Inferring the Shallow Layered Structure at the Chang'E-4 Landing Site: A Novel Interpretation Approach Using Lunar Penetrating Radar

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Abstract

The current paper investigates the shallow layers of the lunar regolith at the Chang'E-4 landing site. Four layers between 0-10 meters were identified using lunar penetrating radar. Based on these outputs, a revised stratigraphic model is suggested for the post-Imbrian ejecta at the Von Karman crater. The layers were previously unseen due to the smooth boundaries between them. The revised model was inferred using an advanced hyperbola-fitting scheme. Applying conventional hyperbola-fitting to non-homogeneous media results in errors and inaccuracies that are often wrongly assumed to be negligible. We propose a novel hyperbola-fitting scheme that is not constrained to homogeneous media and can be applied subject to any arbitrary one-dimensional permittivity distribution. Via this approach, we can estimate the permittivity profile of an investigated area and detect layered structures that were previously transparent to electromagnetic waves due to the gradational dielectric properties at their interfaces.

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¹³ Key Points:

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14	• We suggest a novel hyperbola-fitting technique that assumes an arbitrary permit-
15	tivity distribution with respect to depth
16	• The proposed method is used to map the lunar regolith at the Chang'E-4 land-
17	ing site
18	• A layered structure is revealed at the first 10 meters. A new stratigraphic model

is suggested for the Von Kármán crater

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20 Abstract

The current paper investigates the shallow layers of the lunar regolith at the Chang'E-21 4 landing site. Four layers between 0-10 meters were identified using lunar penetrating 22 radar. Based on these outputs, a revised stratigraphic model is suggested for the post-23 Imbrian ejecta at the Von Kármán crater. The layers were previously unseen due to the 24 smooth boundaries between them. The revised model was inferred using an advanced 25 hyperbola-fitting scheme. Applying conventional hyperbola-fitting to non-homogeneous 26 media results in errors and inaccuracies that are often wrongly assumed to be negligi-27 ble. We propose a novel hyperbola-fitting scheme that is not constrained to homogeneous 28 media and can be applied subject to any arbitrary one-dimensional permittivity distri-29 bution. Via this approach, we can estimate the permittivity profile of an investigated 30 area and detect layered structures that were previously transparent to electromagnetic 31 waves due to the gradational dielectric properties at their interfaces. 32

³³ Plain Language Summary

The landing site of Cheng'E-4 is at the Von Kármán (VK) crater at the South Pole-34 Aitken (SPA) basin. SPA is the oldest and biggest basin on the Moon created at the early 35 stages of its evolution by an impact that is believed that has penetrated the lunar crust 36 and uplifted materials from the top mantle. Understanding the geology and stratigra-37 phy of SPA can help us understand cratering processes and shed a light on the evolu-38 tion of the Moon. In the current paper, we have used lunar penetrating radar data from 39 the Chang'E-4 mission combined with a novel interpretation tool to reveal a previously 40 unseen layered structure for the first ~ 10 m of the VK crater. 41

42 Keywords

South-Pole Aitken (SPA), Chang'E-4, Lunar Penetrating Radar (LPR), Ground
 Penetrating Radar (GPR), hyperbola-fitting.

45 **1** Introduction

Ground penetrating radar (GPR) is a mature geophysical technique (Daniels, 2004) 46 with a unique span of applications ranging from landmine detection (Feng et al., 2012; 47 Giannakis et al., 2016) and concrete inspection (Wai-Lok Lai et al., 2018; Giannakis et 48 al., 2020), to glaciology (Williams et al., 2014) and archaeology (Convers, 2004). In plan-49 etary sciences, GPR has been applied both for satellite (Lauro et al., 2020) and in-situ 50 measurements (Li et al., 2020), with promising results for mapping sub-glacial water bod-51 ies in Mars (Lauro et al., 2020), and for inferring the layered structure of the lunar re-52 golith (Lai et al., 2020; Li et al., 2020; Zhang et al., 2020). 53

Subject to the application and the employed measurement configuration, various 54 GPR processing and interpretation techniques have been suggested over the years (Daniels, 55 2004). From typical signal processing (Li et al., 2015; Cassidy, 2009) and linear Born ap-56 proximations (Boero et al., 2018), to machine learning (Giannakis et al., 2019) and full-57 waveform inversion (Meles et al., 2010). Within that context, hyperbola-fitting is con-58 sidered one of the most mainstream techniques for the interpretation of common-offset 59 GPR data (Mertens et al., 2016). The simplicity and computational efficiency of hyperbola-60 fitting make it an appealing choice for mapping the dielectric properties of an investi-61 gated medium, and for estimating the coordinates of subsurface targets (Mertens et al., 62 2016). 63

Hyperbola-fitting has been used in both Chang'E-3 and Chang'E-4 missions (Li
et al., 2020; Fa, 2020; Dong, Fang, et al., 2020; Dong, Feng, et al., 2020; Lai et al., 2019)
for estimating the electric permittivity of lunar regolith and subsequently inferring its

density and mineralogical composition (Dong, Feng, et al., 2020; Li et al., 2020). Nonethe-67 less, the underlying assumptions of hyperbola-fitting constrain its applicability, especially 68 in complex environments where permittivity varies with depth. To mitigate that, con-69 ventional hyperbola-fitting is often complemented with Dix conversion (Dix, 1955; Dong, 70 Fang, et al., 2020) in order to transform the estimated bulk velocity to actual velocity. 71 Through a series of numerical examples, it is illustrated that this approach (Dong, Fang, 72 et al., 2020) has limited applicability for the lunar regolith and should be used with cau-73 tion. To that extent, we present a novel hyperbola-fitting that tackles this problem by 74 simultaneously fitting multiple hyperbolas subject to any arbitrary 1D permittivity dis-75 tribution. 76

The proposed scheme is applied to the Lunar Penetrating Radar (LPR) data col-77 lected by the Yutu-2 rover during the first two lunar days of the Chang'E-4 mission at 78 the Von Kármán (VK) crater (Li et al., 2020). Four distinct layers –that were previously 79 not visible due to the smooth boundaries between them- were identified within the first 80 10 m. This outcome differs significantly from previous theories suggesting that the first 81 12 m of the landing site are fairly homogeneous, part of the weathered fine-grained re-82 golith that lies on top of the ejecta from the Finsen crater (Zhang et al., 2020). Based 83 on the revised permittivity profile and the available literature on the geology of the Chang'E-84 4 landing site, we suggest a new post-Imbrian stratigraphic model for the VK crater, in 85 which an approximately ~ 3 m weathered fine-grained layer is followed by $\sim 8 - 10$ 86 meters of ejecta from the VK L and L' craters overlaying the ejecta from the Finsen crater. 87

⁸⁸ 2 The Chang'E-4 Landing Site

The Chinese lunar probe Chang'E-4, carrying the Yutu-2 rover, was the first human-89 made object that landed on the far-side of the Moon on 3rd of January 2019 (Li et al., 90 2019; Tang et al., 2020). The landing site is located at the South Pole-Aitkens (SPA) 91 basin – the oldest and biggest crater on the Moon (Huang et al., 2018; Hu et al., 2019; 92 James et al., 2019). The SPA basin is pre-Nectarian in age and has an elliptical shape 93 with an approximate diameter of 2100-2500 km (Moriarty et al., 2013). The transient 94 cavity of the SPA basin has been estimated between 840-1400 km (Potter et al., 2012; 95 Moriarty et al., 2013). The maximum excavation depth of lunar craters is approximately 96 10 % of their diameter (Stopar et al., 2017), which implies that the SPA basin excavated 97 up to 140 km through the lunar crust and into the mantle (Moriarty et al., 2013). This 98 premise is based on the maximum width of lunar crust ~ 60 km, as estimated by the 99 Gravity Recovery and Interior Laboratory (GRAIL) mission (Wieczorek et al., 2013), 100 which is in good agreement with seismic data from the Apollo missions (Khan, 2002). 101 The shallow mantle layer was most-likely melted during the impact (Moriarty et al., 2013) 102 and parts of it are expected to occur within the SPA basin, forming an underlying sheet 103 of non-crustal materials (Potter et al., 2012; Moriarty et al., 2013). These materials are 104 of paramount importance since they can constrain the composition of the upper man-105 tle and provide an insight into the early evolution of the Moon (Moriarty et al., 2013). 106

Based on previous models of lunar evolution –that suggest an upper mantle pre-107 dominantly composed of olivine (Yamamoto et al., 2010) – strong spectral signatures of 108 olivine were expected to be present within the SPA crater (Ivanov et al., 2018). Nonethe-109 less, data from CLEMENTINE and SELENE did not support this premise (Tompkins 110 & Pieters, 1999; Matsunaga et al., 2008; Yamamoto et al., 2010), apart from small oc-111 currences of olivine clusters (Yamamoto et al., 2010) most likely originated from crustal 112 materials, due to their location (the exterior of the SPA) and the high content of feldspar 113 in their near proximity (Moriarty & Pieters, 2018). The SPA is dominated by mafic ma-114 terials and in particular with Mg-rich and low-Ca pyroxene (Moriarty & Pieters, 2018). 115 CLEMENTINE measurements reveal an inner zone with Fe abundance and an outer zone 116 with lower Fe content (Jolliff et al., 2000). Furthermore, using data from the Moon Minerol-117 ogy Mapper (M^3) , Moriarty & Pieters 2018 have divided the SPA into four zones. The 118

first zone is the inner SPA area called SPACA, with characteristic Ca-pyroxene abun-119 dance that lies at the center of the SPA. The second zone surrounds SPACA, and it is 120 an area with Mg-rich pyroxenes. Based on spectral analysis of the central peaks of the 121 craters within SPACA, strong indications were given to support the premise that SPACA 122 lays on top of the Mg-rich area (Moriarty & Pieters, 2018). The third zone is a hetero-123 geneous annulus that consists of pyroxene and feldspar, and acts as the intermediate stage 124 between the SPA and its exterior. The latter is the fourth zone, a mafic-free area with 125 high content of feldspar, similar to lunar highlands (Moriarty & Pieters, 2018). 126

127 The landing site of Chang'E-4 is within the Mg-rich and in particular in the interior of the VK crater (177.588°E, 45.4578°S). VK is an elliptical crater (Zhang et al., 128 2020) with approximately ~ 186 km diameter (Huang et al., 2018). The age of VK was 129 estimated pre-Nektarian (Huang et al., 2018) and recent studies have placed it at $\tilde{4}.2$ Ga 130 (Lu et al., 2021), very close to the formation of SPA (Lu et al., 2021). The creation of 131 Leibnitz crater affected the north part of VK and contributed to the ejecta layer prior 132 to the Imbrian basaltic flood (Huang et al., 2018). Ejecta from Alder crater (dated at 133 3.5 Ga (Lu et al., 2021)) are also expected to the pre-basaltic layers (Huang et al., 2018). 134 The VK crater was flooded with basalts during the Imbrian period (Paskert et al., 2018) 135 around 3.2-3.3 Ga. Subsequently, ejecta from the Finsen crater were deposited at the 136 end of Imbrian and early Eratosthenian (3.1 Ga (Lu et al., 2021)). Recent studies sug-137 gest that Orientale crater might have added to the post-Imbriun VK layers as well (Xiao 138 et al., 2021). Subsequently, the Eratosthenian craters VK L and L' were formed (Zhang 139 et al., 2020). The VK, Leibnitz, Alder, VK L, and L' lay within the Mg-pyroxene an-140 ulus while Finsen is within SPACA (Moriarty & Pieters, 2018). 141

Geological context suggests that the craters VK L, L', Finsen and Orientale have 142 contributed to most of the post-Imbrian ejecta layers of the VK crater (Huang et al., 2018; 143 Di et al., 2019; Xiao et al., 2021). The size of the ejecta from the Finsen crater is esti-144 mated -via numerical simulations (Di et al., 2019) – at ~ 30 meters. This is not in good 145 agreement with the results obtained using dark-halo and non-dark halo craters (Li et al., 146 2020) that suggest a thicker post-basaltic layer, probably due to the presence of Orien-147 tale ejecta (Xiao et al., 2021). Nonetheless, contradicting data (Yue et al., 2020) place 148 the date of Orientale to be older than the Imbrian basaltic flood, which implies that there 149 might be another source that contributed to the post-basaltic VK layers. 150

The surface of the landing site is smooth with a small amount of boulders, most 151 of them being glassy fragments and breccias from secondary craters (Lin et al., 2020). 152 From in situ reflectance data, the visible surface at the landing site is not olivine-pyroxene 153 rich and consists of 56-72% plagioclase, similar to lunar highlands (Hu et al., 2019; Li 154 et al., 2019) with Mg-rich orthopyroxene (Gou et al., 2020). The thickness of the regolith 155 (weathered top soil) is estimated using LROC NAC images at $\sim 2.5 - 7.5$ m (Huang 156 et al., 2018). Based on the M^3 reflectance data, it is estimated that below the top weath-157 ered soil, lays a low-calcium pyroxene (LCP) layer ranging from $\sim 8-13$ m followed 158 by a high-calcium pyroxene (HCP) layer from $\sim 13 - 53$ m (Huang et al., 2018). Be-159 low that, the Imbrian basalt deposits are expected to overlay the ejecta from the Alder 160 and Leibnitz craters on top of the brecciated bedrock from the VK impact (Huang et 161 al., 2018). 162

Further insights on the ejecta at the VK crater are provided by the LPR mounted 163 to the Yutu-2 rover of the Chang'E-4 mission (Li et al., 2020). The first attempt to ex-164 amine the lunar surface with in-situ LPR equipment occurred during the Chang'E-3 mis-165 sion on the near side of the moon (Lai et al., 2019). Similar antenna configurations were 166 167 employed for both Chang'E-3 and Chang'E-4 missions (Li et al., 2020). In particular, two antennas with 500 MHz central frequency (at the bottom of the rover), and one low 168 frequency antenna (mounted at the back of the rover) with 60 MHz central frequency 169 (Li et al., 2020). The low frequency antenna in the Chang'E-4 mission gave thin indi-170 cations of four different lava flows that probably occurred during the Imbrian period (Lai 171

et al., 2020). Unfortunately, the low frequency data in both missions suffer from ring-172 ing noise due to the coupling between the antenna and the rover, which resulted in er-173 roneous reflections and noisy data (Li et al., 2018; Zhang et al., 2020). In contrast to the 174 Chang'E-3 landing site (Lai et al., 2019), in the VK crater, the ilmenite content is fairly 175 low, making the ejecta layers transparent to LPR (Dong, Fang, et al., 2020). This re-176 sulted in good quality data that clearly demonstrated a complex layered structure for 177 the first 50 meters of the VK crater (Zhang et al., 2020; Li et al., 2020). In addition, us-178 ing a conventional hyperbola-fitting (assuming a homogeneous medium) with Dix con-179 version, the electric permittivity of the ejecta layers was estimated, and furthermore used 180 to infer the mineralogical (Fe and Ti content) (Li et al., 2020) and the mechanical (den-181 sity) properties of the lunar regolith (Dong, Fang, et al., 2020; Dong, Feng, et al., 2020), 182 based on semi-empirical formulas fine-tuned for lunar soils (Olhoeft & Strangway, 1975; 183 Carrier et al., 1991; Hickson et al., 2018). The relative electric permittivity at the land-184 ing site monotonically increases from $\sim 3-6$ with respect to depth, as estimated us-185 ing typical hyperbola fitting (Dong, Fang, et al., 2020). This corresponds to a density 186 that starts from $\sim 1 \ gr/cm^3$ at the surface and reaches $2.5 \ gr/cm^3$ at 50 m depth (Dong, 187 Fang, et al., 2020). 188

189 **3** Methodology

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3.1 Advanced hyperbola-fitting

In this section, a novel hyperbola-fitting framework is described, capable of dealing with half-spaces with arbitrary 1D permittivity distributions $\epsilon(y)$ (see Figure 1). Similar to typical hyperbola-fitting, in order to avoid non-uniqueness (Mertens et al., 2016; Giannakis et al., 2019), the proposed scheme assumes that the radius (R) of the investigated target equals with zero. Subject to a varying velocity with depth, the two way travel time t that it takes for the wave to travel from the point $\vec{B} = \langle x, y \rangle$ to the point $\vec{A} = \langle x_0, d \rangle$ via the parametric curve $\vec{q}(m) = \langle q_x(m), q_z(m) \rangle$ (where $m \in [0-1]$ and d is the depth of the target) can be calculated using a scalar line integral over $\vec{q}(m)$

$$t = \frac{2}{c_0} \int_0^1 \sqrt{\epsilon(y)} \left| \left| \frac{\partial \overrightarrow{q}(m)}{\partial m} \right| \right| dm.$$
 (1)

Given a specific velocity structure, the path $\overrightarrow{q}(m)$ can be calculated using Fermat's principle (Aldo, 1996). The notation $||\frac{\partial \overrightarrow{q}(m)}{\partial m}||$ is used to denote the norm of the first derivative of the parametric curve $\overrightarrow{q}(m)$ with respect to the parameter $m \in [0-1]$. It is shown that if we simplify equation (1) and make the assumption that the path $\overrightarrow{q}(m)$ is the straight line that connects the antenna to the center of the target, it leads to an elegant and computationally efficient formulation without compromising accuracy (more details are given in 3.2). The straight line that connects the antenna to the target can be expressed via the parametric curve $\overrightarrow{q}(m) = \overrightarrow{A} + (\overrightarrow{B} - \overrightarrow{A})m$. Substituting this into equation (1) results in

$$t = \frac{2\left|\left|\overrightarrow{B} - \overrightarrow{A}\right|\right|}{c_0} \int_0^1 \sqrt{\epsilon(y)} dm.$$
(2)

The linear path of the integral in equation (2) can be written as $\overrightarrow{q}(m) = \langle x_i + m (x_0 - x_i), y_i + m (d - y_i) \rangle$, where x_i, y_i are the coordinates of the antenna at the *i*th position. Consequently, the y variable in equation (2) can be substituted by $y = y_i + m (d - y_i)$, which implies that $\partial m = \frac{\partial y}{d}$ and that y = d for m = 1. Therefore, equation (2) can be rewritten as

$$t = \frac{2||\vec{B} - \vec{A}||}{c_0 d} \int_0^d \sqrt{\epsilon(y)} dy.$$
(3)

Solving the integral numerically yields

$$t \approx \frac{2||\overrightarrow{B} - \overrightarrow{A}||}{c_0 d} \sum_{s=0}^Q \sqrt{\epsilon(s \cdot \Delta y)} \Delta y \tag{4}$$

where Δy is the discretization step and $Q = d/\Delta y$. Notice that the summation term $N(d, \epsilon) = \sum_{s=0}^{Q} \sqrt{\epsilon(s \cdot \Delta y)} \Delta y$ is independent of the position of the antenna and needs to be calculated just once. The final formulation for the proposed scheme is given by

$$t \approx \frac{2||\vec{B} - \vec{A}||}{c_0 d} N(d, \epsilon), \tag{5}$$

where the only unknowns are the permittivity function $\epsilon(y)$ and the depth of the target d. The parameter x_0 can be easily derived from the apex of the hyperbola at the measured B-Scan. Subject to a given $\epsilon(y)$, the depth of the target is calculated using the apex of the hyperbola (x_0, t_0) , where $||\vec{B} - \vec{A}|| = d$

$$t_0 \approx \frac{2}{c_0} N(d, \epsilon). \tag{6}$$

For a given $\epsilon(y)$, the only unknown in equation (6) is the depth d that is estimated nu-191 merically using the bisection method. Notice that both equation (6) and the summation 192 $N(d,\epsilon)$ in equation (4) need to be evaluated just once. The only term in equation (5) 193 that needs to be updated as the scan progresses is the distance $||\vec{B} - \vec{A}||$. To summa-194 rize, given a permittivity distribution $\epsilon(y)$ and the apex of a hyperbola $[x_0, t_0]$, the depth 195 d of the target is estimated by numerically solving equation (6) using the bisection method. 196 Subsequently, $N(d, \epsilon)$ is evaluated and furthermore used in equation (5) to calculate the 197 arrival times $\mathbf{t} \in \mathbb{R}^n$. 198

The proposed scheme utilizes numerous hyperbolas and tries to find the optimum $\epsilon(y)$ that simultaneously minimizes $\min_{\epsilon(y)} \sum_{i=1}^{Z} ||\mathbf{t}_i - \mathbf{T}_i||$, where $\mathbf{T}_i \in \mathbb{R}^{n_i}$ and $\mathbf{t}_i \in \mathbb{R}^{n_i}$ represent the measured and predicted arrival times for the *i*th hyperbola, Z is the to-199 200 201 tal number of the employed hyperbolas and n_i is the number of discretisation points for 202 the *i*th hyperbola. To further simplify the problem, the permittivity is discretised with 203 K equidistant points and subsequently a cubic interpolation is applied to map ϵ with re-204 spect to y in a continuous manner. Therefore, the minimization is re-written as $\min_{\epsilon(k)} \sum_{k\in\mathbb{R}^K} \sum_{i=1}^Z ||\mathbf{t}_i - \mathbf{T}_i||$ with only K much is for $k \in \mathbb{R}^K$. 205 \mathbf{T}_i with only K number of unknowns. This is a non-linear and non-convex problem that 206 can be solved using global optimizers. A Particle Swarm Optimisation (PSO) (Kennedy 207 & Eberhart, 1995), with 50 particles and uniform PSO parameters, was proven to be very 208 efficient for reconstructing $\epsilon(y)$, given a sufficient number of measured hyperbolas. The 209 number of equidistant points K is estimated by plotting the Error-K curve. This approach 210 is based on the L-curve method (Hansen, 1992) that tries to balance between accuracy 211 and constraints. Within that context, we choose the K value for which the solution bal-212 ances accuracy and simplicity. In particular, the minimization is executed multiple times 213 with increasing K until the error starts to converge. The K value is chosen at the ear-214 liest point of convergence. Greater K values can potentially result (if a sufficient num-215 ber of hyperbolas is not present) in unnecessary complicated permittivity structures with-216 out increasing the fitting accuracy. 217

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3.2 Numerical experiments

Two numerical 2D case studies (illustrated in Figure 2) are used in this section to 219 evaluate the performance of the proposed scheme. Both models are non-dispersive, non-220 conductive, and non-magnetic, with a varying permittivity with respect to depth $\epsilon(y)$. 221 Nine perfect electric conductors (PEC) are distributed randomly within a $2 \times 1 m^2$ do-222 main. The targets have a cylindrical shape with 5 cm diameter and their main axis is 223 perpendicular to the acquisition line. Measurements are taken every 2 cm along the x-224 axis using a line source with 1 GHz central frequency. The offset between the transmit-225 ter and the receiver is 1 cm. The numerical simulations were executed using gprMax (Warren 226 et al., 2016; Warren et al., 2019), an open source electromagnetic solver that uses a sec-227 ond order (in both space and time) finite-difference time domain (FDTD) method (Yee, 228

²²⁹ 1966). The spatial discretization step of the FDTD grid is $\Delta x = \Delta y = 5$ mm, and ²³⁰ the time step Δt is calculated using the Courant limit (Taflove & Hagness, 2000). The ²³¹ boundaries of the domain are truncated using the recursive integration perfectly matched ²³² layer (Giannopoulos, 2008).

From Figure 2, it is apparent that even in these clinical clutter-free numerical ex-233 periments, the reflections from the layers are very weak and not visible in the measured 234 radargrams. This is due to the smooth transition between the layers that can greatly de-235 crease their reflection coefficient (Bano, 2006; Diamanti et al., 2014). This gives the false 236 237 impression that a medium is homogeneous when in fact it can be as complex as Model 1 (see Figure 2), with four clear and distinct layers. This is very important when inter-238 preting radargrams from the lunar regolith, where smooth transitions between layers are 239 expected due to space weathering and the reworking of the materials during crater for-240 mation. 241

The proposed scheme and the typical hyperbola-fitting with Dix conversion (Dong, Fang, et al., 2020) were applied to the radargrams shown in Figure 2. In both models, the proposed methodology outperforms conventional hyperbola-fitting, and manages to sufficiently estimate the permittivity profile and the underlying layered structure in an efficient manner (see Figure 2). Small errors observed in Figure 2 can be due to: the linearpath simplification; manual picking of the hyperbolas (Ding et al., 2020); non-accurate time-zero correction (Yelf, 2004); and/or non-ideal targets i.e. $R \neq 0$.

249 4 Results

The proposed methodology is applied to the high frequency data collected by the 250 Yutu-2 rover at the VK crater during the first two lunar days of the Chang'E-4 mission 251 (Li et al., 2020). During the first two lunar days, the rover followed an irregular path 252 and managed to cover ~ 106 m (Li et al., 2020). The current paper focuses on the first 253 150 ns of the scan in order to effectively map the shallow layers ($\sim 10 - 12$ m) of the 254 regolith. Based on the results, a revised stratigraphy for the VK crater is proposed that 255 takes into account a previously unseen layered structure within the first ~ 10 m of lu-256 nar regolith. 257

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4.1 Lunar penetrating radar results

The radargram was processed using a typical GPR processing pipeline that involves zero-time correction, dewow, time-gain (exponential gain), and background removal (Cassidy, 2009). The resulting B-Scan for the first 150 ns is illustrated in Figure 3 (Li et al., 2020). The overall signal to clutter ratio is substantially higher compared to Chang'E-3 mission (Lai et al., 2019; Li et al., 2020) (potentially due to lack of ilmenite) which results in clear hyperbolic features that can be utilized to deduce the shallow layered structure at the first 10-12 m of the landing site.

Figure 3_A illustrates the resulting permittivity profile using the proposed advanced hyperbola-fitting subject to the hyperbolas shown in Figure 3_B . It is evident that there is a layered structure with four layers in the first 10 m of the regolith. The first and the third layers have low permittivity values while the second and the fourth layers have permittivity up to $\epsilon \approx 10$ (see Figure 3_A). Typical lunar soils have low permittivity values although there are reported high-density lunar samples with relative permittivity up to $\epsilon \approx 10$ (Chung et al., 1970; Olhoeft & Strangway, 1975).

We would like to highlight that current knowledge regarding the permittivity of lunar soils is based primarily on shallow samples brought back to Earth during the Apollo missions. Superficial lunar samples are not representative of deeper layers since they are exposed to space weathering which results in an increased porosity and vitrification (Nash

& Conel, 1973). Moreover, the semi-empirical models tuned for lunar soils are primar-277 ily based on those samples (Chung et al., 1970; Frisillo et al., 1975; Carrier et al., 1991; 278 Shkuratov & Bondarenko, 2001), making them unreliable for estimating the dielectric 279 properties of deeper ejecta. Estimation of the dielectric properties of deeper layers is still an ongoing research area that is primarily based on LPR measurements and typical hyperbola-281 fitting (Dong, Fang, et al., 2020). As shown in section 3, typical hyperbola-fitting is not 282 a reliable approach when applied to inhomogeneous media, and therefore the estimated 283 permittivities using conventional hyperbola-fitting should be used with caution. 284

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4.2 Stratigraphy modeling of the Chang'E-4 landing site

The suggested stratigraphy model is based on the LPR results shown in Figure 3_A 286 and the following premises: 287

• The thickness of the weathered top soil is $\sim 2.5-7.5$ m (Huang et al., 2018) which 288 is consistent with the average weathering rate ($\sim 1.5 \text{ m/Ga}$) derived from the Apollo 289 missions (Gou et al., 2021). 290 Finsen, VK L and L' craters are the predominant sources of the post-Imbrian ejecta 291 in the VK crater (Huang et al., 2018; Zhang et al., 2020). 292 Finsen ejecta at the landing site are estimated via numerical simulations at ~ 35 293 m (Di et al., 2019). 294 • Finsen crater was developed before VK L and L' craters (Zhang et al., 2020). 295 Finsen crater is within the SPACA region and therefore it is expected that its ex-296 cavated materials have an increased HCP/LCP ratio (Moriarty & Pieters, 2018). 297 The peak of the Finsen crater has a low HPC/LCP ratio (Ling et al., 2019), nonethe-298 less, the peak of craters is created in a rebound process that uplifts lower mate-299 rials (Morgan et al., 2016) i.e. materials from the underlying Mg-rich anulus which 300 has low HPC/LPC ratio (Moriarty & Pieters, 2018). 301 The ejecta materials from VK L and L' craters have low HCP/LCP ratio (Ling 302 et al., 2019). 303 Below the weathered top soil there is an LCP layer down to ~ 13 m (Huang et 304 al., 2018). 305 • Below the LCP layer there is a thick layer (> 30 m) with high HCP/LCP ratio 306 (Huang et al., 2018). 307 There is a clear sharp boundary observed on LPR data (Zhang et al., 2020) at \sim 308 13 m, most-likely between the LCP and the HCP layer. 309 The proposed stratigraphy model suggests that the HCP layer overlaying the Im-310 brian basalts is the ejecta from the Finsen crater (Huang et al., 2018) (and maybe Ori-311 entale crater too(Xiao et al., 2021)). This premise is consistent both with the size of this 312 layer (as predicted by numerical simulations (Di et al., 2019)) and with the chemical com-313 position of the Finsen crater (Moriarty & Pieters, 2018). On top of the Finsen ejecta, 314 it is expected to encounter ejecta from Eratosthenian post-Finsen craters. A homoge-315

neous weathered layer with 12 m width as suggested by Zhang et al., 2020 is not con-316 sistent with LROC NAC images (Huang et al., 2018) and by the layered structure re-317 vealed by the proposed hyperbola-fitting scheme (see Figure 3_A). Therefore, we suggest 318 that the top $\sim 10 - 12$ m of the landing site consists of ejecta from the VK L and L' 319 craters. This is in good agreement with the LCP content of the VK L and L' craters and 320 with the layered structure illustrated in Figure 3_A . In addition, a 12-13 m regolith in-321 dicates a weathering rate of $\sim 3-4$ m/Ga which is twice as fast compared to the ones 322 323 derived from the Apollo missions (apart from the landing site of Apollo 16) (Gou et al., 2021). The evolution of the post-basaltic flood ejecta of VK crater is shown in Figure 324 3_C . The ejecta of VK L' (≈ 5.5 m) were deposited on top of the Finsen ejecta at early 325 Eratosthenian. Space weathering degraded the first ~ 1.5 m of the ejecta decreasing its 326 density and consequently its electric permittivity (due to the causal relationship between

permittivity and density (Chung et al., 1970; Olhoeft & Strangway, 1975)). The width 328 of the VK L' regolith is in good agreement with the literature which suggests that rapid 329 weathering is expected at young ejecta, a phenomenon that has also been observed at 330 the Chang'E-3 landing site (Gou et al., 2021). The ejecta from VK L is subsequently de-331 posited on top of the weathered layer creating a top layer with ~ 6 m width. The long 332 weathering process, from early Eratosthenian till now, gave rise to a ~ 3 m of loose lu-333 nar soil with low electric permittivity as predicted by Figure 3_A . This is in good agree-334 ment with the LROC NAC images (Huang et al., 2018) and also with the average weath-335 ering rate (~ 1.5 m/Ga) derived from the Apollo missions (Gou et al., 2021). 336

337 5 Conclusions

A novel interpretation tool was described capable of estimating the permittivity 338 profile of the shallow lunar surface using lunar penetrating radar. The validity and the 339 superiority of the suggested scheme compared to typical hyperbola-fitting was demon-340 strated via a set of numerical experiments that clearly shown that the proposed scheme 341 is capable of reconstructing complicated permittivity profiles using the shape of multi-342 ple hyperbolas as the only inputs. The proposed methodology is suitable for any arbi-343 trary one-dimensional permittivity distribution, which makes it an appealing choice for 344 inferring the mechanical and mineralogical properties of lunar regolith. The advanced 345 hyperbola-fitting was applied to the high frequency data collected during the first two 346 lunar days of the Chang'E-4 mission. The resulting permittivity profile indicates a lay-347 ered structure within the first 10 meters of the regolith. These shallow layers are not vis-348 ible in the measured radargram due to the smooth boundaries between them, making 349 them undetectable using traditional signal processing approaches. It is argued that the 350 multiple layers detected within the shallow lunar regolith can be the ejecta of the Er-351 atosthenian craters Von Kármán L and L', laying on top of the late-Imbrian ejecta of 352 Finsen crater. 353

354 Data Availability Statement

The Chang'E-4 Lunar Penetrating Radar data are available from the Data Publishing and Information Service System of China Lunar Exploration Program http:// moon.bao.ac.cn/searchOrder_dataSearchData.search.

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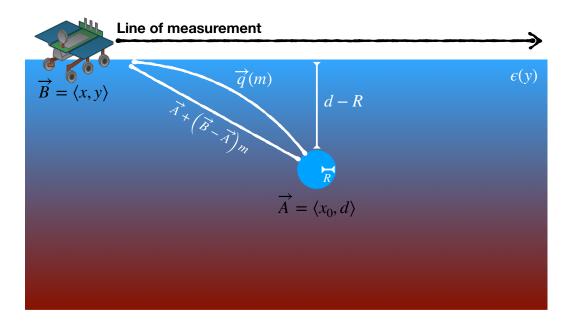


Figure 1. A simple scenario investigating a cylindrical target with radius R buried in a halfspace subject to a 1D electric permittivity distribution with respect to depth $\epsilon(y)$. The vector positions of the center of the target and the antenna are $\vec{A} = \langle x_0, d \rangle$ and $\vec{B} = \langle x, y \rangle$ respectively. The distance between the antenna and the surface of the target equals $||\vec{A} - \vec{B}|| - R$. For both lunar and Earth applications, the permittivity often increases with depth and therefore the velocity is expected to decrease. Due to that, the wave will follow a path similar to the parametric curve q(m) with $m \in [0 - 1]$. The parametric equation of the line that connects the point of measurement to the centre of the target is given by $\vec{A} + (\vec{B} - \vec{A})m$.

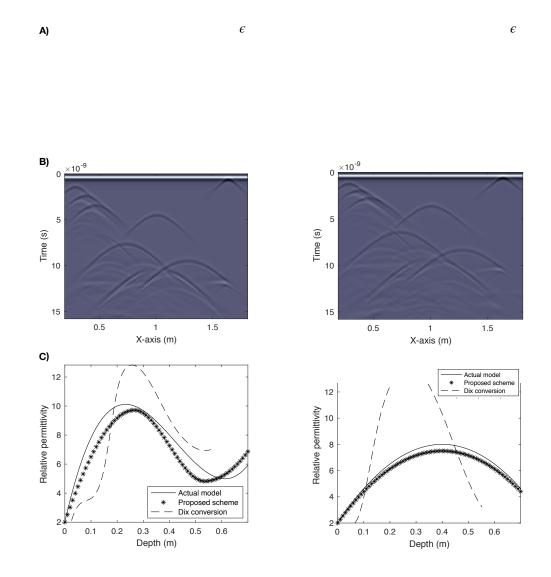


Figure 2. A) The investigated numerical experiments. Nine cylindrical targets are buried in two media with varying permittivity with respect to depth. Measurements are taken every 2 cm (from left to right) using a ground-coupled line source (white star) with 1 GHz central frequency. B) Resulting B-Scans. It is evident that due to the smooth boundaries between the layers, no reflections are visible on the resulting radargrams. The shapes of the hyperbolas are the only features that can be used to infer the permittivity profile. C) The resulting permittivity profile for the models shown in Figure 2_A .

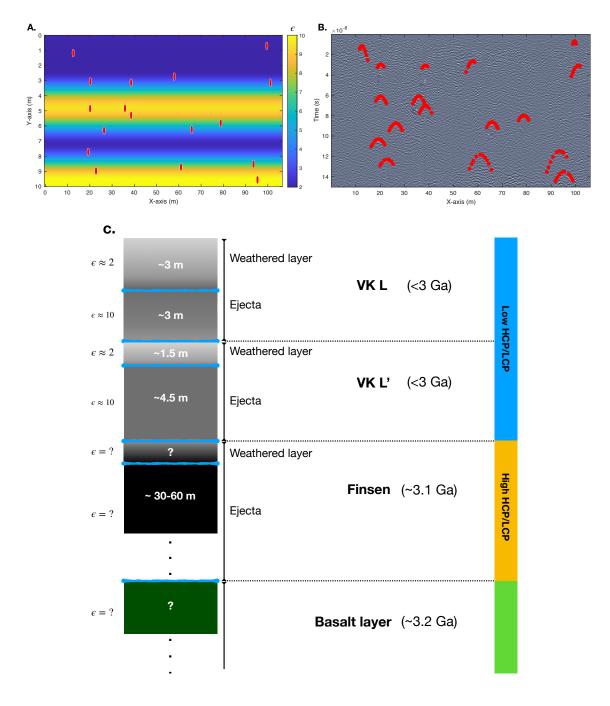


Figure 3. A) The resulting permittivity profile $\epsilon(y)$ at the landing site of Chang'E-4 mission using the advanced hyperbola fitting. The coordinates of the investigated targets are illustrated with red dots. B) The fitted hyperbolas subject to the permittivity profile shown in Figure 3_A. C) The proposed stratigraphy model for the Chang'E-4 landing site. The first ~ -6 m consists of a top weathered layer overlaying the ejecta from VK L crater. Below that, is a low permittivity layer that corresponds to the weathered ejecta of the VK L' crater. The VK L' ejecta extends to ~ -12 m depth, where the Finsen and Alder ejecta lay on top of the Imbrian basaltic layer. Dates are based on (Lu et al., 2021) and the chemical composition on (Huang et al., 2018).

@AGUPUBLICATIONS

Supporting Information for "Inferring the Shallow Layered Structure at the Chang'E-4 Landing Site: A Novel Interpretation Approach Using Lunar Penetrating Radar"

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Contents of this file

- $1.\ {\rm Texts}\ {\rm S1}$ to ${\rm S3}$
- 2. Figures S1 to S3

Introduction

The supporting information includes, Texts S1-S3 and Figures S1-S3. Text S1 describes the conventional hyperbola-fitting that is compared to the proposed interpretation tool. Texts S2 and S3 are the gprMax input files for the numerical models used in Section 3.2, Figure 2 in the manuscript. Figure S1 illustrates the framework within which conventional hyperbola fitting operates. Figure S2 illustrates the landing site for the Chang'E-4 mission and some info for the surrounding craters and the geological setup of the area. Figure S3 zooms in to the fitted hyperbolas subject to the layered model shown in Figure 3_A in the manuscript.

Text S1. Conventional Hyperbola-Fitting with Dix Conversion

Figure S1 illustrates the measurement configuration used in a typical hyperbola-fitting scenario. A cylindrical target with radius R is buried at an arbitrary point $\vec{A} = \langle x_0, d \rangle$, where x_0 and d are the X-ordinate and the depth at the centre of the target. The principal axis of the cylinder is assumed to be perpendicular to the line of measurements. The medium is a homogeneous half-space with relative permittivity ϵ , zero conductivity ($\sigma = 0$) and no magnetic properties ($\mu = 0$). The velocity within this medium is uniform and equals with $c = \frac{c_0}{\sqrt{\epsilon}}$, where $c_0 \approx 2.99 \times 10^8 m/s$ is the velocity of light in free space.

Subject to these constrains, it can be easily deducted that the time (t) of the first arrivals will form a hyperbola in the t - x domain, described by

$$t = \frac{2}{c_0}\sqrt{\epsilon} \left(||\overrightarrow{A} - \overrightarrow{B}|| - R \right).$$
(1)

Notice that the depth d of the target can be calculted from the apex of the hyperbola $[x_0, t_0]$ in the measured radagram via

$$d = \frac{c_0 t_0}{2\sqrt{\epsilon}} + R. \tag{2}$$

Therefore, the only unknowns in equation (1) are the relative permittivity ϵ and the radius of the target R. Hyperbola-fitting tries to find the best set of ϵ and R that minimises the error $\min_{\epsilon,R} ||\mathbf{t} - \mathbf{T}||$ between the measured first arrivals $\mathbf{T} \in \mathbb{R}^n$ and the ones calculated using equation (1) $\mathbf{t} \in \mathbb{R}^n$, where n is the number of points used for the minimization. The minimization $\min_{\epsilon,R} ||\mathbf{t} - \mathbf{T}||$ is singular since they are multiple combinations of (R, ϵ) that fits the measured hyperbola (Mertens et al., 2016; Giannakis et al., 2019). To overcome this, the radius is assumed to be equal with zero R = 0, which implies, that hyperbola-fitting holds true for targets that are relatively small (compared to the scale of the model).

The above framework holds true for homogeneous half-spaces subject to relatively small targets. If the permittivity of a medium varies with depth (which is the most often scenario), then the estimated permittivity using hyperbola-fitting will correspond to the bulk permittivity from the free surface to the investigated target. The bulk permittivity can be mapped with respect to depth using different targets buried at different depths. The Dix conversion (Dix, 1955) is often used in order to transform the bulk permittivity to the actual permittivity (Dong et al., 2020)

$$V_{n+1} = \sqrt{\frac{v_{n+1}^2 t_{n+1} - v_n^2 t_n}{t_{n+1} - t_n}},$$
(3)

where v_n is the average velocity at the time t_n .

X - 4

Text S2. gprMax input file for Model 1, Figure 2

#domain: 1 2 0.005

#dx_dy_dz: 0.005 0.005 0.005

#time_window: 3000

#python:

import numpy as np

p0 = [-187.5000, 212.5000, -60.0000, 10.0000]

nx=np.array([i/100 for i in range(0,80)])

nz = p0[0]*nx**3 + p0[1]*nx**2 + p0[2]*nx + p0[3]

for i in range(0,80):

print("material: $\{\} 0 1 0 \{\}$ ".format(nz[i], i))

#end_python:

#material: 10 10 1 $0~{\rm pp}$

#cylinder: 0.7 0.2 0 0.7 0.2 0.005 0.025 pp

#cylinder: 0.6 0.4 0 0.6 0.4 0.005 0.025 pp

#cylinder: 0.65 0.3 0 0.65 0.3 0.005 0.025 pp

#cylinder: 0.55 1 0 0.55 1 0.005 0.025 pp

#cylinder: 0.3 1.3 0 0.3 1.3 0.005 0.025 pp

#cylinder: 0.45 0.4 0 0.45 0.4 0.005 0.025 pp

#cylinder: 0.25 1 0 0.25 1 0.005 0.025 pp

#cylinder: 0.75 1.7 0 0.75 1.7 0.005 0.025 pp

#cylinder: 0.4 0.7 0 0.4 0.7 0.005 0.025 pp
#waveform: gaussiandot 1 1e9 mypulse
#hertzian_dipole: z 0.8 0.1 0 mypulse
#rx: 0.8 0.105 0
#src_steps: 0 0.02 0
#rx_steps: 0 0.02 0

Text S3: gprMax input file for Model 2, Figure 2

#domain: 1 $2\ 0.005$

 $#dx_dy_dz: 0.005 0.005 0.005$

#time_window: 3000

#python:

import numpy as np

p0 = [-37.5000, 30.0000, 2.0000]

nx=np.array([i/100 for i in range(0,80)])

```
nz=p0[0]*nx**3 + p0[1]*nx**2 + p0[2]*nx + p0[3]
```

for i in range(0,80):

print("material: $\{\} 0 1 0 \{\}$ ".format(nz[i], i))

:

 $\#end_python:$

#material: 10 10 1 $0~{\rm pp}$

#cylinder: 0.7 0.2 0 0.7 0.2 0.005 0.025 pp

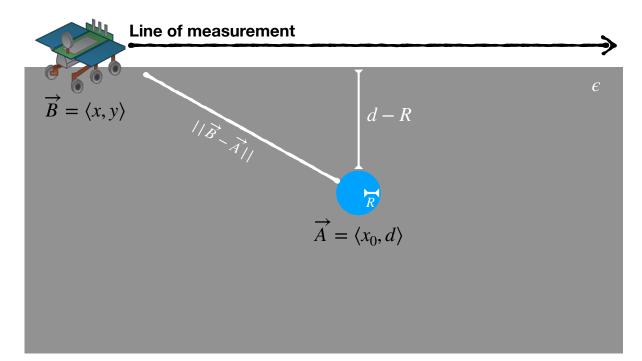
X - 6

#cylinder: 0.6 0.4 0 0.6 0.4 0.005 0.025 pp
#cylinder: 0.65 0.3 0 0.65 0.3 0.005 0.025 pp
#cylinder: 0.55 1 0 0.55 1 0.005 0.025 pp
#cylinder: 0.3 1.3 0 0.3 1.3 0.005 0.025 pp
#cylinder: 0.45 0.4 0 0.45 0.4 0.005 0.025 pp
#cylinder: 0.25 1 0 0.25 1 0.005 0.025 pp
#cylinder: 0.75 1.7 0 0.75 1.7 0.005 0.025 pp
#cylinder: 0.4 0.7 0 0.4 0.7 0.005 0.025 pp
#waveform: gaussiandot 1 1e9 mypulse
#hertzian_dipole: z 0.8 0.1 0 mypulse
#rx: 0.8 0.105 0
#src_steps: 0 0.02 0

#rx_steps: 0 0.02 0

February 5, 2021, 7:36pm

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Figure S1. A typical hyperbola-fitting scenario with a cylindrical target with radius R buried in a homogeneous half-space with electric permittivity ϵ . The vector positions of the center of the target and the antenna are $\overrightarrow{A} = \langle x_0, d \rangle$ and $\overrightarrow{B} = \langle x, y \rangle$ respectively. The distance between the antenna and the surface of the target equals with $||\overrightarrow{A} - \overrightarrow{B}|| - R$.

February 5, 2021, 7:36pm

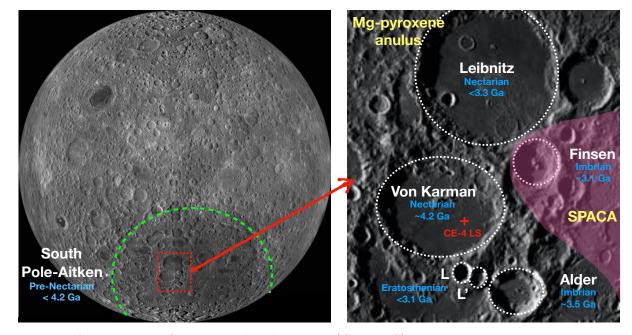


Figure S2. The Chang'E-4 landing site (CE-4 LS) -indicated with red cross- at Von Kármán (VK) crater at 44.45°S, 176.3°E. The Leibnitz crater (Nectarian age) has shaped the north part of the VK crater and provided the initial ejecta layer on top of the brecciated bedrock. VK crater was then flooded with basalts during Imbrium after the creation of Aldrer crater. During the late Imbrium and early Eratosthenian, the craters Finsen, VK L and L' were formed and provided the main ejecta materials on the top surface of VK. All the aforementioned craters are within the Mg-rich anulus while Finsen is at the SPACA zone (pink area). The dates are based on (Lu et al., 2021). The images are available from the Lunar Reconnaissance Orbiter's Wide Angle Camera. Image Credit: NASA, GSFC, Arizona State Univ. Lunar Reconnaissance Orbiter, available at https://apod.nasa.gov/apod/ap161230.html.

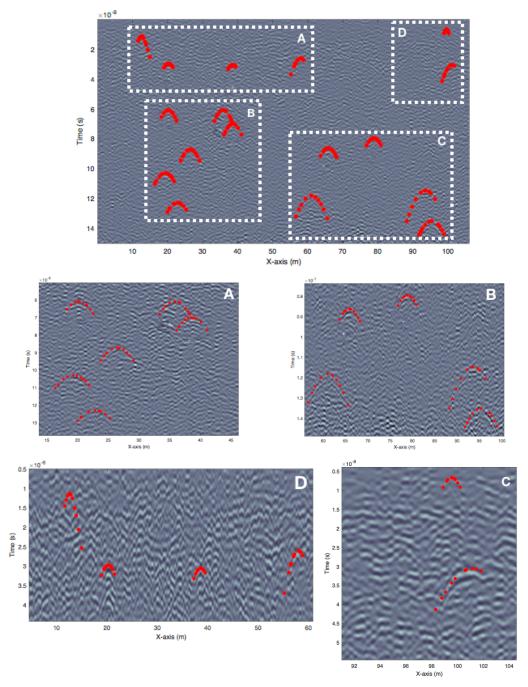


Figure S3. The processed B-Scan using the high frequency LPR antenna from the Yutu-2 rover. With red circles are the fitted hyperbolas for the layered structure illustrated in Figure 3_A in the manuscript. The Chang'E-4 Lunar Penetrating Radar data are available from the Data Publishing and Information Service System of China Lunar Exploration Program http://moon.bao.ac.cn/searchOrder_dataSearchData.search.

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