Breaking the ice: Identifying hydraulically-forced crevassing

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Abstract

Hydraulically-forced crevassing is thought to reduce the stability of ice shelves and ice sheets, affecting structural integrity and providing pathways for surface meltwater to the bed. It can cause ice shelves to collapse and ice sheets to accelerate into the ocean. However, direct observations of the hydraulically-forced crevassing process remain elusive. Here we report a new, novel method and observations that use icequakes to directly observe crevassing and determine the role of hydrofracture. Crevasse icequake depths from seismic observations are compared to a theoretically derived maximum-dry-crevasse-depth. We observe icequakes below this depth, suggesting hydrofracture. Furthermore, icequake source mechanisms provide insight into the fracture process, with predominantly opening cracks observed, which have opening volumes of tens to hundreds of cubic meters. Our method and findings provide a framework for studying a critical process, key for the stability of ice shelves and ice sheets, and hence rates of future sea-level rise.

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11	Key Points:
12	• We demonstrate a novel method for using crevasse icequake depths to discriminate
13	between dry and hydrofracture driven surface crevassing
14	• Icequakes can be used to directly observe and elucidate the crevasse hydrofracture
15	process
16	• Icequakes show tensile crack failure with opening volumes calculated from moment
17	magnitudes
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26 Abstract

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28 Hydraulically-forced crevassing is thought to reduce the stability of ice shelves and ice 29 sheets, affecting structural integrity and providing pathways for surface meltwater to the bed. 30 It can cause ice shelves to collapse and ice sheets to accelerate into the ocean. However, 31 direct observations of the hydraulically-forced crevassing process remain elusive. Here we report a new, novel method and observations that use icequakes to directly observe 32 33 crevassing and determine the role of hydrofracture. Crevasse icequake depths from seismic 34 observations are compared to a theoretically derived maximum-dry-crevasse-depth. We 35 observe icequakes below this depth, suggesting hydrofracture. Furthermore, icequake source 36 mechanisms provide insight into the fracture process, with predominantly opening cracks 37 observed, which have opening volumes of tens to hundreds of cubic meters. Our method and findings provide a framework for studying a critical process, key for the stability of ice 38 39 shelves and ice sheets, and hence rates of future sea-level rise.

40

41 **1 Introduction**

42

43 Hydraulically-forced surface crevassing, also referred to as hydrofracture, has the potential to 44 significantly influence the stability of glaciers, ice sheets and ice shelves (Lai et al., 2020). 45 On glaciers and ice sheets, hydraulically-forced crevassing provides a potential pathway for 46 surface meltwater to reach and lubricate the bed (Das et al., 2008; Van Der Veen, 1998; 47 Weertman, 1973), enhancing basal sliding of ice into the ocean (Rignot & Kanagaratnam, 48 2006), accelerating sea-level rise. Hydraulically-forced surface crevassing on ice shelves can 49 result in catastrophic failure, with melt ponds promoting fracture that can lead to the collapse of the ice shelf (Hughes, 1983; Mcgrath et al., 2012; T. Scambos et al., 2003; T. A. Scambos 50

51 et al., 2000). Following ice shelf collapse, land-based glaciers can accelerate into the ocean,

52 since the buttressing provided by the ice shelf no longer exists, again contributing to sea-level

rise. Understanding the fundamental mechanism of hydraulically-forced surface crevassing is

54 therefore a particularly timely topic within glaciology.

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56 Here, we present icequake observations from Skeidararjökull, an outlet glacier of the Vatnajökull Ice Cap, Iceland. This glacier is an ideal environment for studying potential 57 58 hydraulically-forced crevassing due to the high levels of surface melt present. Previous 59 studies have used icequakes to infer hydraulically-forced crevassing using auxiliary information, such as glacier speed up (Helmstetter et al., 2015), or the presence of meltwater 60 61 (Carmichael et al., 2012, 2015). Others have used seismicity to show that crevassing exhibits 62 tensile faulting (Mikesell et al., 2012; Neave & Savage, 1970; Roux et al., 2010; Walter et al., 2009). We first present a novel method for attributing an icequake to either dry or 63 hydraulically-forced crevassing, providing evidence that the icequakes we observe are likely 64 65 induced by hydrofracture. We then use icequake source mechanisms to confirm the crevassing stress release mechanism. Our results provide for the first time direct evidence of 66 67 hydrofracture, offering insights into this previously elusive process.

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69 2 Methods

Here, we briefly describe the methods for detecting and locating the seismicity, as well as an
overview of how the source mechanism inversions are undertaken and moment magnitudes,
M_w, are calculated. Two additional fundamental methods used in this study are obtaining
crevasse icequake depths from P-to-Rayleigh-wave amplitude ratios and the calculation of a
theoretical maximum-dry-crevasse-depth, based on the rheology of ice. These methods and

- theory are too complex to adequately describe in the main text, so we instead describe them
 in the Supplementary Information (Supplementary Text S1 and S2, respectively).
- 77

78 **2.1 Seismicity**

The seismicity presented in this study is detected using QuakeMigrate (Hudson et al., 2019; 79 80 Smith et al., 2020), with the method and overall catalogue of icequakes detailed by Hudson et al (2019). We relocate the detected earthquakes using NonLinLoc (Lomax & Virieux, 2000) 81 82 to obtain more accurate epicentral locations. For the subset of events presented in detail in 83 Figure 1 and 2, we manually pick P and S phase arrivals before relocation. The crevassing 84 icequake hypocentral depths for the selected events are obtained using P-to-Rayleigh-wave 85 amplitude ratios, with the associated method details given in the Supplementary Information 86 (Supplementary Text S1).

87

88 The icequake source mechanisms are obtained by performing a Bayesian full waveform 89 source inversion using an identical approach to a method detailed by Hudson et al (n.d.). 90 Only P-wave phases are used since the horizontal components are generally too noisy to use, 91 due to the instruments melting out of the glacier. Theoretically, S and surface waves could 92 also be used to constrain the inversion, but the amplitudes of any S arrivals are generally 93 close to the noise levels and we have low confidence in our ability to model the polarity of 94 dispersive surface waves sufficiently accurately for a moment tensor inversion, given the 95 depth dependent velocity structure of the firn layer at the site. We use a finite difference 96 scheme to model the Green's functions used to produce the synthetic seismograms in the 97 inversion. The depth of the source, a critical parameter affecting the source inversion, is 98 constrained using P-to-Rayleigh amplitude ratios.

100	The moment magnitude, M_w , of the icequakes is calculated using a spectral method(Stork et
101	al., 2014). The spectrum of the icequake is calculated by performing multi-taper spectral
102	estimation(Krischer, 2016; Prieto et al., 2009) in order to find the long period spectral level
103	and hence the seismic moment release, M_0 . M_w can then be calculated from (Hanks &
104	Kanamori, 1979),
105	$M_w = \frac{2}{3} \log_{10}(M_0) - 6.0. $ (1)
106	If one assumes that all the moment release for a given icequake is released via tensile failure,
107	then the opening of a crack, ΔV , can be calculated from,
108	$\Delta V = \frac{M_0}{\sigma_T} \tag{2}$
109	where σ_T is the tensile strength of the ice, taken to be 1.5 MPa (Podolskiy & Walter, 2016) in
110	this study.
111	
112	3 Results
113	3.1 Evidence for dry fracture vs. hydrofracture from crevasse depth
114	
115	As a crevasse propagates, the ice fractures, releasing seismic energy as icequakes. Crevasses
116	ordinarily only propagate to a certain depth within the ice column, where the tensile stress
117	field causing crevasse opening is compensated by the ice overburden pressure acting to close
118	the crevasse. We refer to this depth limit as the maximum-dry-crevasse-depth, d^* . However,
119	if the crevasse contains sufficient water, the additional pressure of this water column can
120	overcome the ice overburden pressure and induce hydrofracture, allowing the crevasse to
121	propagate to greater depths (Nick et al., 2010; Van Der Veen, 1998). Therefore, if the
122	observed depth of a crevasse icequake is greater than d^* , then one can infer that the icequake
123	is induced by hydrofracture. This is the fundamental premise of this study.

124

125 However, obtaining sufficiently accurate icequake hypocentral depths for comparison to d^* is 126 non-trivial. Seismometer networks are inherently poor at constraining the depth of an 127 earthquake using traditional body wave methods if the source-receiver epicentral distance is much greater than the source depth. This is generally the case in our study. Since the depth of 128 an icequake is critical evidence for or against hydrofracture, a more accurate method is 129 130 required for constraining hypocentral depth. We use surface-wave information in the form of P-wave to Rayleigh-wave amplitude ratios to constrain hypocentral depth (Heyburn et al., 131 132 2013; Jia et al., 2017; Stein & Wiens, 1986; Tsai & Aki, 1970). Figure 1a shows finite-133 difference full-waveform modelling results (Larsen et al., 2001) and observations of P to Rayleigh amplitude ratios, plotted against epicentral distance for a range of crevasse depths. 134 135 The observed amplitude ratios are compared to the model results to calculate the crevassing 136 depths. We independently verify these crevasse depths using P-S delay-times from receivers close to the source epicentre where possible (See Supplementary Figure S1), giving us 137 138 confidence that the amplitude ratios provide a sufficiently accurate estimation of icequake 139 depth.

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141 The crevassing depths constrained by the observations in Figure 1 can then be compared to 142 the maximum-dry-crevasse-depths, shown in Figure 2b, derived from the surface velocity 143 field shown in Figure 2a. Figure 2c shows the epicentral locations of the near surface 144 seismicity, with the grey scatter points showing the automatically detected icequakes(Thomas 145 S Hudson et al., 2019) and the coloured scatter points showing a subset of manually relocated 146 events. The majority of this subset of icequakes are located below d^{*} (solid red line, Figure 147 2d), on average 7.4 m deeper, from which we infer that they may be induced by 148 hydrofracture.

150	One potential limitation of using the source depth to discriminate between hydrofracture and
151	dry fracture is that we do not account for dynamic rupture, whereby during the rupture, a
152	crack may propagate deeper than the prevailing stress field otherwise allows, initiated by
153	fracture tip instability (Buehler & Gao, 2006). For the purposes of this study we treat each
154	icequake as an instantaneous point source, therefore neglecting dynamic rupture. Although
155	this assumption is does not fully describe the physics of the source, we deem it appropriate
156	here because of the distinct, high-frequency and short-duration phase arrivals observed.
157	
158	Given that the events are predominantly deeper than d^* , we suggest that the majority of these
159	events are likely caused by hydraulically-forced crevassing. In any case, the methodologies
160	developed here, which constrain icequake depth from amplitude ratios and use this source
161	depth to discriminate hydrofracture, are important developments for studying hydrofracture-
162	induced crevassing.
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 162 163 164 165 166 167 168 169 170 171 172 	induced crevassing. 3.2 Crevassing source mechanisms Moment tensor inversions constrain whether icequake source mechanisms include explosive, implosive, crack, or shear components. Icequake magnitudes then give the volume of opening, or fault area and displacement, depending upon the icequake source mechanism. Figure 2c shows the P-wave-constrained moment tensor inversion results for the subset of icequakes for which sufficiently accurate depths have been obtained. The inversion results for

174 waveform polarities are all correctly inverted for. Lune plots (Tape & Tape, 2012) in Figure 175 3b and Figure 3d indicate that the most likely source mechanisms for the two icequakes are a closing and an opening crack, respectively, with a negligible shear component in both cases. 176 177 Such crack mechanisms are the mode of failure one might expect from either dry or hydraulically-forced crevassing. However, after considering the Probability Density Function 178 179 (PDF) of the inversion solutions for the closing crack icequake in Figure 3b, an opening crack mechanism cannot be eliminated. This ambiguity is due to station geometry on the 180 181 focal sphere. In any case, an opening or closing crack of a specific orientation is required to 182 represent the observations adequately, as inferred from previous seismic observations 183 (Mikesell et al., 2012; Neave & Savage, 1970; Roux et al., 2010; Walter et al., 2009). 184 185 All icequake crack orientations in Figure 2c agree with the principal stress directions calculated from the observed surface velocities, as shown by the orange vectors in Figure 2c. 186 187 This confirms interpretations in previous studies (Garcia et al., 2019; Harper et al., 1998). The apparent closing crack observation for the icequake at 64.327° N, 17.21° W may be 188 189 supported by the presence of tensile stresses in both principal stress directions. In such a 190 stress regime, a closing crack may be valid, effectively exhibiting two-dimensional necking 191 in the surface-parallel plane.

192

The moment magnitude of the crevassing icequakes range from -0.4 to -0.9, calculated using a spectral method (Stork et al., 2014). If we approximate all the failure as tensile, then for a tensile strength of ice of 1.5 MPa (Podolskiy & Walter, 2016), the volume associated with crack opening or closing is of the order of 30 m^3 to 150 m^3 .

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We propose several possible mechanisms for generating seismicity below the maximum-drycrevasse-depth. These interpretations are summarised in Figure 4. The mechanisms are: (1) new cracks opening when the combined deviatoric near-surface stress field and hydrostatic pressure are sufficient to overcome the ice overburden pressure and tensile strength of the ice; (2) pre-existing cracks that have closed reopening due to a sufficient head of water in the crevasse; (3) opened pre-existing cracks reclosing as the water is evacuated from the fracture, due to a preferential pressure gradient below the fracture.

205

206 For mechanisms 2 and 3, the crevasse must have propagated to that depth via mechanism 1, 207 therefore suggesting that at least some of the icequakes we observe are likely to be new ice 208 fracture. We observe principal tensile stress amplitudes of greater than 200 kPa (see Figure 209 S2), more than sufficient to overcome an ice tensile strength of ~100 kPa (Paterson, 1994). Mechanism 2 is similar to mechanism 1, except requiring a lower hydrostatic pressure to 210 induce crack opening, and is possible if crevasses have formed upstream and subsequently 211 212 been closed by principal compressive stresses perpendicular to the crevasse. Such 213 refracturing is proposed in scenarios where there are insufficient volumes of surface 214 meltwater to immediately establish a permanent bed connection (Boon & Sharp, 2003). 215 Mechanism 3 is presented more tentatively, partly due to the potential ambiguity of the 216 closing-crack source mechanism (see Figure 3a), but also because these crevasses would have 217 to close over sufficiently short time scales to generate the ~100 Hz source frequencies 218 observed in the P-wave spectra. While ice can suddenly fail or reopen a crack over such a 219 short duration, a possible source of driving stresses or pressures required to close cracks this quickly is less conceivable. A crack at greater depth could reopen, evacuating water from 220 221 above, but envisaging a sufficiently localised stress field is difficult. Alternatively, water may travel through an opening, pre-existing crack sufficiently quickly that the crack then 222

immediately closes, although the magnitude of closing would have to dominate over opening

to explain a closing-crack observation. In summary, we therefore confidently present

225 mechanisms 1 and 2, but suggest that mechanism 3 is unlikely.

226

227 One question that arises is why we do not observe seismicity via mechanism 1 or 2 occurring 228 all the way to the glacier bed, as is proposed in various studies (Boon & Sharp, 2003; 229 Carmichael et al., 2012; Colgan et al., 2016; Van Der Veen, 1998; Weertman, 1973). A 230 reason could be that as such fractures penetrate deeper into the glacier, the energy will be 231 more attenuated, fall below background noise levels and not be detected. Alternatively, the 232 crevasses at Skeidararjökull might never reach the bed. 233 234 These results emphasise the potential information that icequakes hold for elucidating the physics of glacier hydrofracture. Here, we only use P-waves to constrain the mechanisms, but 235 236 if one had a more comprehensive dataset with a greater number of receivers and higher SNR, 237 then it may be possible to constrain the source mechanism better. Furthermore, if one were to

238 invert for a dynamic rupture model of finite length, rather than the instantaneous point source

that we assume here, then one might gain additional insight into the physics governing

240 hydrofracture in ice. Another approach to learn more about the hydrofracture process could

be to compare observations such as ours to theoretical models of crevasse vibrational modes

to infer crevasse geometry (Lipovsky & Dunham, 2015), or even models of supraglacial lake

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drainage (Jones et al., 2013).

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248 4 Implications for ice sheet and ice shelf stability

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250 Our findings provide a method for observing hydrofracture at icesheets such as the Greenland 251 Ice Sheet, where although it has been shown that meltwater can drain from the surface to the 252 bed (Das et al., 2008), the mechanism and pathway has not been imaged previously. Calving 253 at the ocean termini of outlet glaciers of the Greenland Ice Sheet could also be enhanced by hydrofracture. Increased calving could be facilitated by precipitation increasing the 254 255 hydrostatic pressure of water-filled crevasses (O'Neel et al., 2003), or by damage to the 256 upstream ice (Krug et al., 2014), with the depth of this damage through the ice column dependent upon the depth of the crevasses, which we infer here to be controlled by the glacier 257 258 stress state and hydrofracture. Our method could provide observations of the depth of such 259 damage. The above mechanisms are also hypothesised to be important factors that could 260 accelerate the collapse of the West Antarctic Ice Sheet and cause significant retreat of the 261 East Antarctic Ice Sheet (Pollard et al., 2015).

262

Some ice shelves exhibit surface melt ponds before undergoing disintegration, whereas others have similar melt ponds but remain intact (Scambos et al., 2000). Crevassing icequakes could provide insight into whether hydrofracture is occurring unnoticed at these apparently stable ice shelves, potentially leading to sudden future catastrophic collapse, or whether hydrofracture is physically suppressed by another mechanism that affects either the stress regime or the fracture toughness of the ice.

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In conclusion, understanding the stability of ice sheets and ice shelves is important for sealevel-rise projections (Vaughan et al., 2013). Hydrofracture induced crevassing is an
important mechanism that, at least to some extent, controls the stability of such ice bodies.

The methodology and findings we present provide a means of attributing crevassing
icequakes to hydrofracture. We show that such icequakes can then be used as an
observational basis for studying the physical mechanisms associated with hydrofracture
induced crevassing.

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279

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448 Figures







451 *Figure 1 – Obtaining depth for crevassing icequakes. a) Plot of P-to-Rayleigh-wave*

- 452 *amplitude ratio with epicentral distance from the source. Observed P-to-Rayleigh amplitudes*
- 453 for the icequakes presented in Figure 2 are plotted (various coloured scatter points). P-to-
- 454 Rayleigh amplitudes for modelled crevassing icequakes with source depths from 10 to 120 m
- 455 below surface are indicated by the solid lines, with the 2D interpolated field plotted at
- 456 epicentral distances greater than 180 m. b) The velocity model used for the modelled
- 457 *crevassing icequakes*(Gudmundsson, 1989).
- 458



461 *Figure 2 – Summary of crevasse icequake observations. a) The horizontal surface velocity* 462 field at the site, derived using GPS data from the highlighted stations. b) The maximum-dry-463 crevasse-depth, d^{*}, calculated using the velocity field in (a). Uncertainty in these fields are 464 given in Figure S2. c) Map of crevasse icequake locations. Grev scatter points are all the crevasse icequakes detected during the period 19th to 29th June 2014. The icequakes studied 465 in more detail, with derived depths using the P-to-Rayleigh amplitude method are plotted as 466 467 larger scatter points, coloured by depth below the maximum dry crevasse depth. Upper hemisphere moment tensors for these icequakes are also shown. Principal stress vectors 468 derived from the velocity field in (a) are shown in orange. Seismometer and geophone 469 470 locations are shown by the yellow diamonds. Satellite image is from the European Space

- 471 Agency. d) Plot of the crevassing events in (c) with depth vs. latitude projected onto a N-S
- *transect at* 17.225° *W. The solid and dashed red lines indicate the maximum dry crevasse*
- *depth and the associated uncertainty, respectively. The bed topography is derived from*
- 474 ground-penetrating radar(Björnsson, 2017).



Figure 3 – Examples of upper hemisphere crevasse icequake source mechanisms for two of
the events in Figure 2. The source mechanisms are constrained only by P-wave phases. a)
Source mechanism for a closing-crack crevasse icequake. Black waveforms are observed
data, red dashed waveforms are the most likely inversion model result. b) Lune plot (Tape
and Tape (2012)) associated with the event in (a), showing the PDF of the full waveform
inversion result, indicating the most likely source type. Brighter colours indicate higher
probability. c) and d) Same as (a) and (b) except for an opening-crack crevasse icequake.





495 Figure 4 – Interpretation of the possible crevasse failure mechanisms observed. (1) A new

- *opening-crack hydrofracture through previously undamaged ice. (2) An opening-crack*
- *hydrofracture of a pre-existing crack. (3) Closing of a pre-existing crack due to the*
- 498 evacuation of water from the crack. Hypothetical source mechanisms are shown for each

case.

1	Supplementary Information for: "Breaking the ice: Identifying hydraulically-forced
2	crevassing"
3	
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11	
12	Supplementary Text S1: P-to-Rayleigh amplitude ratios and icequake depth
13	
14	The P-to-Rayleigh-wave amplitude ratios are calculated by taking the maximum amplitude
15	within specified windows, as shown for the observed icequake example in Figure S1a. Figure
16	S1c and Figure S1d show the P-to-Rayleigh-wave phase arrivals for one station \sim 450 m from
17	the source. The particle motion of the inferred Rayleigh-wave is elliptical, providing us with
18	confidence that it is indeed a surface wave arrival. P-wave and Rayleigh-wave windows are
19	of fixed duration for all events, as in Figure S1. The uncertainty in the observed P-to-
20	Rayleigh-wave amplitude ratios is defined as the standard deviation of the noise signal
21	observed in a window 1s prior to the P-phase arrivals. Uncertainty in the epicentral distances
22	given in Figure 1 are defined as the epicentral uncertainty output from NonLinLoc (Lomax &
23	Virieux, 2000). The same method of obtaining P-to-Rayleigh-wave amplitudes is employed
24	for the 2D finite difference modelled seismograms for various source depths from E3D
25	(Larsen et al., 2001). The model is run for various source depths from 10 m to 120 m below

26	surface, with the 2D interpolated field from the model runs (see Figure 2a) used to derive the
27	likely crevasse depth from each receiver observation. These individual receiver observations
28	are then combined for each icequake, to provide an overall estimate of the icequake depth.
29	We independently verify crevasse depth by using S-P delay-times from receivers
30	approximately directly above the crevasse. For the event in Figure S1, the S-P delay-time
31	observed at a receiver approximately above the event is 0.014 s. With the velocity model
32	shown in Figure 1b, this corresponds to an icequake depth of ~25 m below surface, compared
33	to a depth of 29 ± 12 m found using the P-to-Rayleigh amplitude ratios. We are therefore
34	confident that the P-to-Rayleigh-wave amplitude ratios provide a good estimation of icequake
35	depth.
36	



38

Supplementary Figure S1 – Example of observed waveforms at seismometers from a crevasse icequake at 14:33:52 on 28th June 2014. a) Record section showing the P-to-Rayleigh-wave arrivals. The red and yellow regions show the windows used to calculate the P-to-Rayleigh amplitude ratios. b) Waveforms for an arrival 43 m from the event epicentre. P and S phase arrivals are indicated by the red and blue lines, respectively. c) Waveforms for an arrival 450 m from the event epicentre. d) Particle motions associated with the P and Rayleigh phase arrivals in (c). Red is the P-wave phase and yellow is the Rayleigh wave phase.

- 46
- 47
- 48
- 49
- 50

51 Supplementary Text S2: Derivation of maximum-dry-crevasse-depth

52

53 The maximum depth to which a crevasse can propagate without hydrofracture is governed by 54 the tensile stress regime near the glacier surface. If the ice is under tensile stress then a 55 crevasse can form. However, as the depth through the ice increases, the ice overburden 56 pressure increases and acts to close the crevasse and prevent further fracture. At a certain depth, the maximum-dry-crevasse-depth, d^* , the maximum principal tensile stress acting to 57 open crevasses becomes equal to the compressive ice overburden pressure. Below this depth, 58 59 the ice overburden pressure is sufficiently high to prevent opening. This crevassing model is 60 commonly referred to as the zero stress model (Colgan et al., 2016), and has been proven 61 effective in predicting real crevasse depths (Mottram & Benn, 2009).

62

63 The above statement assumes that the ice will open under any net tensile stress, which is not strictly correct since the ice also has a tensile failure strength, that we do not account for here. 64 65 Accounting for the tensile strength of the ice would simply make d^* shallower and hence increase the depth difference between icequake depths and the maximum-dry-crevasse-depth 66 equipotential, therefore increasing the likelihood of icequakes observed being associated with 67 68 hydrofracture. We also assume that there is a shallow firn layer at the glacier surface, of 69 lower density than the underlying ice. This lower-density layer acts to make the maximum-70 dry-crevasse-depth deeper. We use the same local seismic refraction survey (Gudmundsson, 71 1989) as used to constrain the seismic velocities in Figure 1b to constrain the density profile 72 of this layer, making the assumption that the change in velocity in the firn-layer is dominated 73 by density rather than the bulk and shear moduli. This simplified firn density correction is 74 assumed adequate for the purposes of this study since the weight estimation of the firn layer is conservative, therefore resulting in an overestimate of the maximum-dry-crevasse-depth. 75

76

To find d^* , one has to calculate the stress field near the glacier surface. This can be approximately obtained using the glacier surface velocity field. For a given point on the glacier, the velocity is defined by,

80
$$\overrightarrow{v_{i,j}} = \begin{pmatrix} u_{i,j} \\ v_{i,j} \\ W_{i,j} \end{pmatrix}, \qquad (3)$$

81 where u, v and w are the velocities in the x, y and z directions, and i, j denotes a particular 82 horizontal location within the velocity field. To obtain the velocity field for the glacier 83 surface at Skeidararjökull, we use GPS location data from the seismometers shown in Figure 2. The GPS data from the seismometers is more poorly constrained compared to dedicated 84 85 dual-frequency GPS instruments, and is sampled only once per hour. Therefore, in order to 86 reduce the GPS noise, we use a seven day moving average for the latitude, longitude and 87 elevation data. We then calculate the average velocity over the ten day period of analysis. Even after applying this processing, data from only 7 stations are of sufficient quality to use. 88 89 We then perform a two-dimensional, second-order interpolation for these velocity data points 90 in order to obtain a horizontal velocity field for the network area. Due to only one station, 91 SKR12, constraining the velocity field for the upper half of the network area, the 92 interpolation scheme performs poorly outside the network, so we only analyse the velocity field approximately within the network, as shown in Figure 2 and Figure S2. 93



Figure S2 - The estimated uncertainty in the interpolated maximum surface velocity,
maximum principal tensile stress and maximum-dry-crevasse-depth fields. (a) to (c) The
lower, actual and upper uncertainty associated with the surface velocity field, respectively.
(d) to (f) The lower, actual and upper uncertainty associated with the maximum principal
stress field, respectively. (g) to (i) The lower, actual and upper uncertainty associated with
the maximum-dry-crevasse-depth, respectively.

106 The velocity field can then be used to obtain the strain rate field for each point on the glacier107 surface. The second order strain rate tensor is given by,

108
$$\dot{\boldsymbol{\varepsilon}} = \begin{pmatrix} \dot{\varepsilon}_{xx} & \dot{\varepsilon}_{xy} & \dot{\varepsilon}_{xz} \\ \dot{\varepsilon}_{xy} & \dot{\varepsilon}_{yy} & \dot{\varepsilon}_{yz} \\ \dot{\varepsilon}_{xz} & \dot{\varepsilon}_{yz} & \dot{\varepsilon}_{zz} \end{pmatrix} = \begin{pmatrix} \frac{\partial u}{\partial x} & \frac{1}{2} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) & 0 \\ \frac{1}{2} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) & \frac{\partial v}{\partial y} & 0 \\ 0 & 0 & \frac{\partial w}{\partial z} \end{pmatrix}.$$
(4)

109 $\dot{\varepsilon}_{xz}$ and $\dot{\varepsilon}_{yz}$ are taken to be zero, assuming no shear with depth, a realistic approximation near 110 the glacier surface. If one also assumes that ice is incompressible, then $tr(\dot{\varepsilon}) = 0$. $\dot{\varepsilon}_{zz}$ can 111 then be found, giving,

112
$$\dot{\varepsilon}_{zz} = \frac{\partial w}{\partial z} = -\left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}\right). \quad (5)$$

113

114 To find the maximum-dry-crevasse-depth, we require the stress tensor. In order to calculate 115 the stress tensor from the strain tensor, we need one final piece of information, the effective 116 viscosity, η_{eff} , for a given horizontal location. Since ice behaves as a non-linear fluid, η_{eff} 117 varies with the strain rate, $\dot{\boldsymbol{\epsilon}}$. The effective viscosity is defined as,

118
$$\boldsymbol{\eta}_{eff} = \frac{B}{2} \left(\dot{\boldsymbol{\varepsilon}}_{eff} \right)^{\frac{1}{n}-1}, \quad (6)$$

119 where B is given by,

120
$$B = A^{-\frac{1}{n}},$$
 (7)

121 where the temperature-dependent rate factor $A = 5.6 \times 10^{-17} Pa^{-3} a^{-1}$ and n = 3,

122 determined from laboratory studies (Glen, 1955; Nick et al., 2010). The effective strain rate, 123 $\dot{\varepsilon}_{eff}$, is defined by,

124
$$\dot{\boldsymbol{\varepsilon}}_{eff} = |\dot{\boldsymbol{\varepsilon}}| = \left(\frac{1}{2} tr(\dot{\boldsymbol{\varepsilon}} \cdot \dot{\boldsymbol{\varepsilon}})\right)^{\frac{1}{2}}.$$
 (8)

126 The net stress tensor, $\boldsymbol{\sigma}$, is then defined as the difference between the opening stress and the 127 ice overburden stress tensor by,

128
$$\boldsymbol{\sigma} = \boldsymbol{\sigma}_{opening} - \boldsymbol{\sigma}_{overburden} , \quad (9)$$

129 which can be written explicitly as,

130
$$\boldsymbol{\sigma} = \begin{pmatrix} 4\eta_{eff}\varepsilon_{xx,i,j} + 2\eta_{eff}\varepsilon_{yy} & 2\eta_{eff}\varepsilon_{xy} & 0\\ 2\eta_{eff}\varepsilon_{xy} & 4\eta_{eff}\varepsilon_{yy} + 2\eta_{eff}\varepsilon_{xx} & 0\\ 0 & 0 & 0 \end{pmatrix} - \rho g z \boldsymbol{I} , \quad (10)$$

131 where ρ is the ice density, g is the gravitational constant of acceleration and z is the depth 132 below the ice surface. $\sigma_{opening,xz}$ and $\sigma_{opening,yz}$ are zero since we have assumed no vertical 133 shear stress with depth and $\sigma_{opening,zz}$ is zero, assuming that the ice is in hydrostatic 134 equilibrium. At the maximum-dry-crevasse-depth is where the maximum principal opening 135 stress equals the overburden stress, at which point z is the maximum-dry-crevasse-depth, d^* . 136 Therefore, to find d^* we need to find the maximum principal opening stress, $\sigma^*_{opening}$. To do 137 this, we rotate σ to maximise the tensile stress,

138
$$\boldsymbol{\sigma}_{opening}^* = \boldsymbol{S} \, \boldsymbol{\sigma}_{opening} \, \boldsymbol{S}^T, \qquad (11)$$

139 where S is a rotation matrix comprising the eigenvectors of $\sigma_{opening}$. The maximum-dry-

140 crevasse-depth at a given point on the glacier surface, d^* , is then given by (Nick et al., 2010),

141
$$d^* = \frac{max(\sigma^*_{opening})}{\rho g}.$$
 (12)

142

The uncertainty associated with the maximum-dry-crevasse-depth field is proportional to the uncertainty in the velocity field. To estimate the uncertainty, we calculate the standard deviation in the average velocity data and randomly perturb the velocity data used to calculate the velocity field by gaussian distributions about the average observed velocities, with the standard deviations used to constrain the width of these distributions. These gaussian distributions are sampled 1000 times. We then calculate the strain, stress, and crevasse depth

149	fields from each perturbed velocity field, and define the lower and upper uncertainties for
150	each field as the minimum and maximum values, respectively, for each point spatially within
151	the fields. This data is shown by the red dashed lines in Figure 2d, and all the fields and their
152	associated uncertainties are shown in Figure S2.
153	
154	
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