Stress Drop Variations in the Region of the 2014 MW8.1 Iquique Earthquake, Northern Chile

Jonas Folesky^{1,1}, Joern Kummerow^{1,1}, and Serge A. Shapiro^{2,2}

¹Freie Universitäet Berlin ²Freie Universität Berlin

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Abstract

We compute stress drops from P and S phase spectra for 534 earthquakes in the source region of the 2014 MW 8.1 Iquique megathrust earthquake in the northern Chilean subduction zone. An empirical Green's function based method is applied to suitable event pairs selected by template matching of eight years of continuous waveform data. We evaluate the parameters involved in the stress drop estimation, consider the effect of the local velocity structure and apply an empirical linear relation between P and S phase related geometry factors (k values). Data redundancy produced by multiple EGFs and the combination of P and S phase spectra leads to a substantial reduction of uncertainty and robust stress drop estimates. The resulting stress drop values show a well-defined log-normal distribution with a median value of 4.36 MPa; most values range between 0.1-100 MPa. There is no evidence for systematic large scale lateral variations of stress drop. A detailed analysis reveals several regions of increased median stress drop, an increase with distance to the interface, but no consistent increase with depth. This suggests that fault regime and fault strength have a stronger impact on the stress drop behavior than absolute stresses. Interestingly, we find a weak time-dependence of the median stress drop, with an increase immediately before the April 1, 2014 MW 8.1 Iquique mainshock, a continuous reduction thereafter and a subsequent recovery to average values. Additionally, the data set indicates a relatively strong dependence of stress drop on magnitude which extends over the entire analyzed magnitude range.

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J. Folesky¹, J. Kummerow¹, S.A. Shapiro¹

¹Freie Universität Berlin, Department of Geophysics, Berlin, Germany

Key Points:

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7	• A comprehensive stress drop distribution for the Iquique Earthquake rupture re-
8	gion is computed using a spectral ratio approach.
9	• The stress drops estimates reveal no large scale pattern or major trend such as
10	a depth dependency.
11	• We describe minor stress drop variations in greater detail and find a relatively strong
12	scaling with moment for the entire data set.

Corresponding author: Jonas Folesky, jonas.folesky[at]geophysik.fu-berlin.de

13 Abstract

- We compute stress drops from P and S phase spectra for 534 earthquakes in the source region of the 2014 $M_W 8.1$ Iquique megathrust earthquake in the northern Chilean subduction zone. An empirical Green's function based method is applied to suitable event pairs selected by template matching of eight years of continuous waveform data.
- We evaluate the parameters involved in the stress drop estimation, consider the effect of the local velocity structure and apply an empirical linear relation between P and S phase related geometry factors (k values). Data redundancy produced by multiple EGFs and the combination of P and S phase spectra leads to a substantial reduction of uncertainty and robust stress drop estimates. The resulting stress drop values show a welldefined log-normal distribution with a median value of 4.36 MPa; most values range between 0.1-100 MPa.

There is no evidence for systematic large scale lateral variations of stress drop. A 25 detailed analysis reveals several regions of increased median stress drop, an increase with 26 distance to the interface, but no consistent increase with depth. This suggests that fault 27 regime and fault strength have a stronger impact on the stress drop behavior than ab-28 solute stresses. Interestingly, we find a weak time-dependence of the median stress drop, 29 with an increase immediately before the April 1, 2014 $M_W 8.1$ Iquique mainshock, a con-30 tinuous reduction thereafter and a subsequent recovery to average values. Additionally, 31 the data set indicates a relatively strong dependence of stress drop on magnitude which 32 extends over the entire analyzed magnitude range. 33

34 Introduction

Stress drop relates the rupture dimension to the seismic moment of earthquakes which makes it a central parameter of earthquake source analysis, having both practical implications, e.g., on high frequency-ground motion, and theoretical ones on the rupture processes of earthquakes in general. The complex nature of earthquake rupture and with it the behavior of stress drop still raise important questions which have not yet been answered conclusively.

Stress drop has been observed to depend on different factors such as depth, stress
conditions and tectonic setting (e.g., Sibson, 1974; Kanamori & Anderson, 1975; Venkataraman & Kanamori, 2004; Allmann & Shearer, 2009; Uchide et al., 2014; Boyd et al., 2017).
Results, however, are not always univocal. For example, Venkataraman & Kanamori (2004)

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and Uchide et al. (2014) report strong dependence on earthquake depth, while Allmann
& Shearer (2009) find evidence for a weak depth dependence with some variability depending on e.g. region or faulting type. Similarly, multiple studies support the self-similarity
of the rupture process, which suggests constant stress drop independent of event magnitude (e.g., Abercrombie, 1995; Shearer et al., 2006; Allmann & Shearer, 2009), but more
recent studies also report a considerable correlation between stress drop and seismic moment for different source regions (e.g., Abercrombie et al., 2016; Trugman & Shearer, 2017).

The interpretation of results is generally complicated by the inherent problem that individual stress drop estimates often scatter heavily for a given study area, and different techniques and models produce significant variability of stress drop estimates. Even for similar approaches, the parameter choice may introduce systematic changes of the resulting stress drop values. Therefore, at least for comparative studies, it is beneficial when stress drops are calculated in a consistent way for a large number of earthquakes, as applied in Shearer et al. (2006) or Allmann & Shearer (2009).

For large data sets with predominantly small to medium-sized earthquakes, one prac-59 tical way to compute stress drops is from the spectra of the recorded seismograms. One 60 popular approach is the spectral decomposition introduced by Shearer et al. (2006) which 61 uses a global empirical Green's function (EGF) obtained by an iterative stacking pro-62 cedure. This method was applied both globally (Allmann & Shearer, 2009) and also in 63 more detail to different regions of the world, e.g., in California (Shearer et al., 2006; Goebel 64 et al., 2015; Trugman & Shearer, 2017) and in the Japan subduction zone (Uchide et al., 65 2014). 66

A second frequently used approach is the spectral ratio technique based on the clas-67 sical empirical Green's function (EGF) concept (e.g., Frankel, 1982; Mueller, 1985) where 68 individual, well selected partner events are used to clean the earthquake spectrum from 69 contributions of ray path and site response. Different realizations have been applied over 70 the years to a variety of data sets, including borehole, local and regional recordings (Hutch-71 ings & Viegas, 2012; Abercrombie, 2014; Abercrombie et al., 2016). Both approaches were 72 compared in a recent study by (Shearer et al., 2019) which concludes that results are com-73 parable if additional constraints on the corner frequencies of the smaller event in the spec-74 tral ratios are introduced. The authors emphasize, however, that the most reliable re-75 sults are achievable by uniform processing of comprehensive data sets which approves 76

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the subsequent interpretation of internal variations. In this study, we follow this guideline.

We study here seismicity in the northern Chilean subduction zone, a region, which 79 experienced two megathrust earthquakes in recent years, the 2007 $M_W 7.7$ Tocopilla event 80 and the 2014 $M_W 8.1$ Iquique event. Despite the occurrence of these two megathrust earth-81 quakes the postulated northern Chilean seismic gap still remains partially unbroken (Schurr 82 et al., 2014; Hayes et al., 2014), and therefore is of great interest. The study area has 83 been monitored intensively since 2006 by the IPOC network (IPOC, 2006). Recently, a 84 comprehensive earthquake catalog of over 100,000 earthquakes for the time period of 2007 85 to 2017 and based on the IPOC seismic station data was published by Sippl et al. (2018). 86 Detailed studies have analyzed various characteristics of the study area such as local seis-87 micity, including the 2007 Tocopilla and 2014 Iquique earthquakes (e.g., Schurr et al., 88 2012; Fuenzalida et al., 2013; Schurr et al., 2014; Hayes et al., 2014), their foreshock and 89 aftershock behavior (Ruiz et al., 2014; Cesca et al., 2016; Hainzl et al., 2019), ground 90 motion and locking in pre-, inter- and post-seismic phases (Li et al., 2015; Hoffmann et 91 al., 2018; Moreno et al., 2018), fluid-migration and velocity ratios (Bloch, John, et al., 92 2018), event mechanisms (Cesca et al., 2016), and source characteristics such as direc-93 tivity (Folesky, Kummerow, & Shapiro, 2018) and corner frequency and radiated energy 94 (Derode & Campos, 2019) for selected subsets of events. 95

One still missing, essential aspect is a comprehensive analysis of stress drop. While the region has been covered by few global stress drop studies which are methodically confined to large earthquakes (Allmann & Shearer, 2009; Ye et al., 2016) the distribution of stress drop for small to medium sized seismicity is still poorly known. Only single studies report for small numbers of particular events in the Iquique region (Derode & Campos, 2019) and in the Tocopilla region (Lancieri et al., 2012).

Simultaneously, the existing data set from northern Chile constitutes an intriguing target because of its long time span, its large spatial extent, the different seismically active units covered (plate interface, upper crust, oceanic crust and mantle, see Sippl et al. (2018)) and in particular the recorded intense seismicity related to the fore- and aftershock series of the 2007 Tocopilla event and the 2014 Iquique event.

In this study, we present a workflow which is adapted to the consistent analysis of stress drops for large data sets by relying on a spectral ratio approach similar to Abercrombie (2014) or Huang et al. (2016). We focus on the particularly rich seismicity data



Figure 1. Map of the research area in northern Chile. The 2610 events used in this study are color coded according to their depth. Events from the catalog of Sippl et al. (2018) are underlain in grey. Epicenters of the M_W 8.1 2014 Iquique event and its M_W 7.6 largest aftershock are plotted in red. The IPOC permanent broadband station network (23 stations) are displayed on the upper right.

in and around the rupture domain of the 2014 Iquique event (Figure 1). We first describe

the method and how we apply it to our data. We discuss the influence of uncertainties

and limitations introduced by event station geometry, EGF event selection, signal band-

width, spectral model used, applied k parameters, seismic velocity model, smoothing,

and seismic moment. We complement this evaluation by an analysis of the robustness

- of the obtained corner frequencies. After this, we study the spatial distribution and tem-
- ¹¹⁶ poral variation of stress drop.

117 Catalog and Data

We use in total the 23 seismic broadband stations of the Integrated Plate Bound-118 ary Observatory Chile (IPOC). The network extends from north to south over a length 119 of about 700 km between 17.6°S and 24.6°S. This study focuses on the sub-region 19-120 $21^{\circ}S$ and 69.5- $71.5^{\circ}W$ which is shown in Figure 1 by a green square. Event origin times, 121 P and S arrival time picks and event locations are taken from the catalog by Sippl et al. 122 (2018) that consists of more than 100,000 double-difference relocated events. The cor-123 responding 100 Hz, three-component waveform data were accessed through the EIDA web 124 service of GFZ Potsdam (Bianchi et al., 2015). 125

In this region, seismicity occurs mainly on the interface between the subducting oceanic Nazca plate and the overlying South American plate, with some additional events in the overlying continental crust and also in an active deeper band, located about 20 to 25 km below the interface within the oceanic mantle.

130 Method

We apply an empirical Green's function (EGF) method called the spectral ratio 131 approach, where an EGF is a smaller earthquake with similar location and focal mech-132 anism as the target event. The method can be used to extract detailed source proper-133 ties of the target event such as source time function or directivity without explicit knowl-134 edge of path effects or attenuation (cf. Hutchings & Viegas, 2012, for an overview). We 135 apply an approach that is based on the fit of an appropriate source model to the spec-136 tral ratio between target event and EGF event to identify the corner frequency of the 137 larger event from the event pair. The procedure is described in the following. 138

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Selection of Suitable Empirical Green's Functions (EGF) Pairs

We start the analysis by selecting 9071 catalog events from the earthquake cata-140 log by Sippl et al. (2018) which are located in the study area and which are well recorded 141 by the neighboring IPOC stations. For each catalog event, we perform a template match-142 ing scan of the continuous waveform data recorded on the vertical components of the five 143 IPOC stations PB01, PB02, PB08, PB11, PB12 for the years 2008 to 2016. A bandpass 144 from 1 to 4 Hz is applied. The templates have a length of 35 s starting 5 s before P pick 145 and include both P and S wave coda. If the normalized cross-correlation coefficient of 146 cc = 0.8 is exceeded at minimum three different stations, the detected and the template 147 event are defined as a potential event pair. The long cross-correlation time window en-148 compassing both the P and the S phase window ensures the appropriateness of the EGF 149 in terms of co-location and similarity of mechanism of both events (Menke, 1999). Us-150 ing this procedure we obtain in total 9950 event pairs. Most of the EGF events are new 151 detections which were not listed in the catalog before. For further analysis we also re-152 quire a minimum magnitude difference of $\Delta M \geq 1$. This is computed from the ratio 153 of the peak amplitude values (velocities) for each target event with its corresponding EGF 154 event at station PB11 where $A_{target}/A_{EGF} \geq 10$. After application of this criterion the 155 number of potential events pairs reduces to 2610 which remain for the analysis. Their 156 locations are highlighted in Figure 1. 157

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Spectral Ratio and Data Fitting

We apply a spectral ratio approach similar to Abercrombie et al. (2016) and Huang et al. (2016) where the spectrum of a target event is divided by the spectrum of its corresponding EGF event. The resulting spectral ratio can be used to assess the corner frequency of the larger and the smaller event as well as the ratio of their seismic moments. In theory, this can be described by the ratio of two events i = 1, 2 under the assumption of a specific spectral source model, e.g., the one of Brune (1970) or Boatwright (1980):

$$\frac{u_1(f)}{u_2(f)} = \frac{\Omega_1}{\Omega_2} \left(\frac{1 + (f/f_{c_2})^{\gamma n}}{1 + (f/f_{c_1})^{\gamma n}} \right)^{\frac{1}{\gamma}},\tag{1}$$

where u_i is the displacement, Ω_i is proportional to the seismic moment M_{0i} , f_{ci} is the corner frequency and n the spectral falloff rate while γ depends on the assumed source model (e.g., $\gamma = 1$ for the Brune model, $\gamma = 2$ for the Boatwright model). The latter model of Boatwright (1980) predicts a sharper cornered source spectrum, and when applied to our data we find a consistently lower RMS compared to the model of Brune (1970). Therefore, the subsequent analysis is performed using the Boatwright model with $\gamma =$ 2. In principal, it is possible to allow for variations of the falloff rate n, but this would introduce additional uncertainties into the estimation of the corner frequency (Kaneko & Shearer, 2014). To ensure better comparability and to limit the degree of freedom for the fitting (Kaneko & Shearer, 2015), we fix the value to n = 2 which matches our data well.

The entire procedure is computed separately for P and S phases. Data are first de-176 trended and then bandpass filtered between 0.8 to 40 Hz, all using built-in Obspy func-177 tions (Beyreuther et al., 2010). We have tested different passbands and we recognize a 178 cutoff at about half the upper corner of the filter as described by Ruhl et al. (2017). Con-179 sequently, we have to remove events that potentially have corner frequencies higher than 180 half the upper bandpass corner (i.e., 20Hz). In this study, we can expect to resolve most 181 events with magnitudes M> 2.5 (see Limitations Section and supplementary Figs. S1 182 and S2 for further explanation). 183

For the P phases, we select a time window starting at 0.5 s before the P phase pick and ending at 1.7 times the catalog based P phase travel time, the approximate S phase arrival. For the S phases, the window is taken relative to this approximate S pick with a 1.7 times longer duration. The minimum duration for both time windows are 10 s and 17 s, respectively.

We compute the event spectrum of each individual trace and compare it with the 189 noise spectrum from the time window directly preceding the P phase. Similar to the ap-190 proach by Shearer et al. (2019), we reject traces with an average SNR of less than 3 in 191 any of five frequency bands (1.5-5 Hz, 5-10 Hz, 10-15 Hz, 15-20 Hz, 20-25 Hz). This is done 192 for main event and EGF-event. We obtain a single, average spectral ratio by taking the 193 median of all individual trace spectral ratios for each frequency point. This step is nec-194 essary to reduce spherical variation of the source characteristics (here f_c , see (e.g. Aber-195 crombie et al., 2017)). We require that minimum four traces satisfy the selection crite-196 ria in order to accept an event. On average 17 traces contribute to an average ratio. In 197 the next step this spectral ratio is smoothed using the approach of Konno & Ohmachi 198 (1998) which was developed originally to stabilize the spectral ratio between horizon-199 tal and vertical components for computing ground motion characteristics. The method 200

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ensures a constant number of points in the given frequency bin to mitigate a overweight of high frequencies while smoothing (Huang et al., 2016).

The theoretical spectral ratio model (Equation 1) is then fitted to the smoothed 203 average spectral ratio. We optimize for the parameters f_{c_1}, f_{c_2} and $\Omega_{1/2}$ using the trust 204 region reflective method from scipy curve_fit to describe the shape of the entire spectral 205 ratio. We constrain the corner frequencies as follows: $1 \text{ Hz} \le f_{c_1} \le f_{c_2} \le 50 \text{ Hz}$. Tests with 206 a fixed fc_2 as proposed by Shearer et al. (2006); Hardebeck & Aron (2009) produced rea-207 sonable fits for many events but also generated some artefacts, especially for events with 208 low corner frequencies f_{c_1} . Additionally, an impact on the absolute value of f_{c_1} was no-209 ticed. Hence we do not fix the corner frequency of the smaller event, f_{c_2} . We could not 210 study the variability of f_{c_2} because for most events it may be biased due to the limita-211 tions by the available frequency band. For further analysis, we only use f_{c_1} , henceforth 212 denoted as f_c . 213

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Computation of Stress Drop

To compute the stress drop we take the circular source model as derived by Eshelby (1957) and Madariaga (1976) and write:

$$\Delta \sigma = \frac{7\pi\mu\overline{D}}{16r} = \frac{7M_0}{16r^3},\tag{2}$$

where r is the approximate fault radius, \overline{D} is the average slip on the fault, μ is the shear modulus, and M_0 is the seismic moment. In general, slip and fault dimensions are not easily determined, and we cannot compute the stress drop directly (Kanamori & Anderson, 1975). We, therefore, resort to a method which derives stress drop from the source displacement spectrum. The approach of Brune (1970) provides a link between source radius and the spherically averaged corner frequency (see also Madariaga, 1976; Kaneko & Shearer, 2014, 2015):

$$f_c = k \frac{\beta}{r},\tag{3}$$

with the shear wave velocity at the source, β , and a constant k that relates to the spherical average of the corner frequency for a specific theoretical source model. By combin-

ing Equations 2 and 3 the sometimes called 'Brune type' stress drop can be computed

$$\Delta \sigma = \frac{7}{16} \left(\frac{f_c}{k\beta} \right)^3 M_0. \tag{4}$$

We described above the procedure to obtain the value for the spherically averaged corner frequency f_c (Eq. 1). To compute the stress drop, we rely on additional information for the other parameters.

Münchmeyer et al. (2020) provide a refined and consistent magnitude catalog for the data set of Sippl et al. (2018). We derive the seismic moment from their corrected local magnitude catalog by presuming sufficient similarity to moment magnitude and then using the standard relation $(M_W = 2/3(log_{10}(M_0) - 9.1)).$

Because of the large spatial extent of our event distribution, shear wave velocities 234 vary considerably, and we use the extrapolated 2D velocity model from Bloch et al. (2014) 235 to determine the shear wave velocity individually for each event pair. For the k param-236 eter we take the standard value from Madariaga (1976): $k_p = 0.32$ for P phases. Follow-237 ing Prieto et al. (2004) and Abercrombie et al. (2016) we estimate the relation of P to 238 S phase derived corner frequencies for our entire data set, as shown in Figure 2. The pro-239 cedure provides a best fitting ratio of $f_{c_p}/f_{c_s} = k_p/k_s = 1.16$ yielding a value of $k_s = 0.28$ 240 for S phases. By choosing both k values accordingly, we obtain comparability of the re-241 sulting stress drop values from P and S phases. 242

When the complete data set is processed we find that many target events have not only one P and S phase based stress drop estimate (which was obtained by taking the median over all recording stations), but they may also have additional EGF events. In these cases we collect the results and take the median of all estimates to enhance stability further. We also make use of the redundancy information from these event families to estimate the robustness of our approach as described in the uncertainty section.

²⁴⁹ Data Example

We illustrate our realization of the spectral ratio approach for one event pair in Fig-250 ures 3 & 4. Figure 3 shows all pre-processed velocity traces available for both events. The 251 selected (here P) phase windows are highlighted in grey. Figure 4 displays the correspond-252 ing spectra, their spectral ratios with the obtained fit curves for the Boatwright spec-253 tral model and the station wise variation of corner frequency with the overall median for 254 the target event. The stress drop value of $\Delta \sigma = 1.7$ MPa is then computed from the 255 average spectral ratio (Figure 5). Note the good consistency between the individual mea-256 surements, their median f_c and the result computed from the average ratio. Additional 257



Figure 2. P phase based versus S phase based corner frequencies. The four different lines are the 1:1 line, the 1:1.23 line illustrative for one of the rupture models of Kaneko & Shearer (2014) where $v_r/\beta = 0.7$, 1:1.52 the value obtained by Madariaga (1976) for $v_r/\beta = 0.9$, and our estimate 1:1.16 obtained by fitting a least square regression line to the data. Using an empirical k_p/k_s ratio allows to combine P and S phase based stress drop estimates.

- figures are given in the supplement, including examples based on S phase spectra, using the Brune model for fitting the corner frequency and from events with different magnitudes (Figs. S3-17).
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Limitations & Uncertainties

In this section we will discuss data limitations of this study. Thereafter we will discuss sources of uncertainty inherent to the stress drop estimation procedure and compute an approximate error for the stress drop computation.

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Limitations

The estimation of spectra- derived properties is always limited by the bandwidth that can be reliably resolved. In this study, we use recorded 100 Hz velocity data which was bandpass filtered from 0.8-40 Hz. To allow a sufficiently high number of frequency points above the corner frequency in order to fit the spectral model to the data, results for f_c were limited between 1-20 Hz. This limitation, however, constitutes a selection bias on possible corner frequencies. As a consequence, high stress drop events or low stress



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Figure 3. Velocity traces with highlighted P phase windows for an exemplary event pair. (Left) Pre-processed velocity traces of the target event, (right) pre-processed velocity traces of the smaller magnitude EGF event. Only the traces which comply with our selection criteria are displayed. The labels contain station and component names. The P picks are taken from the catalog for the target event and they were transferred to the EGF event based on the inter event time. The header specifies event origin times and magnitude of the target event.



Figure 4. Velocity spectra of the example events from Figure 3 (left). Black is the target event, grey the EGF event. The thinner lines are the corresponding noise spectra. The smoothed spectral ratio is computed for each trace and the Boatwright spectral model is fitted to the data (center). Corner frequency (f_c) and RMS values are given for each spectrum. The corner frequencies are then plotted trace wise where stations are sorted from north to south (right) such that azimuthal variability and outliers could be observed. The median value, $\overline{f_c}$, is indicated by the vertical line. The header states event origin times and magnitude of the target event.



Figure 5. Average spectral ratio computed from the median for each frequency point over all traces shown in Figure 4. The curve is smoothed (Konno & Ohmachi, 1998) and then fitted with the Boatwright spectral model (n=2) to obtain the corner frequency, $f_c=4.30$ Hz, of the target event which is used to compute the stress drop, $\Delta\sigma=1.7$ MPa.

drop events may be suppressed systematically. We find evidence for such an effect when studying the scaling relation between moment and corner frequency in the Results & Discussion section.

Due to their long recording period and consistency of data availability, we restrict our analysis to the 23 IPOC stations, which are also the base for the seismicity catalog of Sippl et al. (2018). On average 17 traces contribute to a single stress drop measurement. Having verified that no major variation of statistical properties occurs, we accept results down to 4 contributing traces. Some stress drop values, therefore, are estimated using only relatively few stations.

As a consequence of the event locations and station positions, the station layout 281 for most events is one-sided and we cannot rule out an impact of possible rupture direc-282 tivity on the corner frequency. Also, the event depths and their source plane orientations 283 may impact the stress drop estimates as f_c varies depending on the takeoff angle (Kaneko 284 & Shearer, 2014). Since most events are located close to the plate interface, we make a 285 first order assumption of similar rupture mechanisms (Cesca et al., 2016) and similar lo-286 cations relative to the station network. Then, geometric conditions are comparable for 287 all events, and we expect only a minor effect on stress drop variations between events. 288

Another possible selection bias arises by the choice of suitable empirical Green's function events. Using inappropriate EGF events would result in reduced validity of the

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deconvolution procedure to recover the spectra of the target events. We apply a high cross-291 correlation threshold of cc=0.8 measured over a long time window of 35 s. The thresh-292 old has to be exceeded at a minimum of three stations. Additionally, we require a min-293 imum magnitude difference of $\Delta M \geq 1$ between target and EGF event. These are com-294 parably rigorous restrictions and, as reported in Abercrombie (2015) and Abercrombie 295 et al. (2016), we do not observe any influence on the stress drop estimate by varying the 296 cc or ΔM requirements above the applied thresholds. By application of this criteria, we 297 limit the analysis to regions of high event occurrence rates where EGFs may be found. 298 Other areas remain unsampled. 299

To enhance stability of the computation of the spectral ratio, we smooth each spectrum before fitting (Huang et al., 2016). We use the Konno & Ohmachi (1998) smoothing operator to account for the logarithmic distribution of sample points in each smoothing window. We verified that only a negligible variation of f_c is introduced by the smoothing, using a simple synthetic source spectrum with added Gaussian white noise (please see the electronic supplement and Fig. S22 for further explanation).

The choice of the spectral model has a systematic influence on the estimated cor-306 ner frequency. Because of their spectral shapes, the Brune model provides a lower f_c than 307 the Boatwright model. We tested both models and found that the Boatwright model over-308 all describes our data better (see Fig. S5&S6 ff. in the supplement for an example). We, 309 therefore, selected it for the analysis. By optimizing additionally for the falloff rate n in 310 Equation 1, it is in principle possible to further improve the fitting and decrease the stan-311 dard deviation of the parameter f_c while introducing another uncertainty for n itself (Trug-312 man & Shearer, 2017). We refrain from this approach and fix n = 2 which makes the 313 results somewhat more comparable (Kaneko & Shearer, 2014). 314

Uncertainties

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Keeping in mind the upper mentioned limitations and possible sources of systematic bias, one can analyze the statistical error of stress drop within the data set by an assessment of the uncertainty of the contributing factors in the Brune type stress drop formula.

To evaluate the statistical error of the corner frequency of our analysis we exploit the redundancy of f_c measurements within our data set. Because P and S phase based



Figure 6. Histogram of relative differences to the family-specific median corner frequencies (For each of the 482 target event families one single median f_c is calculated and the individual difference of each f_c estimate (in total 1996) to this median is divided by this median). The distribution is normalized and a PDF with exponential shape is fitted to the data. Note that the great majority of event families show very similar stress drop estimates (difference is smaller 0.5) which means that different phases and different EGFs produce similar corner frequency estimates for a given target event.

corner frequencies are computed separately, most events have at least two independent 322 f_c estimates. Many events also belong to so called event families for which the target 323 event has two or more associated EGF events. We compute the median corner frequency 324 for each target event from all P and S phase based measurements within an event fam-325 ily and calculate the difference of each single estimate to this median value divided by 326 the median value. We refer to this value as the relative difference. Figure 6 shows the 327 distribution of relative differences combined for 482 event families. Counting P and S 328 phase, separately, a total of 1996 EGF events were used. The histogram is scaled to fit 329 a PDF to the data. The best fitting PDF has exponential shape $(PDF = \lambda e^{-\lambda x})$. We 330 compute the corresponding standard deviation $std = 1/\lambda = 0.15$. This value compares 331 well with the range of normalized standard deviations for multiple station estimates pro-332 vided by Abercrombie (2015) (their Figure 4) who explicitly investigated EGF uncer-333 tainty factors. We will use the obtained value as an approximate relative error, i.e., $\delta(f_c)=0.15\%$. 334 The true rupture velocity is almost always unknown and poses another source of 335 uncertainty. In the frame of Brune type stress drop estimation, it is usually treated in 336 combination with the rupture mechanism and the observation geometry, which is expressed 337 by the k value in Equation 2 (Brune, 1970; Sato & Hirasawa, 1973; Madariaga, 1976). 338 Kaneko & Shearer (2014) show in detail that different combinations of k_s and k_p for S 339 and P phases, respectively, can be assigned to different source models and rupture ve-340 locities. In principle, k is also station-specific and depends on the takeoff angle under 341 which the ray leaves the source. Since the event-specific k values are generally unknown, 342 we follow the approach of Prieto et al. (2004) and determine the k ratio empirically. Fig-343 ure 2 displays the event wise and spherically averaged corner frequencies of P phase ver-344 sus S phase for the entire data set. The computed regression line gives the ratio for which 345 both phases provide on average the same stress drop for a given event over the entire data 346 set. According to Kaneko & Shearer (2014) our estimate of $k_p/k_s=1.16$ could represent 347 overall symmetrically rupturing circular sources with a relatively slow rupture velocity 348 of $v_r \approx 0.6\beta$. Figure 2 demonstrates that the uniform k_p/k_s ratio holds well for the ma-349 jority of events, but it also indicates differing ratios for some events. A possible expla-350

nation for this observation are deviations in the rupture characteristics such as rupture
 mechanism, directivity or deviating fault plane orientation.

³⁵³ Next, knowledge of the seismic moment M_0 is required to compute the stress drops ³⁵⁴ (Equation 2). We derive it from the magnitudes provided by Münchmeyer et al. (2020).

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Although uncertainties for the magnitudes are very low in their catalog - the authors give standard deviations in the low percentage range (0.5-2.5%) - this translates to about tenfold relative errors for the corresponding seismic moment, i.e., the relative error for the moments range between 10–30% for most events.

The last parameter in the stress drop equation is the shear wave velocity β . Especially in a subduction zone setting, phase velocity may vary significantly on a 10 km scale. It is consequently important to apply the best velocity model available. We obtain β from a pseudo 3D velocity model created by Bloch et al. (2014)(see Fig. S27) and use individual values for each target event depending on its location. Assuming correct event locations we expect a relative error in the shear wave velocity of about 5%.

Combining the relative errors obtained as explained above ($\delta f_c = 15\%$, $\delta M_0 =$ 365 $30\%, \delta \beta = 5\%$) and conservatively using doubled error values, i.e., two times the stan-366 dard deviation, the relative error from the stress drop computation is about 200% (\approx 367 $3(2\delta f_c + 2\delta \beta) + 2\delta M_0)$ according to Equation 4. Note that this is still much smaller than 368 the variability of the stress drop values in our final result catalog, which vary over 2-3369 orders of magnitude. We conclude that our workflow is reasonably well suited to pro-370 duce meaningful results and that it is capable of resolving actual variations of stress drop, 371 while keeping in mind the limitations that affect the whole data set. 372

373 Results & Discussion

The workflow is applied to the entire data set of 2610 events (Figure 1). The anal-374 ysis yields 1237 P phase based and 1396 S phase based stress drop estimates. These num-375 bers reduce when accounting for the fact that a target event may have multiple EGF events. 376 As explained earlier we combine the P and S phase derived stress drops by fixing the ra-377 tio of the k parameters to the previously calibrated value $k_p/k_s = 1.16$ (Figure 2). For 378 each target event, we then merge the measurements from P and S phases and from ad-379 ditional EGF events, if present, by taking the median over all single estimates. This pro-380 cedure yields stress drop estimates for 534 target events. Their distribution is plotted 381 event wise in Figure 7. The resulting stress drops show a well pronounced log-normal 382 distribution with an overall median stress drop of $\Delta \sigma = 4.36 MPa$ displayed in Fig-383 ure 8. This value is of the same order as the independently estimated stress drops for 384 the Iquique earthquake, $\Delta \sigma = 7.66 MPa$, and its biggest aftershock, $\Delta \sigma = 4.28 MPa$ 385 by Ye et al. (2016), derived with a time domain approach. The stress drop map reveals 386

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Figure 7. Stress drop distribution for 534 target events in map and depth views. Color indicates the stress drop value. The red stars indicate the hypocenters of the $M_W 8.1$ Iquique event and the $M_W 7.6$ largest aftershock. Underlain is the coseismic slip distribution in 0.5 m increments taken from Schurr et al. (2014). The red line in the west–east depth section delineates the slab interface from Hayes et al. (2012).

a heterogeneous distribution. Note that the spectral ratio approach is limited to those
 subregions where suitable EGF events exist. Event density is much higher on the part
 of the interface that lies updip of the maximum slip patch of the 2014 Iquique event. This
 observation reflects the overall very high updip seismic activity related to the megath rust event.

We attempt to identify regions of characteristic stress drop behavior by dividing 392 the study region into grid cells and computing the median stress drops for each cell, sim-393 ilar to the approach by Uchide et al. (2014). The results are shown in Figure 8. No smooth-394 ing is applied between cells. Average values dominate and in principle, stress drop ap-395 pears to be distributed very heterogeneously throughout the map. We noted an inter-396 esting patch of elevated values north of the nucleation point of the $M_w 8.1$ mainshock, 397 as well as a larger patch of increased values west of the hypocenter of the $M_w 7.6$ after-398 shock, both highlighted by black outlines. When interpreted as stress barriers marked 399 by higher roughness, they could possibly indicate domains of the interface which inhib-400 ited further growth of the rupture area of the large Iquique event, as suggested e.g. for 401 the 2011, Tohoku-Oki earthquake by Uchide et al. (2014). The predominant rupture di-402 rectivity of both events, the main event rupturing towards south east and the aftershock 403 towards east (Folesky, Kummerow, Asch, et al., 2018) could then be interpreted as a con-404 sequence of such an existing barrier. 405

- To analyze the spatial dependency further we plot spatial sections in Figure 9. In addition to the estimated stress drops, the median values for bins of 0.1° widths are overlain for better visualization. Again, no smoothing is applied between bins.
- In the west–east section, bin values are continuously close to the overall average,
 with a slight tendency of increase towards east and few elevated values to the east.
- The north-south section also shows mainly close to average values except for a few domains of increase, e.g., at 19.5°S and 20.5°S. These correspond to the higher stress drop value patches observed previously and highlighted in the map view. South of 20.5°S, Sippl et al. (2018) identified increased upper plate seismic activity, which was suggested to correlate with a reduced interplate locking (Li et al., 2015; Moreno et al., 2016). We observe here a bin comprising predominantly small stress drop vales. If this behavior extends further towards the south (neglecting the last bin with only few high stress drop



Figure 8. Stress drop distribution averaged on a regular horizontal grid. In each grid cell the median for all occurring events is computed and displayed in color according to the color scheme of the histogram. The red stars indicate the hypocenters of the M_W 8.1 Iquique event and the M_W 7.6 largest aftershock for orientation. Underlain are the corresponding coseismic slip distributions in 0.5 m increments taken from Schurr et al. (2014). Two regions of increased stress drop are highlighted by a superimposed black contour line (cf. text). The histogram shows the distribution of stress drops for all 534 target events with their median of $\overline{\Delta\sigma} = 4.36$ MPa.

events, which are also located further east), this could corroborate their observation when confirmed with more data.

The depth view reveals fairly stable results of median stress drop for different depths. Abercrombie et al. (2016) report similar observations of non-significant stress drop variation with depth for earthquake sequences in shallow depth ranges (5-35 km). Below, stress drop values are slightly elevated for several kilometers till about 55 km depth and then decrease again. Interestingly, this curve shape is relatively similar to the global observation by Allmann & Shearer (2009) who report a slight rise of values starting at 35 km and falloff at about 55 km depth.

The observation of a stable median stress drop down to 70 km is in contrast to findings from the Japanese subduction zone (Uchide et al. (2014)), where a strong depth dependence was observed. For northern Chile, Derode & Campos (2019) report evidence for depth dependence of stress drop from 96 events of two different clusters. In their study, however, the velocity spectra are directly fitted with Brune's model, and path effects are not corrected for. We do not observe their reported clear depth dependence of stress drops in our extended data set.

The remaining section in Figure 9 shows the stress drop as a function of event dis-434 tance from the slab interface. We use the reference model of Hayes et al. (2012) to com-435 pute this distance. A roughly symmetrical behavior can be noticed. From -7.5 km to 7.5 km 436 close to average values are observed, and beyond these distances, the median stress drop 437 is notably elevated. Here, a possible explanation could be the maturity of the rupture 438 surfaces. While close to the interface rupture surfaces have been activated repeatedly, 439 the intraplate seismicity occurs on more intact fracture zones. These less mature faults 440 could then produce higher stress drop events (e.g. Choy & Kirby, 2004; Sagy et al., 2007). 441 Or, in other terms, the friction coefficient increases when receding from the interface into 442 the plates. In combination with the previously noted only weakly pronounced stress drop 443 dependence with absolute depth, this observation suggests that the fault strength and 444 faulting regime play more important roles than the lithostatic stress. 445

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The long recording period of over 10 years of consistent seismological observations of the northern Chilean subduction zone (IPOC, 2006) also provides a rare opportunity to study the temporal evolution of stress drop. We display the temporal sequence of stress drops in Figure 10 for the time period 2009 to 2017. The data is dominated by the fore-

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Figure 9. Stress drop variation in the spatial domain. The top panel shows stress drop estimates versus longitude. Below, the stress drop distribution is shown from north to south, against depth and relative to the plate interface from left to right, respectively. The binning interval is given in the plot legends. No smoothing is applied. The solid line traces the median value computed for each bin separately. To indicate the spread of values in each bin we plot a blue error bar from the median of the upper to the median of the lower half of values, which are separated by the overall median in the bin. In all plots the median of the entire data set ($\overline{\Delta \sigma} = 4.36$ MPa) is underlain as a grey line. In the last panel positive distance values refer to events located above the plate interface (red line), negative values to events below it.

and aftershock seismicity of the 2014 Iquique earthquake. In general, the 13-week me-450 dian stress drop binned values vary (almost randomly) around the overall median. The 451 variation, however, is based only on a limited number of events and should be interpreted 452 with caution. Zooming into the seismically highly active weeks around the Iquique event 453 shows that average values are measured during the two weeks following the large, $M_w 6.6$ 454 foreshock. A positive jump of stress drop from 4.0 to about 8 MPa is observed just af-455 ter the mainshock (ignoring the high stress drop bin before), followed by a steady de-456 crease of stress drop median values down to about 1 MPa over a time interval of 2 to 3 457 weeks. Then, the trend reverses and the median stress drop rises again to about the av-458 erage value. 459

The average stress drop in the same time window, i.e., the median over two weeks before compared to the median of four weeks after the main event changes from 3.98 MPa to 4.48 MPa while the overall median stress drop from before to after the Iquique event decreases from 4.55 MPa to 4.31 MPa.

Such an observation appears inconsistent until the influence of the spatio-temporal 464 aspect in the data is considered. To illustrate this, we produced additional maps for events 465 that occurred before the main earthquake, after the main event and maps comprising 466 only direct foreshocks or aftershocks. Please see Figs. S.18-21 in the supplement. The 467 maps indicate that the variability of the median stress drop value is likely to arise from 468 variable event occurrence locations in the split data sets. Unfortunately a differential com-469 parison between fore and after main event maps failed due to the limited overlap between 470 event locations. Still, this demonstrates that spatial and temporal stress drop variabil-471 ity has to be interpreted with caution. 472

We notice that the variation of stress drop in time is not independent of the target event magnitudes that were used to compute the stress drop estimates. In fact, the variation of magnitude is similar to the variation of stress drop (Fig. S23). This indicates a correlation between moment and stress drop.

The dependency between stress drop and seismic moment was analyzed in many stress drop studies, with diverging results. Shearer et al. (2006); Abercrombie (1995) reported moment independent stress drops, whereas several recent studies (in parts of the same groups of researchers) observed a relation between stress drop and seismic moment (Abercrombie, 2014; Abercrombie et al., 2016; Trugman & Shearer, 2017; Trugman, 2020).

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Figure 10. Stress drop variation in the time domain. The top panel shows stress drop values for the period from beginning of 2009 to end of 2016. The solid black line traces the median values for bins of 13 weeks time span each. The grey bar indicates the period displayed in the bottom panel. It shows an six week time period of strong seismic activity around the Iquique mainshock starting about two weeks before the event. The three vertical grey lines denote the origin times of the $M_W 6.6$ foreshock, the $M_W 8.1$ mainshock, and the $M_W 7.6$ aftershock. Bin width is four days; no smoothing is applied. To indicate the spread of values in each bin we plot a blue error bar from the median of the upper to the median of the lower half of values, which are separated by the overall median in the bin. In all plots the median of the entire data set $(\overline{\Delta\sigma} = 4.36 \text{ MPa})$ is underlain as a grey line.

Also, regional differences of this correlation have been reported lately (Trugman & Shearer, 482 2017). For the northern Chilean subduction zone interface seismicity, we observe a clear 483 increase of stress drop with moment (Figure 11). Fitting a standard least square regres-484 sion line where $log_{10}(\Delta \sigma) = \varepsilon_0 + \varepsilon_1 log_{10}(M_0)$ to the data yields a slope of $\varepsilon_1 = 0.51$ 485 (cf. Figure 11). Note that the limited bandwidth has a significant impact on event se-486 lection which becomes apparent here. It could contribute to the very strong scaling ef-487 fect observed. In Figure 11, we additionally provide the binned slope values. Here, the 488 bin that should be affected most by the 20 Hz cutoff shows the highest scaling value and 489 the bin which is best resolved (3<M<3.5) has the lowest ε_1 value. We additionally test 490 the influence of an increased SNR threshold onto the scaling and, similar to the study 491 by Chen & Abercrombie (2020), we find the ε_1 value to be lower when selection crite-492 ria are more restrictive (e.g., $\varepsilon_1=0.42$ if SNR=12). Hence, the reported scaling value is 493 only a best estimate and has to be taken with care, as it is sensitive to the parameters 494 applied in the processing. Nevertheless, we find a strong stress drop scaling with moment 495 in our data. Such an observation does not support the self-similarity assumption of rup-496 ture processes for earthquakes. When compared to other stress drop studies our estimates 497 fall into the typical range between 0.1–100 MPa (Figure 12). However, we observe a smaller 498 decrease of corner frequency with seismic moment than expected for moment indepen-499 dent stress drops. Cocco et al. (2016) gather data from several studies and conclude that 500 while some works show moment dependent stress drops for their particular, limited mag-501 nitude ranges the overall picture still shows a self-similar rupture behavior with no pre-502 vailing dependency of stress drop on moment. Note further that the observation of non-503 self-similarity is made under the assumption of a fixed value n = 2. Trugman & Shearer 504 (2017) point out that for their data self-similarity can be obtained by using varied as-505 sumptions, e.g. by fitting the spectral model with a different falloff rate. 506

The observed dependence of stress drop on seismic moment raises the question to 507 what extent the observations of stress drop variability made in this work are due to mag-508 nitude variation. To assess this issue we test the spatial and temporal variability under 509 the assumption of a moment- independent stress drop. For this, we correct the result-510 ing stress drop values for the gradient computed in Figure 11 such that the gradient van-511 ishes and the median stress drop is preserved (see Fig. S24). We then recompute Fig-512 ures 9 and 10. The resulting Figures S25 and S26 show that the earlier observations of 513 spatio-temporal stress drop variability are generally persistent although the range of vari-514

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ability decreases. The initially observed stress drop variation, therefore, is a combina tion of both effects, a change in stress drop and a change in earthquake moments.

The procedure described in this article is designed for large data sets where lim-517 ited knowledge on the events is presumed. As demonstrated by Kaneko & Shearer (2014, 518 2015) rupture processes may be far more complex than we can assess with current seis-519 mological networks. Consequently, it is important to acknowledge the limitations of a 520 given data set. In the case of the IPOC observation system, we deal with a one-sided ob-521 servation geometry for most events of this study, and we can only presume that aver-522 aging over as many stations as possible provides a reasonable estimate of the corner fre-523 quency for a given event. This may be sufficient to extract the more general features of 524 the data set which is the main objective of the present study. When conclusions are drawn 525 from particular observations of a small number of events, special caution should be taken. 526

Theoretically, it is possible, albeit out of the scope of this work, to enhance the pre-527 cision of single event stress drop estimates. For this, the event rupture plane must be 528 known, at best complemented by information on the rupture behavior such as the rup-529 ture velocity and directivity. For our study area information on fault planes exists (e.g. 530 Cesca et al., 2016; Bloch, Schurr, et al., 2018) and it has been demonstrated that a sig-531 nificant amount of events show rupture directivity (Folesky, Kummerow, Asch, et al., 2018; 532 Folesky, Kummerow, & Shapiro, 2018). The inclusion of such information into our work-533 flow is in principal possible, and it could help in the future to further improve the stress 534 drop estimates. 535

536 Conclusions

We compute stress drop estimates for 534 earthquakes in the subduction zone of 537 northern Chile. The events occurred at or close to the plate interface in the rupture re-538 gion of the 2014 $M_W 8.1$ Iquique event. The computed stress drops are log-normal dis-539 tributed and range mostly from 0.1-100 MPa with a median value of 4.36 MPa. The spa-540 tial distribution is heterogeneous but shows no clear dependence on depth, longitude or 541 latitude. We find, however, a slight increase of median stress drop with distance to the 542 plate interface. We also identify a few small patches of increased stress drop. We addi-543 tionally observe a temporal variation of the median stress drop associated with the Iquique 544 megathrust event. Just after the event, average stress drop increases, followed by a steady 545

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Figure 11. Scaling of stress drop with seismic moment. We fit the data with a standard least square regression where $log_{10}(\Delta \sigma) = \varepsilon_0 + \varepsilon_1 log_{10}(M_0)$. The legend gives the result for ε_1 and its standard deviation. At the bottom ε_1 values for the individual bins are displayed. Grey areas are beyond the resolution capacity of this study. Boundaries are defined by the 20 Hz and the 1 Hz lines and M=2.5. A clear dependence of stress drop on seismic moment is observed not only for the entire data but also for each individual bin.



Figure 12. Scaling of corner frequency with seismic moment. The dotted lines indicate constant stress drop levels. The great majority of values lie between 0.1 MPa and 100 MPa with a median of $\overline{\Delta \sigma} = 4.36$ MPa. Note that the decrease of corner frequency with magnitude is less than the rate calculated for a moment independence of the stress drops. Grey areas are beyond the resolution limit of this study (See section Limitations).

decrease lasting for several weeks until the trend reverses and the median stress drop value recovers to the long term average. Furthermore, we find indications that stress drop depends on the seismo-tectonic regime (cf. classification in Sippl et al. (2018)).

The stress drop estimates show a clear scaling with seismic moment. We find the empirical relation $log_{10}(\Delta\sigma) = \varepsilon_0 + 0.51 log_{10}(M_0)$ by fitting a regression line to the data. We show that this relatively strong dependency on moment is impacted by data limitations (frequency range) and decreases when selecting only very high quality data (high SNR). Still, this data set suggests a break of self-similar rupture scaling under the given assumptions.

It is planned to extend the work to the complete data set provided by Sippl et al. (2018) in the near future. Then, not only stress drop estimates for more than the tenfold number of earthquakes will be available, but also events from multiple distinct seismically active regions of the northern Chilean subduction zone will be processed consistently for the first time, potentially allowing for a broader comparative study.

560 Data & Resources

Seismograms used in this study were recorded by the seismic CX-net of the Inte-561 grated Plate boundary Observatory Chile (IPOC, 2006) using STS-2 broadband seismome-562 ters. Data were obtained from the EIDA/GEOPHONE web page (eida.gfz-potsdam.de/webdc3/ 563 or geofon.gfz-potsdam.de/waveform/, accessed on 2017/09/24, doi:10.14470/PK615318). 564 Picks, magnitudes and event hypocenter were taken from Sippl et al. (2018). Data pro-565 cessing and figure production were mainly performed using Python3.5.1 (python.org) and 566 packages IPython4.2.0 (Pérez & Granger, 2007), NumPy (Walt et al., 2011), Matplotlib 567 (Hunter, 2007), ObsPy (Beyreuther et al., 2010) and SciPy (Virtanen et al., 2020). Some 568 figures were refined using Inkscape (inkscape.org). 569 Results from this study are summarized in a table described and made available 570

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in the electronic supplement.

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Supplemetary Materials for Stress Drop Variations in the Region of the 2014 $M_W 8.1$ Iquique Earthquake, Northern Chile

J. Folesky¹, J. Kummerow¹, S.A. Shapiro¹ ¹ Freie Universität Berlin, Department of Geophysics, Berlin, Germany Corresponding author: jonas.folesky[at]geophysik.fu-berlin.de

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Figure S 1: Different bandpass filters lead to different cutoff frequencies which impact the estimated corner frequency value and thus influence the resulting stress drop estimates. We test three filters 1.) 0.8Hz highpass, 2.) 0.8-40Hz bandpass, and 3.) 0.8-20Hz bandpass. The figure shows the apparent cut-off frequencies for each filter. It also shows the shift of individual f_c values introduced by the filter choice. Based on this figure we chose the 0.8-40Hz bandpass filter and limit the corner frequency estimates that are interpreted in this paper to events with M>2.5.



Figure S 2: Isolines of constant stress drop for different magnitudes and expected corner frequencies. The figure was computed based on Equation 4 in the manuscript. The input parameters are k=0.32 and vs=3900m/s. The vertical line is drawn at 20Hz which is half the upper bandpass filter corner (40Hz). Following this plot, the corner frequencies for all events with magnitudes M>2.5 are expected to be resolvable. Only high stress drop event (sd>10 MPa) in the range 2.5 < M < 3 will be affected by the upper cuttoff limit. We therefore exclude such events where $f_c > 20 Hz$ (cf. Figure 11 main manuscript) Deselecting these events, however, appears to have an impact on the estimated scaling relation as discussed in the Results and Discussion section.



Figure S 3: Selected S phase windows for the same event as shown in Figures 3,4 & 5 from the main manuscript. On the left, the target event is shown; on the right, the EGF partner with the smaller magnitude. The utilized time windows are highlighted in grey.



Figure S 4: Left: S phase velocity spectra of the event pair shown in Figure S 3 and corresponding noise spectra. Center: The spectral ratio and the Boatwright spectral model fit. Right: Station-wise corner frequencies with median value. Station sorting is north to south. A corner frequency of 4.0 Hz is estimated.



Figure S 5: Average velocity spectrum of S phase based spectra (Figure S 4). The stress drop value in the figure is preliminary. The correction is made after learning the k-ratio from Figure 2 main manuscript. The given value has to be corrected with a factor of 0.8 which yields a stress drop of $\Delta \sigma = 2.3$ MPa.



Figure S 6: Average velocity spectrum of P phase based spectra similar figure to Figure 5 from the main manuscript. Here, in contrast, the Brune type spectral model was used for fitting. Note that the characteristic shape of the spectrum is poorer described by the Brune type curve shape. This is the case for the great majority of events in our data set. We therefore decided to base our analysis on fitting the Boatwright model in order to obtain the corner frequencies.

2010226T160801.0700Z M = 3.059 2010226T161853.7500Z



Figure S 7: P phase velocity traces for another main and EGF event.



Figure S 8: Velocity spectra, spectral ratios and estimated corner frequencies.

2010226T160801.0700Z M = 3.059 2010226T161853.7500Z



Figure S 9: Same as Figure S 7 but for S phase.



Figure S 10: Same as Figure S 8 but for S phase.



Figure S 11: Average spectral ratio for the traces shown in Figure S 8 and corresponding fit with corner frequency and stress drop estimate.



Figure S 12: Average spectral ratio as in Figure S 11 but fit with Brune spectral model. The curve shape does not fit as well a as the Boatwright model.



Figure S 13: Same as Figure S 11 for S phase. As explained above the stress drop has to be corrected with a factor of 0.8, yielding $\Delta \sigma = 0.51$.



Figure S 14: P wave velocity spectra, spectral ratios and estimated corner frequencies for one more exemplary event.



Figure S 15: Corresponding average velocity spectrum for the event from Figure S 14.



Figure S 16: P wave velocity spectra, spectral ratios and estimated corner frequencies for one more exemplary event.



Figure S 17: Corresponding average velocity spectrum for the event from Figure S 16.



Figure S 18: Stress drop distribution averaged on a regular grid, similar to Figure 8 but showing only events that occurred **before the main Iquique event.**



Figure S 19: Stress drop distribution averaged on a regular grid, similar to Figure 8 but showing only events that occurred **after the main Iquique event.**



Figure S 20: Stress drop distribution averaged on a regular grid, similar to Figure 8 but showing only events that occurred in the two weeks before the main Iquique event.



Figure S 21: Stress drop distribution averaged on a regular grid, similar to Figure 8 but showing only events that occurred in the four weeks after the main Iquique event.



Figure S 22: Influence of smoothing [Konno and Ohmachi, 1998] on the estimated corner frequency. Displayed are ten realizations of the test. On the left, the input spectra (black), the spectra with noise (grey) and the smoothed spectra (brown) of the target and of the EGF event are shown. On the right, the corresponding spectral ratios are shown with their fits, respectively. The input and output parameters are displayed above the plots. The smoothing operator has only a minimal impact on the decrease of the estimated corner frequency. We conclude that it is reasonable to use the smoothing to stabilize the spectral ratio approach with the real data.

Influence of Smoothing on the Corner Frequency Estimates

We test the influence of the Konno-Omachi smoothing on the estimated corner frequency. For this, the spectra of an EGF pair are simulated using the Boatwright spectral model with input parameters Ω_1 , fc_1 , Ω_2 , fc_2 in the range of typical values from the real data. White random noise is added such that the noise amplitude is stable over all frequencies. Noise range is ± 0.5 times the model amplitude of the smaller event. The spectra are then smoothed using the Konno- Ohmachi smoothing function from Obspy, an implementation of the approach of Konno and Ohmachi, 1998. Next, the ratio of the two spectra is computed and the data is fitted using the trust region reflective method from scipy curve-fit. In Figure S 22, ten exemplary event pair curves are shown. The procedure is iterated for different fc_1 values with 1000 runs for each tested corner frequency. The results, shown in Table S 1, demonstrate that the input parameters are recovered reliably. The standard deviation values are in the range of 15%. A minimal systematic shift towards smaller values for fc_1 is seen. We conclude that the smoothing is applicable.

fc_{in}	fc_{out}	fc_{std}
4	4.0	0.7
7	6.9	0.9
10	9.8	1.2
14	13.5	1.9

Table S 1: Results of synthetic smoothing tests for 1000 iterations using varying input values for the corner frequency fc_1 in Hz. All other inputs are fixed $(\Omega_1 = 100, fc_1 = var, \Omega_2 = 10, fc_2 = 25).$



Figure S 23: Variation of event magnitude with time. The figure shows the same time intervals as used for the temporal stress drop variation (Figure 10 main manuscript). The three vertical grey lines in the bottom panel denote the origin times of the $M_W 6.6$ foreshock, the $M_W 8.1$ mainshock, and the $M_W 7.6$ aftershock. In both panels the median magnitude of the entire result ensemble $(M_W = 3.04)$ is underlain as a grey line. Note the principally similar behavior of the curves compared to the stress drop curves in Figure 10 of the main manuscript. The shapes of the two curves show similarity indicating a correlation of event moment magnitude and stress drop which is substantiated in Figure 11 of the main manuscript.



Figure S 24: Scaling of stress drop with seismic moment. The black line and dots are the original values as depicted in Figure 11. Using a linear regression the gradient of $\varepsilon_1=0.51$ was estimated (black line, see main manuscript). Blue dots show stress drops with a removed gradient, i.e., a forced removal of moment dependency. The regression then yields $\varepsilon_1=0$ (blue line). By producing such a corrected data set we are able to test, if the spatio-temporal variability (Figures S 25 and S 26) is based predominantly on moment variability or is a separate signature.



Figure S 25: Stress drop variation with time similar to Figure 10. The moment dependency of the stress drop values was removed as explained in Figure S 24 in order to test if the temporal variability of stress drop is caused by variations of the seismic moment distribution. Note that the overall stress drop variation pattern remains similar to the original results in Figure 10. For example, we recognise a rise of stress drop values prior to the Iquique mainshock (bottom plot, second vertical line) and a gradual decrease afterwards. The range of variability, however, is decreased, indicating that a coinciding effect of both stress drop variation and moment variation are present to obtain the original stress drop variability from Figure 10.



Figure S 26: Stress drop variation in four sections. The figure is similar to Figure 9 in the main manuscript but it shows the corrected stress drop values from Figure S 24. Note that the curves are very similar to those in the original figure but that the overall range of variation is reduced. This indicates that there is stress drop variation and moment variation who both contribute to the resulting stress drop as reported in the original figure.

Velocity model at approx 20°S



Figure S 27: S phase velocity model slice at 20°S taken from Bloch et al. 2014.

Description of Resulting Stress drop Table

File name: stress_drop_tbl_NChile.txt

Columns are: Event origin time, latitude, longitude, depth, moment magnitude, corner frequency, stress drop, number of contributing data traces, internal ID.

Origin time, latitude, longitude, depth are taken from Sippl et al. 2018. Moment magnitudes are taken from Münchmeier et al. 2020.

Note that the internal ID can occur twice. First occurrence is the P phase, second is the S phase based estimate.

Important! Note that P phase based stress drops have been computed with $k_p=0.32$ and S phase based stress drop estimates have been computed with $k_s = 0.276$, resulting from the empirical k-ratio obtained in Figure 2, main manuscript.

The table contains also stress drops estimates that lie beyond the defined resolution limits (M<2.5 and $1 \le f_c \le 20Hz$) which are shown in grey in Figure 11 main manuscript.