the whole Amazon Basin regardless of location and without
450	considering the sub-basin approach. The best parameter set could not be determined
451	using single-variable evaluation. The maximum performance of the model was seen for
452	a wide range of parameters when considered separately; e.g., there were no peaks
453	observed in the Q contour (Figure 9(a),(b)). It is challenging to find the best set of
454	parameters by evaluating only one variable for the SRTM and MERIT DEMs.
455	Single-variable evaluation using Q, WSE, and FA for the CaMa-Flood river
456	hydrodynamic model suggested that Q sensitivity is low and cannot be used for model
457	calibration. Evaluation using WSE showed that the best parameter set obtained using
458	only a single variable can lead to poor accuracy outcomes for the other variables,
459	especially in the case of wrong/poor models (here, the SRTM DEM) (Figure 9(c)).
460	Comparing the WSE contour plot (Figure $9(c)$ ,(d)) with the contour plots for other
461	variables (Q and FA) (Figure 9(a),(b),(e),(f)), the best parameters (peaks in the
462	contours) derived using WSE did not correspond to the best parameters (peaks in the
463	contours) derived using the two other variables, and the model could perform well but
464	for the wrong reasons. By contrast, the optimal value for FA could not be achieved,
465	probably due to errors in the flood topography data, low spatial and temporal resolution
466	of observation data, and low accuracy.



- 468 **Figure 9**: Basin skill score (average NNSE for the whole basin) contour plot
- 469 considering (a) Q for the SRTM DEM, (b) Q for the MERIT DEM, (c) WSE for SRTM,
- 470 (d) WSE for MERIT, (e) FA for SRTM, and (f) FA for MERIT.

471	The new multivariable evaluation technique is flexible, and the weights for each
472	variable can be selected manually according to the user's requirements. The method is
473	flexible enough that the number of variables used for evaluation and averaging can be
474	changed according to the user's requirements. Figure 10 shows an example of metric
475	calculation with different weighting of variables. The overall skill score was calculated
476	by giving weights of 30%, 30%, and 40% to the Q, WSE, and FA observations,
477	respectively. More weight was given to FA to allow optimization of the parameter
478	location for better estimations of FA.
479	The maximum value of 0.49 was obtained with $a = 0.349$ and $b = 0.35$ , corresponding to
480	a depth at the river mouth of 25 m for the MERIT DEM, for the given range of
481	parameters. Figure 11(a)–(c) show the sub-basin skill scores (average NNSE values) of
482	the individual basins for each variable separately. These scores correspond to the
483	parameters Q, WSE, and FA with assigned weights of 30%, 30%, and 40%, respectively.
484	As shown in Figure 11(d) and 11(f), FA predictive performance was enhanced for most
485	of the sub-basins with increases in the weight of the FA variable, whereas the change in
486	Q predictive performance was not significant. The downstream sub-basin performance
487	improved, whereas the FA predictive performance for a few upstream sub-basins
488	appeared to worsen. This may be because a decrease in depth at the mouth further
489	decreases the river depth upstream, which may not represent the true situation.
490	Figure 12 shows observation and simulated time-series plots of Q, WSE, and FA for the
491	best set of parameters for the MERIT DEM with equal weights assigned to the three
492	variables and with greater weighting of FA compared to the other two variables. The
493	results showed significant improvement in FA predictive performance for sub-basin 3

494	with a change in RRMSE value from 27.61% to 17.33%. A significant decline was not
495	observed for sub-basin 18, but the RRMSE value changed from 64.55% to 86.23%. The
496	predictive performance of the other two variables (Q and WSE) did not change
497	significantly for both of these sub-basins. The RRMSE value changed from 13.59% to
498	13.84% for sub-basin 18 Q observations and from 145.17% to 146.18% for sub-basin 3.
499	The RRMSE changed from 2.5% to 3.15% for sub-basin 18 WSE observations and
500	from 1.22% to 1.27% for sub-basin 3, when equal weights were assigned to the
501	variables versus more weight assigned to FA. Our method can be used for the robust
502	evaluation of river hydrodynamic models, and it is flexible enough to allow
503	modification according to the user's requirements global optimization considering
504	multiple variables.





differences in score between more heavily weighted FA and equal weights across 507

variables. 508



510 **Figure 11**: Sub-basin skill scores for (a) Q, (b) WSE, and (c) FA with the MERIT DEM,

with weights of 30%, 30%, and 40% assigned to Q, WSE, and FA, respectively, and

512 differences in sub-basin skill score between more heavily weighted FA and equal

513 weighting of variables for (d) Q, (e) WSE, and (f) FA.

509



Figure 12: Time-series plots of simulated and observed (a) Q, (c) WSE, and (e) FA for sub-basin 18 (Figure 4(c)) and simulated and observed (b) Q, (d) WSE, and (f) FA for sub-basin 3 (Figure 4(c)) with the MERIT DEM using the best parameter set with equal weighting of variables.

Although we used the NNSE as the target metric, the method can be used with other
metrics, e.g., flood extent can be evaluated using performance indices (Aronica et al.,
2002; Bates & De Roo, 2000) that measure the agreement between predicted and
observed flood extent, especially with static data (Hess et al., 2003). The same method

can also be applied using other metrics, such as the Kling-Gupta Efficiency (KGE)
(Gupta et al., 2009) and NSE (Nash & Sutcliffe, 1970), among others. The current
method can be modified such that different specific weights are assigned to the
observations, e.g., assigning greater weight to main river channel observations or
downstream sub-basin observations.

## 528 **5 Summary and Limitations**

529 We developed an integrated multivariable evaluation technique for the robust assessment of river hydrodynamic models and confirmed that the MERIT DEM 530 performed better than the SRTM DEM. The developed multivariable evaluation method 531 uses the NNSE as the evaluation metric for simplicity of calculation. A sub-basin skill 532 score approach for calculating an integrated metric across multiple variables was 533 534 adopted to ease the difficulty associated with the spatial distribution of observations. The results obtained showed that the model can be evaluated across multiple variables 535 at the same time with the proposed technique. With this method, the prediction of 536 537 multiple variables is shown to improve with a better model, and combining multiple variables in the evaluation produces a more balanced estimation of performance. 538

539 The technique was applied to compare the performance of CaMa-Flood with two

different DEMs, the SRTM and MERIT DEMs. As shown in Figure 5 and 6, the

541 maximum value of the integrated metric for CaMa-Flood (OSK) with the MERIT DEM

was 0.51, compared to the value of 0.46 with the SRTM DEM with equal weighting of

543 each variable. The sub-basin skill scores for each variable (Figure 6(a)–(f)) separately

showed significant improvement in WSE prediction as the DEMs (topography) directly

affect the accuracy of WSE simulation. The results shown in Figure 6(g) and (h)

indicate that with the MERIT DEM, the predictive performance for upstream sub-basins 546 improved considerably. This improvement implied that the upstream sub-basins were 547 affected to a greater extent due to tree biases in the SRTM DEM, whereas there was 548 significant bias correction in the MERIT DEM. Single-variable evaluation (see Section 549 4) confirmed that robust evaluation of a hydrodynamic model is challenging to achieve 550 using a single variable at a time. Figure 9(a), 9(b), 9(e), and 9(f) show that Q and FA are 551 not suitable for use in calibration as the sensitivities are low and the same skill score 552 553 values were obtained for a wide range of parameters, whereas the peaks obtained for WSE (Figure 9(c),(d)) did not correspond to the peaks of the other two variables, and 554 the best parameter may be obtained in an incorrect manner. 555

This study had some limitations. Estimating the channel depth using the power law 556 equation is not realistic, as each tributary or river segment can have local characteristics 557 558 that cannot be explained by the power law equation. The river model error cannot be explained only by the channel depth parameter. There are many possible error sources, 559 such as errors in input runoff and flood plain topography, limitations due to 560 561 simplification of physics, and representation of the river as a rectangular channel. Although we did not account for the sizes of the sub-basins and corresponding river 562 sizes when weights were assigned to the observations during the evaluation, the 563 evaluation method can be easily altered to incorporate these variations. The developed 564 method can be used for more robust and accurate evaluation after incorporating new 565 schemes to overcome model limitations in future. 566

The developed integrated multivariable evaluation technique can overcome limitations
such as lower discharge sensitivity for calibration, by incorporating other variables into

the evaluation. This method can reduce errors by considering the required data for 569 evaluation and is flexible enough to be adapted according to the user's requirements. 570 571 The method can modified or use a combination of other metrics, such as the NSE, KGE, and flood performance indices. An evaluation can be performed even if observations for 572 some variables are missing for a few sub-basins by eliminating these variables from the 573 evaluation for those particular sub-basins. Future studies will define sub-basin-scale 574 parameters and evaluate models at the basin scale by including other metrics in 575 576 evaluation process.

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#### 583 Data Availability

All data in this study are publicly available and were accessed at the links given in the

- 585 text (HYBAM, <u>http://www.ore-hybam.org;</u> ENVISAT, <u>http://hydroweb.theia-land.fr/;</u>),
- from the literature (GIEMS, Papa et al., 2010). The Global Hydrodynamic Model
- 587 CaMa-Flood is available from (Yamazaki et al., 2021).

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