

Detection, analysis and removal of glitches from InSight’s 1 seismic data from Mars

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Abstract

The SEIS instrument package with the three very broad-band and three short period seismic sensors is installed on the surface on Mars as part of NASA’s InSight Discovery mission. When compared to terrestrial installations, SEIS is deployed in a very harsh wind and temperature environment that leads to inevitable degradation for the quality of the recorded data. One ubiquitous artifact in the raw data is an abundance of transient one-sided pulses often accompanied by high-frequency precursors. These pulses, which we term “glitches”, can be modeled as the response of the instrument to a step in acceleration, while the precursors can be modeled as the response to a simultaneous step in displacement. We attribute the glitches primarily to SEIS-

internal stress relaxations caused by the large temperature variations to which the instrument is exposed during a Martian day. Only a small fraction of glitches correspond to a motion of the SEIS package as a whole and they are all due to minuscule instrument tilts. In this study, we focus on the analysis of the glitch+precursor phenomenon and present how these signals can be automatically detected and removed from SEIS' raw data. As glitches affect many standard seismological analysis methods such as receiver functions or spectral decomposition, we anticipate that studies of the Martian seismicity as well as studies of Mars' internal structure should benefit from deglitched seismic data.

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Key Points:

- Glitches due to steps in acceleration significantly complicate seismic records on Mars
- Glitches are mostly due to relaxations of thermal stresses and instrument tilt
- We provide a toolbox to automatically detect and remove glitches

Abstract

The instrument package SEIS (Seismic Experiment for Internal Structure) with the three very broadband and three short-period seismic sensors is installed on the surface on Mars as part of NASA's InSight Discovery mission. When compared to terrestrial installations, SEIS is deployed in a very harsh wind and temperature environment that leads to inevitable degradation of the quality of the recorded data. One ubiquitous artifact in the raw data is an abundance of transient one-sided pulses often accompanied by high-frequency spikes. These pulses, which we term "glitches", can be modeled as the response of the instrument to a step in acceleration, while the spikes can be modeled as the response to a simultaneous step in displacement. We attribute the glitches primarily to SEIS-internal stress relaxations caused by the large temperature variations to which the instrument is exposed during a Martian day. Only a small fraction of glitches correspond to a motion of the SEIS package as a whole caused by minuscule tilts of either the instrument or the ground. In this study, we focus on the analysis of the glitch+spike phenomenon and present how these signals can be automatically detected and removed from SEIS' raw data. As glitches affect many standard seismological analysis methods such as receiver functions, spectral decomposition and source inversions, we anticipate that studies of the Martian seismicity as well as studies of Mars' internal structure should benefit from deglitched seismic data.

Plain Language Summary

The instrument package SEIS (Seismic Experiment for Internal Structure) with two fully equipped seismometers is installed on the surface of Mars as part of NASA's InSight Discovery mission. When compared to terrestrial installations, SEIS is more exposed to wind and daily temperature changes that leads to inevitable degradation in the quality of the recorded data. One consequence is the occurrence of a specific type of transient noise that we term "glitch". Glitches show up in the recorded data as one-sided pulses and have strong implications for the typical seismic data analysis. Glitches can be understood as step-like changes in the acceleration sensed by the seismometers. We attribute them primarily to SEIS-internal stress relaxations caused by the large temperature variations to which the instrument is exposed during a Martian day. Only a small fraction of glitches correspond to a motion of the whole SEIS instrument. In this study, we focus on the detection and removal of glitches and anticipate that studies of the Martian seismicity as well as studies of Mars' internal structure should benefit from deglitched seismic data.

1 Introduction

InSight (Interior Exploration using Seismic Investigations, Geodesy and Heat Transport) landed successfully on Mars on November 26, 2018 (Sol 0, a sol is a Martian day with around 24h 40m). Since February 9, 2019 (Sol 73), InSight's main scientific instrument SEIS (Seismic Experiment for Internal Structure) is recording seismic data in its operational configuration (Banerdt et al., 2020). The SEIS package (Lognonné et al., 2019), whose network and station code for the scientific data is XB.ELYSE, consists of two three-component seismometers; one being very broadband (VBB) with a corner period of 16 seconds, and one being short-period (SP) with a corner period of 35 seconds. The noise floor of the two instruments is equivalent only above 5 Hz while it is about ~ 30 dB lower for the VBB at frequencies below 0.1 Hz. It is this frequency dependence of the seismometers' self-noise that determines their names as established for the InSight project (Lognonné et al., 2019), even though the naming convention does not follow terrestrial standards (e.g. Ahern et al., 2012). Due to their different noise floors, the VBB is the main instrument to detect distant Marsquakes, while the SP is used to cover the frequency range of ~ 5 –50 Hz for more detailed analysis of regional events and lander-induced signals. Both seismometers have non-orthogonal sensor orientations (Fig. 1a,c). To date, all six seismic components as well as the acquisition system have functioned nominally, exceeded mission requirements, and delivered unprecedented seismic data from the surface of Mars (InSight Mars SEIS Data Service, 2019). In addition to seismic signals of natural and artificial origins, i.e. Marsquakes (Lognonné et al., 2020; Giardini et al., 2020; for Marsquake catalog see: InSight Marsquake Service, 2020) and records from the HP³-instrument hammering sessions (Spohn et al., 2018), respectively, these data show a variety of non-seismic signals whose origin is not always clear but under investigation. Amongst the most prominent and abundant types of these non-seismic signals are what we termed a "glitch". Glitches influence many of the standard seismological methods such as

receiver functions, polarization analyses, source inversions and spectral decomposition and therefore on Earth data influenced by such disturbances are often discarded especially when coinciding with earthquake phase arrivals (e.g. Zahrádník & Plesinger, 2005). This obviously represents no valid option for the seismic data returned from Mars and hence the correct treatment of the glitches is of high importance for the scientific analyses. The present study focuses on the detection, analysis and removal of glitches and extends Supplement V of Lognonné et al. (2020).

Glitches

In the literature (e.g. Iwan et al., 1985; Zahrádník & Plesinger, 2005; Vacka et al., 2015) the phenomenon we are investigating here is sometimes referred to as "long-period disturbances", "acceleration offsets" or even "mice", all generally describing the same type of data disturbance. Throughout the present publication, however, we choose to apply the term "glitch" to these disturbances as it has been established as such since their first observations in InSight's seismic data and hence been communicated so to a wider audience on various occasions. Whilst we are aware that the word glitch is typically associated to more general data artefacts and alike, we indeed use it here to refer to specific, clearly defined disturbances in the data. A glitch (Fig. 1b,d), thus, is a particular type of transient instrumental self-noise that, in the raw time series data, appears as a high amplitude, one-sided pulse with a duration controlled by the seismometer's transfer function. For the VBB sensors, which have 76% of critical damping, glitches have a fast rise time followed by an exponential decay with a small ($\sim 9\%$) overshoot before almost returning to the baseline after ~ 25 s. For the SP sensors, that are overdamped with 110% of critical damping, glitches have a similar rise time followed by a decay before almost returning to the baseline after ~ 50 s. Glitches may also occur before a previous glitch has sufficiently decayed. The highest order of such "poly-glitches" we observe to date is four. Glitches (and poly-glitches) can occur on all three VBB and all three SP sensors simultaneously but there are many examples where a glitch occurs on only one component. They occur at all times of the sol but are observed more frequently during the quiet parts in the early evening and night (Fig. 2a). This is due the decreased seismic noise level driven by diurnal wind and pressure variations. The largest glitches reach amplitudes of $1\text{e-}7\text{ms}^{-1}$ and more. We observe a few of these per sol, whilst for amplitudes of $\sim 1\text{e-}8\text{ms}^{-1}$ we can observe already hundreds per sol. Especially in the early evening, when the wind and pressure variations have calmed down, we observe a period with many consecutive glitches mostly of lower amplitude (Fig. 2b). Certain types of glitches can furthermore repeat over many consecutive sols at the same local time, thus indicating a driving process behind their generation. In the frequency domain, glitches range from lowest frequencies up to almost 1 Hz, thus influencing analyses of seismic records especially for longer periods.

Glitch Spikes

Many glitches, furthermore, show a high-frequency signal at their very glitch beginning that lasts around 40 samples regardless of the data sampling frequency. We refer to these initial oscillations as "glitch spikes". These spikes occur simultaneously with the glitch onset for both VBB and SP (Fig. 1b,d). Glitch spikes do not represent artifacts caused by the on-board analog or digital electronics. To facilitate the analysis of glitches and help deciphering their origins, we analyse these spikes as well.

2 Glitch Detection

To automatically detect glitches on SEIS' VBB and SP raw data, several groups (MPS, ISAE, UCLA, IPGP) independently developed algorithms in the Python and MATLAB programming languages. The group acronyms stand for the affiliation of the group's leading analyst, i.e. Max-Planck-Institute for Solar System Research (MPS), Institut Supérieur de l'Aéronautique et de l'Espace SU-PAERO (ISAE), Department of Earth, Planetary, and Space Sciences, University of California Los Angeles (UCLA), and Université de Paris, Institut de physique du globe de Paris (IPGP). We describe each approach in the following. The common detection idea, and working hypothesis of this study, is that glitches in the raw data represent steps in acceleration convolved with the seismometer's instrument response while spikes represent steps in displacement convolved with the seismometer's instrument response. The lists of detected glitches in 2019 can be found in the Supplementary Information 1.

2.1 Glitch Detection by Instrument Response Deconvolution (MPS)

This detection algorithm, implemented in Python (Rossum, 1995) and ObsPy (Krischer et al., 2015; Beyreuther et al., 2010), performs the following processing steps on a given period of three-component seismic data (components U, V, W): (i) decimate the data to two samples per second (SPS), allowing all data per seismometer to be run with the same parameters and enabling faster computations, (ii) deconvolve the instrument response on each component and convert to acceleration, (iii) band-pass filter the acceleration data (e.g. 10-1000 s), so the steps in acceleration emerge more clearly, (iv) calculate the time derivative of the filtered acceleration data so the acceleration steps become impulse-like signals, and (v) on this time-derivative, trigger glitches based on a constant threshold. To avoid triggering on subsequent samples also exceeding the threshold but belonging to the same glitch, we introduce a window length in which no further glitch can be triggered. This parameter can be thought of as *glitch minimum length*. We note this parameter is smaller than the typical glitch length for VBB and SP, allowing our detection algorithm to detect poly-glitches.

A glitch simultaneously occurring on multiple components is detected on each affected component but the respective start times may slightly differ. However, after modeling of the full glitch waveform (Section 4) we can retrospectively establish that such glitches occur at the same time to within milliseconds. This holds true for all multi-component glitches observed to date on either VBB or SP, also for data with the highest available sampling frequency of 100 Hz. Therefore, we declare as glitch start time the earliest time detected across the UVW-components. The list of unified glitch starts contains still many false-positive triggers caused by non-glitches with a steep enough acceleration change to be triggered. This is because we choose to apply a constant threshold to the time derivative of the filtered acceleration, rather than a threshold based on the current seismic noise level that undergoes strong diurnal changes (amplitudes varying by a factor of 100 and more) dominated by meteorological influences (e.g. Lognonné et al., 2020; Banfield et al., 2020). To circumvent, we rotate the gain-corrected UVW raw data of the glitch windows into the geographical reference frame (ZNE-components) and perform a 3-D principle component analysis (e.g. Scholz et al., 2017). Theoretically a glitch is linearly polarized as the associated vector of acceleration change is not varying, however slightly altered only by seismic noise. Indeed, most glitches exhibit a high linear polarization >0.9 which we use to discriminate against other triggered signals. The polarization analysis further allows to obtain the apparent glitch azimuth and incidence angles which we use to associate glitches with particular glitch sources (Section 3). Visual inspection reveals the resulting glitch onsets are usually accurate to within ± 1 s (e.g. green lines in Fig. 1b,d).

2.2 Glitch Detection by Cross-Correlation with Impulse Response Function (ISAE)

The principle of this MATLAB-implemented detection algorithm is cross-correlation. It performs the following processing steps on a given period of three-component raw seismic data (components U, V, W): (i) a synthetic glitch is constructed by convolving the poles and zeros of the transfer function of the VBB and SP sensors with a step in acceleration. To increase the temporal resolution to sub-sample range, we synthesise several glitches each with a different sub-sample time shift; (ii) while the frequencies above 2Hz are filtered, the long period variations of the data are extracted using a low-pass filter with 10^{-3} normalised cutoff frequency for VBB and 0.25×10^{-4} normalised cutoff frequency for SP. These are then subtracted from the signal (and added back at the end), before (iii) the synthetic glitch is cross-correlated with the data. A glitch detection is triggered for the maxima of the cross-correlation function that exceed a threshold a on a given component.

Another step is added to prevent non-detection of glitches or false-positives, depending on the correlation threshold. For that, two thresholds are chosen: *threshold a* and *threshold b*, with $a \geq b$. The first step presented above is done for each component, with *threshold a*. Then, for each component, a second cross-correlation with *threshold b* is implemented. For the times of every maximum of cross-correlation exceeding *threshold b*, we come back to the glitches detected on the other components during the first step. If a glitch had indeed been detected at that specific time on another component, a new glitch is declared on the component under study. We can therefore detect small glitches with low signal-to-noise ratio when a strong glitch is detected at the same time on some other component. In addition, in order to be able to detect poly-glitches, a second iteration of the detection algorithm is performed after the glitches from the first iteration have been removed from the data.

2.3 Hierarchical Glitch Detection (UCLA)

This MATLAB based method took into account that glitch amplitudes follow a power law distribution with many more very small glitches than larger ones (see Fig 1 in electronic supplement). Therefore the strategy was to remove the largest glitches first and repeat the process on the smaller ones in an iterative procedure. In this method the raw UVW VEL channel data are inspected for glitches and their spikes. The instrument response to a step in acceleration was termed "Green's function." The 20 sps data were decimated to 2 sps and each channel was tested for correlation with the response function as follows. An inverse filter was designed that turned glitches into narrow Gaussians with rise times equal to the glitch so that each glitch represented one peak without the overshoot. This enables detection of multiple close-spaced glitches. An STA/LTA (short time average / long time average) ratio was found using convolution of the data with two box car functions separated by more than a glitch window. The absolute value of band-passed data was tested for peaks above the STA/LTA threshold. For the first iteration the STA/LTA was set large to remove the largest glitches. The Green function was correlated with the data spanning a peak and if the correlation coefficient was above 0.90 the detection was registered. If multiple peaks occurred close together, multiple Green's functions were fit to the data using nonlinear least squares. The data was then cleaned by removing the glitches. The process was then repeated lowering the STA/LTA threshold=7, and the new glitches removed from the data. For the last iteration the STA/LTA threshold was set to 3, i.e. lowered again and the correlation threshold was also lowered to 0.8. This removed many of the small glitches. Our glitch detection is applicable to SEIS' VBB and SP sensors in both low and high gain modes.

2.4 Triple-Source based Glitch Detection (IPGP)

Implemented in MATLAB, this glitch detection method processes mostly 2 sps continuous data and is therefore focused on long period continuous signals. It first removes the aseismic signals of each raw axis by subtracting the trend and the first 12 sol-harmonics (i.e., up to 1/12 sol period, about 0.13 mHz in frequency). Then the three axes are equalized in digital units by convolving the V and W channels by the convolution ratio of the U/V and U/W transfer functions, in order to correct for the gain and transfer function differences between U, V and W. Note that this process also transforms an impulse response in time on V and W into an impulse response with the U transfer function. As the inversion (below) is a linear one, the glitch search and deglitching can be done either on the UVW or on the ZNE rotated channels, with practically no differences for the inverted glitches.

The glitch detection is done first by identifying all extrema in the signal and then, for all found extrema, least-square testing for the occurrence of a glitch using a modeled glitch. To model a glitch, we convolve a step in acceleration not only for one sample (as all other methods) but for three consecutive samples. As we have equalized all components beforehand, we only use the poles and zeros of the U-component for this step. Continuity of the signal is forced at the beginning and at the end of the glitch window by Lagrangian multipliers. The signal is then considered a glitch when the variance residual after glitch removal is less than 1–2 % of the original data squared energy over a running window of 50 s, starting 5 s before the glitch maximum. To remove the glitch spikes after the glitch removal, a delta impulse is then searched around the glitch time and removed if associated with a 50 % variance reduction of the signal in a window of width ± 3 s. Glitches and spikes amplitudes are inverted on the three axes. We use these amplitudes to calculate dip, azimuth and amplitudes of the spikes that we use to potentially located glitch source (Section 6.1). An average of about 170 glitches per sol is found for 1 % of variance residual and about 100 glitches per sol for 0.5 % of variance residual. For the former case, about 40 % are detected on the three components while the other are on single VBB components. As this approach is detecting the glitch through the success of the functions' fit with data, glitch removal is a sub-product of the method.

2.5 Performance of Glitch Detection Algorithms

A 24 hours comparison of our glitch detection algorithms is illustrated Figure 2. The detection threshold for some methods was set low in order to examine differences in the detections close to the ambient seismic noise levels. For example, ISAE and UCLA used a correlation coefficient threshold of 0.8 which opens the possibility that some of the detections may be noise. Approximately 250 detections were made by UCLA and IPGP, and 140 by MPS and ISAE, however, the latter two detected less glitches during the noise daytime. Figure 2a shows the 73 glitches that were common to all 4 groups,

which correspond to those with the largest amplitude. Table 1 shows the number of detected glitches common to pairs of groups. The non-common glitches are plotted color-coded according to each group. An expanded section (Fig. 2b) reveals that the various criteria detect mutually exclusive glitches as the noise level is approached. We note that the Marsquake Service (MQS, Clinton et al., 2018) continuously monitors InSight’s seismic data to detect and catalogue seismic events (InSight Marsquake Service, 2020). As part of their routine they manually seek and annotate glitches with principal focus on time windows of seismic events. Our detection methods generally compare well with these manual annotations both in amount and onsets of glitches, especially for larger ones. For smaller annotated glitches, i. e. less than $1\text{e}^{-8}\text{ms}^{-1}$ in amplitude, we find that each detection method, if the parameters are chosen sensitive enough, delivers satisfying results with the amount of false detections only slightly increased. However, not each annotated glitch is detected as the noise level is approached and the signal-to-noise ratio hence decreases. Nevertheless, our comparisons show that our algorithms for glitch detection are reliable in most circumstances.

Table 1. Common glitch detections between group pairs for July 1 2019, Sol 211. Based on data of 02.BHV (VBB at 20 sps). Note that all algorithms equally detect the largest 73 glitches.

GROUP	MPS	ISAE	IPGP
ISAE	94		
IPGP	102	95	
UCLA	105	100	121

3 Glitch Analysis

Our working hypothesis is that glitches in SEIS’ time series data represent sudden steps in the sensed acceleration convolved with the instrument response of the respective seismometer, either VBB or SP. We can use that assumption to constrain the physical mechanism that led to the glitch. When interpreted as an inertial acceleration of the seismometer frame, a step in acceleration translates to a unlimited linear change of velocity. This of course becomes quickly non-physical and can be ruled out because it implied that SEIS by now would have left its landing location. On the other hand, accelerometers like the VBB or SP are also sensitive to changes in gravity. One way this can occur is by tilting the instrument, thus changing the projection of the local gravity vector onto the directions of the sensitive sensor axes. For small tilt angles α , this translates into a first order effect for the horizontal components ($\sim \sin(\alpha) \approx \alpha$) but only a second order effect for the vertical component ($\sim [1 - \cos(\alpha)] \approx \alpha^2/2$). The vector sum of acceleration changes in U, V and W due to a tilt of the SEIS sensor assembly (including the leveling system) will therefore point in the horizontal direction. This is true for both SP and VBB. Any other direction cannot be explained by a rigid motion of SEIS and must be due to instrumental artifacts.

It is useful to recall the sign convention for accelerometers: a positive output signal corresponds to a positive acceleration of the frame in the sensitive direction, not the direction in which the proof mass moved. Therefore, if one analyses the apparent glitch azimuth and incidence angles under consideration of the actual sensor orientations as well as the behaviour of these angles over time, one can draw conclusions on possible glitch origins. The analysis of apparent glitch polarizations is therefore our method of choice.

The determination of the apparent glitch azimuth and incidence angles is implemented in our glitch detection algorithm (Section 2.1) and based on a 3-D principle component analysis. To resolve the 180° ambiguity of the azimuths inherent to that method, we used the fact that glitches have a clear one-sided pulse (Fig. 1b,d); a glitch of positive polarity on the N-component is associated with a step in acceleration acting in this direction, its respective azimuth is therefore $\approx 0^\circ$ (assuming there is no glitch on the E-component). The same consideration holds true for a glitch showing on the (reconstructed) vertical component. In the Supplementary Information 2, we have detailed our theoretical considerations of apparent glitch polarizations especially with respect to the non-orthogonal sensor orientations of both the VBB and SP seismometers. There we demonstrate that our polarization

analysis is correct and that some resulting angles may not be intuitive for special cases for VBB and SP.

Figures 3–5 demonstrate the polarization analysis of the VBB and SP glitches for 2019. The plots incorporate two VBB channels 02.BH? and 03.BH? (20 sps and 10 sps, respectively), and two SP channels 67.SH? and 68.SH? (20 sps and 10 sps sample rate, respectively). These are the channels that, depending on the actual satellite down-link capacities, are continuously returned to earth. Besides some minor data gaps in this continuous operation, there is a large period with no data return between Sols 267–288. This is due to the solar conjunction period where Earth-Mars communications were obscured by the sun as consequence of their relative orbital positions. With respect to the Local Mean Solar Time (LMST, local InSight time, e.g. Allison & McEwen, 2000), the polarization patterns prevail over many sols and we discuss some of them in the following to understand the glitch behaviour in more detail. First, we discuss glitches occurring on only one VBB or SP component before building our arguments for multi-component glitches. We conclude this section by looking at glitches that occurred simultaneously on VBB and SP. Note that all details concerning the SEIS sensor assembly and available SEIS channels can be found in Lognonné et al. (2019).

3.1 Glitches on only one seismometer component

For VBB, amplitudes of one-component glitches are usually $<10^{-7}\text{ms}^{-1}$ and are thus not amongst the largest ones observed. Furthermore, a glitch occurring on only one single component cannot be interpreted as the SEIS instrument tilting. Such a glitch would necessarily have an incidence angle of $INC \sim 48^\circ/132^\circ$ (see Supplementary Information 2) whilst the only possible direction of acceleration change would point (nearly) in the horizontal plane for a true SEIS tilt. We hence conclude that VBB one-component glitches can only be related to instrumental artifacts such as (but not limited to) thermally driven stress relaxations in the suspension spring or pivot, displacement of one of the fixed plates of the displacement transducer, voltage offsets in the individual feedback electronics, or tilting of the individual sensor within the SEIS frame. Figure 3a,b shows the VBB one-component glitches. For most identifiable patterns we find their behaviour clearly changed either when the SEIS heaters were turned on (these are mounted on the leveling ring, see Lognonné et al., 2019) on Sol 168 (2019-05-19), or after the solar conjunction period in which the heaters were off and the SEIS instrument cooled down. This plus the fact these glitch patterns emerge due to their recurrence with respect to the local time, i.e. repetitively at the same time of the sol, leads us to conclude that they are indeed thermally driven. What we suspect is that the enormous Martian surface temperature changes, that can reach up 100°C each sol, introduce stresses into the material – possibly within the Evacuated Container. Even though the temperatures inside SEIS do not vary as much as outside, the stresses grow and are released once at a critical temperature is reached, thereby producing a glitch. When the heaters are on, the SEIS’ thermal regime exhibits essentially higher temperatures and, in second order, lower diurnal amplitudes and thermal spatial gradients. This contributes to minimize thermal stresses in this complex assembly, thus diminishing or at least altering glitch production. We demonstrate heater-related glitch behaviour in more detail in the next Section 3.2 for multi-component glitches. We have no good explanation why we observe so many more glitches on VBB W compared to the other two VBB components, especially after the conjunction period during which the SEIS heaters were off. Only after ~ 100 sols after the conjunction the number of one-component glitches (mostly constituted by glitches on VBB W) return to the pre-conjunction level (Fig. 3b).

For SP, a glitch occurring on only one single component could potentially be interpreted as the SEIS instrument tilting if the glitch shows one of the two horizontal components, SP V (2) or SP W (3). The tilt direction must furthermore be orthogonal to the other horizontal component so the glitch could only be seen on one component. More plausible than being caused by SEIS tilt we think is that these glitches are also thermally driven. Figure 3c demonstrates that the horizontal one-component SP glitches change their behaviour / occurrence with heater activation. For SP U, oriented almost vertically, a one-component glitch cannot be explained by instrument tilt because it does not point in the horizontal plane. These glitches therefore must relate to effects on the sensor level. Interestingly, Figure 3d demonstrates that SP U glitches that occur during the morning hours, i.e. when the environment becomes warmer, point upwards whilst during the evening/night hours, i.e. during the cooling cycle, the glitches point downwards. We interpret this behaviour as further evidence for the thermally driven nature of one-component glitches. Glitches occurring on the SP U

and on the (reconstructed) VBB Z in contrast support a non-mechanical origin, possibly related to voltage offsets on the displacement transducers lines.

3.2 Glitches on multiple seismometer components

The multi-component glitches for VBB and SP are illustrated in Figure 4. Especially for VBB, for which we generally detect more glitches, clear patterns emerge over the period of 2019. We discuss five of these patterns in the following.

We observe a glitch pattern with associated acceleration change pointing towards North (blue dots, pattern 1). These three-component glitches are often accompanied by glitch spikes and occur around 1800 LMST and thus when the local temperatures start dropping. The incidence angles are $\sim 90^\circ$ (in the horizontal plane) and hence may represent the SEIS instrument tilting. For this glitch pattern, however, we observe an additional 4.2 Hz ringing in some cases for the duration of the glitch, something not expected for an unhindered SEIS tilt. This occasional ringing could be related to other short duration data artefacts ("donks", still under investigation) we observe mostly in data with higher sampling frequencies (>20 sps). Due to the apparent temperature dependence of this pattern we currently favour the possibility that they are produced by the temperature decrease resulting in slight contractions of the tether and/or Load Shunt Assembly (LSA) – located both at azimuths $\sim 15^\circ$ and connecting SEIS with the InSight lander. This argument is supported by the fact that the heater activation on Sol 168 (2019-05-19) seemed to have no significant effect on these glitches (Fig. 4c), bearing in mind that the heaters are located within SEIS and the LSA/tether is not. Furthermore, the largest of these VBB glitches (amplitudes larger than $1e^{-7}ms^{-1}$) are also observed on SP with agreeing glitch azimuths and incidence angles (Fig. 5) and the same 4.2 Hz ringing. It therefore could be concluded that this glitch pattern is indeed due the SEIS instrument tilting, caused by cooling effects of the tether and/or LSA that also cause the 4.2 Hz ringing. On the other hand, the glitch azimuths of pattern 1 average to $\sim 0^\circ$ and not $\sim 15^\circ$ where the LSA/tether are located. Also, the acceleration changes associated with these glitches point northward and hence suggest SEIS tilting southward, something difficult to reconcile with e.g. the contracting tether "pulling" SEIS. One may therefore suspect not the tether itself as possible glitch cause but instead its connection with SEIS. Interestingly, there is another glitch pattern (green dots, pattern 2) with similar features: azimuths pointing consistently south (instead of north), incidence angles of $\sim 90^\circ$, often preceding glitch spikes, occurrence ~ 1000 LMST (instead of 1800), occasional 4.2 Hz ringing during the glitch, no significant effect of heater activation on glitch amount, and the largest amongst them also visible on SP with coinciding azimuths and incidence angles (Fig. 5). This pattern could represent the counter-part to pattern 1; in the warming cycle of the sol the glitch cause reverses.

The glitches with azimuths $\sim 240^\circ$ occurring around 2100 LMST (pink dots, pattern 3) show clear indications of being thermally driven. These three-component glitches with accompanying glitch spikes, that are not seen on SP, appear just after SEIS heater activation whilst before they were absent. Their consistent incidence angles of $\sim 100^\circ$ prohibit their interpretation of SEIS tilting but instead point towards a thermal effect acting on all VBB sensors. After the conjunction period, during which the heaters were off, they do not immediately reappear with the heater re-activation but only ~ 30 sols later together with azimuths being more variable. Such conjunction-delayed behaviour (before the pre-conjunction state is reached again) it is also readily visible for other multi-component patterns during the night time (red and pink dots at azimuths of $\sim 40^\circ$). For these reasons, such glitch patterns are likely to represent SEIS-internal, thermal effects. This is further supported by the glitch histogram in Figure 4e that clearly shows reduced glitches for the night time just after heater activation (fewer red dots). We note that there is a similar pattern on SP at azimuths of $\sim 350^\circ$ (red dots) that occurs at the same times as the corresponding VBB one.

Another prominent VBB multi-component glitch pattern occurs in the early sol-hours with azimuths mostly due East (yellow-orange dots, pattern 4). These three-component glitches with accompanying glitch spikes, that are not seen on SP, happen during the diurnal cooling cycle. Although there seems to be no obvious influence by the heater activation (or re-activation after conjunction), with increasing sols they occur at earlier hours. This plus the fact that their incidence angles $INC \neq 90^\circ$ exclude a rigid tilt of the SEIS instrument lets us conclude that for this pattern, too, thermal effects are the primary glitch cause.

There is another thermally-driven glitch pattern that appears on both VBB and SP in the early morning (yellow-orange-red dots, pattern 5), which again leads to glitches on the vertical VBB component ($INC \neq 90^\circ$). It is discussed in detail in the next Section 3.3.

Patterns 3–5 are therefore all associated with non-horizontal incidence angles suggesting that the three VBB sensors are not detecting an overall instrument tilt. Instead, each of the three VBBs detects a different tilt that consequently leads to the non-zero glitch on the vertical axis. The VBB sensors are mounted on a titanium plate inside the Evacuated Container through three mounting bolts oriented at azimuths of 105° (IF1), 225° (IF2) and 345° (IF3). So, the first one is pointing roughly due east, while the two other ones point due west and are symmetrically to one another with respect to the West. This configuration produces colder temperatures on the east side during the night than on the west side (and the opposite during the day), with larger gradients between IF1–IF2 or IF1–IF3 than between IF2–IF3. This is likely the primary source of these thermal glitch patterns. We note that the temperatures between the inside and outside of the Evacuated Container are out of phase with the outside being ahead by about 7–9 hours (Pou et al., 2019).

3.3 Glitches on both VBB and SP

Figure 5 shows all glitches that occurred within ± 2 seconds on both VBB and SP. From these 638 glitches, 118 glitches reveal the same azimuths to within $\pm 10^\circ$. Most of the glitches on VBB and SP that match in azimuth were discussed already in the previous Section 3.2 (green and blue dots, parts of patterns 1 and 2). As we pointed out, these glitches show incidence angles of $\sim 90^\circ$ for both VBB and SP and therefore could signify the whole SEIS instrument tilting.

The most prominent glitch pattern in Figure 5 is the one at azimuths of $\sim 145^\circ$ for VBB and $\sim 110^\circ$ for SP (yellow-orange-red dots, pattern 5). From the beginning of SEIS’ operational mode, these relatively strong glitches occurred once every morning with persistent glitch azimuths throughout 2019. Between sols 80–167, so before SEIS’ heater activation, their onset times shift each sol by on average 4 Martian minutes ($\sim 2\%$ longer than SI minutes). This can be interpreted as the glitches occurring at a critical temperature during the cooling cycle that is reached earlier every sol as the Northern hemisphere (where InSight is) is entering the colder season. When the heaters were turned on, leading to SEIS being in a thermally mitigated state, the glitches continued drifting towards earlier times but now with an average rate of less than 2 minutes per sol. After the conjunction period, during which the heaters were turned off, we observe the same as for many other glitch patterns; a more diffuse signature of the glitch azimuths and incidence angles that seem to return to pre-conjunction states only ~ 100 sols later. Also, the onsets time now drift towards later times (red to yellow) each sol which interestingly coincides with the fact that the Martian solstice occurred just after the conjunction on Sol 308. For this pattern as a whole, we were able to clearly identify the critical temperature around which the glitches occur. As Figure 5d,f demonstrates, the glitch onset times strikingly follow the iso-temperature curve at -54°C for both VBB and SP. In addition for VBB, there are more patterns with similar behaviour for which we could find the critical temperatures; these correspond to pattern 3 (red and pink dots, Section 3.2). All this evidence once more supports the fact that most glitches are thermally caused. Note that the temperature sensor we used here is scientific temperature sensor A (SCIT A, channel 03.VKI), located at the northern, inner side of leveling support structure. The temperatures measured at this sensor can also occur elsewhere in the SEIS assembly at the same time.

4 Glitch Removal

Once a glitch has been detected (Section 2), the raw waveforms are modeled as a linear combination of the glitch – the response of the seismometer to a step in acceleration – and the glitch spike – the response of the seismometer to a step in displacement. The two responses can be modeled from the poles and zeros of the transfer function of either the VBB or SP seismometer. Only the amplitudes and the precise timing of the source (which might be between two recorded samples) are to be inverted with such model. Due to the time-limited extent of glitches and spikes as opposed to permanent (ever-lasting) steps in acceleration and displacement, respectively, all methods prefer to correct the raw data rather than the data after conversion to physical units.

The MPS group models a glitch waveform for each detected glitch using three parameters: an amplitude scaling factor, an offset, and a linear trend parameter. To find the best fit within a respective glitch time window, the model is iterated over each (sub-)sample and the best fit for the three parameters is determined using non-linear least squares (NLSQ, via the Trust Region Reflective algorithm). The deglitched data then is obtained by subtracting the fitted glitch without the offset and linear trend from the original data. To avoid introducing tiny DC-offsets in the data caused by the fact that glitches are not yet fully returned to their baseline after e.g. 30 seconds, the fitted glitch is not only removed for the fit windows but for time windows corresponding to 10000 subsequent samples (independent of the data sampling period). The same procedure is done for glitch spikes once a glitch has been removed, however, the sub-sample search grid is finer than for glitches because it has greater impact on the goodness of fits. To prevent our method from removing data where the glitch fit is not good enough, i.e. the model is fitted to data that are in fact no glitches or fitted to glitches that cannot fully be represented by our model of a step in acceleration, we correct glitches only for which we can achieve a variance reduction of e.g. $>80\%$ with respect to the glitch fit window. We find this threshold to generally permit the removal of all large glitches whilst small glitches are also removed if their waveforms represent that of the underlying model well. For cases where such glitch fits do not work well, we repeat the approach but allow for a finite rise time of the acceleration change (as opposed to a zero rise time acceleration step). This does not change the resulting waveform of the glitch model too much whilst improving the data fits in some cases. We note that this limited ramp, i.e. usually less than 5 seconds in length, is linear, a Gaussian-like ramp does not improve the fits. For spikes and their corresponding steps in displacement such finite rise modelling should not be done as it changes the resulting spike waveforms drastically. The MPS method is implemented for all sampling frequencies. An example of its glitch removal is shown in Figure 6.

The UCLA group carries out glitch and spike removal on 10/20 SPS data. Some glitches show symmetric or asymmetric broadening relative to the glitch template, suggesting the source function is more complicated than a Heaviside step in acceleration. As a first approximation, convolution with a unit Gaussian or exponential decay, which adds an extra parameter, significantly improves the fit, but runs the risk of over-fitting data. To minimize this effect, the approach is only applied to data that show >0.9 correlation coefficient with the glitch corresponding to our acceleration step-model. Glitch (sometimes broadened) and spike templates were fit to the glitches and spikes, respectively, using NLSQ. Because of the delta-like shape of the spike over one or two sample intervals, the starting model must find the location to within a fraction of a sample interval (e.g. 0.05 s). Glitches are easier to fit than spikes, being low frequency, and requirements on the starting model are less stringent. Spikes are much smaller in 2 SPS data relative to glitch sizes. Thus 2 SPS data were used to generate a glitch catalog (Section 2). The starting parameters from the 2 SPS fits were then used to fit glitches in the 20 SPS data and residuals were calculated. The residuals were examined for the presence of a spike in the data before the glitch peak, by requiring its amplitude to be greater than 5 standard deviations of the residuals after the peak. If true, an iterative forward model was run by shifting the phase of the spike template about the corresponding peak in the residuals (in steps of sample interval/10), and finding the amplitude and phase of maximum cross correlation. The NLSQ was run again with both spike and glitch templates, and the result checked whether cross-correlation of data and model are above a threshold, and if so, the results are stored. At this stage, for poly-glitches (one on top of another) we search for spikes throughout the sequence. Even though a number of spikes have been removed, there are residuals and transients that remain. Poly-glitches can have several internal spikes, and extreme glitch overlap, making automatic procedures difficult, requiring manual fitting.

The removal algorithm of the ISAE group is basically described in Section 2.2 (glitch detection). Once a glitch has been detected using cross-correlations between the model and data, the model without linear trend and offset is subtracted from the data. This method is implemented for all sampling frequencies available. Spike removal and deviations from the simplified acceleration step-model are not implemented.

The IPGP group inverts three consecutive acceleration step sources for the glitch which allows not only to invert for multi-component glitches occurring within these 3 samples but also to invert for the phase delay through finite-difference approximation of the first and second time derivative. This linear approach allows the inversion to provide identical results in the U, V, W coordinates or in the Z, N, E coordinates, as the rotation between the two coordinates systems is a linear relation. Conversely, the three other methods, through their non-linear part of the inversion or through the

cross-correlation phase fitting, have built-in small reasons to provide different solutions depending on the coordinate systems.

In the end, all the proposed deglitching methods are nevertheless based on the same idea of assuming a step in acceleration and displacement to model a glitch and spike, respectively, by using the instrument impulse response of either the VBB or SP seismometer. Removal differences across the methods are mostly due to thresholds below which a glitch is removed or not, and by how these methods attempt to fit glitches that do not fully correspond to our acceleration step-model. No general rule on the thresholds can be provided as they depend on the data processing target. As an example, all methods provide similar deglitching for the large glitches occurring during the cooling periods and during the night. More freedom is available for fitting longer source duration glitches during the day although some of the latter may represent the real response of SEIS to a small pressure drop (Section 6.3) which can generate nano-tilts of the SEIS instrument. At the same time, while many spikes are fitted by the templates, there are a significant number that have quite different morphology, longer ringing, or longer-period transient behavior. Caution must therefore be exerted when attempting to remove these as it may unintentionally lead to removal of small parts of higher frequency content. To circumvent such effect, spike fitting by those methods who have implemented it is only attempted within a few samples left and right near the theoretical glitch onset and only removed if the fits are good enough. Due to their delta-like overall shape, we argue that this procedure diminishes any unwanted removal. Due to the spikes' relatively high frequency content close to the Nyquist frequency, it is also possible to filter them out rather than removing them from the raw data, however, small artefacts depending on the exact case may remain. All these arguments combined is the reason we do not provide glitch and/or spike corrected data for all available periods but instead make our codes available, enabling own comparisons and removal choices to those interested. An example of glitch removal showing all four methods is demonstrated in Figure 7 for two glitches occurring during marsquake S0173a.

We lastly point out that we have discontinued our deglitching efforts using the stationary wavelet transform as described in the Supplement V of Lognonné et al. (2020). Whilst this approach provided promising and correct results for a fair amount of cases (as far as one can tell), there is no underlying, physical model involved and the implicit data 'correction' therefore seemed too arbitrary. For many cases this approach further introduced DC-offsets in the deglitched data whose amplitudes and lengths depended on the length of data read (and therefore maximum decomposition level); an artifact that we could never manage to fully avoid.

5 Glitch Model

Throughout this paper we have assumed that glitches can be understood as steps in acceleration and glitch spikes as steps in displacement. This model allowed us to successfully detect, analyse and remove one- and multi-component glitches for both VBB and SP. In the following we detail the theoretical considerations behind this simple model.

Let us assume glitches are caused by a small instantaneous tilt. By instantaneous we mean that the time history of the tilting is so short that it cannot be resolved with any given sampling frequency available to us (maximum 100 sps). We are thus allowed to idealize any step in time by a Heaviside function. Physically such short instantaneous events can for example be the result of stick-slip events.

The small tilt is assumed to be the result of a rotation around a horizontal axis, $\vec{a}$. Recall that the VBB is a pendulum seismometer where the (inverted) pendulum is constrained to rotate around a horizontal axis, $\vec{b}$. The sensitive direction, $\vec{s}$, of the pendulum is perpendicular to the $\vec{b}$ axis and is inclined relative to the horizontal plane by a dip angle of $\delta = -29.3^\circ$. Let us also assume for simplicity that all the mass of the pendulum is concentrated in its center of gravity (CoG) - which would be the case for a mathematical pendulum.

Now we can distinguish five cases which differ by the location of the accelerometer relative to the tilt axis, $\vec{a}$:

(1) the two axes $\vec{a}$ and $\vec{b}$ are parallel and $\vec{a}$ passes through CoG: in this case the accelerometer gets only reoriented relative to the gravity vector but the CoG stays in place.

(2) the two axes are parallel and $\vec{a}$ does not pass through CoG but is at the same height as the CoG: in this case the accelerometer gets displaced vertically and reoriented relative to the gravity vector. However this reorientation is negligible because it is only a second order effect.

(3) the two axes are parallel and $\vec{a}$ does not pass through CoG. Furthermore a line parallel to $\vec{s}$ passing through CoG intersects with $\vec{a}$. In this case the accelerometer gets displaced vertically and reoriented. However the displacement is in the direction perpendicular to the sensitive axis and hence is not seen by the accelerometer. Only the reorientation is sensed.

(4) For all other locations of the rotation axis $\vec{a}$ for which $\vec{a}$ and $\vec{b}$ are parallel the accelerometer will see both a displacement and a reorientation relative to the gravity vector.

(5) For the general case where $\vec{a}$ and $\vec{b}$ are not parallel the same arguments can be made but the effect sensed for a given tilt angle will always be reduced relative to the case with parallel axes $\vec{a}$ and $\vec{b}$ since the tilting is reduced.

As soon as the accelerometer gets reoriented relative to the gravity vector we expect to see the response due to a step in acceleration, because the projection of the gravity vector into the sensitive direction is changed. In those cases where the accelerometer gets displaced we expect to see the response due to a step in displacement. The five cases then only differ in the relative size of the displacement and tilting.

What do these signals look like? In Figure 6 we have plotted the response of the VBB sensors to a step in acceleration and the response to a step in displacement, both including the effects of the limited pass-band and down-sampling. To model the instrument responses to these steps, we take the full seed response and evaluate it at the frequencies corresponding to those of the Fourier transform of the input steps using *evalresp* – a piece of software provided by the Data Management Center of the Incorporated Research Institutions for Seismology (DMC / IRIS). Figure 6 also demonstrates how we can use the modelled glitch and spike to remove them from the data.

Can these signals explain the data? As Figure 6 also demonstrates, the modeled responses have been shifted in time and scaled to match the data. The fit is excellent both for the low-frequency glitch and the high-frequency spike. We take this as confirmation that our simple model is capable of explaining the glitch waveform with four parameters: start-time and amplitude of the step in acceleration plus the start-time and amplitude of the step in displacement. In fact we could show that the start times of the acceleration and displacement steps coincide to the millisecond – which is what our model predicts. Thus we only need three parameters: the start time and the amplitudes in displacement and acceleration. Determining the start time requires an excellent calibration of the high frequency part of the sensors transfer functions, as well as high sampling rate. While deglitching on the 20 SPS data is therefore much more precise and has been done for two of the described methods (MPS, ISAE), the deglitching on lower rate data, e.g. 10 SPS (UCLA) or even 2 SPS (IPGP) can be achieved, including for the spike amplitude, however, with the signal-to-noise ratio reduced by the frequency ratio of the bandwidth. Fitting the spike plus glitch with these three parameters implies determining the start time to sub-sample resolution. We provide a more mathematical description of our model for the glitch plus spikes phenomenon in the Supplementary Information 2.

6 Other Observations

In the following we briefly discuss other aspects of glitches and spikes that we encountered during our investigations. This section shall therefore complement our understanding of glitches and detail some more implications.

6.1 Possibly locating SEIS-internal tilts

Our glitch model presented in Section 5 is valid for rotations of the sensor assembly as a whole (e.g. caused by a change at one foot of the sensor assembly), for just the VBB sensors (e.g. caused by stick-slip events originating at the interface between the Evacuated Container and the leveling support structure), but also for an individual sensor (e.g. caused by stick-slip events originating at the sensor-support interface or at the fixed side of the pivot or spring). Each of these cases implies a different value of r : the distance between VBB U to the sensor assembly feet at 16 or 21 cm (Fayon

et al., 2018), or the distance from the sensor’s center of gravity to its pivot with 2.6 cm (Lognonné et al., 2019).

We illustrate this geometry with the glitch example of Figure 6 and recall the glitch and spike characteristics in Table 2. This glitch has a vertical component and can therefore not represent the SEIS instrument tilting as a whole. The azimuth of the glitch opposite (opposite of acceleration) and of the spike (displacement) are 219° and 228° , respectively. These values average 223.5° , which is quite close to one of the plate’s mounting bolts IF2, located at 225° . The opposite signs of the glitch amplitudes of VBB V and VBB W suggests a deformation relatively symmetrical with respect to the IF2 azimuth, while the low amplitude glitch on VBB U suggests the latter to be much reduced between the two other IFs. This glitch is therefore compatible with a radial deformation of the mounting bolts IF2. Further analysis on the impact of the thermo-elastic stresses in the VBB sphere and the resultant glitch generation will however be demonstrated in a future publication.

Table 2. Night time glitch example from Figure 6: calculated spike amplitudes and resulting geometry parameters.

Component	Glitch amplitude (nm/s ²)	Spike amplitude (nm)	Tilt (nrad)	Apparent radius r (m)
U	1.49	0.67	-0.46	-1.270
V	179.50	-2.38	-55.4	0.044
W	-258.89	3.01	80.0	0.038

During the night, very small but also large rotation radii are found, likely resulting from internal deformation of the Evacuated Container triggered by thermal effects, as discussed previously. During the day however, the rotation radii of the glitches are more stable and in the range 10–30 cm, suggesting an external source and therefore rigid tilt of SEIS, likely generated by the atmospheric activity.

6.2 Loading with Arm

The InSight mission includes the Heatflow and Physical Properties Probe (HP³, Spohn et al., 2018) that includes a probe ("mole") intended to hammer itself 3–5 m into the Martian regolith. The mole has had difficulty getting started, and so the lander’s Instrument Deployment Arm (IDA) has been pressed into service to help. On several occasions, the IDA has pushed down on either the regolith or the mole itself. When the IDA pushes down, it induces an elastic response in the regolith, deforming the surface into a funnel shape, inducing a tilt at the seismometer about 1.2 m away. This tilt of about 70 nrad is clearly observable on both the SP and VBB sensors in Figure 8 as steps in the horizontal accelerations.

In this example, at the start of the command sequence the IDA was pushing down lightly on the mole, and was given four commands: 1) move up to get off the mole, 2) move radially outward slightly, 3) move down to just above the mole, and 4) move down again to reload the mole with a downward force. We see in the seismometer data the first move up and the resulting tilt up to the NE. The arm resonates after it loses contact with the mole, and we see that as the 4.2 Hz ringing in the seismometer data. The seismometer does not have a significant response to the radial outward move. Then on the third move, it appears that the IDA actually touched the mole while stopping and then rebounded and resonated while hovering in mid-air just above the mole. Finally the IDA moves down to load the mole and we see a tilt down to the NE at the seismometer.

We also observe several glitches, circled in red, that happen at the same time as the IDA motions. One of the tell-tale signs of a glitch is when we observe an offset in acceleration in the seismic components. We interestingly observe that the BHE-component shows steps of the same sign for both the arm loading and unloading. Two of the glitches further appear to involve the whole sensor assembly as they are seen on both the VBB and SP. Other glitches seem to be limited to one or more components of the VBB. This all points towards that these glitches are internally caused and only triggered by the IDA movement. Attempting to remove these IDA-induced glitches show convincing fits with our acceleration step-model for the BHV and BHW components, however, for the BHU

component the removal is more difficult also because of the additional 4.2 Hz ringing (Fig. 8b, top panels). Nevertheless, IDA movements are limited and therefore this type of glitch does not represent a major contamination of InSight's seismic data.

6.3 Atmospheric Pressure

Pressure effects such as convective vortices ("pressure drops" or "dust devils", e.g. Lorenz et al., 2015; Kenda et al., 2017), turbulence in the atmospheric planetary boundary layer (Murdoch et al., 2017; Banfield et al., 2020), gravity waves (Spiga et al., 2018; Garcia et al., 2020) and acoustic waves (Martire et al., under review in this issue) are all measured by InSight's Auxiliary Payload Sensor Suite (APSS, Banfield et al., 2019) that consists of wind direction and speed, temperature and atmospheric pressure sensors. The aforementioned pressure effects are generating signals on the SEIS components mostly from 0.5 mHz up to about 2 Hz, among which convective vortices are generating the largest physical signals observed by SEIS. Their dominant period, as seen both by atmospheric pressure sensor and SEIS, can be close to the one of the glitches depending on their size, distance to SEIS and wind speed (Murdoch et al., under review in this issue).

At frequencies lower than 0.1 Hz, the compliance response of the ground is dominated by tilt effects which are strongly impacting SEIS' horizontal components (Kenda et al., 2020). These ground responses are usually more complicated than our simple acceleration step-model (Murdoch et al., 2017; Murdoch et al., under review in this issue). We instead often observe that the dust devils' pressure signal convolved with the instrument response of SEIS can match well in shape with the integrated raw waveforms of the observed SEIS glitches. Such ground responses are the reason SEIS signals induced by convective vortices may, wrongly, be detected as glitches. On top of these complexities, the ground deformations induced by convective vortices are sometimes generating real glitches (SEIS' raw data matching perfectly with our acceleration step-model) that can even show on the vertical components. Discriminating between these various SEIS signals is therefore a challenge for all glitch detection methods.

7 Discussion

Glitch Causes

As we established, the majority of glitches is related to internal instrument effects. On Mars, the SEIS sensor assembly is installed in a harsh environment. While shielded by the wind-thermal-shield from wind and direct sun light, all the sensor assembly, tether and regolith on which the hardware rests undergo a large daily temperature cycle.

The ~ 80 K peak-to-peak ambient daily temperature variations are attenuated by the different thermal shields but still reach ~ 15 K inside the evacuated titanium sphere hosting the three VBB sensors. These temperature fluctuations inevitably lead to thermal strains and thermally induced stresses at the contacts between materials with different thermal expansion coefficients. These stresses will in turn lead to additional elastic deformations. Alternatively, these stresses can be relaxed by a variety of irreversible mechanisms such as creep, diffusion of lattice dislocations or stick-slip along mechanical contacts. While we do not know which actual stress relaxation mechanism or which combination of mechanisms is at play, we attribute thermally related glitches to intermittent stress relaxation events such as for example stick-slip events.

The question of whether external events can trigger glitches arises when we inspect marsquake S0173a (Fig. 7), the VBB response to certain pressure drops, or the VBB response to ground loading experiments with the scoop of the instrument deployment arm (IDA, see Fig. 8). In all these cases the seismic waveforms are contaminated by a glitch. We argue that external events alone do not cause glitches. Instead, as the SEIS sensor assembly goes through the daily temperature cycle, internal stresses build up until a threshold is reached and a stick-slip or another stress relaxation event occurs. In other words, an infinitesimally small additional stress may suffice to trigger a glitch if it occurs at the right time, i.e., a time when thermal stresses have almost reached the critical threshold and a relaxation event is about to happen. Any additional external acceleration, be it a marsquake, the passage of a pressure drop, an IDA arm movement, or a soil loading experiment with the IDA scoop will make the glitch occur earlier than it would have without the external event. So in this view

external events alone do not cause glitches, they merely advance their time of occurrence. To look at this closer, we analysed the delays between arrivals of seismic events and glitches detected shortly after them. Since the broadband and low frequency marsquakes were shown to be due to a stationary Poisson process (Knapmeyer et al., under review in this issue) while glitches are distributed unevenly over the sol, one may suspect that triggered glitches occur already within a few seconds after an arrival if following our model. We found no obvious relation (Fig. SI2-3). Whilst the number of events with clear P and S arrivals is small, and a more thorough re-analysis with a larger data set may be worthwhile, all our analyses combined still suggest that the timing of glitches generally has a strong stochastic component next to a deterministic component. This is further supported by the frequency-amplitude distributions of glitches per component that seemingly follow a Gutenberg-Richter relation (Fig. SI2-3), and the presence of the diurnal harmonic and all its integer multiples in a time series composed of modeled glitches (Fig. SI2-4c).

On the other hand, one third of all glitches exhibit quasi horizontal polarization and thus could represent the whole SEIS instrument tilting. Some of these cases may indeed be rooted in the ground tilting and thus be real seismic signal, a scenario demonstrated by Zahradnik & Plesinger, 2005. They found glitches (they use the term "long-period disturbances") during earthquakes phase arrivals solely to occur on the horizontal components, something we also observe for marsquakes but only for a minority of cases. They preferably interpreted such glitches as ground tilt, possibly caused by small-scale material instabilities beneath the station triggered by the incoming waves or thermally or chemically induced micro-cracks that would not require any incoming wave energy. These interpretations of tilt causes, however, are not unique and our investigations did not allow us to narrow down their causes as the InSight setup puts too many variables in question. For example, next to true ground tilt it is further conceivable that horizontally polarized glitches are caused by the SEIS instrument tilting either due to imperfect anchoring of its feet to the ground or by the load shunt assembly (LSA) / tether pushing and pulling on SEIS as reaction to atmospheric changes in temperature, pressure and wind. We have no clear observation that azimuths of such glitches cluster towards the feet of SEIS leveling system (LVL, see Figs. 3–5), however, we cannot finally conclude that the anchoring may not cause such glitches at all. Nevertheless, we find most of the instrument-tilt indicating glitches to point either North or South, that is, either close to the LSA-tether system or diametrically opposed (Fig. 4, patterns 1 and 2). Whilst the picture is not fully conclusive (Section 3.2), there remains the suspicion that the LSA-tether system or even the lander exert influence on SEIS and therefore promote glitch production via mechanisms for which we have no unique interpretations.

Lastly, we mention that glitch spikes seem to largely coincide with "donks", yet another type of data disturbance typically only visible on VBB and SP seismic data of 20 SPS and higher. The relationship between donks and glitch spikes was not analysed within the scope of this paper but will be more detailed in different publications related to non-seismic signals observed on SEIS.

Glitch Mitigation

Given the abundance of glitches and their influence on the data analysis, the question arises how glitches could be mitigated for future installations. For thermally related glitches, the most obvious action would be to decrease the thermal amplitudes the seismic sensors are exposed to. Whilst for the SEIS instrument great care was taken to achieve just that (wind-thermal shield, remote warm enclosure box, vacuum sphere, heaters, thermal compensation device; see Lognonné et al., 2019), the daily temperature cycle still exceeds those of fine terrestrial stations by four orders of magnitude, i.e., ~ 15 K compared to a few mK. Given the harsh environments typically found on extra-terrestrial, planetary bodies, it may not be easy to achieve higher thermal stability however it should be considered by engineers. We can only speculate as to the exact sources of glitch production within the instrument. While we have good candidates (see further above), the fact remains that InSight's seismometers, especially the VBB, are complex devices consisting of many materials, joints and connections. One way to approach thermal glitch reduction may therefore be to use fewer materials and thus minimise potential thermal conductivity gradients, stresses and expansions. A last, ultimate step to achieve thermal stability would be to completely bury the instrument and possibly even the tether but this may not be feasible for many types of reasons. For glitches indicating instrument tilt, one way to mitigate glitches could be to improve on the feet anchoring by usage of even more specialised feet shapes (details on SEIS' leveling system: Fayon et al., 2018; Lognonné et al., 2019) and/or by deploying the

instrument on hard rock as opposed to InSight that is deployed on regolith (e.g. Golombek et al., 2020).

8 Summary

We have developed a possible physical model for the generation of glitches and their associated high-frequency spikes that occur simultaneously with the glitch onsets (Fig. 1). In this model, glitches represent steps in the acceleration sensed by the individual sensors convolved with the instrument responses whilst glitch spikes represent steps in the displacement sensed by the individual sensors convolved with the instrument responses. We used this model to develop different algorithms for the glitch detection that are all able to identify most of the high amplitude glitches for both the VBB and SP seismometers (Section 2, Fig. 2). Based on the model we were further able to demonstrate that most glitches are thermally-driven (Section 3, Figs. 3–5), and could, at times, also be triggered by external events such as convective vortices or movements of InSight’s robotic arm (Section 6, Fig. 8). Such thermal glitches likely represent SEIS-internal tilts that differ amongst the individual sensors and hence produce glitches on the vertical components, an observation that cannot be reconciled with the whole SEIS instrument physically tilting. Only a portion of all observed glitches can be explained by a tilt of the SEIS package, either related to true ground tilt, imperfect feet anchoring or the load shunt assembly / tether pushing and pulling on the SEIS instrument. We illustrate the two cases of most common glitch production in Figure 9.

Whilst terrestrial data influenced by glitches may simply be discarded due to their difficult handling, this represents no valid option for the seismic data returned from Mars. We therefore devoted much of our efforts to develop code for the glitch and spike removal (Section 4). Our algorithms have proven successful in many cases for both seismometers VBB and SP (Figs. 6 and 7). Of course, there remain glitches and spikes especially of smaller amplitudes that we cannot sufficiently well fit and therefore confidently remove. To account for such glitches nevertheless, we have slightly deviated from our step-model in acceleration to improve on their removal, i.e., we introduced fits for non-zero rise times (MPS), for a combination of multiple source-functions (UCLA), and for three consecutive acceleration steps of varying amplitudes (IPGP). The resulting glitch models of these adaptations still produce glitch waveforms close to the ones corresponding to a zero-rise time acceleration step, allowing however to fit for glitches whose responses are broader than the ones corresponding to our simplified step model. As we demonstrate in Figure 10 for VBB long-period spectra to look for Phobos’ tides and for receiver functions of the marsquake S0173a, removing glitches following the approaches presented here indeed allows to improve on the quality of seismic data and may hence help to accomplish InSight’s scientific goals.

As no glitch removal algorithm can warrant a perfect clean-up of all glitches and their spikes, we prefer to not provide a deglitched time series of all available data. Instead, we have assembled our algorithms for glitch detection, glitch polarization analysis, and glitch removal into one Python / ObsPy toolbox. Some convenient functions for data retrieval and handling are also implemented. The package further holds MATLAB scripts to perform glitch detection and removal tasks as presented. Its link is: <https://pss-gitlab.math.univ-paris-diderot.fr/data-processing-wg/seisglitch>. Documentation is available. Together with this code we also provide deglitched data for a selection of seismic events.

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Figures

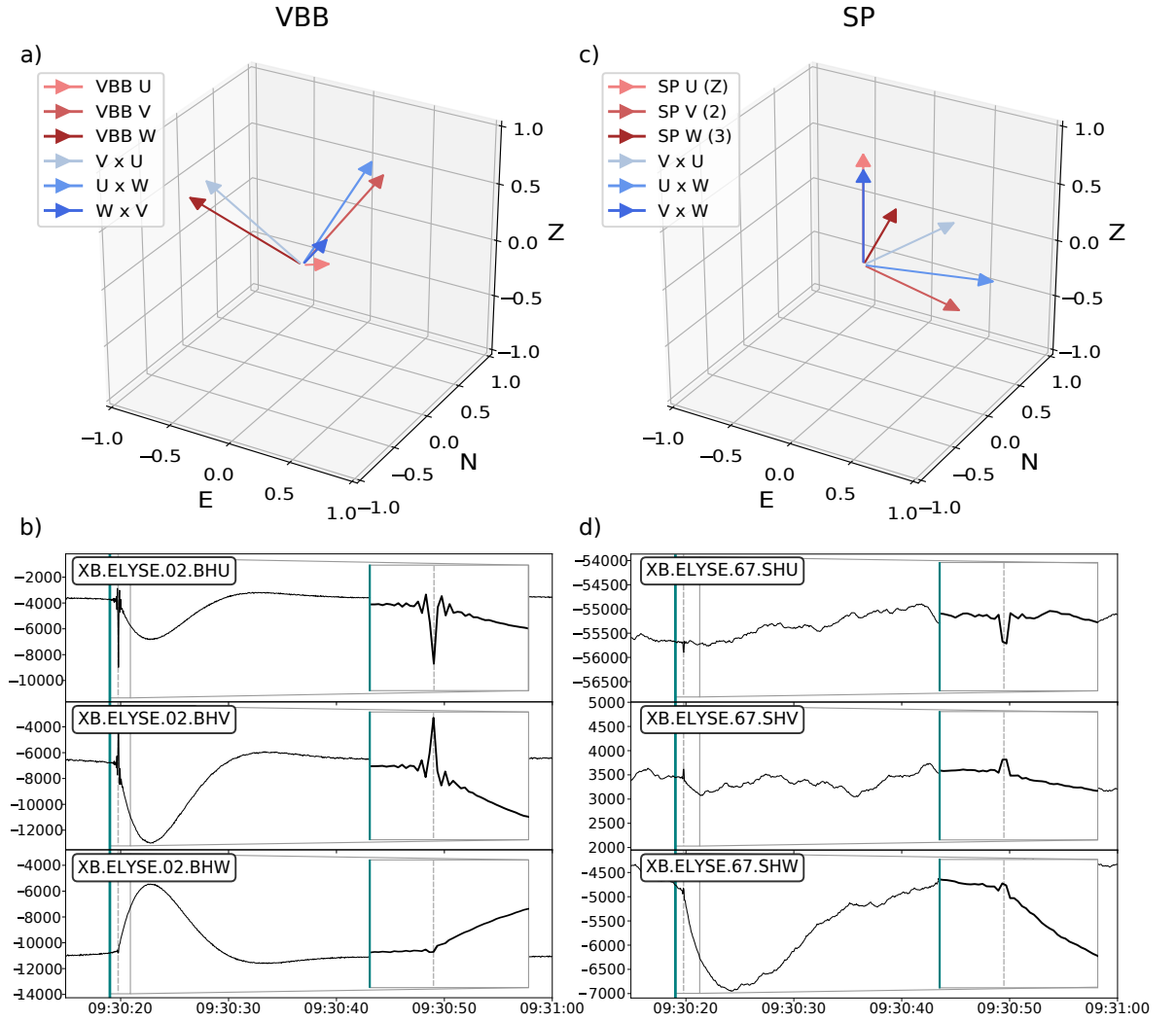


Figure 1. Sensitive directions (red arrows) of the two three-component seismometers that are part of the SEIS package; a) VBB, c) SP. Blue vectors are the pairwise vector cross-products of the sensitive sensor directions of the VBB and SP, respectively, and represent hence the only directions possible for the acceleration associated to one-component glitches (Section 3 and Supplementary Information 2). Multi-component glitch example on 2019-12-16 (Sol 374) occurring on both b) VBB, and d) SP. Green lines: detected glitch onset after MPS method (Section 2.1); gray dashed lines: theoretical glitch onset (according to our step model) that coincide with the maximum / minimum of the glitch spike (inlays, showing 1.5 s of data). Note there is no glitch visible on SP U and SP V. The glitch spikes are visible on all six seismic components, however much less on SP.

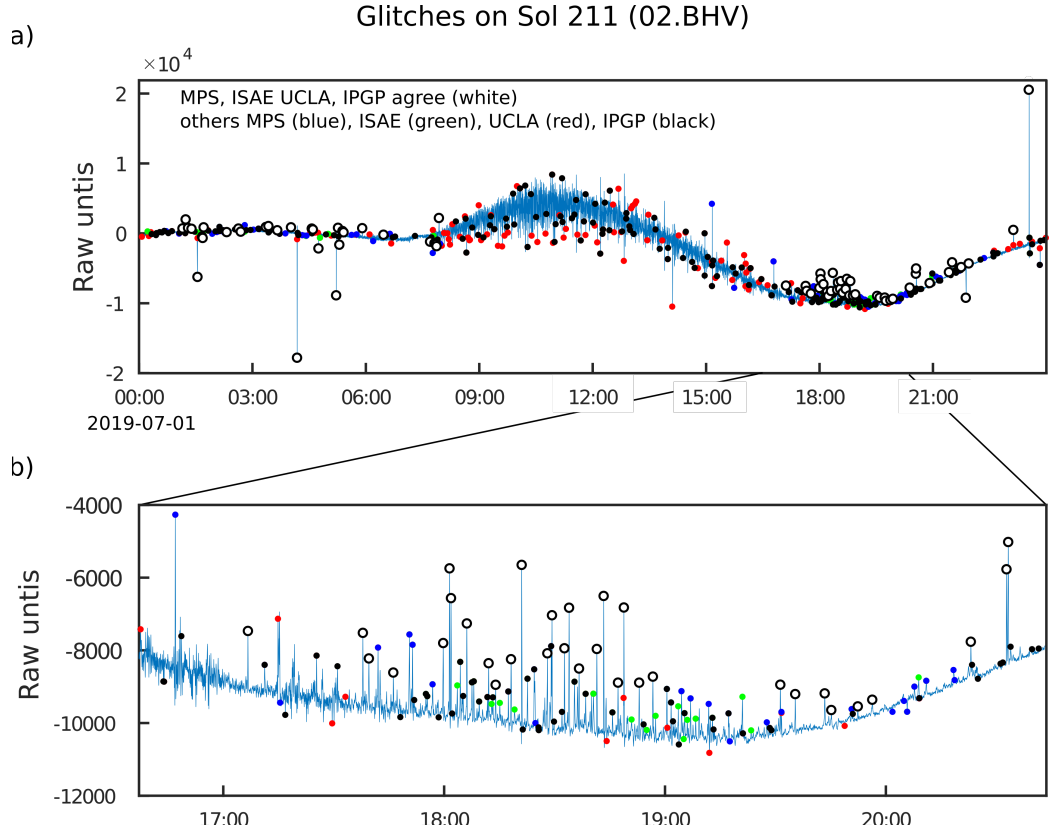


Figure 2. a) Comparison between glitches detected on 02.BHV (VBB) on July 1 2019 (Sol 211) by our four groups: MPS, ISAE, IPGP, and UCLA. White circles are common glitches for all groups. Color coded symbols correspond to glitches for the different groups that are not common to all. Those common to sub-groups are plotted on top of each other and so the last plotted is shown. b) Expanded section showing that as the threshold for declaring a glitch, either in terms of signal-to-noise or correlation with the template, is lowered. Results differ markedly, and some possible candidate glitches may have been missed.

One-component Glitches

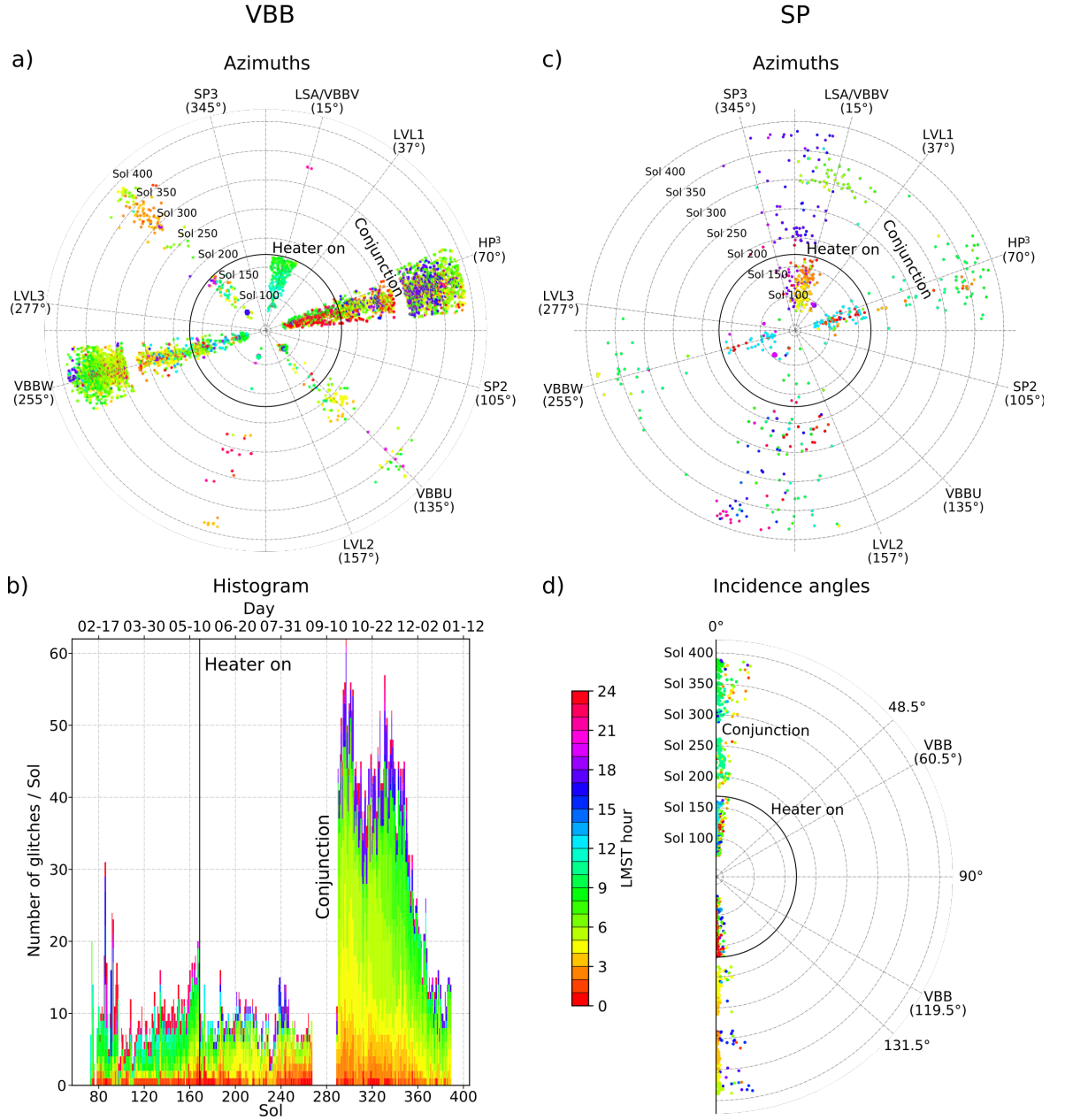


Figure 3. One-component glitches of VBB and SP for 2019 as detected by our MPS algorithm: a) VBB one-component glitches. Glitch azimuths align with azimuths of VBB components, incidence angles are, as expected, $INC \sim 48^\circ/132^\circ$ (not shown), b) histogram of a). Note the rate change of glitches after heater activation (Sol 168) and conjunction (Sols 267–288), the latter mostly caused by VBB W, c) SP one-component glitches for the horizontal components SP V and SP W, and d) one-component glitches for the (almost) vertical SP U component. Color code refers to local mean solar time (LMST, in hours) of glitch onsets.

Multi-component Glitches

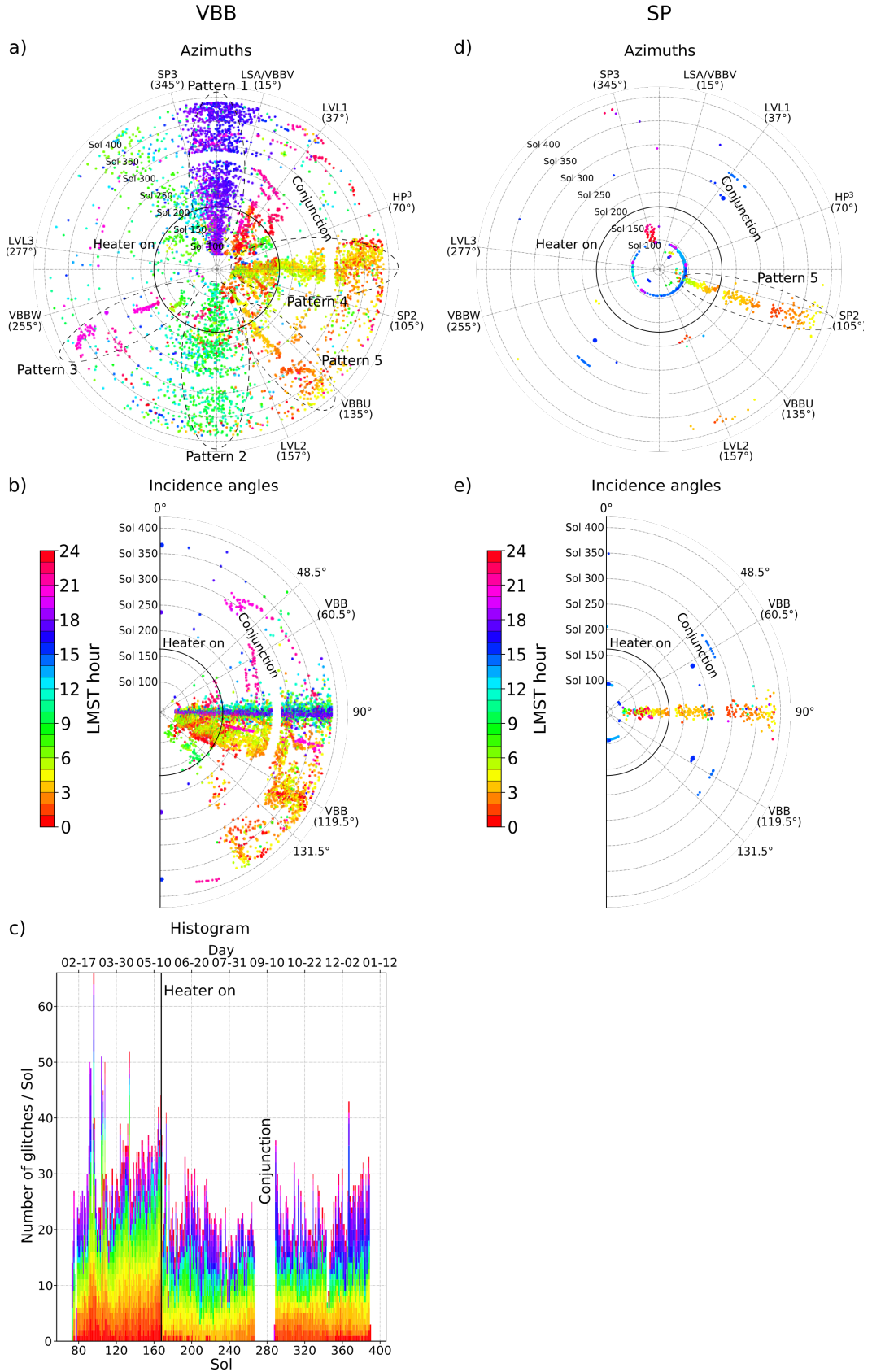


Figure 4. Multi-component glitches of VBB and SP for 2019 as detected by our MPS detection algorithm: a) VBB glitch azimuths. Marked are the five most prominent patterns (Section 3.2 for details), b) VBB glitch incidence angles point only for patterns 1 and 2 into the horizontal plane, c) histogram of a) and b). Note the rate change of night time glitches (red colors) after heater activation (Sol 168), d) SP glitch azimuths. Pattern 5, that also occurs on VBB, is marked. The blue dots mostly refer to false glitch detections caused by HP³-hammering sessions and InSight's robotic arm movements, e) SP glitch incidence angles, demonstrating that multi-component SP glitches occur only among the horizontal SP V and SP W components. Color code is same as in Fig. 3.

Glitches on both VBB and SP

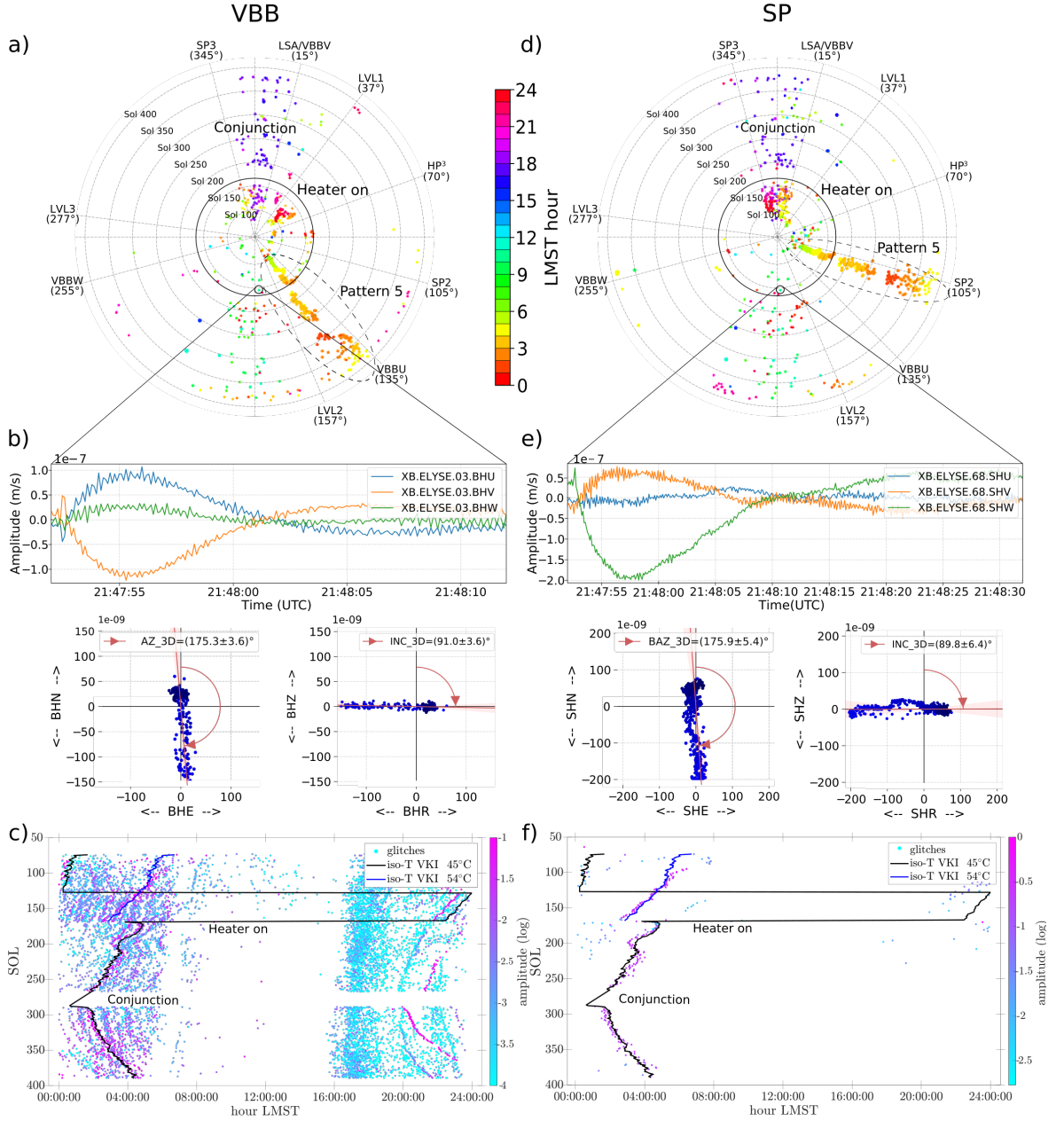


Figure 5. a,d) Glitches in 2019 that occurred simultaneously on VBB and SP. Glitch azimuths agree for patterns 1 and 2 (blue and green dots, compare Fig. 4) but not for pattern 5. Color code is same as in Fig. 3; b,e) example of our polarization analysis of the same glitch for VBB and SP on 2019-07-24T18:50:01 (Sol 234). The azimuths and incidence angles for this glitch are almost identical on VBB and SP. c,f) normalised glitch amplitudes as a function of sols over local mean solar time (LMST; different detection method than in sub-plots a-d). Note how the iso-temperature curve at -54°C (scientific temperature sensor A, channel 03.VKI) matches the glitches corresponding to pattern 5, thus supporting thermal causes for glitches of this pattern. Figure SI2-1 in the Supplementary Information 2 shows Figures 3–5 compiled into one plot.

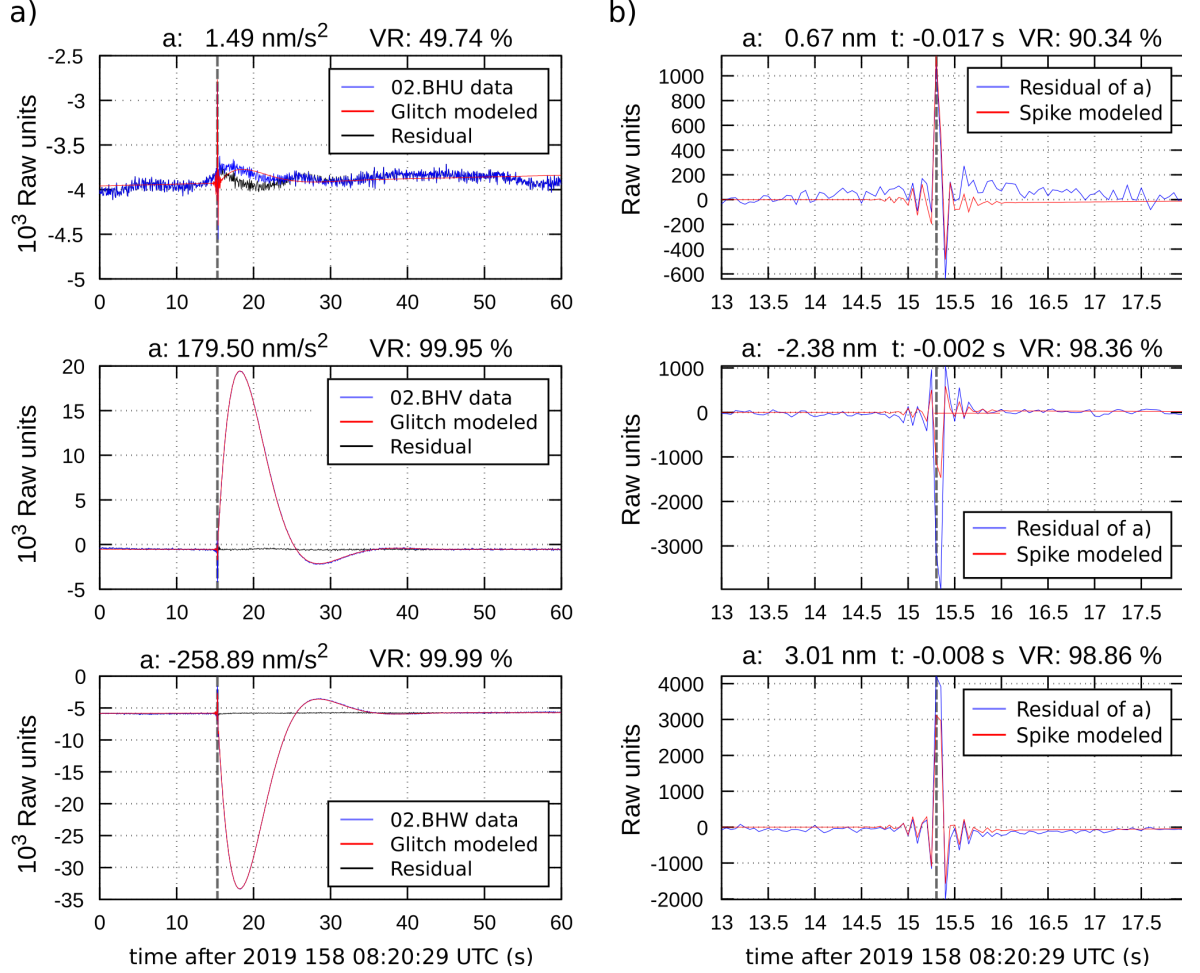


Figure 6. Automated glitch removal for VBB at 20 SPS at work: a) we fitted the glitches in the data (blue lines) with the nominal VBB responses to a step in acceleration (red lines). The deglitched data (black lines) were obtained by subtracting only the scaled version of the synthetic glitches from the original data, i.e. without offset and linear trend parameters. b) high-frequency spikes (red lines) were modeled with the nominal VBB responses to a step in displacement and fitted to the deglitched data of a) (blue lines). Our glitch model allows to fit both the glitch and the glitch spikes very well, even if small mismatches remain. Gray vertical lines: theoretical onsets identical for glitch and spike; a: calculated amplitudes of glitches and spikes; t: time difference between calculated glitch and spike onsets smaller than sampling period (sub-sample fitting); VR: achieved variance reduction.

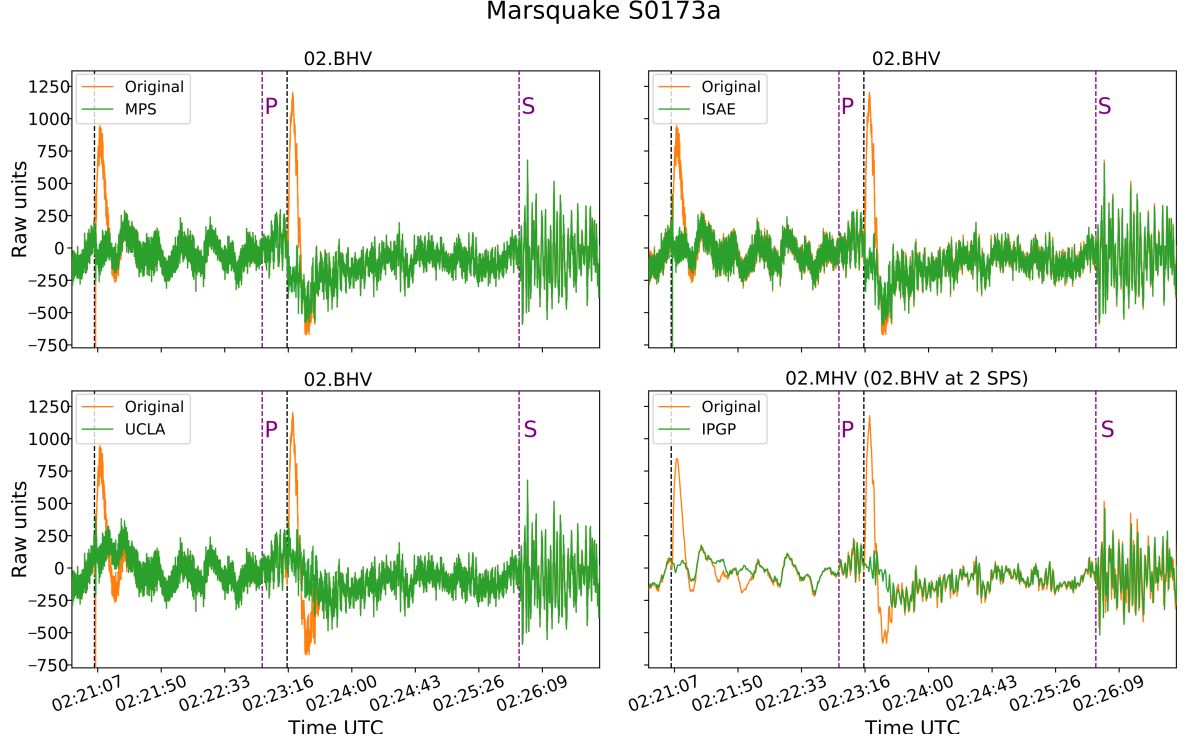


Figure 7. Comparison of VBB raw data at 20 SPS with the corrected data according to our four deglitching methods. The ISAE method does not correct for glitch spikes. The IPGP method only processes 2 SPS data. Linear trends were removed for plotting purposes. The data show marsquake S0173a on 2019-05-23T02:23 (Sol 173), one of the best-quality low frequency events identified to date by the Marsquake Service (MQS, Clinton et al., 2018, catalog: InSight Marsquake Service, 2020). Vertical purple lines; P- and S-phases as identified by MQS; vertical black lines: glitches as annotated by MQS (Section 2.5). Clearly visible right after the P-phase onset is a prominent glitch. In the reconstructed ZNE-data this glitch is almost only present on the horizontal components ($AZ=330^\circ$, $INC=99^\circ$). All four methods remove the glitch sufficiently however not fully equally. We note that this glitch is a prime example of glitches that do not perfectly fit our step-model of acceleration but show a slightly broader response that calls for adaptations in the removal algorithms (Section 4).

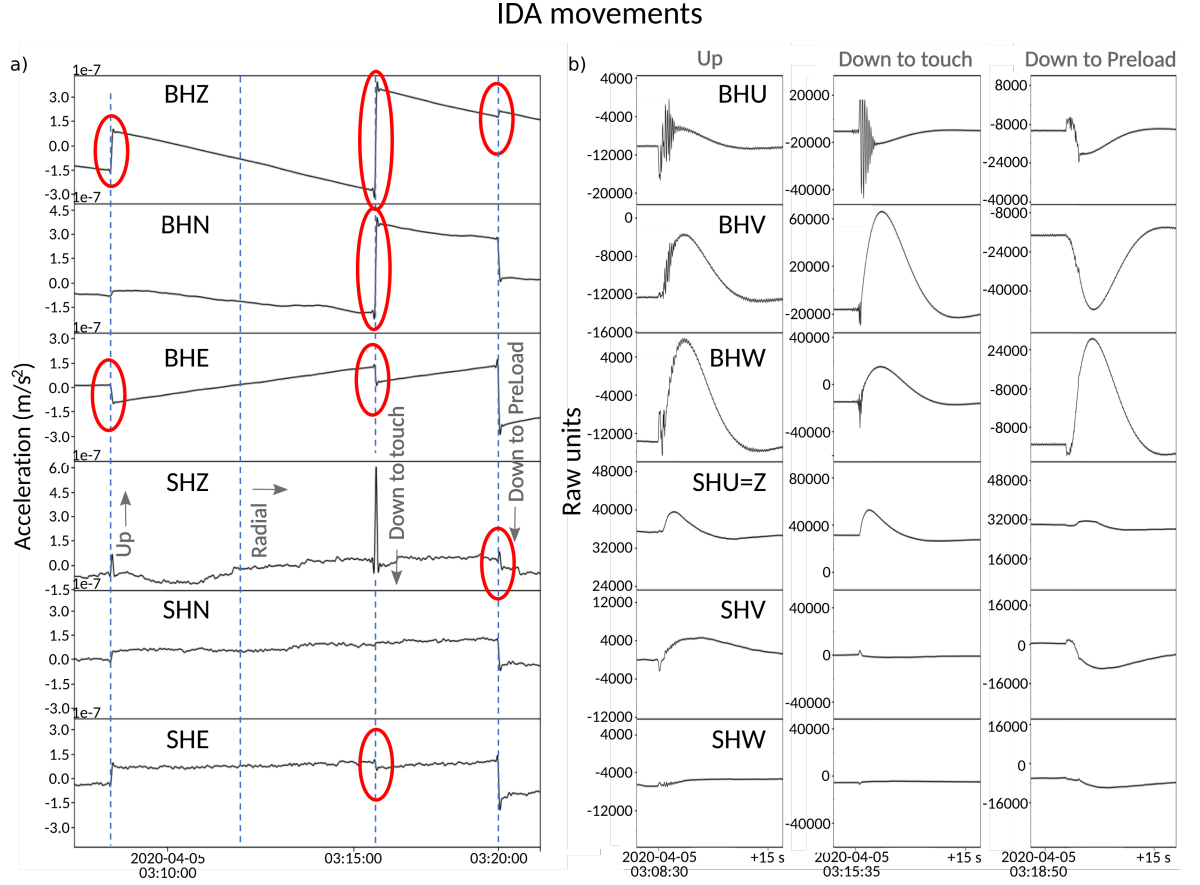


Figure 8. VBB and SP data at 20 SPS during Instrument Deployment Arm (IDA) pushing on the HP³-Mole at around 2020-04-05T03:00:00 (Sol 482). a) The arm started the sequence while pushing down on the Mole (Section 6.2). Likely glitches are identified with red ellipses in the Z, N, E plots on the left for VBB (top, BH?) and SP (bottom, SH?). The time axis spans about 12 minutes. b) 20 second windows of the raw U, V, W components for the three vertical arm movements indicated in a). On many of these glitches, the canonical displacement spike is present.

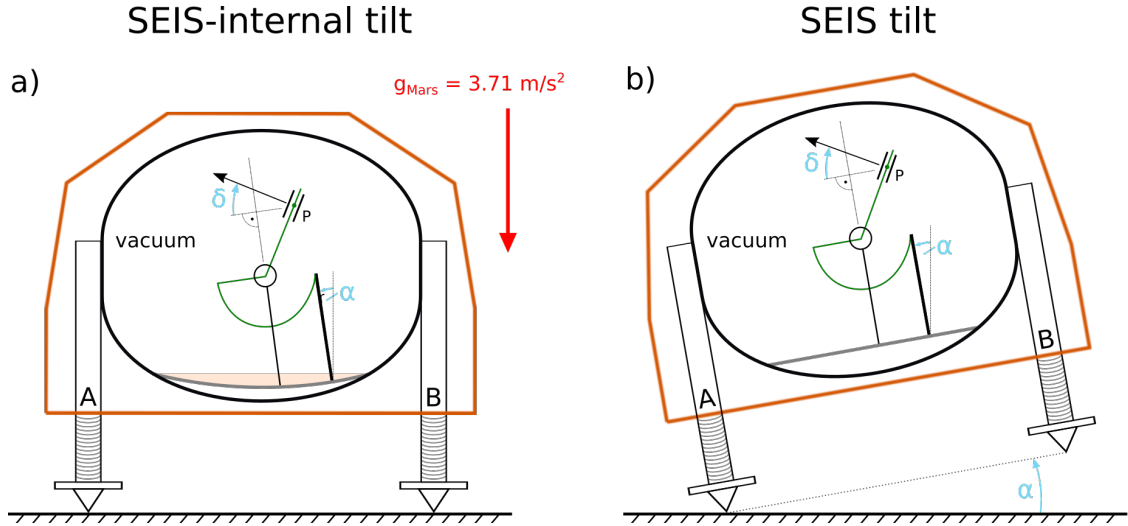


Figure 9. Simplified sketch of a cross-section through the instrument package SEIS showing only one VBB sensor: a) SEIS-internal tilt α caused e.g. by the plate that supports the VBB sensors bending (grey line and orange area). Each VBB sensor (only one illustrated) may see a different tilt, all together yielding a non-zero glitch on the (reconstructed) vertical component ($INC \neq 90^\circ$). We suspect such effects to be the primary reason for thermally-caused multi-component glitches such as shown in patterns 3–5 (Fig. 4). b) SEIS tilt α , corresponding to a true, rigid motion of the whole instrument. Our analysis suggests that the minority of glitches, e.g. patterns 1–2 (Fig. 4), are caused by this scenario. Note that in both cases the VBB sensors may experience a tilt and a displacement (Sections 5 and 6.1). Similar considerations apply for the SP sensors (not shown) that are mounted on the leveling system (SEIS feet) support structure (Fayon et al., 2018). This support structure is connected to the Evacuated Container containing the VBB sensors via three mounting bolts (Sections 3.2 and 6.1). The heaters are mounted to the support structure, too (not shown, Section 3.1). For an accurate illustration of the SEIS sensor assembly, see Lognonné et al. (2019). Green lines: moving pendulum parts; P: proof mass; δ : VBB sensor dip $\sim -30^\circ$. The tilt α is here depicted as 10° for both cases but is in reality in the order of nano-radian.

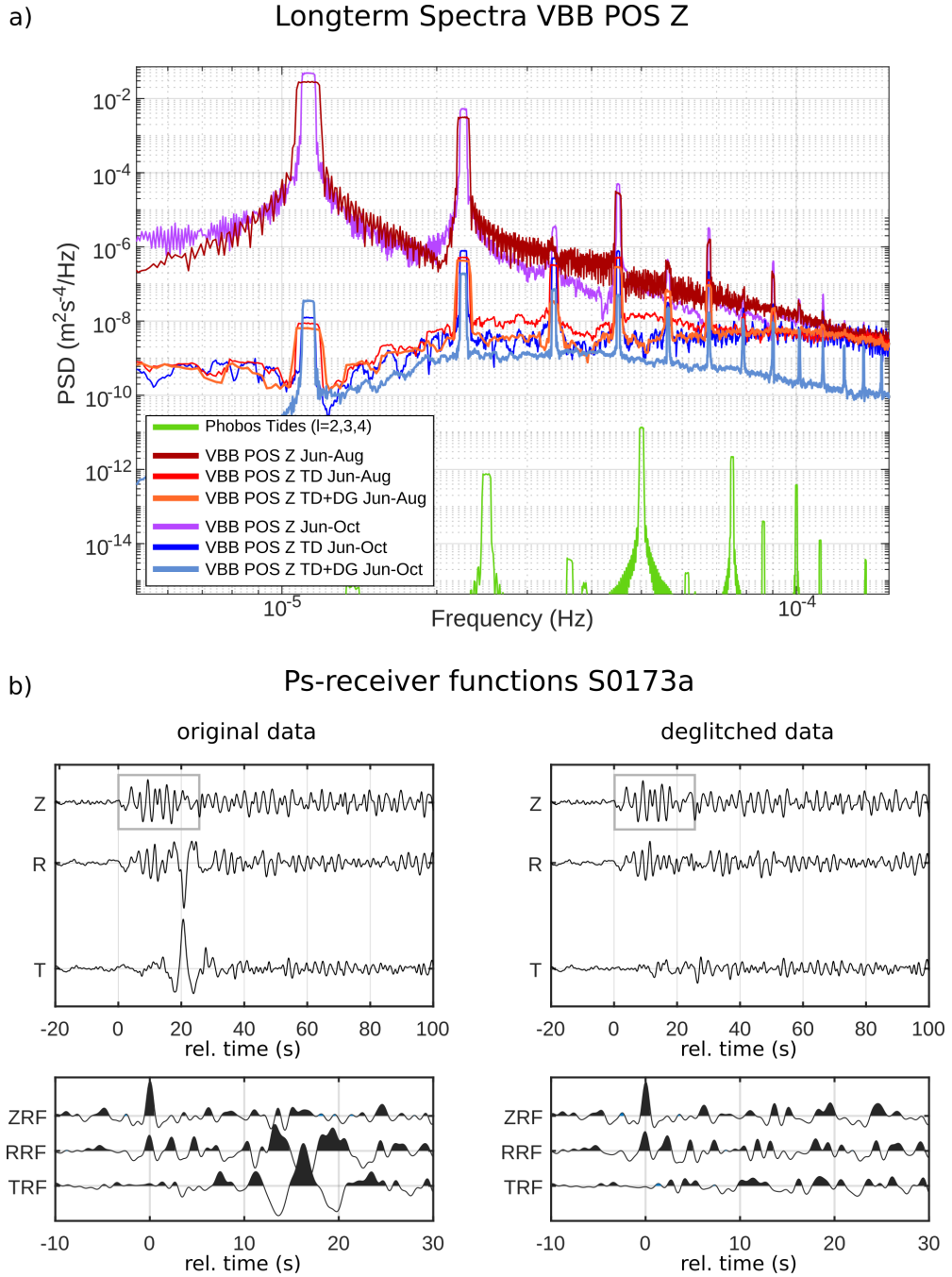


Figure 10. a) Spectra of VBB POS Z-component (see Lognonné et al., 2019) between June–August and June–October, 2019. The data are shown before and after temperature decorrelation (TG), the latter which is needed to hunt for Phobos’ tidal signal in the SEIS data (Pou et al., 2019; Van Hoolst et al., 2003). The deglitched data (DG, ISAE method) after temperature decorrelation show reduced spectral peaks that are caused by the glitches. This is true for both time spans shown, indicating our deglitching is stable over different periods and improves the data quality. b) Comparison of raw data (left) and deglitched data (right, UCLA method) and their Ps-receiver functions for marsquake S0173a. Top panels: waveform data around P-wave onset of S0173a, band-pass filtered between 0.1–0.8 Hz where most of the signal energy is located, and rotated into radial and transverse directions. Note the prominent glitch around 20 s that is still dominating the horizontal components after filtering. Gray boxes: time window used for the deconvolution in Ps-receiver function calculation shown in lower panels: the long-period contamination by the glitch becomes apparent after 8 s on the horizontal components, masks any later arrivals, and also casts doubts on the reliability of earlier phases. For example, an additional arrival near 7.3 s is now clearly visible on the radial component, a phase that is also observed in receiver functions for other marsquakes that are not contaminated by glitches (Lognonné et al., 2020, Supplement IV).

901 Supplementary Information

- 902 • SI1: Lists of glitches detected by our different methods**
- 903 • SI2: Theoretical considerations for apparent glitch polarizations, mathematical description of**
- 904 glitch plus spike origins, and additional figures**

Supplementary Information 2: Detection, analysis and removal of glitches from InSight's seismic data from Mars

1 Theoretical considerations for apparent glitch polarizations

The glitch polarization describes the direction (azimuth and inclination) in which the SEIS sensor assembly (Seismic Experiment for Internal Structure, Lognonné et al., 2019) must be accelerated in order to produce the observed glitch signal on the three sensors U, V and W of the very broadband (VBB) and short-period (SP) seismometer, respectively. Thus, irrespective of analyzing a one-component or a multi-component glitch, we map the non-orthogonal UVW-components (Fig. 1a,c in main paper) into the orthogonal ZNE-components before computing azimuth and inclination of the glitch polarization. For a one-component glitch the non-orthogonality of the VBB components leads to the non-intuitive result in that the glitch azimuth differs slightly from the azimuth of the sensitive direction of the affected sensor while the incidence angle of the same one-component glitch differs by $\sim 12^\circ$ from the sensor's dip angle. We demonstrate this relation in the following.

Projecting the seismometer components from the orthogonal basis vectors Z (positive up), N (positive North), and E (positive East) onto the arbitrarily oriented basis of UVW, we must start with the following linear system of equations:

$$\begin{pmatrix} U \\ V \\ W \end{pmatrix} = \underbrace{\begin{pmatrix} -\sin(\delta_U) & \cos(\delta_U) \cos(\phi_U) & \cos(\delta_U) \sin(\phi_U) \\ -\sin(\delta_V) & \cos(\delta_V) \cos(\phi_V) & \cos(\delta_V) \sin(\phi_V) \\ -\sin(\delta_W) & \cos(\delta_W) \cos(\phi_W) & \cos(\delta_W) \sin(\phi_W) \end{pmatrix}}_A \cdot \begin{pmatrix} Z \\ N \\ E \end{pmatrix}, \quad (1)$$

where A represents the base transformation matrix, δ_i the sensor dip of sensor i , and ϕ_i the sensor azimuth of sensor i clockwise from N. Note that sensor dips are defined as positive downwards from the horizontal plane (e.g. Ahern et al., 2012), which is taken into account in A . To reconstruct data recorded in the UVW-system into the ZNE-system, we must use the inverse operation:

$$\begin{pmatrix} Z \\ N \\ E \end{pmatrix} = A^{-1} \cdot \begin{pmatrix} U \\ V \\ W \end{pmatrix}, \quad (2)$$

with A^{-1} the inverse matrix of A . If we now consider a glitch that occurred only on VBB U with an amplitude $U = 1$ ($V = 0, W = 0$), insert those values into Equation 2, and use the following equations to determine the apparent glitch azimuth defined clock-wise from N, AZ , and apparent glitch incidence INC defined as the angle with respect to the Z-axis, it follows:

$$AZ = \text{atan2}(E, N) = \text{atan2}(A_{31}^{-1}, A_{21}^{-1})$$

$$INC = \text{acos} \left(\frac{\langle [Z, 0, 0]^T, [Z, N, E]^T \rangle}{\| [Z, 0, 0]^T \| \cdot \| [Z, N, E]^T \|} \right) = \text{acos} \left(\frac{A_{11}^{-1}}{\sqrt{(A_{11}^{-1})^2 + (A_{21}^{-1})^2 + (A_{31}^{-1})^2}} \right). \quad (3)$$

We can calculate the inverse matrix elements $(A^{-1})_{j1}$ with the known VBB sensor azimuths $\phi_U = 135.1^\circ$, $\phi_V = 15.0^\circ$ and $\phi_W = 255.0^\circ$, and VBB sensor dips $\delta_U = -29.7^\circ$, $\delta_V = -29.2^\circ$ and $\delta_W = -29.4^\circ$. One finds:

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$$\begin{aligned}
AZ &= 134.6^\circ \neq 135.1^\circ = \phi_U \\
INC &= 48.5^\circ \neq 60.3^\circ = 90.0^\circ + \delta_U.
\end{aligned}
\tag{4}$$

Thus, the apparent azimuth and incidence angles of a one-component VBB glitch will *not* point in the direction of the sensitive direction of the affected VBB sensor. Instead, the polarization vector is parallel to the vector cross-product of the remaining two components that do not show the glitch. Due to the similar arrangement of all VBB's sensors (see Fig. 1a in the main paper), the case demonstrated for VBB U holds true for VBB V and VBB W, too. Therefore for all VBB components, a one-component glitch polarization analysis will deliver azimuth angles (almost) parallel to the sensor azimuths and hence be intuitive, whilst incidence angles will be $INC \sim 48^\circ$ (or 132°) as opposed to the sensor incidences of $90.0^\circ + \delta_i \approx 60^\circ$ (or 120°). For multi-component VBB glitches similar considerations disclose the calculated azimuths will also be intuitive, however, for a two-component glitch the incidence must be $INC \simeq 30.0^\circ$ – 150° (within a plane orthogonal to the third component), whilst for a three-component glitch the incidence can cover the whole parameter space of $INC = 0^\circ$ – 180° . It follows immediately that any VBB glitch for which we observe an $INC < 30^\circ$ or $INC > 150^\circ$ must, necessarily, involve all three VBB components.

Doing the same exercise for SP, with azimuths of $\phi_U = 285.0^\circ$, $\phi_V = 105.2^\circ$ and $\phi_W = 345.3^\circ$, and dips of $\delta_U = -89.9^\circ$, $\delta_V = 0.0^\circ$ and $\delta_W = 0.0^\circ$ (Fig. 1c in main paper), one finds that for SP U (Z) the azimuth and incidence angles will follow one's intuition closely and be 0° and 0° , respectively. For the horizontal components SP V and SP W the case is different: a SP V glitch will reveal an incidence angle of $INC = 89.9^\circ$ – 90.1° as expected, but an azimuth of $AZ \sim 075^\circ/255^\circ$, which is not intuitive given its sensor azimuth of $\phi_V = 105.2^\circ$. Similarly for SP W, the incidence angle will be $INC = 89.9^\circ$ – 90.1° but the azimuth $AZ \sim 015^\circ/195^\circ$, as opposed to the sensor azimuth of $\phi_W = 345.2^\circ$. A direct consequence is that any SP glitch pointing parallel to the SP V or SP W sensor azimuths must be in fact a multi-component SP glitch. For multi-component SP glitches, we did not detect any glitches that occur on the vertical SP U component in combination with either one or two of the horizontal components SP V and SP W. That is, the only multi-component SP glitches are two-component glitches on SP V and SP W. Multi-component SP glitches are therefore always oriented in the horizontal plane.

The message from these theoretical considerations is that our glitch polarization analysis will deliver azimuths and incidence angles that correctly account for the non-orthogonality of VBB and SP; the vectors defined by these angles point into the only physically possible directions for a given one-, two- or three-component glitch, assuming a rigid motion of SEIS. On the other hand, for the interpretations of these angles, it must be born in mind that VBB incidence angles may carry counter-intuitive information whilst SP azimuth angles for one-component glitches will not align with the respective sensor azimuths but diverge by $\sim 30^\circ$.

At this stage we also note that whilst the poles and zeros of the VBB and SP seismometer responses are well determined, the same does not apply fully for the generator constants (gains). In the worst case they may differ up to 10% from the absolute values known by pre-mission tests. To convince ourselves of the correctness of determined glitch azimuths and incidences with respect to these constants we conducted a test: we took the raw data of one- and multi-component glitches of different amplitudes and divided the respective components by their gains that we allowed to vary each by up to $\pm 10\%$. For each permutation, we then rotated into the ZNE-system and performed the polarization analysis. For VBB, we find that glitch azimuths and incidences generally stay within $\pm 5^\circ$ and $\pm 4^\circ$, respectively. For SP, we find that glitch azimuths and incidences generally stay within $\pm 3^\circ$ and $\pm 1^\circ$, respectively, the latter of which is because SP multi-component glitches occur only on the horizontal components. All these values are smaller than the typical errors of polarization measurements and we can therefore assume the resulting glitch patterns to be reliable.

2 Mathematical description of the glitch plus spike origins

Let us consider a general geometry such as depicted in Figure 9 in the main paper where a cross section through a VBB sensor perpendicular to its hinge is graphed. In this figure, the SEIS sensor assembly is rotated around the tip of leg A by a small angle α such that the tip of leg B is raised by $d \cdot \alpha$, with d being the distance between the tips of the legs. The sensitive axis of the VBB accelerometer, denoted with the unit vector $\hat{\sigma}$, is inclined relative to the horizontal by the angle δ which is close to -29° , depending on the VBB sensor.

The force of gravity acting on the proof mass M and which the suspension spring has to counterbalance is:

$$F_o = g \cdot M \cdot \sin(\delta), \quad (5)$$

where $g = 3.71\text{m/s}^2$ is the surface gravity on Mars. After the tilting of SEIS by the angle α , the projection of $\vec{g}$ onto the sensitive axes changes and it follows:

$$F = g \cdot M \cdot \sin(\delta + \alpha). \quad (6)$$

The change in acceleration $\ddot{u}$ produced by the tilting thus is:

$$\frac{F - F_o}{M} = \ddot{u} = g \cdot \alpha \cdot \cos(\delta). \quad (7)$$

Since the rotation axis does not go through the center of gravity P of the proof mass M , the rotation leads also to a displacement of the proof mass. In our case this displacement, y , is a small arc segment of a circle with radius $r = \overline{AP}$ around the tip of leg A: $y = r \cdot \alpha$. The accelerometer only senses the projection of this displacement onto its sensitive direction. If we define the unit vector $\hat{r}$ as:

$$\hat{r} = \frac{\vec{AP}}{|\vec{AP}|}, \quad (8)$$

the sensed displacement then becomes:

$$u = r \cdot \alpha \cdot |\hat{r} \times \hat{\sigma}|. \quad (9)$$

What is the time history of this tilt and the simultaneous displacement? As we shall see, the data can be very well modeled by assuming that the time dependence follows a Heavyside function, that is the tilt and the displacements occur over a time interval much shorter than can be resolved with the given sampling interval. In the analyzed glitches we see little to no indication for a slowly progressing tilt.

Now we have to account for the fact that inertial accelerometers like the VBB and SP seismometers in the SEIS package have a frequency dependent sensitivity to ground motion. This is described by the impulse response $T(t)$. In the time domain the output of the seismometer then becomes the convolution of the input convolved with the impulse response where the input can be the ground displacement, ground velocity or ground acceleration. The seismometer response to a Dirac impulse in displacement, velocity or acceleration are denoted $T_{DIS}(t)$, $T_{VEL}(t)$ and $T_{ACC}(t)$, respectively. They are related by:

$$T_{DIS}(t) = \dot{T}_{VEL}(t) = \ddot{T}_{ACC}(t). \quad (10)$$

The summed output U from the acceleration step due to the tilting at time t_o and the associated displacement step then becomes:

$$U(t) = g\alpha \cos(\delta) \cdot H(t - t_o) * T_{ACC}(t) + r \cdot \alpha \cdot |\hat{r} \times \hat{\sigma}| \cdot H(t - t_o) * T_{DIS}(t). \quad (11)$$

Since the impulse responses due to ground displacement is the second time derivative of the impulse response due to ground accelerations, we anticipate that the acceleration step produces a low-frequency response while the displacement step should be dominated by high frequencies. This is exactly what the Figures 1 and 6 in the main paper show. The step in acceleration leads to the glitch while the step in displacement leads to the high-frequency spike.

When modeling the glitches and their spikes, we obtain the time of the occurrence of the glitch, t_o , as well as the amplitude of acceleration and displacement steps. From the acceleration step, $\ddot{u}$, we can infer the tilt angle α based on Equation (7). What is not possible is to infer the location of the rotation axis given the observed step in displacement, u , and the rotation angle α . Only if we assume that $\hat{r}$ and $\hat{\sigma}$ are at right angles can we infer an effective distance $r_{eff} = u/\alpha$ between rotation axis and the proof mass.

To see if the mathematical simplifications are justified we plug in numbers for the glitch in Figure 6 in the main paper (see also Table 2 in main paper): the step in acceleration is 259 nm/s^2 . The inferred tilt of SEIS which is responsible for that glitch is then:

$$\alpha = \frac{\ddot{u}}{g \cdot \cos(\delta)} = \frac{259 \text{ nm/s}^2}{3.71 \text{ m/s}^2 \cdot \cos(29.3^\circ)} \simeq 80.0 \text{ nrad}. \quad (12)$$

So indeed, these are tiny tilt angles. The displacement obtained from modeling the spike of this glitch is $u = 3 \text{ nm}$. The effective distance r_{eff} of the rotation axis away from the center of gravity of the proof mass is then:

$$r_{eff} = \frac{u}{\alpha} = \frac{3 \text{ nm}}{80 \text{ nrad}} = 3.7 \text{ cm}. \quad (13)$$

In summary, we have shown that an accelerometer which gets rotated around a horizontal axis that does not go through the center of gravity of the proof mass senses two signals: the response to the tilt and the response to the resulting displacement. While the former shows up in the data as the low frequency glitch, the latter leads to the high-frequency spike signal.

3 Additional Figures

In this section, we provide some additional figures we have created while investigating the glitch plus spike phenomenon. We will not put each figure into context but would simply like to refer to their captions for understanding.

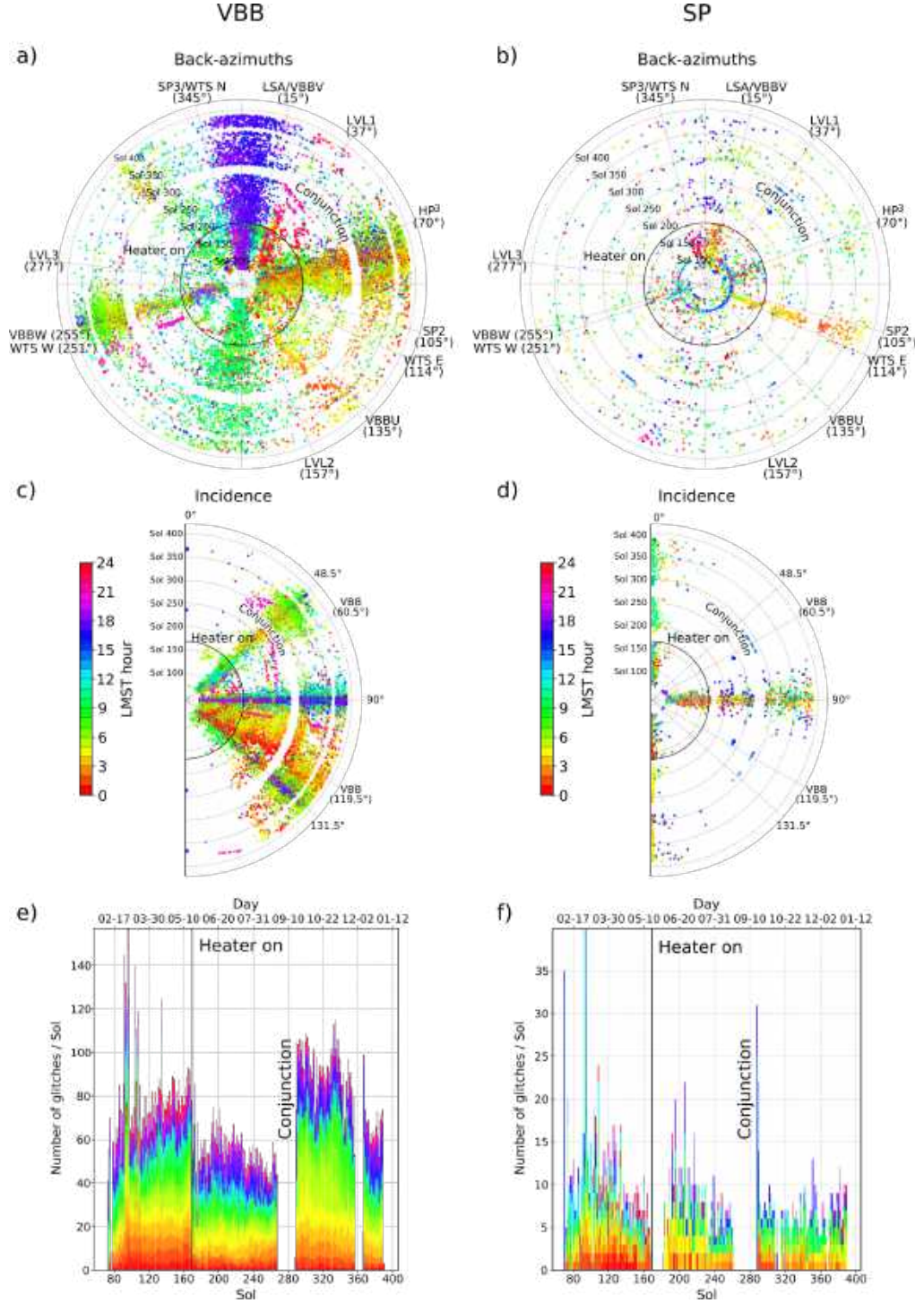


Figure SI2-1: Detected VBB glitches for 2019 (MPS method), corresponding to Figures 2–5 in the main paper. Here, all glitches have been combined into one plot instead of detailing certain aspects in three different plots.

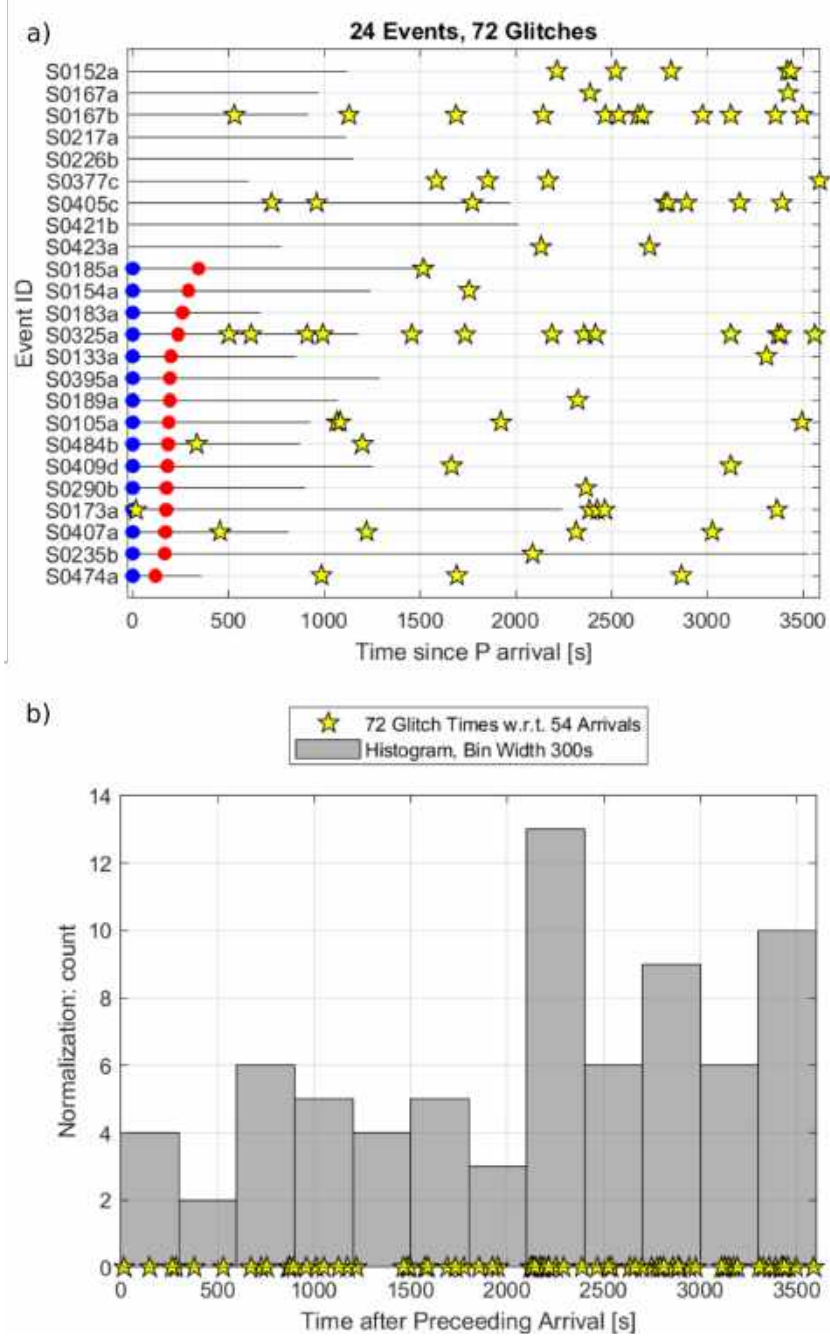


Figure SI2-2: Correlation of detected glitches (MPS method) with marsquake arrivals as identified by the MarsQuakeService (Clinton et al., 2018, for catalogue see: InSight Marsquake Service, 2020). To investigate a possible triggering of glitches by seismic arrivals, we compare detected glitches with low-frequency and broadband events of qualities A–C ('A' is best quality). a) All detected glitches within one hour after the P-arrival, or the beginning of the visible signal where no clear arrival could be identified. Events with arrivals are sorted by S-P time, others by sol. Blue: P arrivals, red: S arrivals, horizontal lines: time windows of visible quake signal, stars: glitches. b) Time between glitch and the last preceding arrival (P or S). Stars: Glitches, Histogram: number of glitches in 5 min time windows. Only 6 of 72 considered glitches occur within 10 min after the last arrival. Given this small number, we do not consider the difference between the first and the second bin as significant, indicating that glitches during seismic events are not occurring significantly more than during periods of no seismic events.

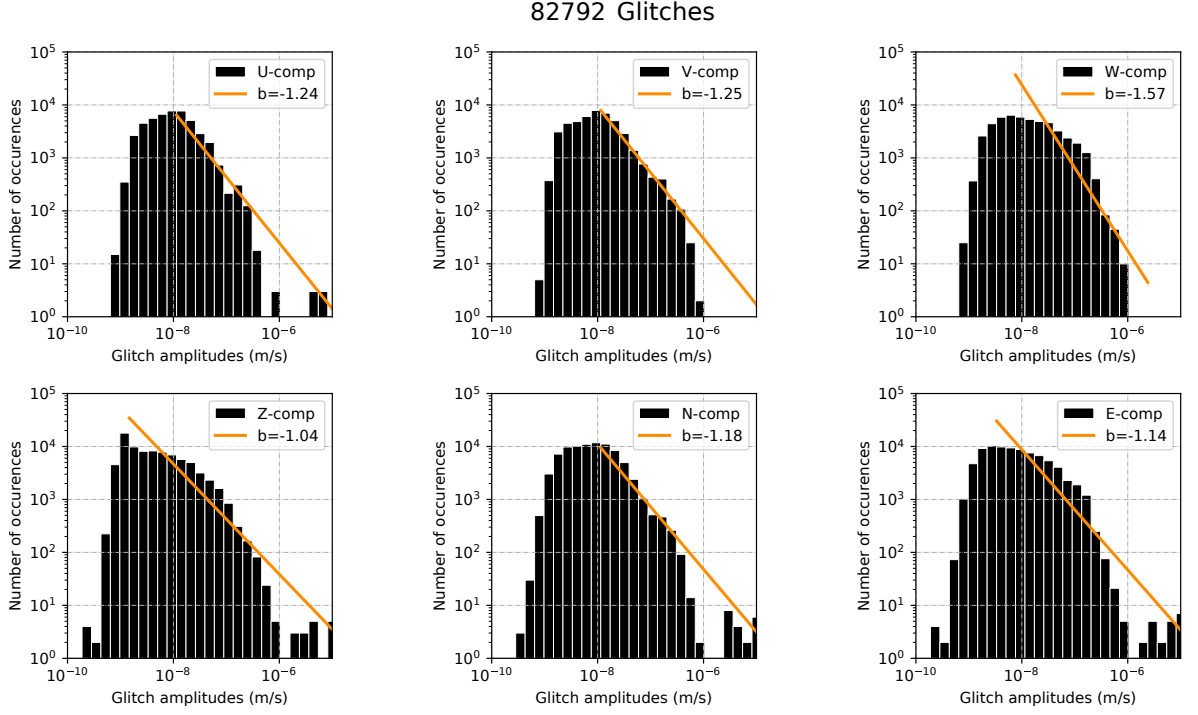


Figure SI2-3: 2019 VBB glitch histograms per component, detected by the MPS method with more sensitive glitch detector settings than utilised in the main paper. We find a seemingly stable Gutenberg-Richter relation with b-values of $\sim 1-1.3$, and roll-off glitch amplitudes of $\sim 1e-8$ m/s (RAW data corrected for gain. The velocity response is flat for periods shorter than 16 seconds). This may indicate an underlying stochastic process behind the glitch production that, perhaps, points once more to thermal causes of glitches.

VBB deglitching

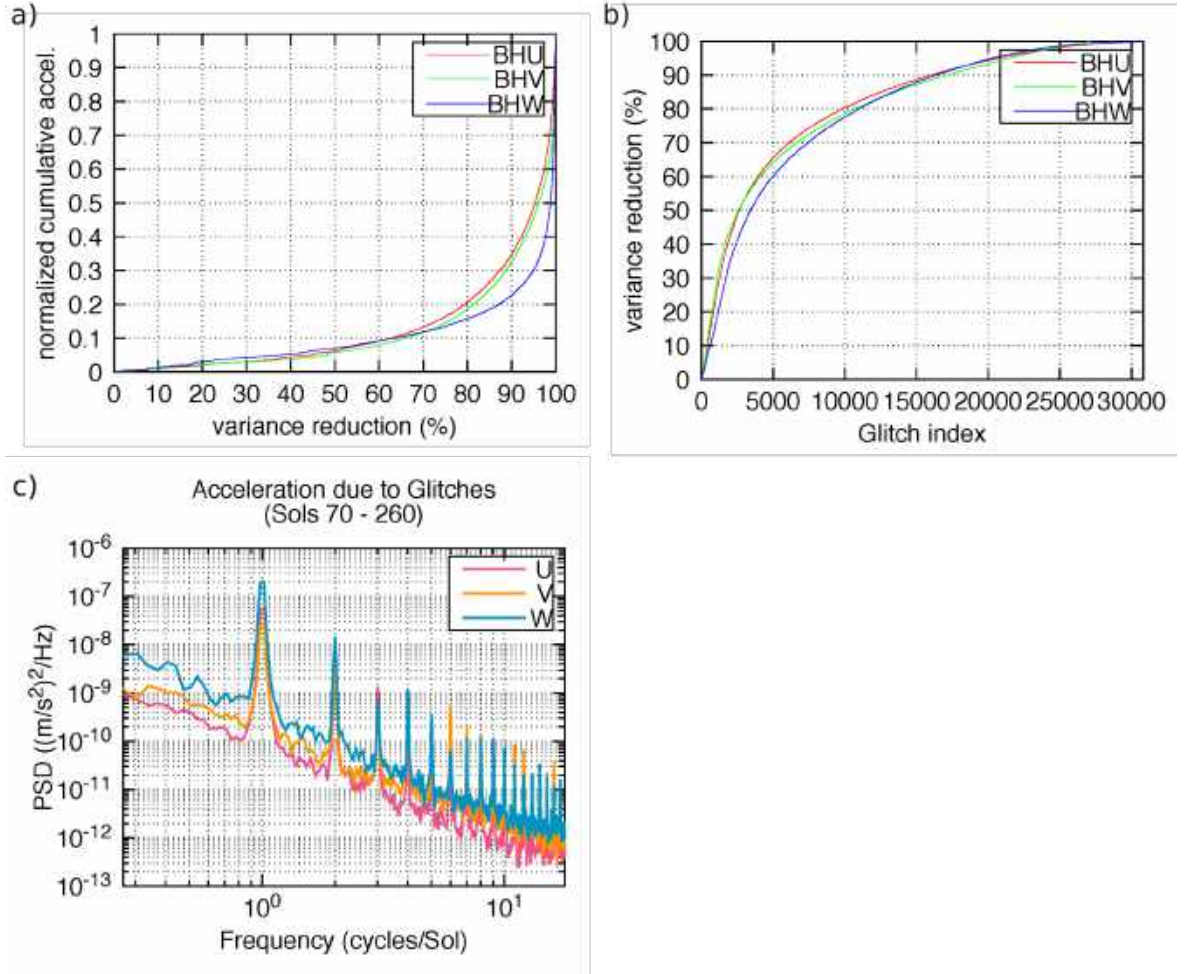


Figure SI2-4: a) Cumulative contribution of glitches to the total acceleration signal. The glitches have been sorted by their variance reduction obtained from the glitch modeling. This panel shows that poorly modeled glitches (variance reduction of less than e.g. 85%) make up only a small fraction of the total acceleration signal: 25%, 25% and 18% for U, V and W respectively. b) Glitches sorted by variance reduction: For the chosen sensitivity of the MPS detector in the main paper and for the time interval Sol 70 through Sol 260, there are 13000 glitches with variance reduction less than 85% and 18000 with variance reduction greater than 85%. Taken together panels (a) and (b) show that the largest contribution in terms of signal amplitude comes from the large and well modeled glitches. In terms of signal power the contribution of the large and well modeled glitches becomes even more dominant. c) Contribution of all modeled glitches to the acceleration background for the three VBB components U, V and W. All glitches for Sols 70 through 260 for which the variance reduction in the glitch modeling stage exceeded 85% are included. A glitch corresponds to a step in acceleration at a particular time. Here we have added up in the time domain 18000 step functions, one for each glitch, with the step size corresponding to the glitch amplitude. The power spectral density of the resulting stair case like, noise free time series has been analyzed. The harmonics at integer multiples of 1 cycle/Sol are a strong indication that the glitches have a thermal cause. This analysis is a complementary method to quantify the contribution of glitches to the VBB analysis presented in figure 10a of the main paper.

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