A single-point method to quantitatively diagnose the magnetotail flapping motion

Zhaojin Rong¹, Chi Zhang¹, Lucy Klinger², Yong Wei³, Chao Shen⁴, and Weixing Wan⁵

¹Key Laboratory of Earth and Planetary Physics, Institute of Geology and Geophysics, Chinese Academy of Sciences
²Beijing International Center for Mathematical Research, Peking University
³Institute of Geology and Geophysics, Chinese Academy of Sciences
⁴Harbin Institute of Technology
⁵Institute of Geology and Geophysics, Chinese Academy of Sciences

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Abstract

Quantitatively estimating magnetotail flapping motion is critical to understanding and characterizing the dynamics of flapping behaviors. Such an estimation could be achieved in principle by the multipoint analysis of spacecraft tetrahedron, e.g. Cluster or MMS mission, but, owing to the inability of single-point measurement to separate the spatial-temporal variation of magnetic field, would be inadequate for a spacecraft. Since single-point missions dominate explorations of planetary magnetotail, we have developed a single-point method based on the magnetic field measurement that quantitatively estimates the parameters of flapping motion, including spatial amplitude, wavelength, and propagation velocity. A comparison with the application of multi-point analysis of Cluster demonstrates that our method can be reasonably be applied to infer the average parameters over a flapping period. Thus, this method could be applied widely to the "big dataset" accumulated by single-point spacecraft missions in order to study magnetotail flapping dynamics.

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4	Z. J. Rong ^{1, 2, 3} , C. Zhang ^{1, 2} , Lucy Klinger ⁴ , Y. Wei ^{1, 2, 3} , C. Shen ⁵ , and W. X. Wan ^{1, 2, 3}									
5	¹ Key Laboratory of Earth and Planetary Physics, Institute of Geology and Geophysics,									
6	Chinese Academy of Sciences, Beijing, China									
7	² College of Earth Science, University of Chinese Academy of Sciences, Beijing, China									
8	³ Beijing National Observatory of Space Environment, Institute of Geology and									
9	Geophysics, Chinese Academy of Sciences, Beijing, China									
10	⁴ Beijing International Center for Mathematical Research, Peking University, China									
11	⁵ Harbin Institute of Technology, Shenzhen, China									
12										
13	Corresponding author: Z. J. Rong (rongzhaojin@mail.iggcas.ac.cn)									
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15	Key Points:									
16 17	• A single-point method based on magnetic field measurement is developed to quantitatively diagnose the magnetotail flapping motion.									
18 19	• An application demonstrates that this method can reasonably infer the average flapping parameters during the whole flapping period.									
20 21	• This method could be applied widely to single-point spacecraft missions in history for studying planetary magnetotail flapping dynamics.									
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24 Abstract

Quantitatively estimating magnetotail flapping motion is critical to understanding and 25 26 characterizing the dynamics of flapping behaviors. Such an estimation could be achieved in principle by the multipoint analysis of spacecraft tetrahedron, e.g. Cluster 27 or MMS mission, but, owing to the inability of single-point measurement to separate 28 the spatial-temporal variation of magnetic field, would be inadequate for a spacecraft. 29 Since single-point missions dominate explorations of planetary magnetotail, we have 30 developed a single-point method based on the magnetic field measurement that 31 32 quantitatively estimates the parameters of flapping motion, including spatial amplitude, wavelength, and propagation velocity. A comparison with the application 33 of multi-point analysis of Cluster demonstrates that our method can be reasonably be 34 35 applied to infer the average parameters over a flapping period. Thus, this method could be applied widely to the "big dataset" accumulated by single-point spacecraft 36 missions in order to study magnetotail flapping dynamics. 37

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39 Plain Language Summary

The oscillation of a magnetotail current sheet, known as the magnetotail flapping motion, plays an important role in dissipating the magnetic field energy stored in a magnetotail. This flapping motion is a fundamental dynamic behavior of a magnetotail, which has been observed widely in the other planets of our solar system, no matter whether the magnetotail is intrinsic (Earth-like) or induced (Venus-like). The comparative study of the planetary magnetotail flapping motion is essential to

understand the flapping mechanism. Unfortunately, single-point measurements of 46 planetary spacecraft are unable to calculate the flapping velocity of tail current sheet 47 directly, which greatly constrains the lucubration of flapping dynamics. To overcome 48 this difficulty, we present a new single-point method, based on the magnetic field 49 measurement and reasonable assumptions, to quantitatively estimate flapping 50 parameters such as spatial amplitude, wavelength, and propagation velocity. A 51 comparison with the multi-point analysis of Cluster tetrahedron shows the validity and 52 reliability of our single-point method as applied to a flapping case of Earth's 53 54 magnetotail. Thus, our method could be broadly applied to the "big dataset" accumulated by single-point spacecraft missions in history in order to study the 55 flapping dynamics of planetary magnetotails. 56

57

58 1. Introduction

The flapping motion of a magnetotail current sheet is a fundamental dynamic phenomenon in the Earth's magnetotail, which refers to the back and forth motion of a current sheet, and is manifested as multiple crossings of a current sheet by a spacecraft within a short time (e.g. Lui et al., 1978; Sergeev et al., 1998; Speiser & Ness, 1967; Toichi & Miyazaki, 1976).

Quantitatively diagnosing the characteristics of the flapping motion is important to understand flapping behavior and the role it plays in magnetotail dynamics. In the past twenty years, based on the multipoint measurements of the Cluster tetrahedron on the Earth's magnetotail, many studies unambiguously revealed that flapping motions,

68	being triggered by some sources around the midnight, are able to propagate
69	azimuthally as kink-like waves toward both flanks with velocities of a few tens of
70	kilometers per second, amplitude 1-3 R_E (Earth radius, 6371 km), and wave length
71	$4 \sim 8 R_E$ (e.g. Zhang, et al., 2002, 2005; Sergeev et al., 2003, 2004; Petrukovich et al.
72	2006; Shen et al., 2008; Rong et al., 2010, 2015a, 2018a; Runov et al., 2005). In
73	addition to the kink-like flapping motion, the magnetotail current sheet sometimes just
74	flaps up and down but does not propagate as waves, as Rong et al. (2015a) reported,
75	this new flapping type is referred to as steady flapping motion. Based on a statistical
76	survey on the two flapping types, Gao et al.(2018) suggested that the up and down
77	motion of steady flapping around the midnight region could induce the kink-like
78	flapping waves that propagate toward both flanks of the magnetotail.

Based on quantitative analysis of kink-like flapping waves, theoretic models proposed different accounts for the flapping mechanism. For example, it might be magnetohydrodynamic ballooning-type waves (Golovchanskaya & Maltsev, 2005); it could be the drift kink mode of current sheet instability (e.g. Karimabadi, et al., 2003a, 2003b; Sitnov et al., 2006; Zelenyi et al., 2009); or it could be interpreted as magnetohydrodynamic waves related to a double-gradient current sheet model (Erkaev et al., 2007).

The magnetotail flapping motions are observed not only in the Earth's magnetotail but also in the magnetotails of other planets, such as Mercury (Zhang et al., 2020), Venus (Rong et al., 2015b), Mars (DiBraccio et al., 2017), and Saturn and Jupiter (Volwerk et al., 2013). To delineate the characteristics of planetary magnetotail 90 flapping motions is beneficial to understand the general mechanism of the flapping 91 motion. Nonetheless, in contrast to the multipoint measurements of the Cluster 92 tetrahedron, the single-point measurements of planetary spacecraft missions are 93 unable to calculate the moving velocity of the flapping current sheet directly. 94 Therefore, to study the flapping motion of a planetary magnetotail, the major 95 challenge is figuring out how to use single-point measurement to discover flapping 96 properties.

Rong et al. (2015a) presented a single-point method based on the magnetic field
measurements to qualitatively diagnose the flapping types and, if a kink-like type, the
propagation direction. In studies of the flapping motion of planetary magnetotail, this
method has been applied successfully to Earth (Wu et al., 2016), Venus (Rong et al.,
2015b), Mars (DiBraccio et al., 2017), and Mercury (Zhang et al., 2020).

As continuation of Rong et al. (2015a), we present here a new method based on the single-point magnetic field measurement to quantitatively estimate the spatial amplitude, wavelength and propagation velocity of the kink-like flapping motion.

105 The paper is organized as follows. In Section 2, we present our method. In Section 106 3, we apply the method to a typical kink-like flapping case in the Earth's magnetotail 107 and compare our results with a multi-point analysis of the Cluster. Finally, we give a 108 summary and discussion in Section 4.

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110

112 **2. Method**

Before studying the flapping current sheet, we consider the undisturbed current sheet first. The normal of the undisturbed current sheet is **N**, pointing northward. The anti-parallel magnetic field lines on the opposite sides of the current sheet are orientated along direction **L**, which points Earthward. Thus, as shown in Figure 1a, local coordinate (**L**, **M**, **N**) can be set up to describe the field structure of an undisturbed current sheet, where $\mathbf{M} = \mathbf{N} \times \mathbf{L}$. The local coordinate system is a prerequisite to our method.

Previous studies demonstrate that the magnetic field over the Earth magnetotail current sheet can be well approximated by a 1-D Harris sheet model (Harris, 1962; Thompson et al., 2005; Zhang et al., 2006). The approximation also makes sense in the Venusian magnetotail (Rong et al., 2014) and the Mercury magnetotail (Rong et al., 2018b). Therefore, in local coordinate, we assume that the spatial profile of the magnetic field over the undisturbed magnetotail current sheet can be represented by a Harris sheet model, that is,

127
$$B_L = B_0 \tanh\left(\frac{z_N - z_0}{L_0}\right)$$
(1)

128 , where, B_0 is the lobe field, z_0 is the location of the sheet center, z_N is the normal 129 distance to the sheet center, and L_0 is the characteristic scale of the sheet.



Figure 1. The sketched diagrams show, from top to bottom: (a) the configuration of 132 undisturbed current sheet in the local coordinate (L, M, N); (b) the kink-like flapping 133 current sheet; and (c) the recorded oscillation of B_L component by spacecraft during 134 the flapping period. The current sheet is represented by a thick black line. The 135 kink-like flapping current sheet is assumed to propagate as a wave towards the 136 direction of -M with velocity V_{f} , spatial amplitude A, and wavelength λ . The 137 horizontal blue line represents the relative trajectory of the spacecraft crossing the 138 waves towards the direction of **M**. The normal of the crossed current sheet, **n**, is tilted 139 from the undisturbed normal N by angle α . The recorded B_L reaches the trough B_1 at 140 time t_1 , and crest B_2 at time t_2 . 141

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As seen in Figure 1b and Figure 1c, due to the up-down motion of the current sheet during the flapping period, the spacecraft would record a signal of the oscillated magnetic field. The temporal variation of the oscillated magnetic field can be written

146 as

147
$$\frac{dB_L}{dt} = \frac{B_0}{L_0} \left[1 - \tanh\left(\frac{z_N - z_0}{L_0}\right)^2 \right] \frac{dz_N}{dt}$$
(2)

- 148 Considering $\frac{dz_N}{dt} > 0$, when the current sheet is moving downward and vice versa,
- 149 the up-down moving velocity of current sheet, V_N , can be derived as

150
$$V_N = -\frac{dz_N}{dt} = -\frac{dB_L}{dt} \frac{L_0}{B_0} \left[1 - \left(\frac{B_L}{B_0}\right)^2 \right]^{-1}$$
 (3)

151 Note that both L_0 and B_0 are assumed constant during the flapping period.

152 Accordingly, the spatial amplitude of the flapping current sheet can be estimated as

$$A = \frac{1}{2} \int_{t_2}^{t_1} V_N dt = -\frac{1}{2} \int_{t_2}^{t_1} \frac{dB_L}{dt} \frac{L_0}{B_0} \left[1 - \left(\frac{B_L}{B_0}\right)^2 \right]^{-1} dt = \frac{-L_0 B_0}{2} \int_{B_2}^{B_1} \frac{dB_L}{B_0^2 - B_L^2}$$

$$= \frac{L_0}{2} \left[a \tanh\left(\frac{B_2}{B_0}\right) - a \tanh\left(\frac{B_1}{B_0}\right) \right]$$
(4)

154 , where t_1 and t_2 are the time when the spacecraft recorded the trough and crest of 155 oscillated B_L during a half-period, while B_1 and B_2 are the corresponding values of B_{L} , 156 when B_L reaches the trough and crest respectively.

As shown in Figure 1b, if the flapping motion can propagate azimuthally as kink-like waves towards -**M**, and the local normal of the crossed current sheet can be evaluated as **n**, then the half wavelength can be roughly estimated as

160
$$\frac{\lambda}{2} = \frac{2A}{\tan \alpha}$$
(5)

161 , where
$$\alpha$$
, the tilt angle of the local current sheet, is the angle between **n** and **N**.

162 Accordingly, the propagation speed of the kink-like waves can be roughly 163 estimated as

164
$$V_f = \frac{\lambda}{2(t_2 - t_1)} = \frac{2A}{(t_2 - t_1)\tan\alpha}$$
 (6)

166 **3. Application and Test**

To test the validity of our method, we apply it to a magnetotail flapping case observed by the Cluster tetrahedron, so that a comparison with multi-point timing analysis can be made.

In this case, magnetic field data points with 4 s resolution (Balogh et al., 2001) are used in geocentric solar magnetospheric (GSM) coordinate, where +x points toward Sunward, +z points nearly northward and in the plane is constituted by an x-axis and a dipole axis, and +y completes the right-handed system.



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Figure 2. The measured magnetic field by the four spacecraft of Cluster in GSM on 5
August 2004. The interval when the spacecraft experienced a flapping period is
shaded. The magenta lines represent the moving average of magnetic field recorded
by C3 with span 2 hours. The locations of C3 in GSM are listed in the bottom.

179

180 This case occurred on 5 August 2004, during the period of 13:50–16:00, when the 181 Cluster tetrahedron is averagely located at (x = 16.0, y = 9.2, z = 2.7) R_E (R_E = 6371 182 km, Earth radius). The typical scale of the Cluster tetrahedron is about 1200 km at this 183 time. As shown in Figure 1, each crossing of the tail current sheet, when the x 184 component of magnetic field, B_x , reverses its sign, is marked by a vertical dashed line. 185 Using the multi-point timing analysis of Cluster, Zhang et al. (2005) previously found 186 that the multiple crossings of current sheet are induced by the kink-like flapping 187 motions of the tail current sheet, travelling azimuthally dawnwards with a speed of 188 tens of km/s.

189

190 **3.1 Local Coordinate of an undisturbed current sheet**

191 It's worthwhile to note that, due to the tail flaring effect of field lines (Fairfield, 192 1979), the B_y component is positively proportional to the B_x component at the dawn 193 side (Y<0), and it's no surprise to find in Figure 2 that the B_y component oscillates 194 with the same phase as the B_x component. The flaring effect is prominently close to 195 both flanks but negligible around midnight. Thus, to remove the tail flaring effect, we 196 have to set up local coordinate first for an undisturbed tail current sheet.

To set up local coordinate that relies on single-point measurement, knowledge of minimum variance analysis on magnetic field (MVAB) is necessarily required (Sonnerup and Scheible, 1998). By performing MVAB on the sampled magnetic field data points over the crossing of a discontinuity, we can obtain the characteristic directions of the varied magnetic field by solving the magnetic variance matrix $M_{\mu\nu} = \langle B_{\mu}B_{\nu} \rangle - \langle B_{\mu} \rangle \langle B_{\nu} \rangle$, where the subscripts μ and ν denote the x, y, and z components in a given Cartesian coordinate system, e.g. the GSM coordinate. The matrix $M_{\mu\nu}$ has three eigenvalues: λ_1 , λ_2 , and λ_3 ($\lambda_1 \ge \lambda_2 \ge \lambda_3 \ge 0$), and the corresponding eigenvectors **l**, **m**, and **n**. The three eigenvectors are orthogonal and represent the directions of maximum, intermediate, and minimum variance of magnetic field. Taking the magnetotail current sheet as an example, **l** is basically along the local lobe field; **n** is the local normal of the current sheet, and **m**= **n**×**l** is tangentially to the surface of the current sheet.

With MVAB, there are two ways to construct the local coordinate of a tail current 210 sheet. (1) We could perform MVAB for each crossing of the current sheet, and take 211 212 the average of I for all crossings as L. M is perpendicular to L and the +Z-axis of GSM, i.e. $M = L \times Z/|L \times Z|$, and $N = L \times M$. This has been adopted in some previous 213 studies (Rong et al., 2015a, 2015b; DiBraccio et al., 2017; Zhang et al., 2020). (2) We 214 215 could smooth out the fluctuated magnetic field, and perform MVAB on the smoothed field data. In this case, the smoothed field data could be seen as the field of the 216 undisturbed current sheet, and the yielded l, m, and n by MVAB, seen as L, M, and N 217 218 respectively, could constitute the local coordinate.

We arbitrarily use single-point field measurements of C3 to trial both of these ways. We find that (1) can well remove the flaring effect during the period of crossing current sheet, but the minor positive correlation between B_L and B_M in the local coordinate system is still present when $|B_L|>20$ nT (not shown here). The reason, we found, is caused by the variable configurations of tail field lines, which, as shown in Figure 3, can be indicated by the variable proportion between B_x and B_y during the whole period 08:00-22:00.



226 227

Figure 3. The variation of B_x *against* B_y *during the period* 08:00-22:00.

Thus, we could alternatively adopt (2) to set up the local coordinate. Using (2), we 229 230 have to smooth the field data first. For a flapping period of 20~50 min, we adopt the technique of a moving average with a span of 2 hours to smooth the oscillation of the 231 magnetic field recorded by C3. The moving averaged magnetic field could be seen as 232 233 the undisturbed magnetic field of the current sheet (see the magenta lines in Figure 1). With the smoothed field data, we performed MVAB on nested sets of different data 234 interval centered at the current sheet's center ($B_L = 0$). We chose the interval when the 235 236 output eigenvectors are insensitive to interval increases, and finally obtained three orthogonal eigenvectors, i.e. L=(0.94, 0.33, -0.04), M=(0.33, -0.94, -0.02), and N=237 (0.05, 0.00, 1.00), where N=L×M. The ratio of eigenvalues with λ_1 : λ_2 : λ_3 =86: 3: 1 238 indicates that the yielded eigenvectors are well distinguished. 239

240 **3.2 Fit with the Harris sheet**

Given its local coordinate system (L, M, N) and a smoothed magnetic field (see Figure 4a), we fit the undisturbed current sheet to the Harris sheet model

243 $B_L = B_0 \tanh\left(\frac{z_N - z_0}{L_0}\right)$. The fitted parameters, with 95% confidence bounds, are B_0 = 244 32.28±0.28 nT, L_0 = 3.51±0.06 R_E, and z_0 = 7343±87 km. The coefficient of the 245 Adjusted R-square for the fit is 0.97, which indicates the fitting is quite good (the 246 closer one is, the better the fit). Figure 4b shows the spatial distribution of the fitted 247 B_L component.



248

Figure 4. (a) The time series of smoothed magnetic field in the local coordinate of current sheet. (b) The variation of the smoothed B_L component against the normal distance to current sheet center; the black line is the Harris fitting of smoothed B_L component.

253

3.3 The normal of the local flapping current sheet

255 Knowledge of the normal of the local current sheet is essential for estimating

256 flapping parameters.

257 Because the significant time lag of crossing the current sheet in the Cluster

- tetrahedron favors multi-point timing analysis (Harvey, 1998), as shown in Figure 5a,
- 259 we consider six crossings of the current sheet that occurred during the period
- 13:50-15:50, so that a comparison with that timing analysis can be made.



Figure 5. Cluster observations of a flapping tail CS event on 05 August 2004 in GSM
coordinate. Panel a shows the recorded B_x component by the four spacecrafts of
Cluster. Panel b shows the recorded magnetic field, including its three components in
GSM and the field strength, by C3. The dashed lines mark the crossings of tail
current sheet.

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Timing analysis can derive the normal direction and the associated normal velocity, V_n , of a local current sheet if the sheet is seen as a moving plane. These directions and velocities are tabulated in Table 1. It should be noted that all derived normal directions are dawnwards (n_y<0), which means that the flapping current sheets are travelling dawnward as kink-like waves.

273 Meanwhile, by employing the MVAB technique (introduced in subsection 3.1), we 274 can also infer the normal orientations that rely on the single-point measurement of C3. 275 The yielded normal orientations, \mathbf{n} , for the six crossings in GSM and in local 276 coordinate, are tabulated respectively in Table 1. However, in contrast to the timing 277 normal, both \mathbf{n} and $-\mathbf{n}$ are valid eigenvectors of MVAB. Thus, one cannot judge the 278 type of flapping or the propagation direction (in the case of kink-like flapping)

279	directly according to the normal MVAB.
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280	Given the MVAB normal in local coordinate, Rong et al. (2015a) constructed a
281	parameter k, defined as $k = sig(n_M \times n_N) \times sig(\Delta B_L)$, to diagnose the flapping types and
282	ascertain the propagation velocity of flapping waves, where n_{M} and n_{N} are the M and
283	N components of n , respectively, and $\Delta B_L > 0$, if the polarity of B_L varies from
284	negative to positive and vice versa. Rong et al. (2015) notes that if the flapping
285	motion is propagating toward M (+ M) as kink-like waves, the yielded value of k at
286	each crossing of the current sheet would be $+1(-1)$ always; if the flapping motion is
287	just steady flapping, the sequence of k would change its sign alternately. Therefore,
288	the sequence of k can be used to indicate the flapping type and, if the type is kink-like
289	flapping, its propagation direction.

291 Table1. Timing and MVAB Analysis on Current Sheet Crossings

		Timing results					
No.	Time ^a	$\Delta t^{b}(s)$	λ_2/λ_3^c	Normal in GSM	Normal in LC ^d	Normal in GSM	V _n ^e (km/s)
1	13:57:47	80	63	-0.64, 0.72, 0.28	-0.37, -0.89, 0.25	0.48, -0.63, -0.61	18
2	14:07:27	56	215	0.64, -0.76, 0.13	0.35, 0.92, 0.16	0.63, -0.69, 0.35	38
3	14:14:55	160	14	-0.46, 0.74, 0.50	-0.21,- 0.86, 0.47	0.19, -0.34, -0.92	37
4	14:32:35	48	21	0.40,-0.56, 0.73	0.16, 0.65, 0.75	0.50, -0.81, 0.32	19
5	15:00:59	96	2	-0.24,0.36, 0.90	-0.14, -0.44, 0.89	0.20, -0.53, -0.82	36
6	15:28:22	48	17	0.44, -0.79, 0.42	0.13, 0.89, 0.44	0.27, -0.71, 0.66	10

^{*a*} The time when C3 crosses the center of the current sheet ($B_L=0$);

^b The length of the used time interval for MVAB, which is centered at the CS center;

- ^c The ratio of λ_2/λ_3 ; the larger the ratio, the more distinguished the normal **n** becomes from the intermediate direction **m**;
- ^d The MVAB normal of C3 in local coordinate (LC);
- ^e *The normal velocity of the current sheet inferred by timing analysis.*

- According to the derived MVAB normal in local coordinate (see Table 1), we find that k, at each crossing, keeps +1 always, which indicates that the type of flapping motions observed by C3 are kink-like and that these kink-like waves are propagating towards $-\mathbf{M}$ or dawnward. Evidently, diagnosing flapping motion with the single-point technique of Rong et al. (2015a) is consistent with the results of multiple-point timing analysis.
- 305 Quantitatively estimating flapping parameters is the main task of this study. We 306 show specific procedures for doing so in the following section.
- **307 3.4 The parameters of flapping motion**
- 308 Having established local coordinate and fitted an undisturbed current sheet to a
- Harris sheet, we are now in a position to study flapping parameters using the methoddescribed in Section 2.
- 311 To estimate the amplitude of flapping motion via Eq. (4), we have to identify time
- 312 t_1 and t_2 , when the spacecraft recorded the trough and crest of oscillated B_L during a
- half-period, and obtain the corresponding values of B_L , B_l , and B_2 .



Figure 6. The oscillated magnetic field by C3 in local coordinate. The half-period for each crossing of the current sheet is shaded.



The flapping magnetic field in Figure 6 shows, as expected, that B_L becomes the 318 major field component in the local coordinate system. We have identified the trough 319 and crest of B_L for each crossing, and shaded the corresponding interval of half-period. 320 Note that, due to the irregular waveform of oscillated $B_{\rm L}$, the identified half-periods 321 for the neighboring crossing of the current sheet are not adjacent necessarily. Given 322 the identified interval of half-period, and the value of B_L , B_1 and B_2 at trough and crest 323 respectively for each current sheet crossing, we estimate the spatial amplitude using 324 325 Eq. (4) and tabulate the specific results in Table 2. The estimated results demonstrate that the spatial amplitude during this period is about $1\sim 2 R_{\rm E}$, which is consistent with 326 the typical amplitude reported in previous studies (e.g. Sergeev et al., 2003; 327 Petrukovich et al., 2006; Rong et al., 2018a). 328

Because the estimated MVAB normal, **n**, may not be strictly coplanar with **M** and N as depicted in Figure 1, one has only to consider the projected component of **n** in the MN plane to infer the tilt angle, α , for each crossing of the current sheet. The estimated title angles, in terms of the MVAB and timing normals respectively, are 17/25 tabulated in Table 2.

334	With the derived tilt angle of the MVAB normal, the wavelength and propagation
335	speed for each half-period can be estimated via Eq. (4) and Eq. (5), respectively. As
336	listed in Table 2, we find the estimated wavelength is about $1\sim 3 R_E$ at crossings 1-3,
337	but can significantly increase up to ~9 R_E at crossing 4, and ~17 R_E at crossing 5, then
338	down to 2.5 $R_{\rm E}$ at crossing 6. The estimated propagation speed, $V_{f, MVAB}$, in tens of km/s,
339	is varied from 13 to 60 km/s, which is comparable to the propagation speed estimated
340	by timing analysis (see " V_f " in Table 2).

341

Table 2. The estimated flapping parameters for each crossing of current sheet

No.	Interval ^a	Half-period (s)	B ₁ (nT)	B ₂ (nT)	α_1^{b} (°)	α_2^{b} (°)	A (R _E)	λ (R _E)	$V_{f, MVAB}^{c}$ (km/s)	V _{f, timing} ^c (km/s)	$V_{f}^{' \ d}$
											(km/s)
1	13:55:43-13:59:19	216	-14.9	13.7	77	53	1.7	1.6	24	75	23
2	14:04:51-14:09:19	268	-12.2	14.0	80	66	1.5	1.1	13	32	42
3	14:09:19-14:17:51	512	-12.2	10.4	62	24	1.3	2.7	17	73	92
4	14:28:39-14:36:19	460	-20.9	9.9	41	70	1.9	8.7	60	20	20
5	14:49:51-15:06:15	984	-21.1	15.4	28	36	2.3	17.1	55	41	61
6	15:27:07-15:33:43	396	-18	3.0	64	48	1.3	2.5	20	37	13

^a The identified interval of half-period for each crossing of the current sheet.

344 ^b The tilt angle of current sheet. α_1 (α_2) is the angle between the MVAB normal (timing 345 normal) and N.

^c V_{f, MVAB} (V_{f, timing}) is the propagation speed estimated via Eq.(6) using the MVAB normal
(timing normal).

348 *d* The propagation speed from timing analysis, it is estimated as $V_f = V_n / \sin \alpha_2$.

350 4. Summary and discussion

In this paper, we present a single-point method, based on magnetic field 351 measurements made by spacecrafts, to quantitatively estimate flapping motion 352 parameters of a magnetotail current sheet. Amplitude, wavelength, and propagation 353 velocity can be estimated from our method. For a typical flapping case of the Earth's 354 magnetotail, we demonstrated that our estimated average parameters are well 355 consistent with the multi-point timing analysis of Cluster. Thus, our method could 356 potentially be applied to studying flapping dynamics when multi-point measurements 357 358 are unavailable, particularly in the case of planetary spacecraft missions.

Building on the single-point method by Rong et al. (2015a), we can now summarize the complete procedure of diagnosing tail flapping motions based on a single-point magnetic field measurement as follows:

- 362 1) We set up local coordinate (**L**, **M**, **N**) for the current sheet, where the 363 undisturbed current sheet lies in the LM plane, +**L** is basically along the local 364 lobe field pointing earthward, the normal current sheet is along the +**N** direction, 365 and $\mathbf{M} = \mathbf{L} \times \mathbf{N}$ points duskward.
- Given the local coordinate, we fit the magnetic field structure of an undisturbed
 current sheet to the Harris sheet model, so that the structure of undisturbed
 current sheet can be roughly obtained.
- 369 3) At the crossing of each current sheet, we perform MVAB to calculate the local
 370 normal of the current sheet, and check the sequence of calculated parameter k in
 371 the local coordinate system. Based on the obtained sequence of k, we can

- determine the flapping type and the propagation direction of kink-like flapping
 waves using the technique developed by Rong et al. (2015a).
- 4) With knowledge of the fitted Harris sheet model and the local normal of each current sheet from local coordinate, we can estimate the spatial amplitude of flapping motion via Eq.(4). Based on our diagnosis of flapping types, we can further estimate the wavelength and propagation speed of kink-like flapping waves via Eq. (5) and Eq.(6) respectively.
- By comparing the inferred propagation speed with the one from timing analysis 379 (see the column of V_{f} in Table 2), which could be seen as the true propagation 380 speed, we find that our estimated speeds at each crossing (see ' $V_{f, MVAB}$ ' in Table 2) are 381 not necessarily equal to the speeds estimated by timing analysis, even though the 382 383 modification of the current sheet normal by the timing normal is considered (see ' V_{f_i} timing' in Table 2). The multiple error sources, e.g. uncertainty of the MVAB normal, 384 the irregularity waveform of flapping current sheet, and the temporal variation of 385 undisturbed current sheet etc., may contribute together to affect the accuracy of 386 estimated parameters. 387
- Despite a discrepancy with timing analysis at each crossing of the current sheet, the mean propagation speed ($\langle V_{f, MVAB} \rangle \sim 32$ km/s) is, from our estimation, comparable to the mean propagation speed obtained by timing analysis ($\langle V'_{f} \rangle \sim 42$ km/s). Thus, our single-point method is suitable for calculating average parameters during the whole flapping period, but would probably be unable to estimate such parameters accurately at each crossing of the current sheet.

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