

# $\Delta\text{O}_2/\text{N}_2'$ as a Tracer of Mixed Layer Net Community Production: Theoretical Considerations and Proof-of-Concept

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## Abstract

The biological oxygen ( $\text{O}_2$ ) saturation anomaly  $\Delta\text{O}_2/\text{Ar}$  is a tracer for net community production (NCP) in marine surface waters, with argon (Ar) normalization used to correct for physical effects on  $\text{O}_2$  supersaturation. Ship-board mass spectrometry has been used for  $\Delta\text{O}_2/\text{Ar}$  measurements, but this approach may not be accessible to many research groups. Here, we present a proof-of-concept for NCP estimates based on underway measurements of  $\Delta\text{O}_2/\text{N}_2$ , which can be obtained from deployments of  $\text{O}_2$ -Optodes and gas tension devices (GTD). We used a one-dimensional mixed layer model, validated against field observations, to evaluate divergence in  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}/\text{N}_2$  resulting from differences in the sensitivity of Ar and nitrogen ( $\text{N}_2$ ) to various physical processes. Changes in sea surface temperature and responses in air-sea exchange most strongly decouple surface Ar and  $\text{N}_2$  with additional excess  $\text{N}_2$  associated with bubble-injection during high-wind conditions and vertical mixing in regions of elevated subsurface  $\text{N}_2$ . In contrast, biological  $\text{N}_2$ -fixation has a negligible contribution to the observed divergence between Ar and  $\text{N}_2$ . Based on readily available environmental data, we present an approach to correct for Ar and  $\text{N}_2$  differences, yielding a new tracer,  $\text{N}_2'$ , that is a near analog of Ar. We show that  $\Delta\text{O}_2/\text{N}_2'$  provides an excellent approximation to  $\Delta\text{O}_2/\text{Ar}$ , and that uncertainty and biases in  $\Delta\text{O}_2/\text{N}_2'$  are small relative to other errors in NCP calculations. Our results demonstrate the potential for  $\Delta\text{O}_2/\text{N}_2'$  measurements to expand NCP estimates from oceanographic research surveys, vessels of opportunity or autonomous surface vehicles.

# **$\Delta\text{O}_2/\text{N}_2'$ as a Tracer of Mixed Layer Net Community Production: Theoretical Considerations and Proof-of-Concept**

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## **Key Points:**

- Numerical simulations are used to evaluate physically-induced changes in mixed layer  $\text{N}_2$  and Ar saturation from environmental forcing data
- A new tracer,  $\text{N}_2'$ , is derived, using simple computations to correct for differential physical effects on  $\text{N}_2$  and Ar saturation
- $\Delta\text{O}_2/\text{N}_2'$  is shown to be an excellent alternative to  $\Delta\text{O}_2/\text{Ar}$  for calculations of surface net community production

## Abstract

The biological oxygen ( $O_2$ ) saturation anomaly ( $\Delta O_2/Ar$ ) is a tracer for net community production (NCP) in marine surface waters, with argon (Ar) normalization used to correct for physical effects on  $O_2$  supersaturation. Ship-board mass spectrometry has been used for  $\Delta O_2/Ar$  measurements, but this approach may not be accessible to many research groups. Here, we present a proof-of-concept for NCP estimates based on underway measurements of  $\Delta O_2/N_2$ , which can be obtained from deployments of  $O_2$ -Optodes and gas tension devices (GTD). We used a one-dimensional mixed layer model, validated against field observations, to evaluate divergence in  $\Delta O_2/Ar$  and  $\Delta O_2/N_2$  resulting from differences in the sensitivity of Ar and nitrogen ( $N_2$ ) to various physical processes. Changes in sea surface temperature and responses in air-sea exchange most strongly decouple surface Ar and  $N_2$ , with additional excess  $N_2$  associated with bubble-injection during high-wind conditions and vertical mixing in regions of elevated subsurface  $N_2$ . In contrast, biological  $N_2$ -fixation has a negligible contribution to the observed divergence between Ar and  $N_2$ . Based on readily available environmental data, we present an approach to correct for Ar and  $N_2$  differences, yielding a new tracer,  $N_2'$ , that is a near analog of Ar. We show that  $\Delta O_2/N_2'$  provides an excellent approximation to  $\Delta O_2/Ar$ , and that uncertainty and biases in  $\Delta O_2/N_2'$  are small relative to other errors in NCP calculations. Our results demonstrate the potential for  $\Delta O_2/N_2'$  measurements to expand NCP estimates from oceanographic research surveys, vessels of opportunity or autonomous surface vehicles.

## Plain Language Summary

Marine net community production, NCP, represents the difference between biological oxygen ( $O_2$ ) production through photosynthesis and  $O_2$  consumption through respiration. This quantity reflects the ocean's capacity to support marine life and remove carbon dioxide from the atmosphere. One common approach to estimate NCP employs mass spectrometry to measure the oxygen-to-argon ratio ( $\Delta O_2/Ar$ ) in surface seawater. Since Ar is biologically inert and has similar physical properties to  $O_2$ , this approach is used to examine marine biological production. However, the instrumentation required to measure  $\Delta O_2/Ar$  is expensive and requires significant technical oversight, thus limiting the coverage of observations. Here, we use simple numerical simulations to show that NCP can be accurately derived from the seawater  $O_2$ -to-nitrogen ratio ( $\Delta O_2/N_2$ ). We derive a new term,  $\Delta O_2/N_2'$ , that corrects for small differences between  $\Delta O_2/N_2$  and  $\Delta O_2/Ar$  resulting from the enhanced sensitivity of  $N_2$  to bubbles, seawater temperature changes and mixing effects. NCP calculated from  $\Delta O_2/N_2'$  provides an excellent alternative to  $\Delta O_2/Ar$ -based estimates, and uncertainty in  $\Delta O_2/N_2'$  is low relative to other error sources in NCP calculations. As  $\Delta O_2/N_2$  can be measured autonomously at sea with simple instrumentation, our results demonstrate the potential to expand coverage of NCP estimates from a variety of sampling platforms.

## 1 Introduction

Net community production (NCP) quantifies the balance between gross photosynthetic production and community-wide respiration, and serves as an important metric of the metabolic state of an ocean region. Integrated over seasonal timescales, NCP constrains upper limits on marine biomass production and carbon export from the ocean surface via the biological pump.

As such, the spatial and temporal distribution of marine NCP has significant implications for food web dynamics and global biogeochemical cycles. To understand and predict the response of marine systems to future environmental change, it is therefore important to quantify NCP on ecologically-relevant time and space scales.

An increasingly common approach for deriving oceanic NCP estimates at high spatial resolution employs ship-based mass spectrometry to obtain underway measurements of the seawater oxygen-to-argon ratio ( $O_2/Ar$ ). This approach relies on the nearly identical solubility properties of  $O_2$  and its biologically-inert analog Ar, which make  $O_2/Ar$  largely insensitive to temperature or salinity-dependent solubility changes, or bubble injection processes (Craig & Hayward, 1987; Fig. S1). The biological saturation anomaly ( $\Delta O_2/Ar$ , Eq. 1) thus provides a specific tracer for net biological  $O_2$  production, and can be derived by normalizing measured  $O_2/Ar$  ( $[O_2/Ar]_{sw}$ ) to the seawater equilibrium ratio ( $[O_2/Ar]_{eq}$ ).

$$\Delta O_2/Ar = \left( \frac{[O_2/Ar]_{sw}}{[O_2/Ar]_{eq}} - 1 \right) \cdot 100 \% \quad (1)$$

Net community production is then equated to the air-sea flux of biologically-produced excess  $O_2$  (i.e. the “bioflux” of  $\Delta O_2/Ar \cdot [O_2]_{eq}$ ; Jonsson et al., 2013; Kaiser et al., 2005; Teeter et al., 2018). This approach has been applied to obtain broad spatial coverage of NCP estimates from ship-based surveys, thus improving our understanding of marine carbon cycling (e.g. Hamme et al., 2012; Howard et al., 2010; Izett et al., 2018; Juranek et al., 2019; Lockwood et al., 2012; Rosengard et al., 2020; Tortell et al., 2015; Ulfso et al., 2014). However, the expense of mass spectrometers and the technical expertise required to run these instruments may be prohibitive to some research groups. Additionally, mass spectrometers can have significant power consumption requirements and are generally not capable of fully-autonomous deployments, thus limiting their use to scientific research vessels with dedicated infrastructure and personnel. Truly autonomous gas measurements on ships of opportunity, or in-situ platforms such as autonomous surface vehicles (e.g. Saildrone), would significantly expand the global coverage of NCP estimates from underway surveys, helping to integrate these measurements with a growing suite of autonomous biogeochemical and ecological observations (Gordon et al., 2020; Johnson et al., 2017; Mordy et al., 2017; Pelland et al., 2018; Plant et al., 2016; Yang et al., 2017).

The development of  $O_2$  Optodes (Tengberg et al., 2006) and Gas Tension Devices (GTDs; McNeil et al., 2006a; Reed et al., 2018) capable of stable, accurate measurements during extended in-situ deployments provides new opportunities for autonomous NCP surveys. Using observations of  $O_2$  from the Optode and the seawater total dissolved gas pressure (i.e. the sum of all gas partial pressures) from the GTD, it is possible to obtain estimates of seawater nitrogen ( $N_2$ ) concentrations (McNeil et al., 1995). Nitrogen has roughly similar physical properties to  $O_2$  (i.e. salinity and temperature solubility dependence; Fig. S1), such that NCP could, in principle, be approximated from  $N_2$ -based calculations of the biological  $O_2$  saturation anomaly (i.e.  $\Delta O_2/N_2$ , following Eq. 1).

To date,  $O_2$  and  $N_2$  measurements have been combined to estimate NCP time-series from Optode and GTD deployments on moorings and/or floats (e.g. Bushinsky & Emerson, 2015; Emerson & Stump, 2010; Weeding & Trull, 2014; Yang et al., 2017). These applications employ simultaneous observations of sea surface temperature, salinity and wind speed to estimate the contribution of physical processes driving changes in  $O_2$  solubility, thereby isolating a biological signature of NCP without the need for Ar or  $N_2$  normalization. In these studies, mooring-based

N<sub>2</sub> measurements are commonly used to estimate the effects of physical processes on the mixed layer O<sub>2</sub> budget, most importantly air-sea flux via bubbles (Emerson et al., 2019). Thus far, direct estimates of NCP from O<sub>2</sub> and N<sub>2</sub> measurements have only been obtained from ship-based depth profiles (McNeil et al., 2006b) or in-ice measurements (Zhou et al., 2014). To our knowledge, no previous work has derived NCP from underway surface  $\Delta\text{O}_2/\text{N}_2$ , although Tortell et al. (2015) used simultaneous O<sub>2</sub>/N<sub>2</sub> and O<sub>2</sub>/Ar data to describe physical and biological controls on O<sub>2</sub> across various hydrographic regimes in the Southern Ocean.

A key challenge in the use of  $\Delta\text{O}_2/\text{N}_2$  measurements as an NCP tracer is accounting for divergences in mixed layer  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2$  resulting from the slightly different solubility properties of Ar and N<sub>2</sub> (Fig. S1). Nitrogen is less soluble in water than O<sub>2</sub> and Ar, and is therefore more susceptible to bubbled-induced supersaturation (Craig & Hayward, 1987; Weiss, 1970; Woolf & Thorpe, 1991). Moreover, small differences in the temperature-sensitivity of O<sub>2</sub>/Ar and O<sub>2</sub>/N<sub>2</sub> induce differential responses to surface warming or cooling. Finally, N<sub>2</sub>, unlike Ar, is not entirely inert, as its concentration can be altered by N<sub>2</sub>-fixation, denitrification, and annamox. If differences between Ar and N<sub>2</sub> supersaturation anomalies ( $\Delta\text{Ar}$  and  $\Delta\text{N}_2$ , respectively) are sufficiently large and unaccounted for, interpretations of NCP estimated from  $\Delta\text{O}_2/\text{N}_2$  could be biased, with significant implications for the interpretation of oceanic net tropic status and metabolic state.

The primary goal of this article is to demonstrate the utility of  $\Delta\text{O}_2/\text{N}_2$  measurements as an alternative to  $\Delta\text{O}_2/\text{Ar}$  for NCP estimates. We present simulations from a simple one-dimensional model, validated against in-situ N<sub>2</sub> and O<sub>2</sub> measurements, to evaluate differences between  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2$  resulting from  $\Delta\text{Ar}$  and  $\Delta\text{N}_2$  divergence in surface waters. Based on the simulations, we tested a framework for predicting these differences from readily-available environmental data, and derived a new tracer, N<sub>2</sub>' ("N<sub>2</sub>-prime"), which accounts for excess  $\Delta\text{N}_2$  relative to  $\Delta\text{Ar}$ . We conclude by evaluating the uncertainty in NCP calculations based on  $\Delta\text{O}_2/\text{N}_2'$  measurements. Our results demonstrate the potential for underway, ship-based observations of  $\Delta\text{O}_2/\text{N}_2$  (and derived  $\Delta\text{O}_2/\text{N}_2'$ ) to expand coverage of NCP estimates in oceanic waters. In the supporting information (SI), we provide details and software code for the application of the N<sub>2</sub>' approach to field surveys. In related articles (Izett & Tortell, 2020) we describe an underway measurement system for ship-board O<sub>2</sub>/N<sub>2</sub> surveys, and provide a field-validation of the approach proposed here (manuscript in preparation).

## 2 Methods

### 2.1 One-dimensional mixed layer physical gas model

We developed a simple one-dimensional mixed layer box model to evaluate mechanisms driving the divergence between  $\Delta\text{Ar}$  and  $\Delta\text{N}_2$  under various environmental forcing conditions (i.e.  $\Delta C = (C/C_{\text{eq}} - 1) * 100 \%$ , where  $C_{\text{eq}}$  is the equilibrium solubility concentration at ambient sea level pressure). We also tested an empirical approach for correcting these offsets, which is described in section 2.2. The model predicts the evolution of mixed layer gas concentrations resulting from physical perturbations, including temperature-dependent solubility changes, air-sea exchange, and vertical mixing. The following budget was applied to O<sub>2</sub>, Ar and N<sub>2</sub>:

$$\text{MLD} \cdot \frac{dC}{dt} = F_d + F_B + F_M. \quad (2)$$

Here, MLD is the mixed layer depth,  $dC/dt$  is the change in gas concentration over time,  $F_d$  and  $F_B$  are the air-sea gas exchange fluxes via diffusion and bubbles (from both fully- and partially-collapsing bubbles), respectively, and  $F_M$  represents the sum of diapycnal mixing, upwelling and entrainment of water from below the mixed layer. We employ a two-box domain, with prescribed hydrographic properties in the subsurface and mixed layers (see below). Unless otherwise stated, we excluded biological production of  $O_2$  and  $N_2$  and ignored lateral fluxes (see below).

We used the air-sea exchange parameterization of Liang et al. (2013) in ice-free simulations. For Arctic simulations (fractional ice cover  $>1\%$ ) we excluded explicit bubble fluxes, but scaled bulk gas exchange rates with the fraction of ice-free water following Butterworth & Miller (2016). Net air-sea exchange fluxes differ by less than 5 % between these two parameterizations at winds speeds below  $\sim 10\text{ m s}^{-1}$ , thus justifying our exclusion of bubble processes in waters with  $>1\%$  ice coverage. We note that the time-series of  $N_2$  and Ar predicted by our simulations, and the relative differences between them, will depend on the air-sea diffusion rates of these gases applied in our model domain. The Liang et al. (2013) bubble-mediated flux model is based on Ar diffusion rates which are believed to exceed those of  $N_2$  (Fig. S1). There is, however, some disagreement in the literature, with suggestions that  $N_2$  diffusion may exceed Ar (e.g. Wise & Houghton, 1966). Nonetheless, the results presented here are consistent with the majority of studies describing surface diffusion rates (e.g. see within Wanninkhof, 2014), and the Liang et al. model has been validated for  $N_2$  and other similar gases (Emerson & Bushinsky 2016; and see below, section 3.3). The analyses presented throughout this manuscript are thus based on the assumption that Ar diffusion rates exceed those of  $N_2$ .

The mixing flux term encompasses diapycnal mixing, upwelling and entrainment, and is proportional to the vertical gas gradient (i.e.  $dC/dZ = (C_{\text{deep}} - C_{\text{surf}}) / dZ$ , where  $C_{\text{deep}}$  is the subsurface gas concentration). Terms for these fluxes are derived from a prescribed eddy diffusivity coefficient ( $\kappa_z$ ), Ekman pumping velocity ( $\omega$ , proportional to wind speed; Hartmann, 1994) and the rate of MLD deepening ( $d\text{MLD}/dT$ ), respectively. These parameterizations are described briefly below, with full details presented in section S1 of the SI. Model code for performing simulations is also provided at [doi.org/10.5281/zenodo.4024952](https://doi.org/10.5281/zenodo.4024952).

We performed sensitivity analyses comparing our simulated gas time-series with in-situ observations (see below section 3.3) to determine appropriate parameterizations for the bubble scaling factor,  $\beta$ , and the integration depth scale,  $dZ$ , over which vertical mixing fluxes are estimated.

From these analyses, we found that a bubble flux scaling coefficient,  $\beta$ , of 0.5 produces best results, and is consistent with results from Yang et al. (2017) and Emerson et al. (2019). A vertical mixing depth scale,  $dZ$ , proportional to the thermocline depth, is also most appropriate, but is generally insensitive to small variability (e.g.  $\pm 10\text{ m}$ ). In the experimental simulations,  $dZ$  was set to a constant value (25 m) based on an empirical relationship between MLD and the thermocline depth.

The model was initialized and forced with either real observations or simulated values, as described below. Unless otherwise stated, sea level pressure (SLP), salinity and MLD were held constant, and gas concentrations were initialized at 100 % saturation using the solubility equations of Garcia & Gordon (1993) and Hamme & Emerson (2004). Subsurface Ar ( $\Delta\text{Ar}_{\text{deep}}$ ) was set based on previously published observations, and  $\Delta\text{N}_{2,\text{deep}}$  was varied in each model run

by adjusting subsurface  $\Delta N_2/Ar$  (i.e.  $\Delta N_2/Ar_{deep} = (N_{2,sat,deep} / Ar_{sat,deep} - 1) \cdot 100 \%$ ). Our simulations neglect lateral fluxes as they are generally small in a Eulerian framework, and irrelevant to underway surveys which measure gas concentrations that have been modified along a Lagrangian flow path (Teeter et al., 2018).

### 2.1.1 Model simulations

We performed six simulations with our gas model to examine the main drivers of  $\Delta Ar$  and  $\Delta N_2$  divergence. Table 1 summarizes the different forcing conditions used for these simulations. For all model runs, we performed calculations in 0.25-day time increments, and omitted the first 90 days of output so that the simulated results were independent of initial conditions. Four of the simulations (denoted as ‘experimental’ and named with the prefix ‘Ex’) were designed to represent the impacts of extreme temperature (SST) and wind speed ( $u_{10}$ ) variability in ice-free (runs Ex-IF 1, Ex-IF 2, and Ex-IF 3) and partially ice-covered (run Ex-IC 1) waters. Two additional simulations (denoted as ‘realistic’ and named with the prefix ‘real’) included more realistic environmental forcing, based on in-situ observations at Ocean Station Papa in the Subarctic Pacific (real-OSP) and Baffin Bay (real-BB) in the eastern Arctic, respectively.

In the experimental runs, initial conditions (temperature and salinity profiles) were derived from representative 2019 observations from Ocean Station Papa (50 °N, 145 °W; runs Ex-IF 1–3) and northern Baffin Bay (67 °N, 62.5 °W; Ex-IC 1) (data provided by the Institute of Ocean Sciences, DFO Canada at [www.waterproperties.ca/linep](http://www.waterproperties.ca/linep) and by Amundsen Science Data Collection, 2019 at [www.polardata.ca](http://www.polardata.ca)). To simulate extreme environmental change, we introduced two rapid step-changes in  $u_{10}$  (between 7 and 15 m s<sup>-1</sup>) and SST ( $\pm 4$  °C) based on observed variability in Subarctic NE Pacific and Arctic field studies (R. Izett and P. Tortell unpublished results). Mixed layer depth, salinity, subsurface properties and  $dZ$  were derived from the initial conditions and held constant throughout the run. For each set of conditions, we performed three runs (details in Table 1): (a) no mixing; (b) dampened mixing; (c) full mixing. For runs b and c, we prescribed  $\kappa_Z$  values and scaled  $\omega$  (upwelling velocity) with  $u_{10}$ . Entrainment was set to zero, because the MLD was constant. We set the value of  $\Delta N_2/Ar_{deep}$  to 1.5 % in the experimental simulations based on the observed upper range of  $\Delta N_2/Ar$  just below the mixed layer in most ocean basins (e.g. Hamme et al., 2017, 2019; Hamme & Emerson, 2013; Nicholson et al., 2010). Although subsurface  $\Delta N_2/Ar_{deep}$  can range from <0 % to >2 % (Chang et al., 2010, 2012; Hamme et al., 2019; Shigemitsu et al., 2016), values greater than ~1.5 % are rare outside of tropical and sub-tropical zones impacted by near-surface water column denitrification.

In the realistic simulations,  $u_{10}$  and SST data were obtained from in-situ mooring observations (real-OSP) or gridded reanalysis products (real-BB). In the Subarctic Pacific runs, we approximated a two year cycle (2011–2013) using  $u_{10}$ , SST and SLP data from the NOAA PMEL mooring at OSP (provided by NOAA PMEL at [www.pmel.noaa.gov](http://www.pmel.noaa.gov)). For the Baffin Bay simulations (representing May – October, 2019),  $u_{10}$  data were obtained from the CCMP vector product (provided by Remote Sensing Systems at [www.remss.com/measurements/ccmp/](http://www.remss.com/measurements/ccmp/); Atlas et al., 2011), while SST and sea ice percent-coverage were from the NOAA High Resolution OI Dataset (provided by NOAA ESRL at [psl.noaa.gov](http://psl.noaa.gov); Reynolds et al., 2007) and SLP was from the NCEP/NCAR reanalysis 2 product (provided by NOAA ESRL at [psl.noaa.gov](http://psl.noaa.gov); Kalnay et al., 1996). In both realistic simulations, we applied a time-variable MLD based on density

measurements obtained on the OSP mooring line (real-OSP), or from the NOAA MIMOC mixed layer depth climatology (real-BB; provided by NOAA PMEL at [pmel.noaa.gov/mimoc](http://pmel.noaa.gov/mimoc); Schmidt et al., 2013). We performed two simulation runs representing different mixing scenarios (Table 1), omitting the weak mixing scenario (i.e. run b). In run c of the OSP simulation (i.e. full mixing), we applied time-varied  $\kappa_z$  by extrapolating the results from Cronin et al. (2015) onto our model domain. In real-BB run c, time-variable  $\kappa_z$  was set based on eddy diffusivity values obtained from NEMO model simulations of the Arctic and N. Atlantic (NEMO model simulations described in Castro de la Guardia et al., 2019). Subsurface gases were set based on calculated equilibrium concentrations at the deep temperature and salinity conditions, and from supersaturation anomalies based on archived observations below the MLD in the subarctic Pacific and Labrador Sea (provided at [www.bco-dmo.org](http://www.bco-dmo.org); Hamme et al., 2019). In real-OSP run c,  $\Delta A_{\text{deep}}$  and  $\Delta N_2/A_{\text{deep}}$  were interpolated from observations from multi-year sampling at OSP in February, June and August to the model run time (ranges 0-1 % and 0-0.5 %, respectively). In real-BB run c,  $\Delta A_{\text{deep}}$  and  $\Delta N_2/A_{\text{deep}}$  were held constant 0 % and 0.5 %, respectively. Temperature, salinity and  $O_2$  in the “deep” boxes (i.e. the layer beneath the MLD) were based on observations at the OSP mooring (real-OSP) or from profile measurements and NEMO model output in northern Baffin Bay (real-BB). In the real-OSP and real-BB simulations, we applied biological production terms to the  $O_2$  budget (Eq. 2) based on field observations from the respective regions to better reflect seasonal  $\Delta O_2$  variability (mean annual cycle at OSP from Fassbender et al., 2016 and constant NCP in BB from R. Izett and P. Tortell unpublished results).



**Table 1.** Summary of model simulation conditions. Vertical advection and entrainment fluxes were set to zero in run a of all simulations, and were proportional to wind speed and the rate of MLD deepening in runs b and c, respectively. Initial conditions were obtained from ship-based observations at Ocean Station Papa (OSP) in the Subarctic Pacific, NOAA mooring data at OSP, or ship-based measurements in Baffin Bay (BB). The three numbers listed for SST and  $u_{10}$  correspond with values used during each of three forcing time segments (days 0-12, 12-65, and 65-120 in Fig. 1). In the real-OSP and real-BB run c, we derived time-variable  $\kappa_z$  from Cronin et al. (2015) and NEMO model simulations, respectively, while  $\Delta N_2/\text{Ar}_{\text{deep}}$  was based on archived values from Hamme et al. (2019). Both terms were set to zero in run a of the realistic simulations. We did not perform intermediate mixing scenarios (i.e. run b) for the realistic simulations. The results of these simulations are shown in Figs. 2-4.

Simulation (duration)	deep & initial conditions	Forcing				Mixing	
		SST [°C]	$u_{10}$ [m s <sup>-1</sup> ]	ice [%]	SLP [mbar]	$\kappa_z$ [m <sup>2</sup> s <sup>-1</sup> ]	$\Delta N_2/\text{Ar}_{\text{deep}}$ [%]
<b>Ex-IF 1</b> (120 days)	OSP profile	10, 10, 10	7, 15, 7	0	1013.25		
<b>Ex-IF 2</b> (120 days)	OSP profile	10, 14, 10	7, 7, 7	0	1013.25	Run a: 0 Run b: $10^{-5}$ Run c: $10^{-4}$	Run a: 0 Run b: 1.5 Run c: 1.5
<b>Ex-IF 3</b> (120 days)	OSP profile	6, 10, 14	7, 15, 7	0	1013.25		
<b>Ex-IC 1</b> (120 days)	BB profile	0, 4, 8	7, 15, 7	50	1013.25		
<b>real-OSP</b> (Jan. 2011- Jan. 2013)	NOAA OSP mooring profile	NOAA OSP mooring	NOAA OSP mooring	0	NOAA OSP mooring	Run a: 0 Run c: Cronin	Run a: 0 Run c: Hamme
<b>real-BB</b> (May – Oct. 2019)	BB profile	NOAA OI SST product	CCMP product	NOAA OI ice product	NCEP/ NCAR reanalysis	Run a: 0 Run c: NEMO	Run a: 0 Run c: 0.5

## 2.2 Derivation of $N_2'$

Based on our simulations, we developed a framework to reconcile the differences between surface water  $\Delta O_2/\text{Ar}$  and  $\Delta O_2/\text{N}_2$  resulting from differential solubility effects and physical fluxes of Ar and  $\text{N}_2$ . From this analysis, we derived a new tracer,  $N_2'$  (“ $\text{N}_2$ -prime”) that corrects for these differences and provides an Ar analog. For this approach, we used a slightly simplified version of the gas budget described in Eq. 2 to predict the difference between  $\Delta N_2$  and  $\Delta \text{Ar}$  occurring over a timescale relevant to NCP calculations. We then subtracted this estimated offset from  $\Delta N_2$  derived from the full model simulations. We modified Eq. 2 by combining all vertical mixing processes into a single term, expressing the rates of diapycnal mixing and advection with a single coefficient,  $\kappa$ . We excluded entrainment from the simplified budget because temporal variability in MLD (i.e.  $d\text{MLD}/dt$ ) cannot be estimated readily from ship-based sampling. The simplified budget is represented by:

$$\text{MLD} \cdot \frac{dC}{dt} = F_d + F_C + F_P + \frac{C_{\text{deep}} - C}{dz} \kappa \quad (3)$$

where  $F_d$ ,  $F_C$  and  $F_P$  are the diffusive, small bubble and large bubble air-sea exchange fluxes, as described above. We evaluated this budget for Ar and  $N_2$  over one mixed layer  $O_2$  re-equilibration timescale,  $\tau_{O_2}$  (defined in section 3.1.2, Eq. 6, and derived in section S1 of the SI), prior to each calculation derived from the full model simulations. As in the full simulations, we set the starting gas concentrations to equilibrium values (i.e.  $C(t-\tau_{O_2}) = C_{\text{eq}} \frac{SLP}{1 \text{ atm}}$ ) and performed calculations in 0.25-day increments. The same environmental data used to force the full model simulations (i.e.  $u_{10}$ , SST and SLP) were applied in Eq. 3. Finally, we obtained  $\Delta N_2'$  by subtracting the derived difference between  $\Delta Ar$  and  $\Delta N_2$  ( $\Delta N_2^{\text{est}} - \Delta Ar^{\text{est}}$ ) from the corresponding  $\Delta N_2$  value predicted by the full model ( $\Delta N_2^{\text{true}}$ )

$$\Delta N_2' = \Delta N_2^{\text{true}} - (\Delta N_2^{\text{est}} - \Delta Ar^{\text{est}}) \quad (4)$$

and recalculated  $\Delta O_2/N_2'$  from  $\Delta N_2'$  following Eq. 1.

In field studies,  $\Delta N_2^{\text{true}}$  will be the measured value, and  $\Delta N_2^{\text{est}}$  and  $\Delta Ar^{\text{est}}$  will be values predicted by the simplified gas budget (Eq. 3) using environmental data over one  $\tau_{O_2}$  before observations. An example of the approach is presented in the SI (Fig. S2). Whereas estimates of  $u_{10}$ , SST and SLP over  $\tau_{O_2}$  can be obtained from readily available reanalysis products, the time-histories of MLD, surface salinity, and sub-surface conditions are more difficult to estimate. For compatibility with field studies, we therefore fixed these terms (MLD, salinity, deep temperature, deep salinity,  $\kappa$ ,  $\Delta N_2/Ar_{\text{deep}}$ ) over  $\tau_{O_2}$  at values corresponding with the time of  $\Delta N_2^{\text{true}}$  (i.e. the time of in-situ sampling during field sampling). Moreover, given the paucity of in-situ subsurface noble gas measurements, we set  $\Delta Ar_{\text{deep}}$  to 0 % in all  $N_2'$  calculations, and held  $\Delta N_2/Ar_{\text{deep}}$  constant at values from the full model run corresponding with the time of  $\Delta N_2^{\text{true}}$ . In section 3.4.3, we evaluate errors in  $\Delta N_2'$  and  $\Delta O_2/N_2'$  resulting from these simplifying assumptions.

### 3 Results and Discussion

Differences between mixed layer  $\Delta O_2/Ar$  and  $\Delta O_2/N_2$  are most simply represented using the term  $\Delta N_2/Ar$  (i.e.  $([N_2/Ar]/[N_2/Ar]_{\text{eq}} - 1) \cdot 100 \%$ ), which is not sensitive to  $\Delta O_2$ , and thus not dependent on biological  $O_2$  production in our modeling framework (Figs. S3, S6). Our experimental simulations (Ex-IF and Ex-IC; section 3.1) were designed to evaluate the effects of different physical factors on  $\Delta N_2/Ar$ , including bubble-mediated and diffusive gas transfer, vertical mixing and sea ice cover. The realistic simulations (real-OSP and real-BB; section 3.2) allowed us to evaluate the combined influence of these processes, and test our  $N_2'$  framework under typical oceanographic conditions. Below, we discuss the relative effects of different processes on gas variability, present a validation of the model against field observations, and show that our  $N_2'$  approach can correct for most of the difference between  $\Delta N_2$  and  $\Delta Ar$  saturation. We conclude by evaluating  $\Delta O_2/N_2'$  as an NCP tracer and identifying the main sources of uncertainty associated with the use of this approach. In a subsequent paper, we will present a field validation of  $\Delta O_2/N_2'$  measurements for NCP derivation. The SI of the present manuscript contains details and annotated software scripts for applying the  $N_2'$  approach to field data (section S3).

### 3.1 Mixed layer model experimental simulation results

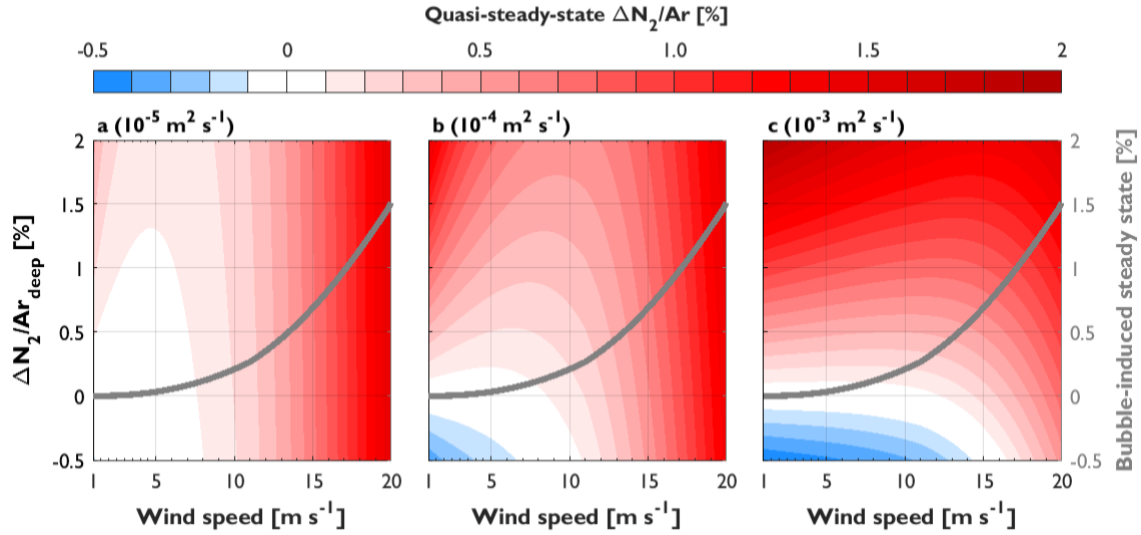
A quasi-steady-state condition can be predicted from the MLD budget described in Eq. 3. Analysis of these conditions in our model reveals that bubble processes, mediated by sustained high wind speeds, can induce the largest  $\Delta N_2/Ar$  disequilibria, with values potentially exceeding 1.5 % at  $u_{10}$  of 20 m s<sup>-1</sup> (Fig. 1). Notably, elevated wind speeds always produce positive  $\Delta N_2/Ar$  (i.e.  $\Delta N_2 > \Delta Ar$  and  $\Delta O_2/Ar > \Delta O_2/N_2$ ), because of the lower solubility of N<sub>2</sub> relative to Ar (Fig. S), and its greater sensitivity to small bubble injection (Hamme et al., 2019; Liang et al., 2013). However, the bubble effect can be either dampened or enhanced by vertical mixing processes, such that the quasi-steady-state value of  $\Delta N_2/Ar$  represents the relative influence of bubble processes and sustained mixing, which may increase or decrease  $\Delta N_2/Ar$ , depending on  $\Delta N_2/Ar_{deep}$ . The role of these two processes is reflected in the equation for the quasi-steady-state gas concentration,  $C_{ss}$ , derived in section S1 of the SI from the analytical solution to the N<sub>2</sub>' MLD gas budget (Eq. 3):

$$C_{ss} = \frac{k_T C_{eq} (1 + \Delta_{eq}) \frac{SLP}{1 atm} + \frac{\kappa}{dz} C_{deep}}{k_T + \frac{\kappa}{dz}}. \quad (5)$$

Here,  $k_T$  is the combined  $u_{10}$ -dependent diffusive and bubble-mediated exchange velocity, and  $\Delta_{eq}$  is the bubble-induced steady-state supersaturation anomaly. Evaluating Eq. 5 for Ar and N<sub>2</sub> enables derivation of the quasi-steady-state  $\Delta N_2/Ar$  value.

As shown in Fig. 1, surface  $\Delta N_2/Ar$  depends, to first order, on  $u_{10}$ , vertical mixing rates and the value of  $\Delta N_2/Ar$  below the mixed layer. As rates of vertical mixing increase and/or  $\Delta N_2/Ar_{deep}$  decreases, bubble effects are dampened. For example, for  $\kappa$  and  $\Delta N_2/Ar_{deep}$  values of 10<sup>-3</sup> m<sup>2</sup> s<sup>-1</sup> and -0.5 %, respectively, our model predicts negative quasi-steady-state  $\Delta N_2/Ar$  across a range of wind speeds ( $u_{10} < 15$  m s<sup>-1</sup>). Without vertical mixing,  $\Delta N_2/Ar$  is set by the relative bubble-induced supersaturation states,  $\Delta_{eq}$ , of N<sub>2</sub> and Ar (grey lines in Fig. 1), while in the absence of bubble processes, the quasi-steady-state  $\Delta N_2/Ar$  falls between  $\Delta N_2/Ar_{deep}$  and zero, depending on the strength of mixing (evaluate Eq. 5 for  $\Delta_{eq}$  set to 0 %). This analysis illustrates the importance of bubble processes and vertical mixing in setting baseline  $\Delta N_2/Ar$  in marine surface waters.

As described below, variability in  $u_{10}$ , SST and mixing strength on shorter time-scales (i.e. days) can induce significant transient signals in  $\Delta N_2/Ar$ . In contrast, atmospheric pressure alters all gas saturation states equally, such that SLP variability has no effect on  $\Delta N_2/Ar$  (Hamme et al., 2019).



**Figure 1.** The combined effects of wind speed and mixing on steady-state  $\Delta N_2/Ar$  derived from model simulations. Colour scaling represents the quasi-steady-state surface  $\Delta N_2/Ar$  predicted by our model at SST and salinity values of 10 °C, and 34 PSU, respectively, based on equations presented in section S1.2 of the SI. The thick grey line represents the average bubble-induced steady-state condition (i.e. proportional to  $\Delta_{eq,N_2}/\Delta_{eq,Ar}$ ) without mixing over a range of SST (0–25 °C). Panels represent a gradient from weakest (a) to strongest (c) mixing, with values of the mixing coefficient,  $\kappa$ , given at the top left of each panel.

### 3.1.1 Effects of variable wind speed, temperature and sea ice coverage

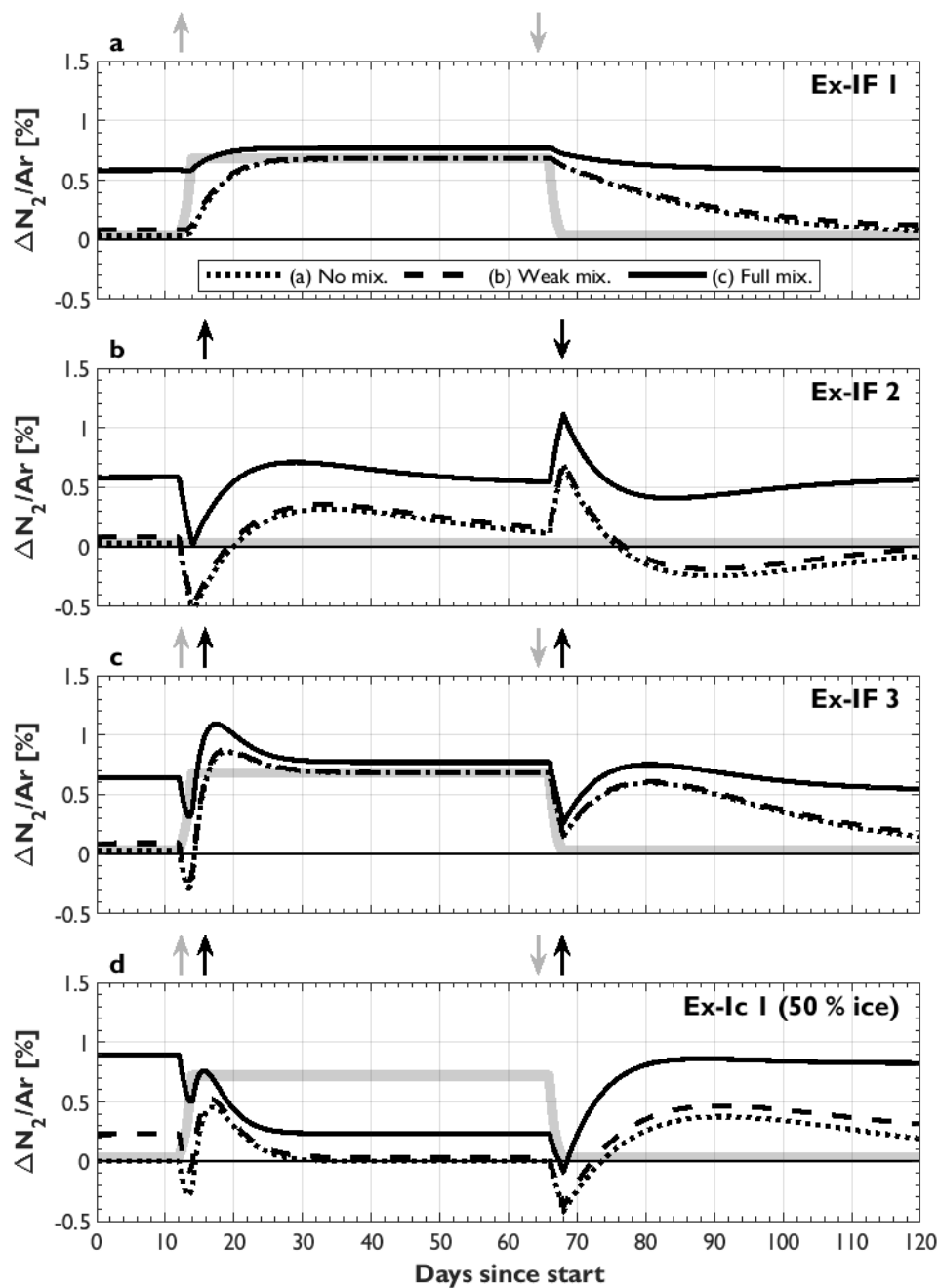
In practice, the ocean mixed layer rarely exists in a steady-state condition, and it is thus necessary to understand the dynamic response of mixed layer gases to transient physical perturbations. We used our experimental simulations to examine the response of  $\Delta N_2/Ar$  to rapid changes in  $u_{10}$  (Ex-IF 1, 3, 4), SST ( $\Delta SST$ ; Ex-IF 2, 3, 4) and sea ice cover (Ex-IC 1). In these simulations,  $u_{10}$  variability induces large responses in surface  $\Delta N_2/Ar$  resulting from bubble processes, with the rate of re-equilibration to steady-state values also depending on  $u_{10}$  (Fig. 2a, c). In our simulations without mixing or rapid SST changes (Ex-IF 1a; Fig. 2a), the maximum  $\Delta N_2/Ar$  was  $\sim 0.7\%$  at a wind speed of  $15\text{ m s}^{-1}$ , but values can exceed  $1.5\%$  for speeds  $>20\text{ m s}^{-1}$  (Fig. 1).

Temperature changes can enhance or dampen  $\Delta N_2/Ar$  disequilibria by affecting gas saturation states over both long (i.e. seasonal) and shorter (days to weeks) time-scales (e.g. Emerson & Stump, 2010; Hamme et al., 2019; Hamme & Emerson, 2002; Hamme & Severinghaus, 2007; Steiner et al., 2007). If air-sea exchange rates are low, temperature-driven  $\Delta N_2/Ar$  disequilibrium can persist for extended periods, while rapid  $\Delta SST$  or periodic elevated wind events induce near-instantaneous disturbances in  $\Delta N_2/Ar$ , preventing gases from reaching steady-state values. In the absence of mixing, gas supersaturation anomalies will increase (decrease) if the rate of warming (cooling) exceeds the rate of re-equilibration via air-sea exchange. While bubble processes only produce positive  $\Delta N_2/Ar$ , temperature changes can lead to negative  $\Delta N_2/Ar$  (i.e.  $\Delta O_2/Ar < \Delta O_2/N_2$ ). Such SST effects occur through two mechanisms, which are represented in the Ex-IF 2 and Ex-IF 3 simulations (Fig. 2b, c). The first is a transient

response to rapid warming (day 12), which causes  $\Delta\text{Ar}$  to increase more than  $\Delta\text{N}_2$  as a result of the greater SST-dependent solubility of Ar (Fig. S1a). Subsequently, as SST stabilizes, and/or ventilation rates increase, the sign of  $\Delta\text{N}_2/\text{Ar}$  reverses (i.e.  $\Delta\text{N}_2 > \Delta\text{Ar}$ ; days 20-65), as Ar re-equilibrates more rapidly via diffusive air-sea exchange (Fig. S1c). Conversely,  $\Delta\text{N}_2/\text{Ar}$  can increase transiently following rapid cooling (Fig. 2b, days 65-68), before air-sea exchange effects dominate once again to produce values lower than steady-state conditions. This response is attributable to the greater cooling-induced increase in Ar solubility, followed by faster Ar re-equilibration (Fig. 2b, >day 68), resulting in  $\Delta\text{Ar} > \Delta\text{N}_2$  and potentially negative  $\Delta\text{N}_2/\text{Ar}$ .

Temperature effects can persist for long time-periods if air-sea exchange is weak (Fig. 2b-d; >day 75) or if SST continues to change steadily. Notably, rapid warming (cooling) will not always produce transiently negative (positive)  $\Delta\text{N}_2/\text{Ar}$ , as the resulting gas perturbation depends on the magnitude of  $\Delta\text{SST}$ , prior gas conditions, and other gas fluxes (e.g. vertical mixing; section 3.1.2). For example, during the second warming event in Ex-IF3 (Fig. 2c, day 65)  $\Delta\text{N}_2/\text{Ar}$  remains positive, but decreases, since prior values were near the  $u_{10}$ -dependent quasi-steady-state condition. This scenario may be more likely in real conditions, as  $\Delta\text{N}_2/\text{Ar}$  is often positive in oceanic surface waters (see section 3.2 below).

In simulations conducted with partial ice cover (50 %; Ex-IC), the presence of ice dampened  $u_{10}$  effects and accentuated SST controls on gas saturation states (Fig. 2d). The effects of  $\Delta\text{SST}$  persisted for significantly longer in ice-covered conditions due to reduced ventilation rates. Moreover, gases approached 100 % saturation, rather than the bubble-induced supersaturation states (grey line in Fig. 2d). The exact response depends on the gas exchange model employed and the fraction of ice cover but a sensitivity analysis with different gas exchange parameterizations (Butterworth & Miller, 2016; Islam et al., 2016; Loose et al., 2014) produced the same general results, albeit with slightly variable re-equilibration times (not shown). Our results thus reproduce the expected effects of sea ice dampening of gas exchange, and the persistence of gas disequilibria caused by other physical factors (DeGrandpre et al., 2020; Manning et al., 2017). The suppression of bubble effects under ice-covered conditions (Nilsson et al., 2001) reflects the reduction in sea states and wave breaking activity (Liang et al., 2017; Voermans et al., 2019; Woolf & Thorpe, 1991). Under partial or full ice-cover, other physical processes are therefore more significant in generating mixed layer  $\Delta\text{N}_2/\text{Ar}$  disequilibria (see section 3.2). These results demonstrate the potential impact of sea ice dynamics in driving  $\text{O}_2$ , Ar and  $\text{N}_2$  saturation anomalies. Future work should characterize the contributions of ice formation or melt to  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2$  deviations.



**Figure 2.** Results from model simulations showing derived  $\Delta N_2/Ar$  under different experimental perturbations. The three black lines in each panel represent the different mixing scenarios (described in panel a), and the thick light grey lines depict expected steady-state  $\Delta N_2/Ar$  values resulting from bubble-induced supersaturation in each model run (grey lines in Fig. 1). Arrows above the panels represent step changes of increasing (up arrow) or decreasing (down arrow) wind speed (light grey) and SST (black). Details of imposed experimental conditions are presented in Table 1. The first three panels present simulations for ice-free conditions, while the bottom panel presents results with simulations containing 50% ice cover.

### 3.1.2 The role of vertical mixing

The results from our simulations excluding vertical mixing (run a) are consistent with Hamme & Emerson (2002) who demonstrate the first-order control of temperature changes and bubble-mediated gas exchange in controlling surface inert gas conditions. However, our simulations including mixing processes (runs b, c) highlight the key role of mixing in altering surface  $\Delta N_2/Ar$ . For example, vertical mixing of water parcels with different temperatures can induce supersaturation in  $O_2$ ,  $Ar$  and  $N_2$  due to the non-linear temperature-dependence of gas solubility (Fig. S1; Hamme et al., 2019; Ito & Deutsch, 2006). Since temperature effects on  $O_2$  and  $Ar$  are nearly identical, surface  $\Delta O_2/Ar$  will be largely insensitive to mixing if subsurface gas anomalies are negligible (i.e. subsurface  $\Delta O_2/Ar$  near 0 %). However, throughout most of the ocean, waters below the mixed layer are depleted in  $O_2$  so that surface  $\Delta O_2/Ar$  and  $\Delta O_2/N_2$  will be negatively biased in regions of active vertical mixing (see below; Izett et al., 2018; Teeter et al., 2018). Moreover, decoupling between surface  $\Delta O_2/Ar$  and  $\Delta O_2/N_2$  will occur through mixing of water masses with differing temperatures (or salinities, to a lesser-degree) as a result of the lower temperature-sensitivity of  $N_2$  solubility (Fig. S1a), or from mixing of water parcels with subsurface  $\Delta N_2/Ar$  not equal to 0 % (as observed throughout most of the ocean; Shigemitsu et al., 2016).

These mixing effects are represented in our model simulations, where weak vertical fluxes (run b; dashed lines in Fig. 2) lead to only minor deviations in surface  $\Delta N_2/Ar$  from the bubble-induced value (compare dotted, dashed and grey lines in Fig. 2). Conversely, higher mixing fluxes (run c) may result in significantly elevated  $\Delta N_2/Ar$ . As predicted by our quasi-steady-state analyses (Fig. 1), surface  $\Delta N_2/Ar$  in simulations including mixing is weighted between end members represented by the bubble-induced supersaturation ratio of  $N_2$  and  $Ar$ , and  $\Delta N_2/Ar_{deep}$ . The resulting mixed layer value depends on the relative influence of air-sea exchange (i.e.  $k_T$ ) and vertical mixing ( $\kappa/dZ$ ). At low wind speeds or high mixing rates, surface  $\Delta N_2/Ar$  is closer to  $\Delta N_2/Ar_{deep}$  (Fig. 2; days <12 and >68) and potential deviations from the bubble-induced steady-state value can exceed ~2 % (Fig. 1c). In contrast, at higher  $u_{10}$  (Fig. 2a, c; days ~12-65) or low  $\kappa$ , air-sea exchange fluxes drive surface  $\Delta N_2/Ar$  towards the bubble-induced supersaturation value, thus minimizing the effect of mixing fluxes.

While mixing can produce large  $\Delta N_2/Ar$  anomalies, the results from Ex-IF 2-4 demonstrate that the effects of rapid  $\Delta SST$  and sea ice coverage are similar, regardless of the mixing scenario. Specifically, mixing shifts the baseline in  $\Delta N_2/Ar$ , but the transient responses to  $\Delta SST$  in Ex-IF 2 are similar in all mixing scenarios. Similarly, as sea ice dampens the wind effect, strong mixing caused surface  $\Delta N_2/Ar$  to approach  $\Delta N_2/Ar_{deep}$  rather than the bubble-induced supersaturation state.

Throughout most of the ocean, the rate of air-sea exchange will typically exceed turnover via mixing ( $k_T > 3.3 \text{ m d}^{-1}$  at wind speeds  $> 7 \text{ m s}^{-1}$  and canonical  $\kappa_z$ ,  $10^{-4} \text{ m}^2 \text{ s}^{-1}$ ; Cronin et al., 2015; Whalen et al., 2012). This implies that mixing can cause baseline shifts in surface  $\Delta N_2/Ar$  (Figs. 1-4), but that elevated wind events should still dominate on short time-scales, as observed in our experimental simulations (Ex-IF 1,3 and Ex-IC). Nonetheless, vertical mixing remains important in decreasing the re-equilibration timescale of mixed layer gas anomalies. When  $\kappa$  is high, gas residence times are reduced, more rapidly erasing any potential bubble-induced supersaturation effects. The analytical solution to our simplified MLD budget is useful for

diagnosing this effect as  $\kappa$  appears in the exponential term of the solution (Eq. 5), and therefore influences the rate constant of gas re-equilibration. Our definition of  $\tau_{O_2}$  (Eq. 6), the  $O_2$  re-equilibration time-scale over which  $N_2$  calculations are performed (see sections 2.2, 3.4.1 and S1 in the SI), also includes the mixing coefficient  $\kappa$ .

$$\tau_{O_2} = \frac{-\ln(0.01) \cdot \text{MLD}}{\left(k_T + \frac{\kappa}{dz}\right)} \quad (6)$$

### 3.2 Realistic simulations

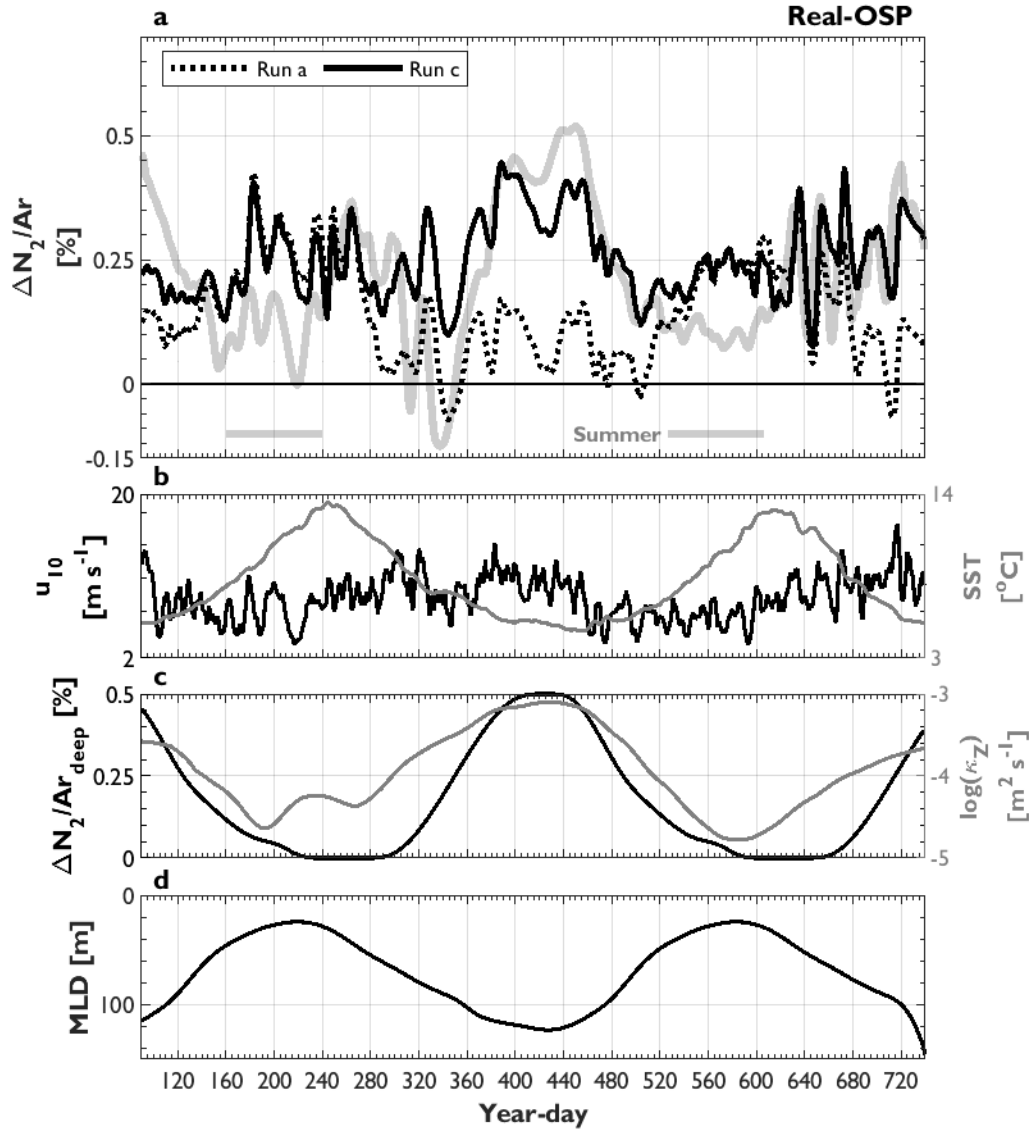
The main processes driving variability in  $\Delta N_2/Ar$  in our experimental runs are also apparent in the realistic simulations (real-OSP in Fig. 3, and real-BB in Fig. 4). Under the more realistic scenarios, however, SST and differential gas exchange rates exerted the strongest controls on  $\Delta N_2/Ar$  over long time-scales. Indeed, in both the real-OSP and real-BB simulations,  $\Delta Ar$  and  $\Delta N_2$  followed seasonal changes in SST, with transient modifications during periods of elevated wind-speeds (Figs. S4, S5). The OSP and Baffin Bay runs without mixing generally resemble the results of experiment Ex-IF 2a ( $\Delta SST$  at constant  $u_{10}$ ). The elevated spring and summertime  $\Delta N_2/Ar$  in both sets of runs (days ~155-255 and ~520-620 in real-OSP, Fig 3; and days ~190-230 in real-BB, Fig. 4) is consistent with increased gas supersaturation states, and the slower re-equilibration rate of  $N_2$  over  $Ar$  following positive  $\Delta SST$ . In the real-OSP run without mixing (run a), a net warming of ~9 °C during the spring and summer caused  $\Delta N_2/Ar$  to increase to ~0.4 % (corresponding with  $\Delta N_2$  and  $\Delta Ar$  increases to ~3 %; Figs. S4, S5). In real-BBa, the equivalent  $\Delta SST$  raised  $\Delta N_2/Ar$  to ~0.8 % ( $\Delta N_2$  and  $\Delta Ar$  increase to ~11 %; Fig. S5). These positive  $\Delta N_2/Ar$  values, which exceed the quasi-steady-state conditions (thick grey lines in Figs. 3, 4), thus reflect seasonal warming. During conditions of elevated  $u_{10}$  and net cooling (days ~260-400 and >~620 in real-OSP and >day 250 in real-BB), the decline in  $\Delta N_2/Ar$  is again more consistent with temperature-dependent solubility effects, with short-term modifications by bubble processes. In these realistic scenarios, the decline in  $\Delta N_2/Ar$  during cooling periods resembled the response in Ex-IF 2 (i.e. decreased  $\Delta N_2/Ar$ ; Fig. 2b, c).

As observed in the experimental runs, the real-OSP and real-BB simulations also demonstrated a mixing effect on gas conditions, with vertical fluxes elevating surface gas anomalies, particularly during autumn and winter periods. The mixing effect on  $\Delta N_2/Ar$  was most significant at higher  $\kappa$ , during MLD deepening (Figs. 3c, 4c), or under sea ice cover (Fig. 4b), when  $\Delta N_2/Ar$  approached  $\Delta N_2/Ar_{\text{deep}}$ . In the full mixing runs of both realistic simulations,  $\Delta N_2/Ar$  was almost always higher than in the non-mixing runs. Exceptions occurred during periods of reduced summertime mixing in real-OSP (annotated in Fig. 3) when  $\Delta N_2/Ar$  was equivalent in both mixing scenarios (and in all sensitivity model runs; see section 3.3), and between days 220 and 240 in real-BB, when mixing dampened the warming effect. Ultimately, seasonal variability in the mixing response will be sensitive to intra-annual variability in  $u_{10}$ ,  $\Delta N_2/Ar_{\text{deep}}$  and  $\kappa z$ , which we attempted to capture in our real-OSP simulations (Table 1).

In contrast to the experimental runs,  $\Delta N_2/Ar$  in the realistic simulations seldom achieved the quasi-steady-state condition (grey lines in Figs. 3, 4 predicted by Eq. 5). This reflects the high variability in environmental forcing, and the fact that thermal disequilibrium can persist for long periods (up to 60 days in our experimental simulations) under low wind speeds. This result demonstrates the simultaneous effects of various fluxes on gas saturation states. Only under

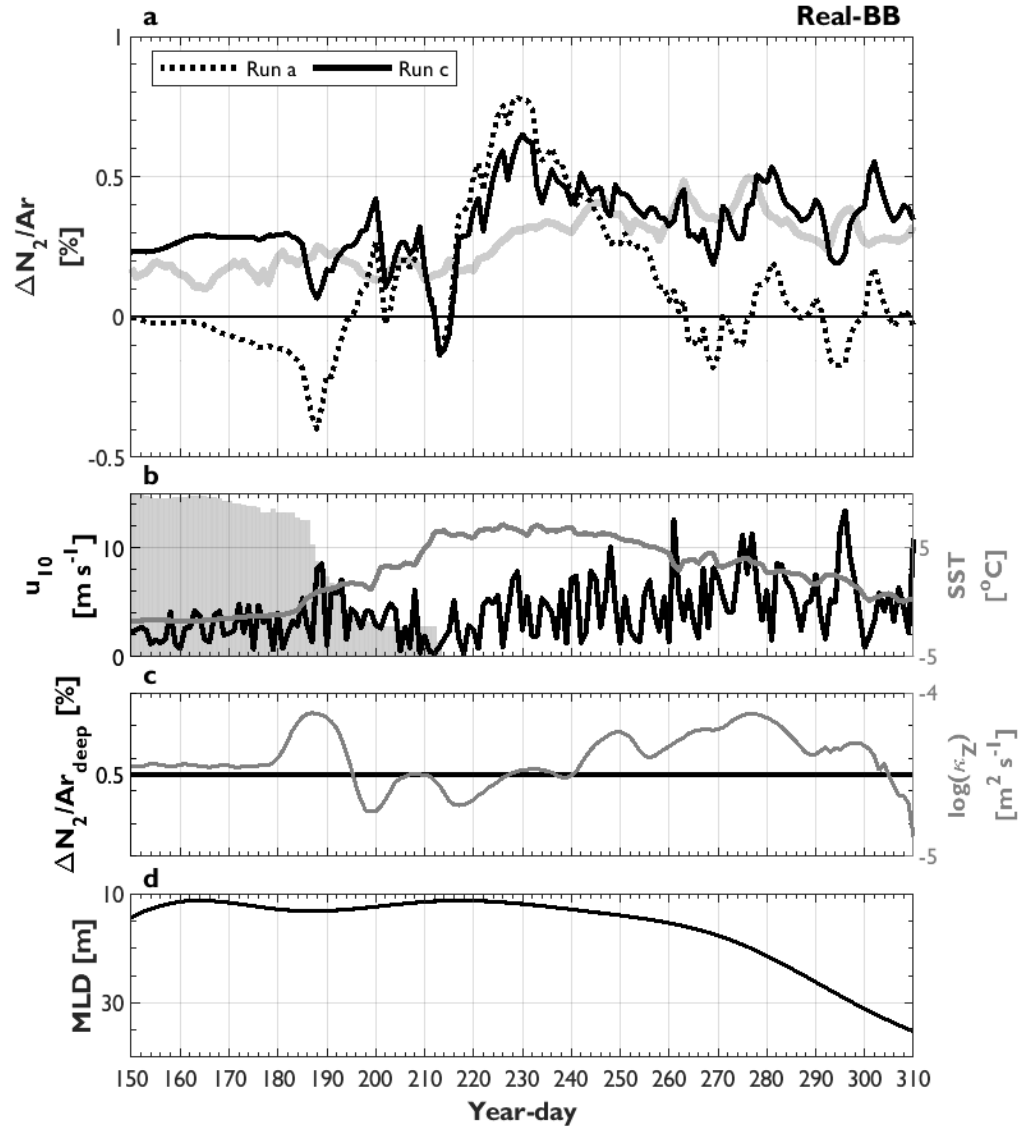


518 conditions of significant ice cover and high mixing does  $\Delta N_2/Ar$  remain near to the steady state  
 519 values.



520

521 **Figure 3.** Results from realistic model simulations of OSP in the Subarctic Northeast Pacific.  
 522 Panel (a) shows  $\Delta N_2/Ar$  in runs without (run a; dotted lines) and with (run c; solid lines) mixing,  
 523 while panels (b)-(d) represent the forcing environmental data (details in Table 1). The x-axes  
 524 represent the 2011 year-day (Jan. 2011 – Jan. 2013). The thick grey line in (a) depicts the quasi-  
 525 steady-state condition (Eq. 5; Fig. 1) corresponding with run c. The grey bars in (a) (labelled  
 526 “summer”) represent periods of weak mixing between June and September, and correspond with  
 527 data shown in Fig. 6.



**Figure 4.** Results from realistic model simulations of Baffin Bay in the eastern Arctic. The x-axes represent the 2019 year-day (May – Oct.). The grey shading in (b) represents the ice-coverage as a percent of the figure y-scale. Refer to Fig. 3 caption and Table 1 for details.

### 3.3 Model validation and sensitivity tests

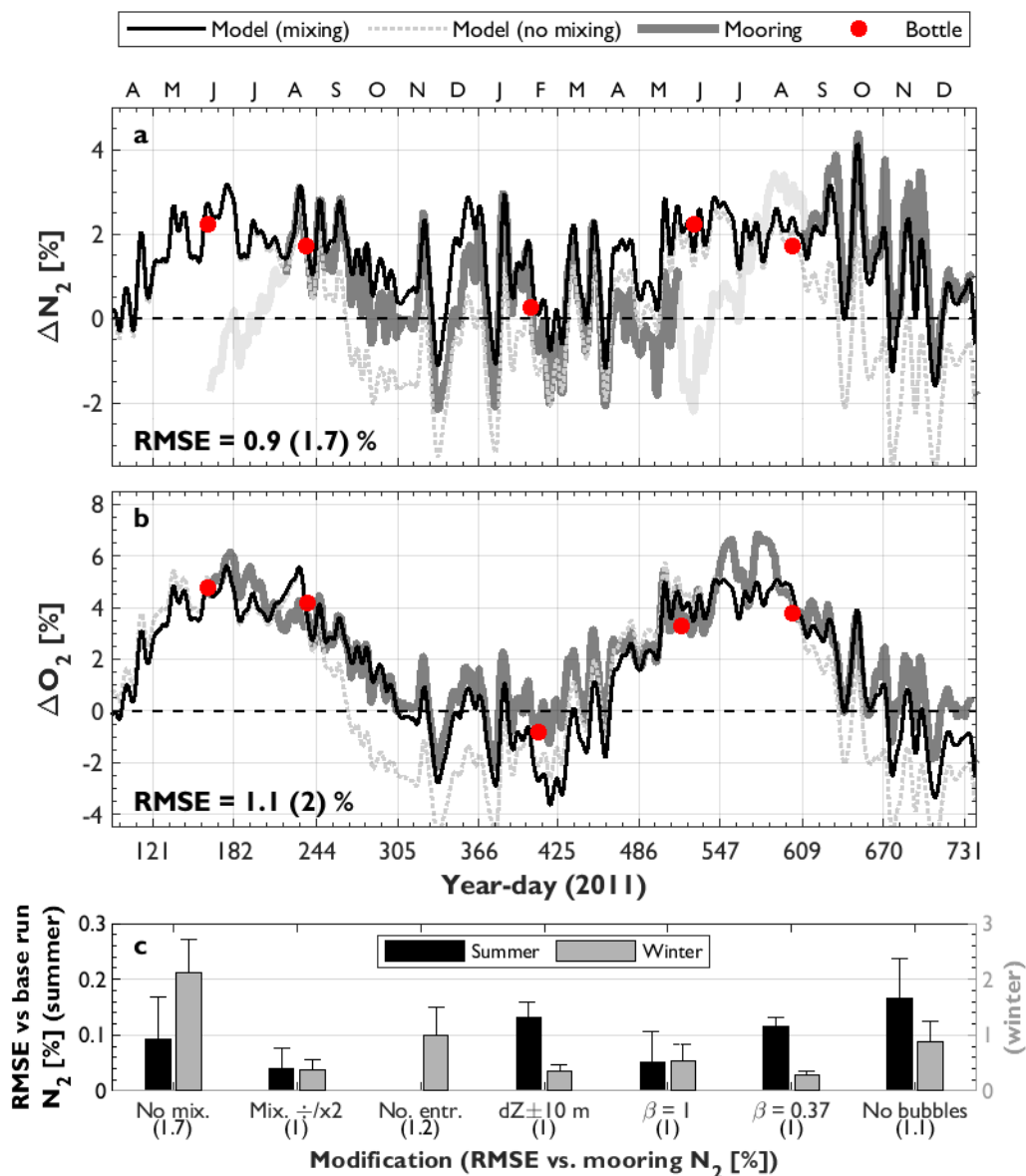
To validate our modelling approach in support of the subsequent  $N_2'$  analysis (section 3.4.1), we compared  $N_2$  and  $O_2$  from our real-OSP run c simulation against a two-year cycle of surface measurements from the NOAA PMEL OSP mooring (provided by S. Emerson at [https://www.nodc.noaa.gov/ocads/oceans/Moorings/Papa\\_145W\\_50N.html](https://www.nodc.noaa.gov/ocads/oceans/Moorings/Papa_145W_50N.html); Emerson et al., 2017). As shown in Fig. 5a, b, our model calculations forced with relevant environmental data and time-variable mixing terms agree well with the mooring gas data. The model is able to reproduce both short-term (associated with wind events) and long-term (associated with seasonal

SST and mixing variability) responses of  $N_2$  to environmental drivers, with an overall root mean square error (RMSE) between the model and data of 1.0 % (range of offset between modeled and observed  $N_2$   $\sim 0 - 2.4$  %). Moreover, our modelled  $O_2$ , which was forced with a mean annual NCP time-series and subsurface  $O_2$  observations at OSP, recaptures the observed annual cycle with equally-small deviation from the in-situ time-series (RMSE = 1 %; range 0 – 3.1 %).

Residual differences between the model and observations can be explained by several factors, including the potential effects of lateral advection (Emerson & Stump, 2010), which are neglected in our calculations, and the smoothed mixed layer and mixing forcing conditions applied in our model runs. In addition, interpolation of sparse  $\Delta Ar_{deep}$  and  $\Delta N_2/Ar_{deep}$  observations from discrete gas sampling at OSP (February, June and August data from Hamme et al., 2019) may not fully represent subsurface conditions across the full seasonal cycle. Indeed, the poorest alignment between model and observed  $\Delta N_2$  occurs during the fall and early winter (e.g. days  $\sim 260-390$ ), when no subsurface gas observations were available. Moreover, while we applied  $\kappa_z$  values corresponding with the location and timing of our model setting (from Cronin et al., 2015), it is also possible that uncertainty in the  $\kappa_z$  dataset may contribute to differences between the model and observed gas data. Importantly, however, the model run with realistic mixing fluxes was able to better replicate the full seasonal cycles of  $N_2$  and  $O_2$  than the simulation run without mixing (light grey line in Fig. 5a,b). Indeed, the model run without mixing often under-estimates  $\Delta N_2$ , demonstrating the importance of vertical mixing in supplying relatively high- $N_2$  to surface waters.

We tested the model sensitivity to flux parameterizations by performing additional simulations in which the mixing terms ( $\kappa_z$ ,  $dZ$ , entrainment) and bubble scaling coefficient ( $\beta$ ) were modified from the real-OSP full mixing run (Fig. 5c). Overall, we find that the model skill at reproducing observed  $N_2$  at OSP is most sensitive to the exclusion of bubble processes and vertical flux terms. This result is consistent with other studies (e.g., Emerson et al., 2019; Emerson & Bushinsky, 2016; Hamme & Severinghaus, 2007), which noted that explicit bubble flux terms are required to explain gas observations. Moreover, we find that the model sensitivity is greater in the wintertime at OSP. This reflects the reduced significance of bubble fluxes and vertical mixing during summer months, as a result of lower wind speeds and upper ocean turbulence. The weak sensitivity of the model to parameterizations in the summer months is a key result as it supports the application of the present approach during time-periods when NCP and carbon export are typically elevated, and when in-situ sampling from research vessels is most common. Indeed, results vary by less than 0.25 % across all modified simulations between June and August, as compared with deviations exceeding 1 % in winter periods.

Based on the comparisons of modeled and observed  $N_2$ , we believe that our model captures the main drivers of  $N_2$  saturation variability in oceanic surface waters, particularly during biologically-productive summer months. Although the model cannot be equally-validated for Ar due to a lack of observations, we expect that our conclusions apply to this gas as well. This exercise should also be taken as a rough validation of the Liang et al. (2013) bubble-flux parameterization, which was previously evaluated in the North Pacific by Emerson & Bushinsky (2016) using a similar model as that employed here. Importantly, the strong agreement between our model results and observations over a two-year cycle justifies the air-sea flux and mixing parameterizations used in our model simulations, and provides confidence in the  $N_2$  approach described below.



**Figure 5.** A comparison of modeled (thin lines) and observed (thick grey line)  $N_2$  (a) and  $O_2$  (b) supersaturation anomalies over a two-year cycle at OSP in the Subarctic Northeast Pacific. The modelled gas results are from the full mixing (run c; black line) and no mixing (run a; light grey line) real-OSP simulations and correspond with results and forcing parameters presented in Fig. 3 and Table 1. Gas observations were obtained from the NOAA PMEL mooring at OSP. The light, thick-grey section of the mooring  $N_2$  time-series in (a) represents a section of the record where the  $N_2$  data may be biased by sampling artifacts (S. Emerson personal communication, 2020). All lines represent 1-day smoothed values. The red dots in (a) and (b) represent discrete observations. The  $N_2$  data (a) are mean February, June and August  $N_2$  values from Hamme et al. (2019), and  $O_2$  data (b) are from Rosette sampling at the specified times. The RMSE values presented at the top-right represent differences between modelled and mooring values for real-OSP run c (run a value in brackets). Values on the x-axis correspond with 2011 year-day, and labels at the top represent month. Panel (c) represents a sensitivity analysis on our model

parameterizations where the real-OSP with full mixing simulation ( $\beta = 0.5$  and  $dZ = \text{MLD to thermocline depth}$ ) was modified as indicated by the labels on the x-axis. The model sensitivity was evaluated during summer (July-Aug.; left axis) and a winter (Nov.-Feb.; right axis) segments. The bars represent the mean difference between the base and modified runs during these segments, with error bars depicting the range of values. The numbers below the x-axis labels are the overall RMSE between each modified model run and the real mooring  $\text{N}_2$  data from OSP. Note that the summer sensitivity results are represented by the left y-axis, which is a factor of 10 smaller than the scale on the left axis, representing the winter results.

### 3.4 NCP calculations from $\text{O}_2$ and $\text{N}_2$ measurements

Divergence between mixed layer  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2$  (non-zero  $\Delta\text{N}_2/\text{Ar}$ ) can lead to significant uncertainty in NCP estimates calculated from  $\text{O}_2$  and  $\text{N}_2$  observations. For a realistic range of  $\Delta\text{O}_2$  and  $\Delta\text{N}_2/\text{Ar}$  in the ocean, absolute differences between  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2$  may exceed 2 % (Fig. S6a), which is of the same magnitude as  $\Delta\text{O}_2$  observed in many low productivity ocean regions. Relative differences between NCP tracers can exceed 100 % for low  $\Delta\text{O}_2$ , and will likely be significant over a large range of ocean conditions (Fig. S6b). These biases will propagate as errors in NCP estimates derived from observations of the biological  $\text{O}_2$  saturation anomaly calculated following Kaiser et al., (2005):

$$\text{NCP} = k_{\text{O}_2} \cdot \Delta\text{O}_2/\text{N}_2 \cdot [\text{O}_2]_{\text{eq}} \quad (7)$$

Over a realistic range of SST (0-30 °C), salinity (30-35 PSU) and  $u_{10}$  (2-10  $\text{m s}^{-1}$ ), a bias in  $\Delta\text{O}_2/\text{N}_2$  of 0.3 % (the mean value of  $\Delta\text{O}_2/\text{Ar} - \Delta\text{O}_2/\text{N}_2$  in our realistic simulations; Table S1) would introduce  $\sim 6 \text{ mmol O}_2 \text{ m}^{-2} \text{ d}^{-1}$  error in NCP estimates, while a bias of 1.1 % (the upper range in our simulations) would contribute up to  $\sim 19 \text{ mmol O}_2 \text{ m}^{-2} \text{ d}^{-1}$  uncertainty. These errors may be comparable to those resulting from diel  $\text{O}_2$  variability (up to  $\sim 5$  to  $>100 \text{ mmol O}_2 \text{ m}^{-2} \text{ d}^{-1}$ ; Wang et al., 2020) and vertical mixing of subsurface  $\text{O}_2$ -deplete waters ( $\sim 0$ -50 and 60-190  $\text{mmol O}_2 \text{ m}^{-2} \text{ d}^{-1}$  in offshore and coastal waters, respectively; Izett et al., 2018), depending on the ocean region sampled. However, the differences between  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2$  in our realistic simulations are almost as large in magnitude as reported  $\Delta\text{O}_2/\text{Ar}$  values in many offshore regions of all ocean basins, which are typically smaller than  $\sim \pm 5$ -10 % (e.g. Eveleth et al., 2014, 2017; Giesbrecht et al., 2012; Hamme & Emerson, 2006; Izett et al., 2018; Juranek et al., 2019; Lockwood et al., 2012; Munro et al., 2013; Palevsky et al., 2016; Ulfssbo et al., 2014; Wang et al., 2020). Thus, biases in the quantification of the biological  $\text{O}_2$  saturation anomaly could lead to erroneous interpretations of NCP estimates from  $\Delta\text{O}_2/\text{N}_2$  measurements and, in some regions, false conclusions regarding the metabolic status of surface waters (i.e. implied net heterotrophy from negative  $\Delta\text{O}_2/\text{N}_2$  versus autotrophy from positive  $\Delta\text{O}_2/\text{Ar}$ ; represented by outlined region in Fig. S6). These limitations motivate the need to correct  $\Delta\text{O}_2/\text{N}_2$  observations for excess physical  $\text{N}_2$  saturation, particularly in offshore waters where other biases are smaller.

Fortunately, our analyses demonstrate that differences between  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2$  respond systematically to differential physical gas fluxes and environmental perturbations, enabling us to apply appropriate corrections. We thus derived a new term,  $\text{N}_2'$  (calculations described in section 2.2 and software scripts provided at [doi.org/10.5281/zenodo.4024952](https://doi.org/10.5281/zenodo.4024952)), which holds significant value as a tracer for physically-induced changes in the mixed layer  $\text{O}_2$ . As we discuss below,  $\Delta\text{O}_2/\text{N}_2'$ , derived from Optode ( $\text{O}_2$ ) and GTD ( $\text{N}_2$ ) measurements and

calculations from a simplified MLD budget, provides a good analog for  $\Delta\text{O}_2/\text{Ar}$ -based NCP estimates.

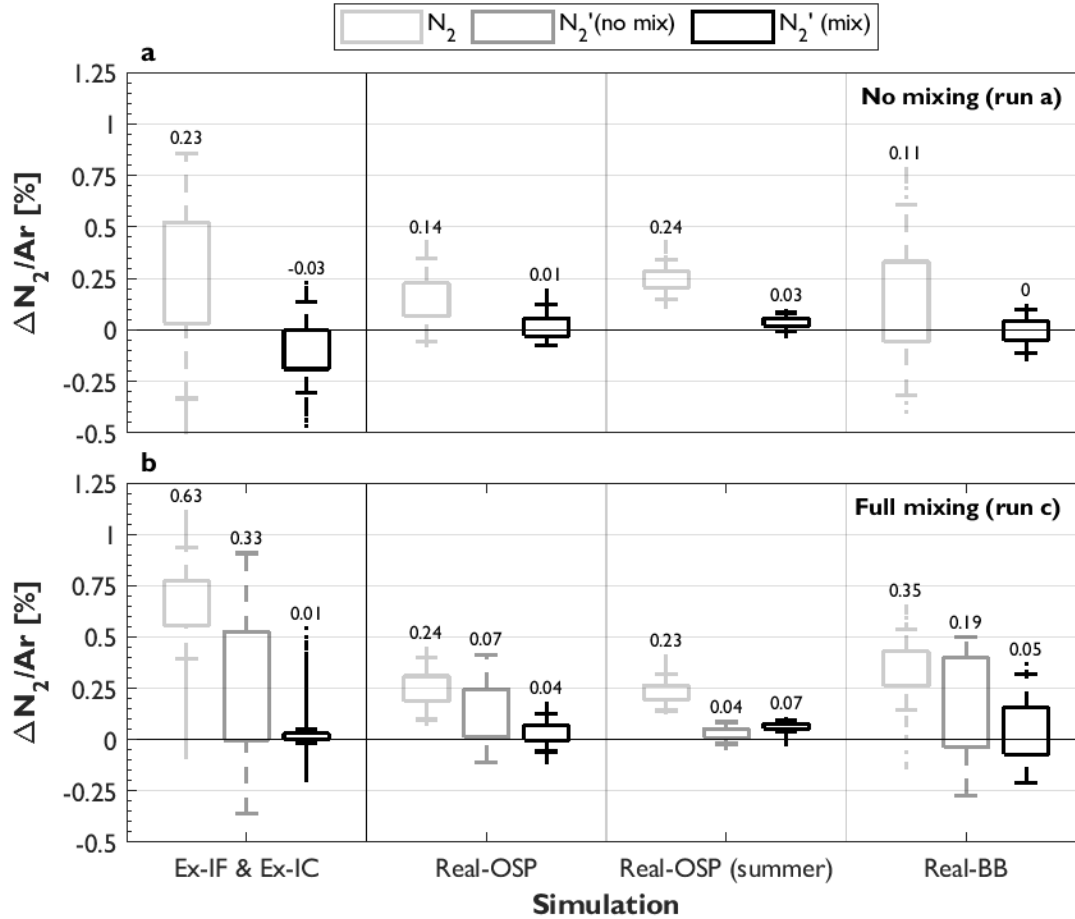
### 3.4.1. $\text{N}_2'$ in mixed layer model setting

We tested the performance of our  $\text{N}_2'$  approach using the experimental and realistic simulations (Figs. 2-4). We treated the simulated gas values as “true” (i.e. analogous to in-situ ocean observations; see Eq. 4) and applied the  $\text{N}_2'$  approach based on readily-available data from reanalysis products or field observations. In deriving  $\Delta\text{N}_2'$ , we thus applied the same environmental forcing data (SST,  $u_{10}$  and SLP) as in the full model simulations, but assumed constant values backwards in time for MLD, surface salinity,  $\kappa$ , and  $\Delta\text{N}_2/\text{Ar}_{\text{deep}}$ , to mirror the information available from field studies (see below, section 3.4.3).

Overall,  $\text{N}_2'$  successfully corrects for differences in surface water  $\Delta\text{Ar}$  and  $\Delta\text{N}_2$ , thereby reducing biases between  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2$  (Fig. 6). Across all experimental simulations, median  $\Delta\text{N}_2'/\text{Ar}$  was  $\sim 0\%$  and  $\sim 0.01$  in the runs without (a) and with (c) mixing, respectively. In comparison, uncorrected  $\Delta\text{N}_2/\text{Ar}$  was significantly larger than 0, with median values of 0.23 and 0.63 % (maximum 1.1 %). In the realistic simulations, median  $\Delta\text{N}_2'/\text{Ar}$  and  $\Delta\text{O}_2/\text{Ar} - \Delta\text{O}_2/\text{N}_2'$  were  $\sim 0.01$  (range -0.24 to 0.3 %; Fig. 6, Table S1), demonstrating that differences between  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2$  can be corrected using simple MLD budget computations performed over an estimated  $\text{O}_2$  re-equilibration time (Eq. 6).

The remaining  $\Delta\text{N}_2'/\text{Ar}$  disequilibria is attributable to the simplifying assumptions in the  $\text{N}_2'$  approach, which we discuss in section 3.4.3. We observed the largest remaining biases in  $\Delta\text{N}_2'/\text{Ar}$  during the summer period of the real-BB full mixing simulation (Fig. S9b). These relatively large remaining offsets between  $\Delta\text{N}_2'$  and  $\Delta\text{Ar}$  resulted from significant temporal variability in subsurface gas concentrations in the BB simulations, which cannot be represented in  $\text{N}_2'$  calculations (see sections 2.1.1, 3.4.3 and S2.2 for details). However, we believe that these biases represent the upper limit of values expected from application of the present approach to real data sets, as subsurface gas conditions are likely to vary less in reality than in our model. Additional remaining biases in  $\Delta\text{N}_2'/\text{Ar}$  occurred during the autumn months of the real-OSP full mixing scenario when vertical entrainment was significant ( $\sim$ days 230-330 and  $>600$  in Fig. S9a), and in early summer ( $\sim$ days 160-200 and  $\sim 525$ -565) when the  $\text{N}_2'$  budget was unable to resolve the relatively strong mixing occurring prior to this time. Despite these offsets,  $\text{N}_2'$  is useful in reducing differences between  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2$  observations, and  $\Delta\text{N}_2'/\text{Ar}$  was almost always lower than  $\Delta\text{N}_2/\text{Ar}$  in all of our simulations.

Given the sparsity of oceanic mixing rate estimates (e.g. Whalen et al., 2012) or subsurface Ar and  $\text{N}_2$  measurements (e.g. Hamme et al., 2019), it may be difficult to constrain the mixing flux terms in our  $\text{N}_2'$  model (see below, sections 3.4.2 and 3.4.3). We therefore performed an additional set of  $\text{N}_2'$  calculations to test our approach when vertical mixing fluxes are neglected. This term, which we denote as  $\Delta\text{N}_2'(\text{no mix.})$ , was derived by setting  $\kappa$  to  $0 \text{ m}^2 \text{ s}^{-1}$  in the  $\text{N}_2'$  calculations. We find that  $\Delta\text{N}_2'(\text{no mix.})/\text{Ar}$  does not fully correct for differences between  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2$  in most simulations (Fig. 6). However, in a subset of real-OSP run c corresponding with mid-June to September (labelled bars in Fig. 3),  $\text{N}_2'(\text{no mix.})$  successfully reduced  $\Delta\text{N}_2'/\text{Ar}$  to a median value of  $\sim 0.04\%$ . This result is promising for in-situ applications in stratified ocean regions, when vertical mixing is small relative to other gas flux terms.



**Figure 6.** Distribution of  $\Delta N_2/Ar$  and  $\Delta N_2'/Ar$  in the experimental (left) and realistic (right) simulations runs without mixing (run a) and with mixing (run c) (details in Table 1). The numbers above each box represent the median  $\Delta N_2/Ar$  or  $\Delta N_2'/Ar$  values. A value of zero implies that  $N_2'$  provides a perfect analog for Ar. A subset of the OSP simulation is included to represent results in more stratified waters during summer months in the Subarctic Northeast Pacific (highlighted in Fig. 3a).

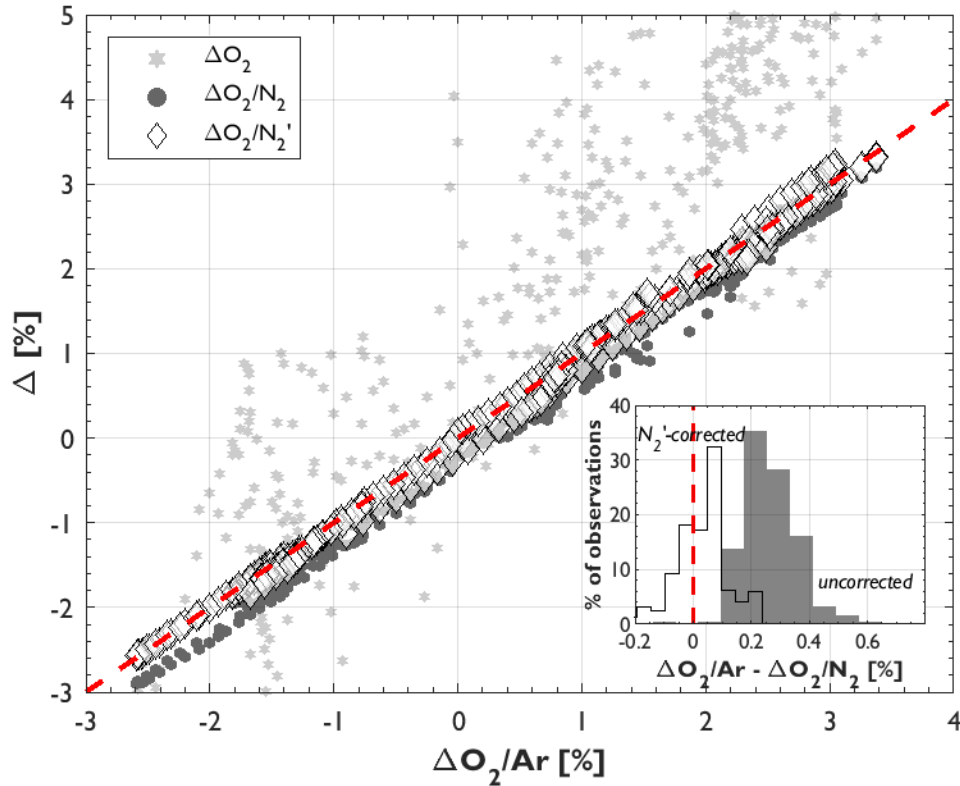
### 3.4.2 $\Delta O_2/N_2'$ as an in-situ NCP tracer

Our work demonstrates that  $\Delta O_2/N_2'$  offers a robust analog for  $\Delta O_2/Ar$  measurements. Indeed, we found that  $\Delta O_2/N_2'$  performed significantly better than either  $\Delta O_2$  or uncorrected  $\Delta O_2/N_2$  in reproducing  $\Delta O_2/Ar$ . As shown in Fig. 7,  $\Delta O_2/N_2'$  was tightly correlated to  $\Delta O_2/Ar$ , with a linear regression slope that was not significantly different from unity, and an RMSE of 0.03 %. This result suggests that NCP calculations based on  $\Delta O_2/N_2'$  should be nearly-equivalent to  $\Delta O_2/Ar$ -derived estimates, providing an alternative approach to isolate biological influences on mixed layer oxygen dynamics. Moreover, we have observed strong coherence between  $\Delta O_2/Ar$  and  $\Delta O_2/N_2'$  in observations obtained from underway ship-board surveys across broad spatial scales and hydrographic gradients (manuscript in preparation).

Field-based application of the  $N_2'$  approach will depend on proper characterization of environmental histories and mixing environments. Quantification of the mixing terms,  $\kappa$  and  $\Delta N_2/Ar_{deep}$ , will likely constitute the largest source of uncertainty in  $\Delta O_2/N_2'$  (see section S2 of the SI), as these values are generally poorly constrained by limited observations and strong spatial or temporal variability. Recent work has provided several approaches to approximating  $\kappa$  from direct or indirect estimates of turbulent dissipation rates (Chanona et al., 2018; Scheifele et al., 2018; Whalen et al., 2012), and by proxy relationships with temperature and salinity (Cronin et al., 2015), nitrous oxide (Izett et al., 2018) or inert gas measurements (Ito & Deutsch, 2006). It is also possible to estimate  $\Delta N_2/Ar_{deep}$  and  $\kappa$  from archived datasets (e.g. Hamme et al., 2019) or circulation models (e.g. Castro de la Guardia et al., 2019; Shigemitsu et al., 2016). Moreover, as demonstrated in Fig. 1, and in the simulations with weak or no mixing (Figs. 2, 3), vertical fluxes have a relatively small impact on surface  $\Delta N_2/Ar$  when mixing rates fall below  $\sim 10^{-4} \text{ m}^2 \text{ s}^{-1}$ , or when  $\Delta N_2/Ar_{deep}$  is less than  $\sim 0.25 \%$ . Indeed, in our real-OSP and real-BB simulations forced with time-variable and realistic  $\kappa_z$  and  $\Delta N_2/Ar_{deep}$ , surface  $\Delta N_2/Ar$  converged on similar values for both mixing scenarios between days during summer periods, when  $\kappa_z$  was small (Figs. 3, 4). This suggests a negligible contribution of vertical fluxes to surface gas budgets during periods of stratification, consistent with observations of reduced summertime vertical gas fluxes in mid-latitude oceanic waters (e.g. Emerson & Stump, 2010; Izett et al., 2018; Pelland et al., 2018; Plant et al., 2016). The implication of these results is that mixing terms can potentially be neglected in  $N_2'$  corrections under conditions of moderate to strong stratification. Such conditions occur over much of the ocean during periods of summer productivity.

In dynamic coastal waters where vertical mixing may contribute to a significant divergence between  $\Delta O_2/Ar$  and  $\Delta O_2/N_2$ , particularly in regions of subsurface or benthic denitrification (see below, section 3.4.3), the resulting bias in NCP estimates may be small compared with errors resulting from vertical mixing fluxes of  $O_2$  and diel variability (section 3.4). Moreover, if  $\Delta O_2$  is elevated ( $>5 \%$ ) by strong biological production, relative differences between  $\Delta O_2/Ar$  and  $\Delta O_2/N_2$  will remain smaller than the  $\sim 20 - 40 \%$  uncertainty in gas transfer parameterizations (Fig. S6b; Bender et al., 2011; Wanninkhof, 2014). In offshore waters, where  $\Delta O_2$  is typically nearer to equilibrium, and other biases in  $O_2$  are small,  $N_2'$  corrections will be necessary to minimize errors in NCP calculations. Overall, we conclude that underway  $\Delta O_2/N_2$  measurements from Optode and GTD sampling, combined with careful application of the  $N_2'$  calculations described here, can serve as an effective alternative to  $\Delta O_2/Ar$ -based NCP sampling across a wide range of oceanic conditions. This approach thus has the potential to significantly increase the spatial and temporal coverage of marine NCP estimates.





**Figure 7.** The relationship between  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2$  (light grey stars),  $\Delta\text{O}_2/\text{N}_2$  (dark grey circles) and  $\Delta\text{O}_2/\text{N}_2'$  (black/white diamonds) in the realistic model simulations (real-OSP and real-BB, simulations with full mixing only). The dashed red line shows the 1:1 fit. The inset shows the distribution of  $\Delta\text{O}_2/\text{Ar} - \Delta\text{O}_2/\text{N}_2$  before (filled grey) and after (outlined) applying  $\text{N}_2'$  corrections.

### 3.4.3 Remaining biases and uncertainty in $\Delta\text{O}_2/\text{N}_2'$

Despite strong the coherence between  $\Delta\text{O}_2/\text{N}_2'$  and  $\Delta\text{O}_2/\text{Ar}$  (Fig. 7), and general agreement of  $\Delta\text{Ar}$  and  $\Delta\text{N}_2'$  some biases remain. These are attributable to the simplifying assumptions in the  $\text{N}_2'$  calculations (i.e. constant MLD, salinity,  $\kappa$  and  $\Delta\text{N}_2/\text{Ar}_{\text{deep}}$ ), made necessary by the limitation of field observations. The time-history of  $u_{10}$ , SST, and SLP prior to ship-board sampling in a given location can be obtained from remote sensing and reanalysis products, but estimates of MLD and salinity are most reliable from ship-board measurements. The subsurface and mixing terms ( $\kappa$  and  $\Delta\text{N}_2/\text{Ar}_{\text{deep}}$ ) may be derived from measurements made at the time of underway gas sampling (see above), but will normally be obtained from external sources and assumed constant over  $\tau_{\text{O}_2}$ . Across our realistic simulation runs, we found that the contribution of these simplifying assumptions to uncertainty in  $\Delta\text{O}_2/\text{N}_2'$  was  $\sim 0.07\%$  (Table S1; details in section S2 of the SI), which is small relative to other sources of error in NCP calculations, as discussed above. In general, these errors were largest during times of significant subsurface hydrographic and gas variability, as was the case in our real-BB simulation. While the settings in our BB runs may not be entirely representative of reality, and we were unable to validate the modeled time-series in this location, the  $\text{N}_2'$  results from these model runs should be

seen as upper limits of values expected from field studies. Errors associated with these assumptions can only be reduced by quantifying the time-variability of the relevant terms, which may be feasible from Argo floats near to cruise track observations, additional reanalysis products or numerical model output.

Additional uncertainty in field applications of the  $N_2'$  approach arises from the parameterization uncertainty in each of the terms ( $u_{10}$ , SST, SLP,  $F_d$ ,  $F_c$ ,  $F_p$ ,  $\beta$ , MLD,  $\kappa$  and  $\Delta N_2/Ar_{deep}$ ) used to predict  $\Delta N_2/Ar$  (Eq. 3). To evaluate the magnitude of these errors, we performed a Monte Carlo analysis on the realistic simulations (real-OSP and real-BB, run c only) by randomly varying each of the input variables around their estimated parameter uncertainty (details in section S2 of the SI). We estimated a combined absolute parameterization error in  $\Delta O_2/N_2'$  of 0.09 %, with the largest contributions coming from the SST product (Table S1). This is unsurprising given the seasonal controls of SST variability in driving intra-annual variability in gas conditions (see above, sections 3.1-3.2). The bubble terms ( $F_c$ ,  $F_p$ ,  $\beta$ ) contributed relatively small errors, due to the low prevalence of elevated wind speeds (Figs. 3-4). Calculations of  $N_2'$  will, nonetheless, depend on the air-sea exchange model employed in the budget evaluations. We used the bubble-mediated model of Liang et al. (2013) because it has been validated against in-situ  $N_2$  and noble gas measurements (here and in Emerson & Bushinsky, 2016), and was parameterized for weakly-soluble gases similar to  $O_2$ . When possible, we recommend that future studies employ air-sea exchange parameterizations that have been validated for the region of interest.

An additional consideration is the influence of biological processes on  $\Delta N_2/Ar$ . Unlike Ar,  $N_2$  concentrations can be altered by several bacterially-mediated processes, including surface  $N_2$ -fixation, and subsurface or sedimentary denitrification and anammox. These processes could, in principle, impact  $\Delta O_2/N_2'$ -based NCP estimates, but their influence is likely to be small under most conditions. Rates of  $N_2$ -fixation are orders of magnitude smaller than air-sea gas fluxes over most oceanic regions, minimizing the influence of this process on  $\Delta N_2/Ar$  (Figs. S7, S8). In nitrate-deplete waters of the subtropical and tropical ocean, where  $N_2$ -fixation is most important (Deutsch et al., 2007; Gruber & Sarmiento, 1997) the upper range of  $N_2$ -fixation rates is  $\sim 220$  mmol  $N_2$   $m^{-2}$   $yr^{-1}$  ( $\sim 0.6$  mmol  $N_2$   $m^{-2}$   $d^{-1}$ ). Elsewhere, mean estimates of  $N_2$ -fixation in subtropical, temperate and polar waters range from about  $<0.01$  to  $0.24$  mmol  $N_2$   $m^{-2}$   $d^{-1}$  (Blais et al., 2012; Sipler et al., 2017; Tang et al., 2019, 2020). Net air-sea exchange fluxes almost always exceed the maximum rate of  $N_2$ -fixation (Fig. S8), so that any  $\Delta N_2$  anomalies produced by biological processes should be rapidly erased at wind speeds above  $\sim 3$   $m$   $s^{-1}$ . Neglecting the influence of other physical gas fluxes (e.g. vertical mixing), maximum rates of  $N_2$ -fixation applied to our model will only induce a quasi-steady-state  $\Delta N_2$  anomaly larger than 0.05 % at  $u_{10}$  below  $6$   $m$   $s^{-1}$  (Fig. S8b), which only occurs consistently in a narrow latitude band near the equator. Regardless, periodic elevated sea states should rapidly erase any accumulated  $N_2$  deficits (Shigemitsu et al., 2016). Indeed, in an additional real-OSP run forced with constant global maximum  $N_2$ -fixation rate, simulated  $\Delta N_2$  always differed from values in the base run by less than 0.05 %. We thus conclude that  $N_2$ -fixation should not have a significant impact on the derivation of  $N_2'$ , or on  $\Delta O_2/N_2'$ -based NCP estimates.

The influence of denitrification and anammox on surface  $\Delta O_2/N_2'$  will also be small and indirect, as these processes elevate  $\Delta N_2/Ar_{deep}$  (Deutsch et al., 2007; Gruber & Sarmiento, 1997; Kana et al., 1998; Tortell, 2005), but do not alter surface  $N_2$  directly. Their contribution to potential vertical mixing of excess  $N_2$  into the mixed layer may only be prominent in regions

where  $O_2$  and nitrate depletion occurs in the upper few hundred of meters of the water column (e.g. Arabian Sea, Eastern Tropical North and South Pacific, suboxic inlets and estuaries; Chang et al., 2010, 2012; DeVries et al., 2012; Tortell, 2005; Wu et al., 2013) or overlying shallow continental shelves where benthic and sedimentary denitrification occur (DeVries et al., 2013). Taking an extreme upper limit of subsurface  $\Delta N_2/Ar$  of  $\sim 2$ -2.5 % in these regions (Chang et al., 2010; 2012; Shigemitsu et al., 2016), surface  $\Delta N_2/Ar$  anomalies will be less than 2.5 % (Fig. 1).  $N_2'$  corrections can minimize this bias, but even without such corrections, the error associated with a 2.5 % underestimation of  $\Delta O_2/N_2$  may be smaller than errors associated with vertical  $O_2$  mixing fluxes in continental shelf regions (see above).

Other processes which we have not evaluated in the present study, such as freshwater input, lateral mixing and ice melt/formation can also cause divergence between  $\Delta Ar$  and  $\Delta N_2$  (e.g. Beaird et al., 2015; Crabeck et al., 2014; Eveleth et al., 2017; Hamme et al., 2019; Hamme & Emerson, 2013; Loose & Jenkins, 2014; Top et al., 1988), but their contributions to surface  $\Delta N_2/Ar$  disequilibria, and the resulting uncertainty in  $\Delta O_2/N_2'$ -based NCP estimates are likely to be small in most ocean regions. As our model evaluation suggests (section 3.3, above), the framework we presented here captures the main drivers of inert gas and  $N_2$  variability in oceanic waters. Additional fluxes will be larger in coastal, or polar regions, but biases in NCP estimates resulting from vertical  $O_2$  fluxes or diel  $O_2$  variability are likely to be more significant in these regions (see above).

## 4 Conclusions

Global coverage of marine NCP estimates is constrained by the limitation of mass spectrometry to obtain underway  $\Delta O_2/Ar$  measurements. Recent advances in Optode and GTD technology have made high-resolution  $\Delta O_2/N_2$  sampling feasible, providing potential avenues to expand NCP from low-cost and user-friendly instrument systems (Izett & Tortell, 2020). Differences between Ar and  $N_2$  solubility properties necessitate careful interpretation of in-situ  $O_2/N_2$  measurements in order to accurately isolate biological  $O_2$  signatures. In the present study, we used a model to evaluate the main mechanisms controlling surface water uncoupling between  $\Delta O_2/Ar$  and  $\Delta O_2/N_2$ . Critically, our model, when parameterized with relevant environmental forcing and time-variable mixing terms, accurately captures the main processes driving surface ocean inert gas and  $N_2$  evolution.

From our numerical simulations, performed under experimental and realistic conditions, we find that seasonal SST variability exerts long-term control on  $\Delta O_2/Ar$  and  $\Delta O_2/N_2$  decoupling, with transient and baseline modifications resulting from enhanced bubble fluxes during periods of elevated wind-speeds, and variable vertical mixing fluxes. Due to differences in the sensitivity of Ar and  $N_2$  to SST variability and small bubble injection, nominal  $\Delta N_2/Ar$  anomalies are generally positive over a range of conditions, so that NCP estimates derived from raw  $\Delta O_2/N_2$  measurements could be biased low. Fortunately, the predictability of these anomalies to environmental perturbations permits corrections to  $\Delta N_2$  measurements, based on a new tracer,  $\Delta N_2'$ , which we derived from simple MLD budget calculations performed over a relevant NCP time-scale,  $\tau_{O_2}$ . Applying this  $\Delta N_2'$  approach using readily available reanalysis data products allows us to reconcile differences between  $\Delta O_2/Ar$  and  $\Delta O_2/N_2$ , making  $\Delta O_2/N_2'$  a robust NCP tracer.

The overall uncertainty in  $\Delta\text{O}_2/\text{N}_2'$ , resulting from model parameterization errors and necessary simplifying assumptions, is generally smaller than other sources of uncertainty in NCP calculations. Field application of the present approach will depend on the accuracy of environmental data products, and assumptions about the time-variability of mixed layer hydrography. Yet, even when differences between  $\Delta\text{O}_2/\text{Ar}$  and  $\Delta\text{O}_2/\text{N}_2'$  cannot be reduced to zero,  $\text{N}_2'$  is still a valuable tracer for minimizing NCP errors based on  $\text{O}_2/\text{N}_2$  measurements. This approach is expected to be most accurate in stratified waters and during summer conditions, when surface productivity is elevated, and mixing contributions to  $\Delta\text{N}_2/\text{Ar}$  decoupling may be neglected in  $\text{N}_2'$  calculations. In most ocean regions,  $\text{N}_2$ -fixation, denitrification and anammox will have a negligible impact on NCP estimates derived from underway  $\Delta\text{O}_2/\text{N}_2'$ .

Our work demonstrates the feasibility of deriving  $\Delta\text{O}_2/\text{N}_2'$ -based NCP estimates from underway  $\text{O}_2$  and  $\text{N}_2$  measurements and simple computations. The approach we describe here has the potential to greatly expand NCP coverage from research vessels, volunteer observing platforms and/or autonomous surface vehicles. This approach, combined with our upcoming field validation (manuscript in preparation) constitutes a significant advance in our ability to accurately quantify NCP and oceanic metabolism across a range of relevant space and time spaces.

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**$\Delta O_2/N_2'$  as a Tracer of Mixed Layer Net Community Production: Theoretical Considerations and Proof-of-Concept**

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**Introduction**

This supporting information provides supplementary figures, tables and explanations for the interpretation of the main text. Additional formulae derivations (S1) and error analyses (S2, Table S2) are also presented. A more detailed description of field applications of the  $N_2'$  approach presented in the main text is provided in section S3, with accompanying Matlab code and examples in a toolbox repository (available at <https://doi.org/10.5281/zenodo.4024952>, with link to [github.com/rizett/O2N2\\_NCP\\_toolbox](https://github.com/rizett/O2N2_NCP_toolbox) repository). Matlab code and output from the 1D numerical simulations described in the main text are also provided at the same repository.

## S1. One-dimensional mixed layer physical gas model

As per Eq. 2 in the main text, we applied the following mixed layer budget to O<sub>2</sub>, Ar and N<sub>2</sub>:

$$MLD \cdot \frac{dC}{dt} = F_d + F_B + F_M. \quad (S1.1)$$

In this equation, MLD is the mixed layer depth (m), dC/dt represents the change in gas concentration over time resulting from physical processes, F<sub>d</sub> represents the diffusive air-sea exchange flux, F<sub>B</sub> is the combined small and large bubble fluxes (representing air-sea exchange processes via complete bubble injection, F<sub>C</sub>, or partial exchange, F<sub>P</sub>, respectively), and F<sub>M</sub> is the sum of vertical diapycnal mixing (F<sub>k</sub>), upwelling (F<sub>w</sub>) and entrainment during mixed layer deepening (F<sub>e</sub>). We used the model of Liang et al. (2013) to parameterize the air-sea exchange terms (F<sub>d</sub>, F<sub>C</sub> and F<sub>P</sub>) in ice-free waters, and the model of Butterworth & Miller (2016) (which excludes explicit bubble fluxes) in partially-ice covered waters. We estimated the vertical mixing terms from subsurface gas concentrations (C<sub>deep</sub>) and mixing rates as described in the main text. Equation S1.1 can be expanded as:

$$MLD \cdot \frac{dC}{dt} = F_d + F_C + F_P + F_k + F_w + F_e. \quad (S1.2)$$

$$MLD \cdot \frac{dC}{dt} = \left[ k_d \left( C_{eq} \cdot \frac{SLP}{1 \text{ atm}} - C \right) \right] + \left[ \beta \cdot k_p \left( C_{eq} \cdot (1 + \Delta P) \cdot \frac{SLP}{1 \text{ atm}} - C \right) + \beta \cdot F_C \right] + \left[ \kappa_Z \cdot \frac{dC}{dz} \right] + \left[ \omega \cdot \frac{dC}{dz} \cdot MLD \right] + \left[ \frac{dMLD}{dt} \cdot (C_{deep} - C) \right] \quad (S1.3)$$

where k<sub>d</sub> and k<sub>p</sub> are the diffusive and bubble-mediated air-sea exchange coefficients, ΔP is the supersaturation increase caused by partially-dissolving bubbles, and F<sub>C</sub> is the small bubble flux, all parameterized in Liang et al. (2013) and Butterworth & Miller (2016) (F<sub>P</sub> and F<sub>C</sub> are zero in ice-covered conditions). Sensitivity analyses comparing our simulation results with in-situ observations at Ocean Station Papa suggest that a bubble-mediated gas flux scaling coefficient, β, of 0.5 is appropriate, as in Yang et al. (2017) (see Fig. 5 in the main text). C<sub>eq</sub> (mmol m<sup>-3</sup>) is the gas solubility at equilibrium, per Garcia & Gordon (1993) for O<sub>2</sub> and Hamme & Emerson (2004) for Ar and N<sub>2</sub>. SLP represents the sea level pressure (atm). The mixing terms are represented by the eddy diffusivity coefficient (κ<sub>Z</sub>; m<sup>2</sup> d<sup>-1</sup>), advection velocity (ω, proportional to wind speed; m d<sup>-1</sup>), the rate of mixed layer deepening (dMLD/dt; m d<sup>-1</sup>), the surface-to-subsurface gas gradient (dC/dZ = (C<sub>deep</sub> - C)/dZ; mmol m<sup>-4</sup>) and the deep gas concentration (C<sub>deep</sub>; mmol m<sup>-3</sup>). We set Ar<sub>deep</sub> and N<sub>2,deep</sub> values by adjusting subsurface ΔAr and ΔN<sub>2</sub>/Ar (i.e. ΔN<sub>2</sub>/Ar<sub>deep</sub>), while holding O<sub>2,deep</sub> constant at equilibrium concentrations (experimental simulations) or set to values based on observations (realistic simulations). The entrainment term is zero when the mixed layer shoals, and all mixing terms were set to zero in run a (no mixing) of the experimental and realistic simulations.

Matlab code for performing simulations with our 1D gas model is provided in the O2N2\_NCP\_toolbox on Zenodo (<https://doi.org/10.5281/zenodo.4024952>) and GitHub ([github.com/rizett/O2N2\\_NCP\\_toolbox](https://github.com/rizett/O2N2_NCP_toolbox)). Users can define forcing input (e.g. environmental data, initial conditions, and mixing coefficients) and experimental settings (e.g. see details in table 1 in the main text), and can specify the air-sea flux parameterization.

## S1.2 N<sub>2</sub>' budget: Quasi-steady-state conditions and estimating O<sub>2</sub> re-equilibration timescale

The N<sub>2</sub>' term is derived by predicting N<sub>2</sub> and Ar divergence over a MLD O<sub>2</sub> re-equilibration time scale (defined below in Eq. S6.3), and subtracting this value from observed N<sub>2</sub> saturation. To derive N<sub>2</sub>', we simplified the MLD budget described in Eq. S1 by combining all mixing processes into a single term. We set F<sub>e</sub> to zero, and collapsed the remaining fluxes with a single coefficient,  $\kappa$  ( $\kappa = \kappa_z + \omega^* dz$ ; m<sup>2</sup> d<sup>-1</sup>):

$$F_k + F_w + F_e \approx \frac{dC}{dz} \kappa \quad (S2)$$

Combining Eqs. S1.2 and S2 yields the simplified budget used to perform N<sub>2</sub>' calculations (Eq. 3 in the main text), which was evaluated over one O<sub>2</sub> re-equilibration time,  $\tau_{O_2}$  (Eq. S6.3), prior to observations (Fig. S2).

$$MLD \cdot \frac{dC}{dt} = \left[ k_d \left( C_{eq} \cdot \frac{SLP}{1 atm} - C \right) \right] + \left[ \beta \cdot k_p \left( C_{eq} \cdot (1 + \Delta P) \cdot \frac{SLP}{1 atm} - C \right) + \beta \cdot F_c \right] + \frac{dC}{dz} \kappa \quad (S3)$$

Using this budget, we calculated the expected divergence between Ar and N<sub>2</sub> saturation states at the end of the  $\tau_{O_2}$  time period, and subtracted this difference from the true  $\Delta N_2$  (Eq. 4 in the main text; Fig. S2). In the model setting, true  $\Delta N_2$  (i.e.  $\Delta N_2^{true}$ ) is the N<sub>2</sub> supersaturation anomaly predicted by the full MLD budget (Eq. S1), and in field studies,  $\Delta N_2^{true}$  is the measured N<sub>2</sub> supersaturation. Figure S2 shows a representation of calculations performed with the full and condensed N<sub>2</sub>' MLD budgets. The approach to estimating N<sub>2</sub>' was repeated for all time points in the full model simulations. In field studies, calculations will be performed over the O<sub>2</sub> re-equilibration timeframe prior to each observation, in an analogous approach to calculations of a weighted piston velocity (Reuer et al., 2007). Matlab code, and example data are provided at <https://doi.org/10.5281/zenodo.4024952>. Refer to section S3 for further details.

The analytical solution to Eq. S3 describes the quasi-steady-state gas condition, and can be derived by further simplifying the gas budget to combine the air-sea exchange terms, following (Woelf, 1997) and Eq. 2 in Liang et al. (2013):

$$F_d + F_c + F_p \approx -k_T \left( C - C_{eq} (1 + \Delta_{eq}) \frac{SLP}{1 atm} \right) \quad (S4)$$

Here  $k_T$  is the pooled diffusive and bubble-mediated gas transfer coefficients (i.e.  $k_d + \beta \cdot k_p$ ) and  $\Delta_{eq}$  is the bubble-induced steady-state gas supersaturation. This approximation simplifies the derivation of the analytical solution, and matches the net air-sea flux predicted by the full parameterization (as in Eq. S1) with a relative accuracy of ~2 % over a range of wind speeds (0-25 m s<sup>-1</sup>) and gas saturation states (90-110 %; results not shown). The analytical solution can subsequently be derived by discretizing the simplified gas budget into sufficiently short time

increments,  $dt$ , so that  $MLD$ ,  $k_T$ ,  $\Delta_{eq}$ ,  $C_{deep}$  and  $\kappa$  can be considered constant. Below, we derive the analytical solution to the simplified budget through the following steps:

1) Expand Eq. S3 with simplified gas flux terms.

$$\frac{dC}{dt} = \frac{-k_T}{MLD} \left( C - C_{eq} (1 + \Delta_{eq}) \frac{SLP}{1 atm} \right) + \frac{C_{deep} - C}{dz} \frac{\kappa}{MLD} \quad (S5.1)$$

2) Simplify  $k_T/MLD$  and  $\kappa/(dz \cdot MLD)$  as  $K_1$  and  $K_2$ , respectively, and re-write the equation by combining terms.

$$\frac{dC}{dt} = -(K_1 + K_2) \cdot C + K_1 \cdot C_{eq} \cdot (1 + \Delta_{eq}) \frac{SLP}{1 atm} + K_2 \cdot C_{deep} \quad (S5.2)$$

3) Further simplify by expressing  $(K_1 + K_2)$  as  $P$ ,  $\left( K_1 \cdot C_{eq} \cdot (1 + \Delta_{eq}) \cdot \frac{SLP}{1 atm} + K_2 \cdot C_{deep} \right)$  as  $Q$ , and  $dC/dt$  as  $C'$ . Apply an integration factor of  $e^{Pt}$ .

$$C' = -P \cdot C + Q \quad (S5.3)$$

$$C' \cdot e^{Pt} + P \cdot C \cdot e^{Pt} = Q \cdot e^{Pt} \quad (S5.4)$$

4) Note that  $d/dt(C \cdot e^{Pt}) = C' \cdot e^{Pt} + P \cdot C \cdot e^{Pt}$  by the product rule.

$$\frac{d}{dt}(C \cdot e^{Pt}) = Q \cdot e^{Pt} \quad (S5.5)$$

$$C \cdot e^{Pt} = Q \cdot \int e^{Pt} dt \quad (S5.6)$$

5) Since  $P$  and  $Q$  (defined above in step 3) are considered constant over  $dt$ , Eq. S5.6 can be integrated simply. In Eq. S5.7,  $R$  is the integration constant.

$$C = \frac{Q}{P} + R \cdot e^{-Pt} \quad (S5.7)$$

6) Finally, by setting  $C(t=0)$  to be the initial condition,  $C_0$ , we derive a single analytical solution, by re-substituting the simplifying terms ( $P$  and  $Q$  defined above in step 3) for the gas flux terms.

$$R = C_0 - \frac{Q}{P} \quad (S5.8)$$

$$C = \frac{k_T \cdot C_{eq} \cdot (1 + \Delta_{eq}) \cdot \frac{SLP}{1 atm} + \frac{\kappa}{dz} \cdot C_{deep}}{k_T + \frac{\kappa}{dz}} + \left( C_0 - \frac{k_T \cdot C_{eq} \cdot (1 + \Delta_{eq}) \cdot \frac{SLP}{1 atm} + \frac{\kappa}{dz} \cdot C_{deep}}{k_T + \frac{\kappa}{dz}} \right) \cdot e^{-\left( \frac{k_T}{MLD} + \frac{\kappa}{dz \cdot MLD} \right) t} \quad (S5.9)$$

When mixing is negligible (i.e.  $\kappa \approx 0 \text{ m}^2 \text{ d}^{-1}$ ), Eq. S5.9 simplifies to

$$C = C_{eq} \cdot (1 + \Delta_{eq}) \cdot \frac{SLP}{1 \text{ atm}} + \left( C_0 - C_{eq} \cdot (1 + \Delta_{eq}) \cdot \frac{SLP}{1 \text{ atm}} \right) \cdot e^{-\left(\frac{k_T}{MLD}\right)t} \quad (S5.10)$$

The analytical solution is useful for understanding quasi-steady-state gas conditions, and the rate of response to perturbations. For example, the quasi-steady-state gas concentration,  $C_{SS}$ , can be predicted from Eq. S5.9 as  $t$  approaches infinity, and  $C$  approaches the value of the first term:

$$C_{SS} = \frac{k_T \cdot C_{eq} \cdot (1 + \Delta_{eq}) \cdot \frac{SLP}{1 \text{ atm}} + \frac{\kappa}{dz} \cdot C_{deep}}{k_T + \frac{\kappa}{dz}} \quad (S5.11)$$

Subsequently, the mixed layer  $O_2$  re-equilibration timescale,  $\tau_{O2}$ , can be estimated as the time required for air-sea gas exchange and vertical mixing processes to re-establish the quasi-steady-state condition. We thus estimated  $\tau_{O2}$  by setting  $(C - C_{SS}) / (C_0 - C_{SS})$  to be 0.01 (i.e.  $C - C_{SS} < C_0 - C_{SS}$ ) and  $t$  to  $\tau_{O2}$ :

$$C = C_{SS} + (C_0 - C_{SS}) \cdot e^{-\left(\frac{k_T}{MLD} + \frac{\kappa}{dz \cdot MLD}\right)\tau_{O2}} \quad (S6.1)$$

$$\frac{C - C_{SS}}{C_0 - C_{SS}} = 0.01 = e^{-\left(\frac{k_T}{MLD} + \frac{\kappa}{dz \cdot MLD}\right)\tau_{O2}} \quad (S6.2)$$

$$\tau_{O2} = \frac{-\ln(0.01) \cdot MLD}{\left(k_T + \frac{\kappa}{dz}\right)} \quad (S6.3)$$

The MLD  $O_2$  re-equilibration time calculated by this approach represents several MLD  $O_2$  residence times, which is typically approximated by  $MLD/k_T$ .

Since the exponential weighting function used to calculate  $O_2$  piston velocities is typically negligible after ~30 days (Teeter et al., 2018), calculation of gas transfer coefficients (i.e. Eq. 5 in the main text) will not be significantly impacted by the choice to weight  $k_{O2}$  over  $\tau_{O2}$  or  $MLD/k_T$ . However, calculating  $\tau_{O2}$  by this approach reflects the contribution of vertical mixing (proportional to  $\kappa$ ) in reducing  $O_2$  cycling in surface waters, and more fully represents the timeframe of gas re-equilibration within the MLD. This timescale,  $\tau_{O2}$ , is therefore more appropriate for  $N_2'$  calculations relevant to NCP derivation. Indeed, when the  $N_2'$  calculations are performed over a timescale represented by  $MLD/k_T$ , differences between Ar and  $N_2$  relevant to NCP calculations are not fully reconciled (Fig. S2b). In ocean environments, where MLD,  $k_T$  and  $\kappa$  vary in time,  $\tau_{O2}$  should be estimated using 30- to 60-day weighted values for these terms, where possible, or from ship-based observations.

## S2. Uncertainty analyses

### S2.1 $\Delta N_2'$ parameter uncertainty



We performed a Monte Carlo analysis on the real-OSP and real-BB full mixing (run c) simulations to determine the contributions of individual and combined parameterization uncertainty to errors in  $\Delta\text{O}_2/\text{N}_2'$ . This analysis was conducted by randomly varying each of the input variables (wind speed, SST, SLP, MLD), air-sea flux ( $F_d$ ,  $F_P$ ,  $F_C$ ,  $\beta$ ) and mixing terms ( $\kappa$ ,  $\Delta\text{N}_2/\text{Ar}_{\text{deep}}$ ) in the  $\text{N}_2'$  MLD budget (Eq. S4 above, and Eq. 3 in the main text) around their estimated uncertainties (Table S1), and performing 100 (for individual parameter errors) or 1000 (for combined errors) iterations of  $\text{N}_2'$  calculations.

We used uncertainties of  $\pm 2.5 \text{ m s}^{-1}$ ,  $\pm 0.75 \text{ }^\circ\text{C}$  and  $\pm 2 \text{ mbar}$  in the wind speed, SST and SLP data based on a comparison of in-situ observations (from ships, moorings and weather buoys) with various gridded products. For observations based in the Subarctic NE Pacific, the Cross-Calibrated Multi-Parameter (CCMP) wind speed product (provided by Remote Sensing Systems at [www.remss.com](http://www.remss.com); Atlas et al., 2011), NOAA High Resolution SST Dataset (provided by NOAA ESRL at <https://psl.noaa.gov/>; Reynolds et al., 2007), and NCEP/NCAR reanalysis 2 SLP (provided by NOAA ESRL at [psl.noaa.gov](http://psl.noaa.gov); Kalnay et al., 1996) products compared best with observations from moorings in coastal and off-shore waters. In the Arctic, the NCEP/NCAR Reanalysis 2 wind product performed best.

The air-sea flux terms ( $F_d$ ,  $F_P$  and  $F_C$ ) depend on the choice of gas transfer parameterization. In the present study, we use the bubble-mediated model of Liang et al. (2013), as it was parameterized for  $\text{O}_2$  and  $\text{N}_2$ , and is considered valid for gases with similarly low solubility. Over a range of wind speeds and temperatures, we estimate the relative uncertainty in these terms to be  $\sim 18\text{--}24 \%$ , based on the standard deviation of values derived using several gas transfer parameterizations (Stanley et al., 2009; Sweeney et al., 2007; Vagle et al., 2010; Wanninkhof, 2014; Woolf, 1997). These errors are roughly consistent with Wanninkhof (2014), who estimated a mean total error in the air-sea gas flux of  $\sim 20 \%$ . We therefore followed Bushinsky & Emerson (2015) by assigning a relative error of  $15 \%$  to  $F_d$ ,  $F_P$  and  $F_C$  in our Monte Carlo analysis. Finally, we ascribed an error of  $\pm 5 \text{ m}$  to estimates of the MLD, following Izett et al. (2018), an error of  $\pm 0.14$  to  $\beta$  based on Emerson et al. (2019), and conservative uncertainties of  $\pm 10^{-5} \text{ m}^2 \text{ s}^{-1}$  and  $0.25 \%$  to

Overall, we find that uncertainty in the sea surface temperature product (mean  $0.07 \%$ ) contributes the largest individual errors to  $\Delta\text{O}_2/\text{N}_2'$ . This is unsurprising as seasonal SST variability, which drives diffusive air-sea exchange, contributes to strong variability in  $\Delta\text{N}_2/\text{Ar}$  (see main text). Errors in the mixing coefficient term were next greatest (mean  $0.02 \%$ ), while errors in the bubble-flux terms ( $\beta$ ,  $F_C$ ,  $F_P$ ) were generally small, due to the low prevalence of high wind speeds. Errors associated with these terms were typically larger during autumn to spring, when wind speeds were elevated. The combined uncertainty from all parameterizations is  $0.09 \%$ , on average, across both real-OSP and real-BB simulations.

## S2.2 Assumption uncertainty

The  $\text{N}_2'$  approach assumes constant values of MLD, salinity,  $\kappa$ , and  $\Delta\text{N}_2/\text{Ar}_{\text{deep}}$ , based on the availability of data products and at-sea measurements (see main text for details). To evaluate the uncertainty in  $\text{N}_2'$  incurred by these assumptions, we compared calculations on the real-OSP and real-BB full mixing (run c) simulations in which these values were held constant against calculations in which they were allowed to vary, based on values in the full model simulations. Across both simulations, we found mean errors in  $\Delta\text{O}_2/\text{N}_2'$  from these assumptions of  $0.07 \%$

(range ~0.001 – 0.3; Table S1). This value is similar to the combined parameterization uncertainty, but can only be reduced through accurate estimation of the time-history of MLD, salinity  $\kappa$ , and  $\Delta N_2 / Ar_{\text{deep}}$  terms. This may not be feasible for many field measurement programs.

In general, the uncertainties associated with the  $N_2'$  assumptions were larger in the real-BB simulation (Fig. S9b) due to significant and rapid variability in subsurface temperature, and therefore subsurface  $N_2$  and Ar concentrations, invoked in our model. These uncertainties, and the remaining biases in  $\Delta N_2' / Ar$  ( $\Delta O_2 / Ar - \Delta O_2 / N_2'$  almost as large as  $\Delta O_2 / Ar - \Delta O_2 / N_2$  in Fig. S9b), are likely represent the upper range errors in the approach presented here, as subsurface inert gas concentrations likely do not vary as much in reality as they do in our modeled environment. In the absence of time-series observations of subsurface gas concentrations in Baffin Bay, we necessarily set  $N_{2,\text{deep}}$  and  $Ar_{\text{deep}}$  equivalent to their equilibrium concentrations at the time-variable temperature and salinity conditions of the deep box layer. The large amplitude in temperature variability in this deep box layer results from significant shoaling of the MLD as the model progresses into summer months, and contributed to significant variability in subsurface  $N_2$  and Ar concentrations. As the  $N_2'$  approach assumes these values are constant over the duration of calculations, failure to represent this variability will result in large remaining biases in  $\Delta N_2' / Ar$ . If deep gas concentrations do not vary to such large degrees in reality, the errors in  $N_2'$  would be significantly smaller, as in the real-OSP simulation.

### S2.3 Uncertainty from $N_2$ -fixation

We estimated the potential uncertainty in  $N_2'$  and  $\Delta O_2 / N_2'$  due to  $N_2$ -fixation by applying constant rates of  $N_2$  removal (see main text for details) in 1D model simulations without vertical mixing over a range of constant  $u_{10}$  and SST. We compared the steady-state  $\Delta N_2$  from these runs against values obtained with  $N_2$ -fixation rates of zero. For the upper range of  $N_2$ -fixation observed in the ocean, we calculate a maximum steady-state deviation of ~0.3 % at very low wind speeds, but values are always less than 0.05 % above wind speeds of  $6 \text{ m s}^{-1}$  (Fig. S8c). Applying a constant  $N_2$ -fixation rate equivalent to the global observed maximum (see main text) to the real-OSP full mixing run resulted in deviations of less than 0.05 % in  $N_2$  saturation when compared against the run excluding  $N_2$ -fixation. We thus conclude that  $N_2$ -fixation will have a negligible effect on  $\Delta O_2 / N_2'$  calculations in most oceanic waters.

### S2.4 Total uncertainty

Our error analyses produce a total average uncertainty in  $\Delta O_2 / N_2'$  of 0.01 % (range 0.04 – 0.3; Table 1) resulting from the parameterization and assumption errors. On average, this is smaller than the offset between  $\Delta O_2 / Ar$  and uncorrected  $\Delta O_2 / N_2$ . The upper range of uncertainty in  $\Delta O_2 / N_2'$  (including potential contributions from  $N_2$ -fixation) is represented in Fig. S9, which presents  $\Delta O_2 / Ar - \Delta O_2 / N_2'$  from the realistic OSP and BB simulations (full mixing scenario / run c only). Since the assumption errors contribute the largest proportion to total  $\Delta N_2'$  uncertainty, the total error in  $\Delta O_2 / N_2'$  is smallest when these values are small during periods of reduced MLD,  $\kappa$  and  $\Delta N_2 / Ar_{\text{deep}}$  variability (see Figs. 3-4 in the main text). In field studies, the error approximated here and potential uncertainty from in-situ  $O_2$  and  $N_2$  measurement accuracy will contribute to total uncertainty in  $\Delta O_2 / N_2'$ .

We exclude the RMSE derived from the  $N_2$  validation against observations (0.9 %; see main text) from the total estimated  $N_2'$  uncertainty, as this likely over-estimates the relative differences between Ar and  $N_2$ .

### S3 Application of the $N_2'$ approach to field data

In field-based applications, derivation of  $N_2'$  estimates requires measurements of surface gas concentrations ( $N_2$ ), hydrographic data (temperature and salinity) and best estimates of the MLD and the mixing terms  $\kappa$  and  $\Delta N_2/Ar_{deep}$  at the time of sampling. MLD can be derived by interpolating between CTD casts or using climatological datasets, whereas mixing terms can be estimated from observations, numerical models or archived datasets (see main text for details). Information on ocean conditions (SST,  $u_{10}$ , and SLP) prior to gas measurements, during the  $O_2$  re-equilibration time frame (typically ~60-90 days in ice-free waters; Eq. 6.3), are also necessary to perform calculations. These "historic" data can be obtained from reanalysis or satellite products. The MLD,  $\kappa$  and  $\Delta N_2/Ar_{deep}$  will commonly be assumed constant backwards in time, based on values at the time of ship-board gas observation, or based on alternative sources (see main text).

In Eq. 4 in the main text,  $\Delta N_2^{obs}$  is the measured gas supersaturation condition, and  $\Delta N_2^{est}$  and  $\Delta Ar^{est}$  are predicted by the calculations described above in section S1.2.  $N_2'$  calculations are performed in a similar approach to piston velocity weighting (Reuer et al., 2007), and the weighting function (Eq. 4 in Teeter et al., 2018) should be applied to the historic estimates of wind speed and  $\kappa$  when evaluating the  $O_2$  re-equilibration and  $N_2'$  timescale from Eq. 6.3. All input data should have the same spatial resolution as continuous  $O_2/N_2$  observations, with  $N_2'$  calculations applied independently to each underway gas measurement.

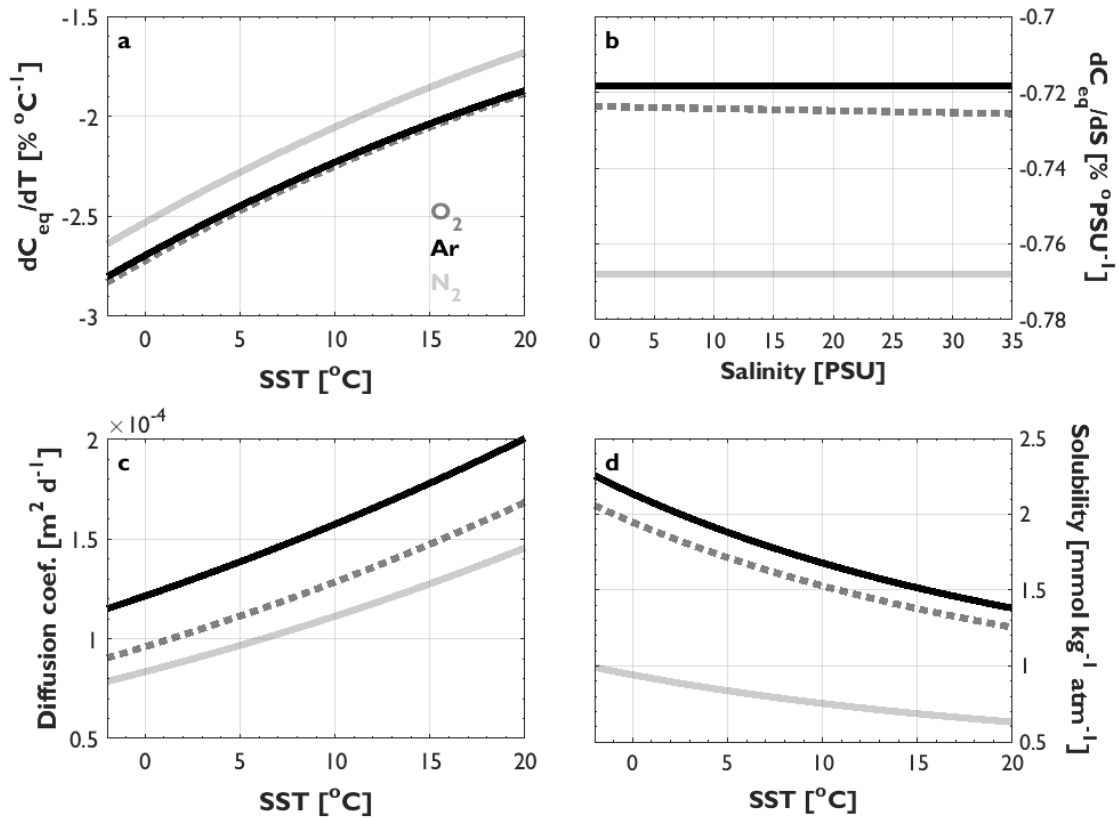
In using our Matlab codes (with examples in the O2N2\_NCP\_toolbox; <https://doi.org/10.5281/zenodo.4024952>), users provide the historic datasets, observed  $\Delta N_2$ , and specify the gas transfer parameterization (including  $\beta$  gas scaling term) best suited to their region of study. These codes can be used as templates for future studies, and can be modified to incorporate future developments. The main codes we provided were written by R. Izett, with additional scripts cited accordingly.

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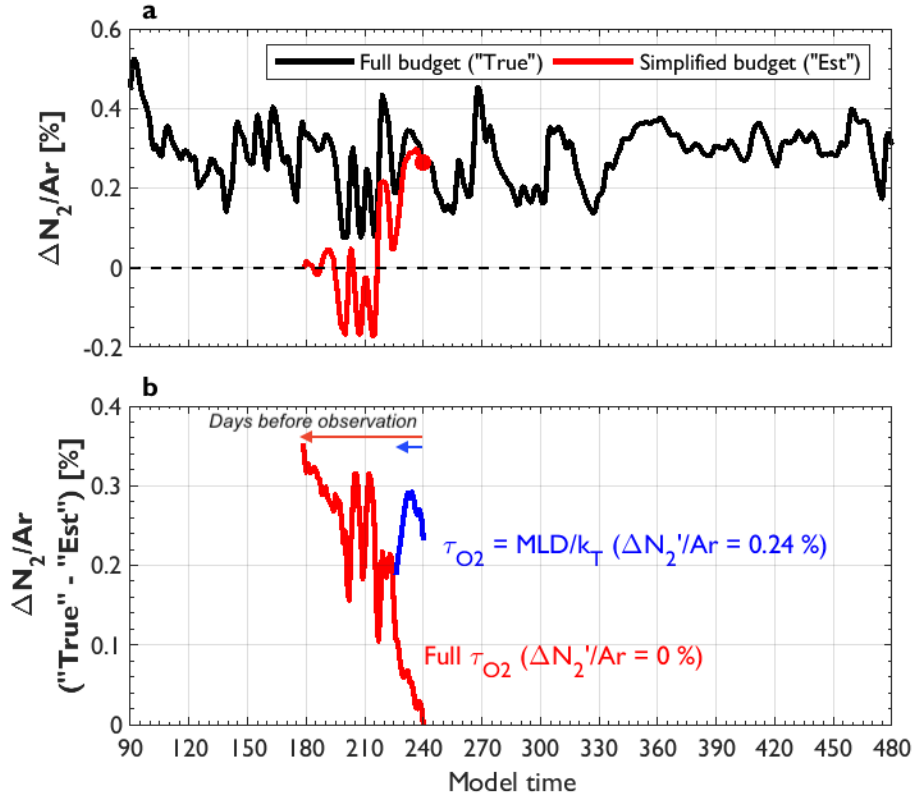
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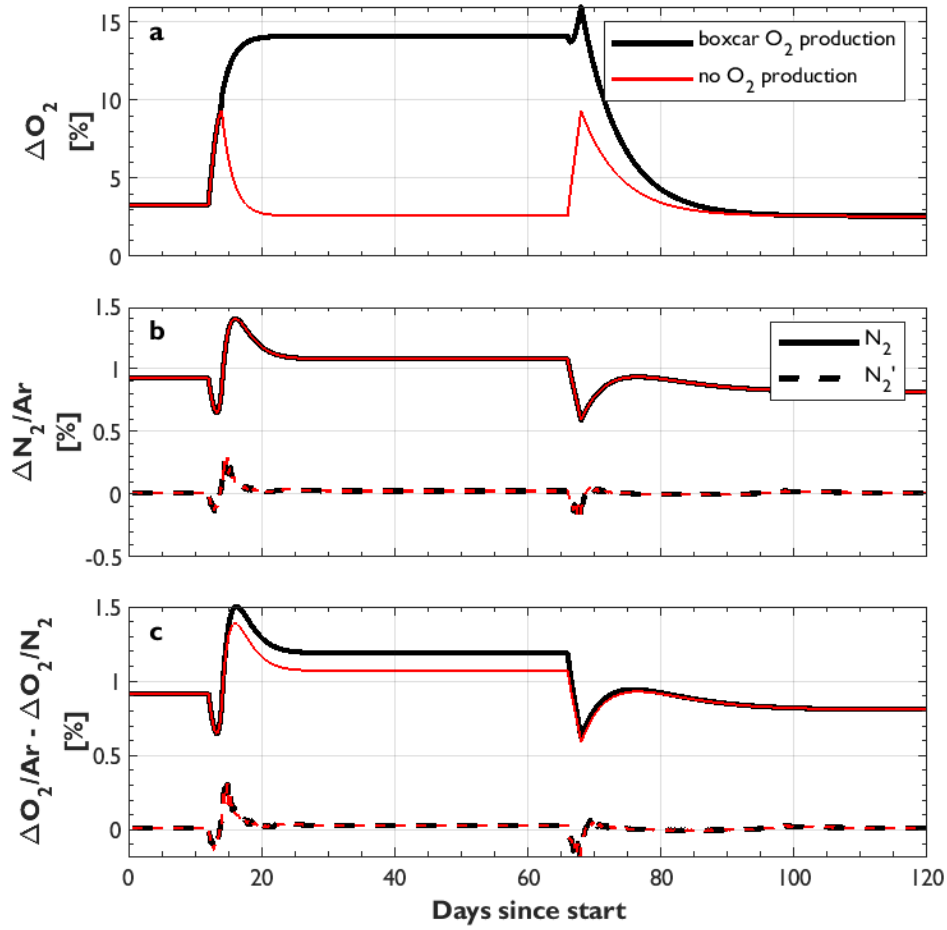
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**Figure S1.** The differential physical properties of  $O_2$  (dotted grey), Ar (black) and  $N_2$  (solid grey) across a range of temperatures and salinities. Panels (a) and (b) represent the solubility-temperature and -salinity dependence of each gas, respectively, panel (c) presents their air-sea diffusion exchange coefficients, and panel (d) shows the Henry's Law solubility for each gas in one standard atmosphere of dry air. Lines represent average values over a salinity range of 0-35 PSU (panels a, c and d) or a temperature range of -2 to 10  $^{\circ}C$  (panel b).

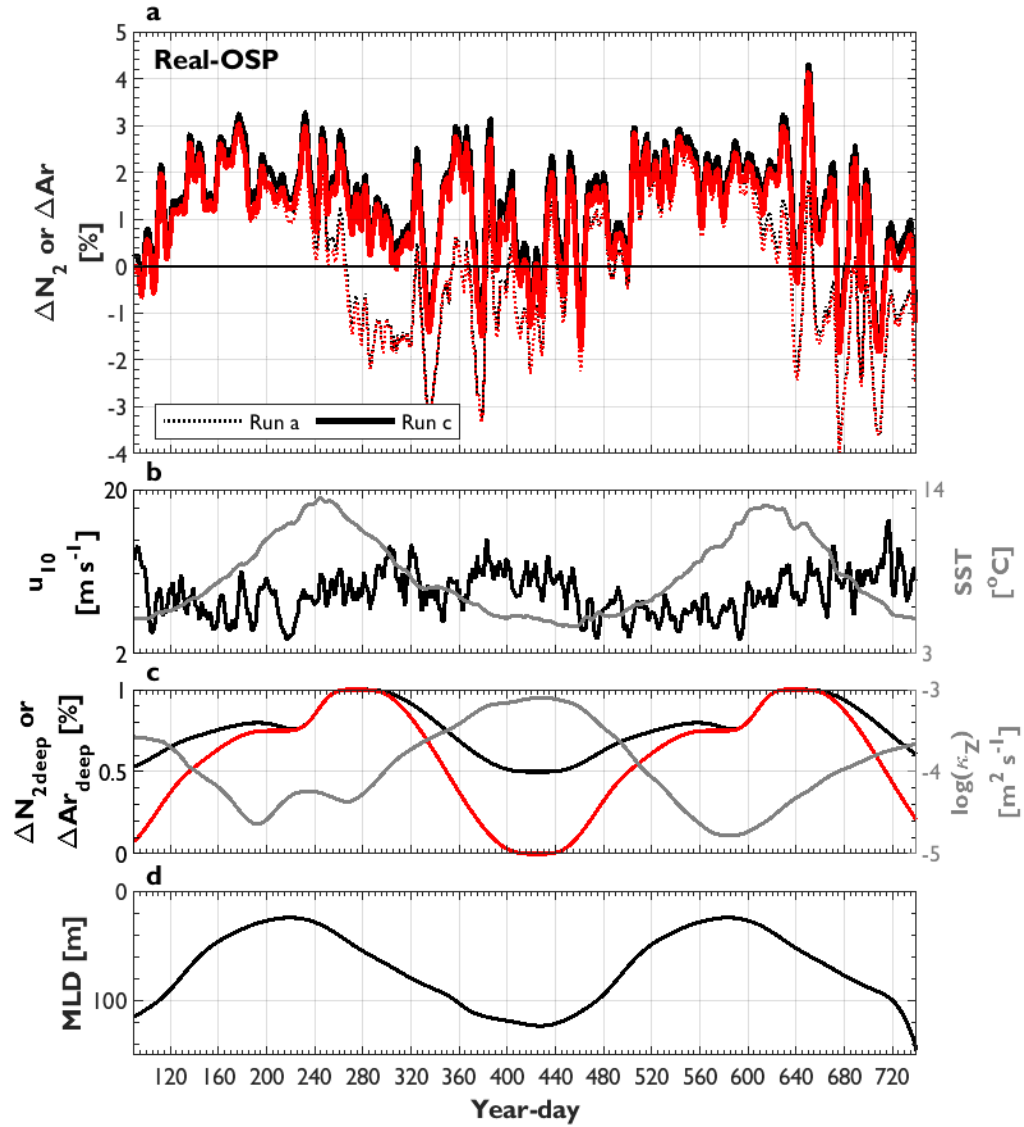


**Figure S2.** An example of the application of the  $N_2'$  approach. Panel (a) shows  $\Delta N_2/Ar$  predicted in a full model simulation (i.e. based on  $\Delta N_2^{\text{true}}$  and  $\Delta Ar$  from a real-OSP simulation with mixing; black line), and one example of values calculated using  $\Delta N_2^{\text{est}}$  and  $\Delta Ar^{\text{est}}$  (red line, Eq. 4 in the main text) derived by evaluating the  $N_2'$  budget over the  $O_2$  re-equilibration timescale,  $\tau_{O_2}$  before the time of observation (Eq. 3 in the main text and Eq. S3 above).  $\Delta N_2'$  was estimated by subtracting the estimated difference between  $\Delta N_2$  and  $\Delta Ar$  (i.e.  $\Delta N_2^{\text{est}} - \Delta Ar^{\text{est}}$ ) obtained from the simplified model from  $\Delta N_2^{\text{true}}$  at the time marked by the red dot. This was repeated for all time points obtained from the full model simulation. Panel (b) represents the difference in  $\Delta N_2/Ar$  predicted by the full model and the simplified model over the time frame of calculations. Two sets of calculations are shown: one for the full  $\tau_{O_2}$  (estimated from Eq. S6.3) and one set performed over an  $O_2$  residence time, approximated as  $MLD/k_{O_2}$ . Note that the latter is too short of a time period to fully-reconcile  $\Delta N_2$  and  $\Delta Ar$  differences relevant to NCP calculations.

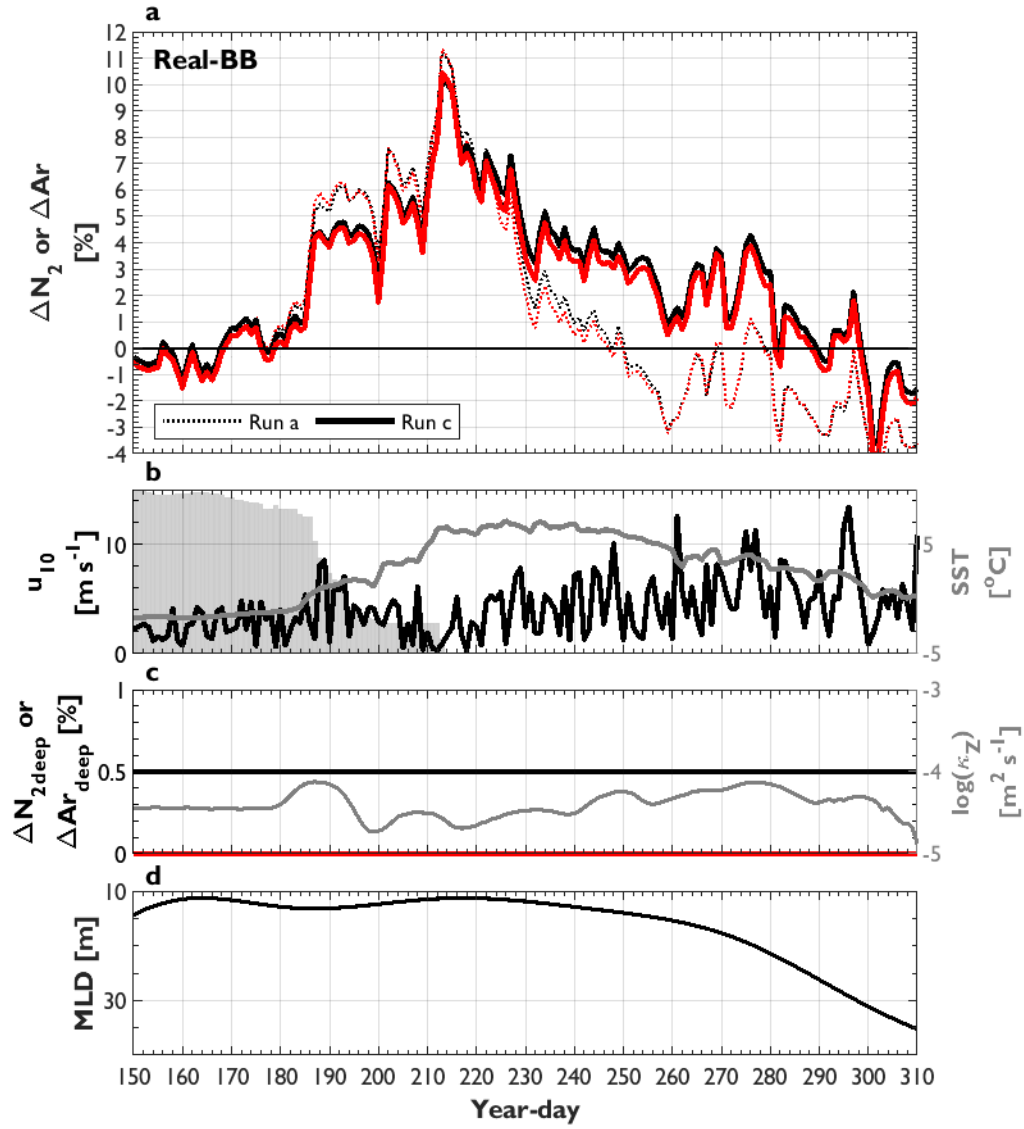


**Figure S3.** Results from a numerical simulation (Ex-IF 3) exploring the impact of biological  $O_2$  production on surface gas concentrations. Black and red lines represent simulation results obtained with (black) and without (red) biological  $O_2$  production ( $20 \text{ mmol } O_2 \text{ m}^{-2} \text{ d}^{-1}$ ). Productivity transients were applied as a boxcar step change corresponding with the changes in environmental forcing (Table 1). The results represented by the red lines correspond with the results presented in Fig. 2c in the main text. Panels (b) and (c) demonstrate that the  $N_2'$  approach is equally skillful in representing excess  $\Delta N_2$  with both high and low rates of biological  $O_2$  production, and that  $\Delta N_2'$  is insensitive to  $\Delta O_2$ .

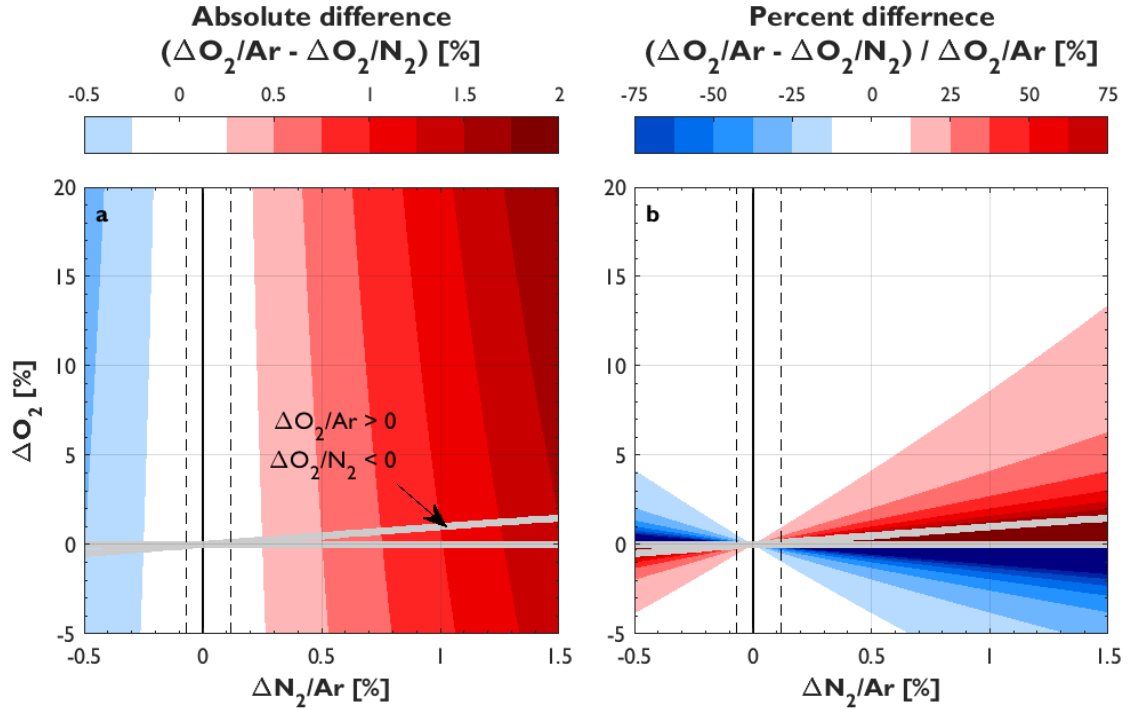




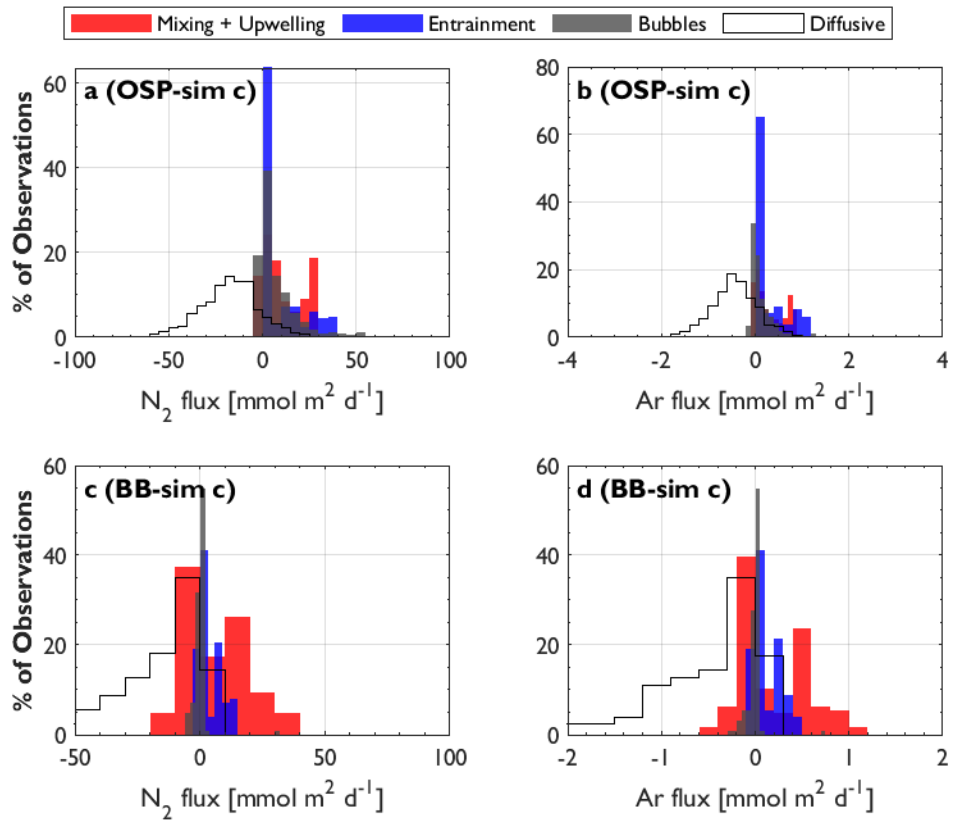
**Figure S4.**  $\Delta N_2$  (black) and  $\Delta Ar$  (red) in the realistic OSP simulation, with corresponding forcing parameters. In panel (a), solid lines represent output from the full-mixing simulation (i.e. run c), and dotted lines represent output from simulations with no mixing (run a). In panel (c), the black line represents subsurface  $\Delta N_2$ , while the red line represents subsurface  $\Delta Ar$ . The x-axes represent April 2011-Jan. 2013. Refer to Figs. 3, 4 and Table 1 in the main text for further details.



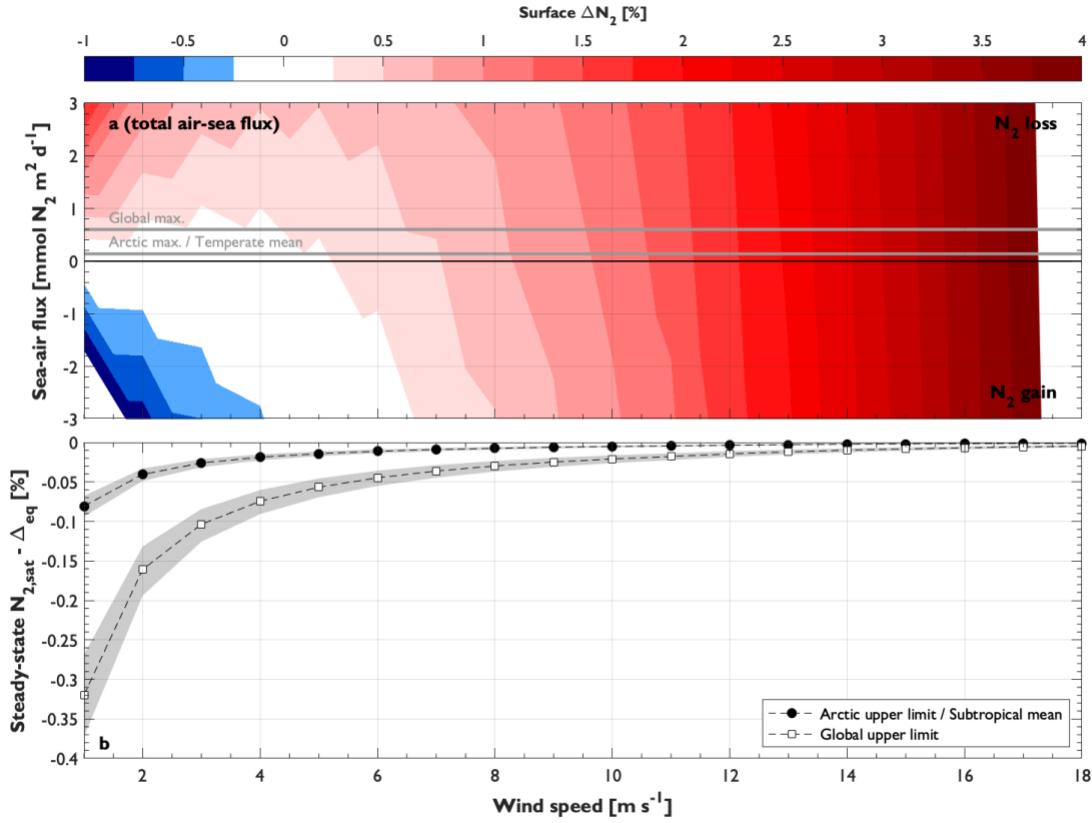
**Figure S5.**  $\Delta N_2$  (black) and  $\Delta Ar$  (red) in the realistic BB simulation, with corresponding forcing parameters. The x-axes represent 2019 year-day. Refer to Fig. S4 (above) and Figs. 3, 4 and Table 1 in the main text for further details.



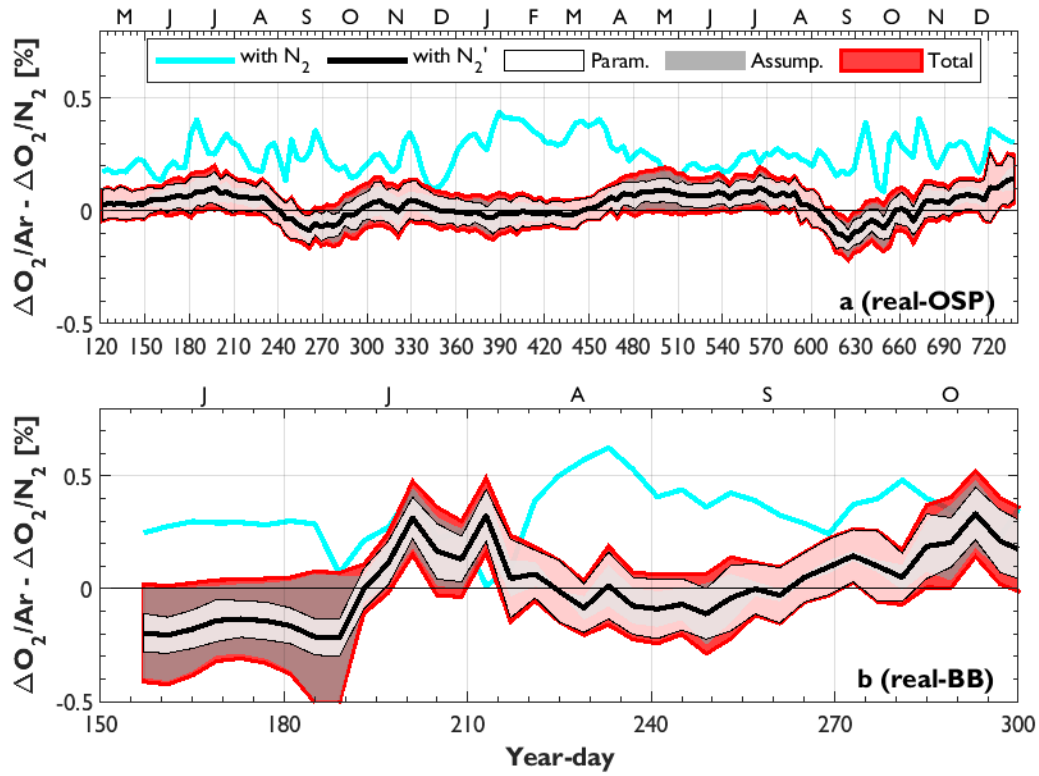
**Figure S6.** The absolute (a) and relative (b) differences between  $\Delta O_2/Ar$  and  $\Delta O_2/N_2$  over a realistic range of surface  $\Delta O_2$  in the ocean, and  $\Delta N_2/Ar$  produced in the model simulations. Differences represent uncertainty in NCP estimates derived from  $O_2/N_2$  if corrections for excess  $N_2$  supersaturation are not made. The grey outlined region in both panels represents scenarios where  $\Delta O_2/Ar$  and  $\Delta O_2/N_2$  have opposite signs, leading to false interpretation of net tropic status from  $\Delta O_2/N_2$  measurements. The vertical dashed lines represent the range of  $\Delta N_2/Ar$  (i.e. after correcting for excess  $N_2$  supersaturation) in the realistic model simulations.



**Figure S7.** The frequency distribution of mixed layer fluxes in the realistic real-OSP (a, b) and real-BB (c, d) model run c (left = N<sub>2</sub>; right = Ar). A positive flux represents an increase in the gas in the mixed layer.



**Figure S8.** Relative importance of  $N_2$  fixation and sea-air flux on surface  $N_2$  supersaturation. Panel (a) shows the effect of total sea-to-air flux at various wind speeds, based on the Liang et al. (2013) exchange parameterization. Estimates of the global maximum and Arctic maximum / global subtropical mean  $N_2$ -fixation rates are shown as grey lines (details in main text), and the solid black line represents a  $N_2$ -fixation rate of zero. Biological  $N_2$  removal is only significant when the magnitude of  $N_2$ -fixation exceeds the air-sea flux, which only occurs over a narrow range of conditions. Panel (b) shows the quasi-steady-state deviation of  $\Delta N_2$  from the bubble-induced supersaturation state ( $\Delta_{eq, N_2}$ ; Liang et al., 2013) for various wind speeds. Lines depict results calculated using different estimates of  $N_2$ -fixation rates, and shading represents the range of results over a range of temperate (0-25 °C) and salinity (0-35 PSU). A steady-state deviation value of 0 % means that bubble-mediated air-sea flux processes dominate over  $N_2$ -fixation. Other physical processes, including vertical mixing are ignored here. The x-scales on both panels are truncated at 18  $\text{m s}^{-1}$  because air-sea fluxes almost always exceed  $N_2$ -fixation rates above this threshold.



**Figure S9.**  $\Delta O_2/Ar - \Delta O_2/N_2$  in the real-OSP (a) and real-BB (b) run c (full mixing) simulations. Uncertainty in  $\Delta O_2/N_2'$  is represented as shaded regions around model-derived  $\Delta O_2/Ar - \Delta O_2/N_2'$  values (black lines represent values with  $N_2'$ , and blue lines are values with uncorrected  $N_2$ ). The light grey patch represents the combined parameterization uncertainty, the dark grey patch is uncertainty from  $N_2'$  assumptions, and the red patch is the estimated total uncertainty, including the upper range of potential  $N_2$ -fixation. Mean uncertainty estimates are summarized in table S1.

**Table S1.** Sources of uncertainty in  $\Delta\text{O}_2/\text{N}_2'$ , based on the full mixing runs of the realistic simulations (real-OSP run c, and real-BB run c). We performed Monte Carlo simulations by randomly applying parameter errors to each variable separately and in combination. Reported uncertainty (upper section, right column; in order of descending importance) represents the range and mean (in parentheses) of values across the model simulations. The error associated with the  $\text{N}_2'$  budget assumptions (i.e. constant salinity, MLD,  $\kappa$ , and  $\Delta\text{N}_2/\text{Ar}_{\text{deep}}$ ) was evaluated by running an additional simulation in which these terms were set to the true values from the full 1D simulation environment. The total uncertainty presented at the bottom of the upper section was derived by summing in quadrature each of the underlined errors. Additional biases and uncertainty in NCP calculations are shown in the lower section of the table. NCP errors are based on Eq. 5 in the main text, over a realistic SST, salinity and  $u_{10}$  range.

Parameter	Parameter Error	Absolute $\Delta\text{O}_2/\text{N}_2'$ uncertainty [%] Range (mean)
Sea surface temperature, SST	0.75 °C	0.02 – 0.1 (0.07)
Mixing coefficient, $\kappa$	$10^{-5} \text{ m}^2 \text{ s}^{-1}$	0.001 – 0.05 (0.02)
Wind speed, $u_{10}$	$2.5 \text{ m s}^{-1}$	0.002 – 0.06 (0.01)
Bubbled flux scaling coefficient, $\beta$	0.14	<0.001 – 0.05 (0.01)
Diffusive air-sea flux, $F_d$	15 % (relative)	0.001 – 0.03 (0.008)
Mixed layer depth, MLD	5 m	<0.001 – 0.03 (0.006)
Partial bubble flux, $F_p$	15 % (relative)	<0.001 – 0.02 (0.004)
Subsurface $\Delta\text{N}_2/\text{Ar}$ , $\Delta\text{N}_2/\text{Ar}_{\text{deep}}$	0.25 %	0.001 – 0.02 (0.004)
Sea level pressure, SLP	2 mbar	<0.001 – 0.004 (0.002)
Small bubble flux, $F_c$	15 % (relative)	<0.001 – 0.007 (0.002)
<b>Combined parameterization</b>		<u>0.04 – 0.2 (0.09)</u>
<b>All assumptions</b>		<u>0.001 – 0.3 (0.07)</u>
<b>Total</b>		<b>0.04 – 0.3 (0.1)</b>
<b>Surface <math>\text{N}_2</math>-fixation</b>		<0.05
<b>Additional biases</b>		
Parameter	Parameter value [%] Range (mean)	NCP error [mmol $\text{O}_2 \text{ m}^{-2} \text{ d}^{-1}$ ]
$\text{N}_2$ validation	0.9	N/A
Ex $\Delta\text{O}_2/\text{Ar} - \Delta\text{O}_2/\text{N}_2$	0 – 1.1 (0.4)	0 – 19 (<7)
Real $\Delta\text{O}_2/\text{Ar} - \Delta\text{O}_2/\text{N}_2$	0 – 0.8 (0.3)	0 – 14 (<6)
Ex $\Delta\text{O}_2/\text{Ar} - \Delta\text{O}_2/\text{N}_2'$	0 – 0.5 (0.01)	0 – 9 (<0.2)
Real $\Delta\text{O}_2/\text{Ar} - \Delta\text{O}_2/\text{N}_2'$	0 – 0.4 (0.01)	0 – 7 (<0.02)
Offshore mixing	N/A	0 – 50 (Izett et al., 2018)
Nearshore mixing	N/A	60 – 190 (Izett et al., 2018)
Diel $\Delta\text{O}_2/\text{Ar}$ variability	N/A	0 – 26 (Wang et al., 2020)