# The mechanical response of a magma chamber with poroviscoelastic crystal mush

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#### Abstract

Improved understanding of the impact of crystal mush rheology on the response of magma chambers to magmatic events is critical for better understanding crustal igneous systems with abundant crystals. In this study, we extend an earlier model by (Liao et al, 2018) which considers the mechanical response of a magma chamber with poroelastic crystal mush, by including poroviscoelastic rheology of crystal mush. We find that the coexistence of the two mechanisms of poroelastic diffusion and viscoelastic relaxation causes the magma chamber to react to a magma injection event with more complex time-dependent behaviors. Specifically, we find that the system's short-term evolution is dominated by the poroelastic diffusion process, while its long-term evolution is dominated by the viscoelastic relaxation process. We identify two post-injection timescales that represent these two stages and examine their relation to the material properties of the system. We find that better constraints on the poroelastic diffusion time are more important for the potential interpretation of surface deformation using the model. We also find that the combination of the two mechanisms causes magma transport to reverse direction in the system, which would successively expose crystals to magma with different chemical compositions.

## The mechanical response of a magma chamber with poroviscoelastic crystal mush

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#### Key Points:

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8	• Features of magma chamber deformation with poroviscoealstic crystal mush are
9	examined using a mechanical model
10	• Coexistence of poroelastic diffusion and viscoelastic relaxation causes non-monotonous
11	evolution in pressure, stress, and magma transport
12	• The evolution of magma chamber is described by two characteristic time scales
13	depending on the material properties

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#### 14 Abstract

Improved understanding of the impact of crystal mush rheology on the response of magma 15 chambers to magmatic events is critical for better understanding crustal igneous systems 16 with abundant crystals. In this study, we extend an earlier model by Liao et al. (2018) 17 which considers the mechanical response of a magma chamber with poroelastic crystal 18 mush, by including poroviscoelastic rheology of crystal mush. We find that the coexis-19 tence of the two mechanisms of poroelastic diffusion and viscoelastic relaxation causes 20 the magma chamber to react to a magma injection event with more complex time-dependent 21 behaviors. Specifically, we find that the system's short-term evolution is dominated by 22 the poroelastic diffusion process, while its long-term evolution is dominated by the vis-23 coelastic relaxation process. We identify two post-injection timescales that represent these 24 two stages and examine their relation to the material properties of the system. We find 25 that better constraints on the poroelastic diffusion time are more important for the po-26 tential interpretation of surface deformation using the model. We also find that the com-27 bination of the two mechanisms causes magma transport to reverse direction in the sys-28 tem, which would successively expose crystals to magma with different chemical com-29 positions. 30

### Background: magma chamber model with poroelastic/viscoelastic mush

Petrological studies and thermodynamic models have long indicated that crustal 33 magmatic reservoirs (i.e., magma chambers) contain an abundance of crystal mush, where 34 'mush' refers to a system with melt contained in a framework of crystals (Cashman et 35 al., 2017). In recent decades, many research efforts have been devoted to understand-36 ing how crystal mush evolves and interacts with magma, using principles in thermody-37 namics, geochemistry, and geophysics. These models demonstrate the importance of crys-38 tal mush in a magma chamber's thermal and chemical evolution, as well as in some phys-39 ical processes such as the segregation of a liquid phase (Sparks & Cashman, 2017: Bach-40 mann & Huber, 2016; Singer et al., 2018; McKenzie, 2011, e.g.,). However, fewer stud-41 ies have evaluated the impact of crystal mush on magma chamber deformation, pressur-42 ization, stress evolution in the host rocks and surface deformation (Gudmundsson, 2012; 43 Liao et al., 2018). Liao et al. (2018) demonstrated that crystal mush can significantly 44 alter the response of a mushy chamber to magma injection events relative to the con-45 ventional mush-less, fluid-filled chamber. The model examined two possible rheologies 46 of crystal mush, poroelasticity and viscoelasticity, which are two end members of a more 47 general rheology of poroviscoelasticity. Liao et al. (2018) showed that poroelasticity and 48 viscoelasticity cause similar features in the magma chamber's post-injection evolution 49 (e.g., post-injection pressure decrease and stress increase), but did not examine how the 50 chamber behaves when poroelastic and viscoelastic mechanisms coexist. Here, we expand 51 on the poroelastic/viscoelastic model in Liao et al. (2018) to explore the effects of poro-52 viscoelastic mush on the response of a magma chamber to a magma injection event and 53 the resulting ground deformation. 54

#### <sup>55</sup> 2 Magma chamber model with poroviscoelastic mush in a half-space

For ease of comparison with previous mechanical magma chamber studies (Dragoni & Magnanensi, 1989; Karlstrom et al., 2010; McTigue, 1987; Segall, 2016; Liao et al., 2018, e.g.,), we adopt the same spherical geometry of the poroelastic chamber model as Liao et al. (2018) shown in Figure 1a. The magma chamber consists of a three-dimensional spherical core of liquid magma within a shell of poroviscoelastic mush with pre-injection porosity  $\phi_o$ . The magma chamber is hosted in a half space of linear elastic crust with a traction-free upper surface. We approximate the surface deformation in vertical and



Figure 1. (a) Geometry of the mushy magma chamber model (adapted from (Liao et al., 2018)), with several important quantities marked including: core pressure  $P_l$ , pore pressure  $P_f$ , tensile stress  $\sigma^{\theta\theta}$ , force balance on the two interfaces, and transport of magma in the mush region (red curved arrows). The chamber is at depth d from a free surface with radius  $R_o$  and liquid core radius  $r_o$ . (b)Accumulated amount of injected magma  $M_{inject}$  (y axis on the right) and injection rate  $r_{inject}$  (y axis on the left) as functions of time,  $t_{inj}$  is the length of the injection. The shaded area indicates the syn-injection period  $0 \le t \le t_{inj}$ .

horizontal directions following the same approach used in earlier studies (Segall, 2016,
 2019; McTigue, 1987).

<sup>65</sup> We assume a simplified magma injection event, where magma enters into the liq-<sup>66</sup> uid core at a constant injection rate during the injection period  $0 \le t \le t_{inj}$  (Figure 1b), <sup>67</sup> leading to the accumulated mass of injected magma  $M_{inject} = \frac{t\delta M}{t_{inj}}$  for  $t \le t_{inj}$  and <sup>68</sup>  $M_{inject} = \delta M$  for  $t > t_{inj}$ .

<sup>69</sup> During and after the injection, magma is allowed to flow across the liquid-mush in-<sup>70</sup> terface and within the mush, driven by the gradient of pore pressure  $P_f$ . The motion of <sup>71</sup> pore magma follows Darcy's law and mass conservation

$$\vec{q} = -\frac{\kappa}{\eta_f} \nabla P_f \tag{1a}$$

$$\frac{\partial m}{\partial t} + \nabla \cdot \left(\rho_f \vec{q}\right) = 0 \tag{1b}$$

<sup>72</sup> where  $\vec{q}$  is the Darcy velocity (positive values indicates the flow direction from magma <sup>73</sup> core to the chamber wall),  $\kappa$  is the permeability of the mush,  $\eta_f$  is the magma viscos-<sup>74</sup> ity, and  $\rho_f$  is the density of pore magma. The variation in fluid content is described by <sup>75</sup> the function m(r, t), which is defined as the change in pore fluid mass per un-deformed <sup>76</sup> volume of mush located at radius r (positive value m > 0 indicates that the pores in <sup>77</sup> the mush gain magma). The integration of m across the mush shell leads to the total <sup>78</sup> amount of magma transported between the liquid and the mushy region

$$M_{leak} = \int_{r_o}^{R_o} 4\pi r^2 m(r,t) \mathrm{d}r \tag{2}$$

where  $M_{leak}(t)$  is the accumulated amount of magma transported across the magma-mush boundary.  $M_{leak} > 0$  indicates that magma is flowing from the liquid core to the mushy shell (i.e., 'leaking'). We calculate the pressure change  $P_l$  in the liquid core upon mass injection assuming isothermal compression, which depends on the amount of injected magma  $M_{inject}$ , the amount of magma exchanged between the core and mush  $M_{leak}$ , and the volume change of the liquid core indicated by the radial displacement  $u_m(r_o)$  on the coremush interface. After linearization, the pressure change is (Liao et al., 2018):

$$P_{l}(t) = K_{l}\left(\frac{M_{inj}(t)}{M_{o}} - \frac{M_{leak}(t)}{M_{o}}\right) \left(1 - 3\frac{u_{m}(r_{o}, t)}{r_{o}}\right)$$
(3)

where  $K_l$  is the bulk modulus (1/compressibility) of the core and injected magma, and  $M_o$  is the pre-injection magma mass in the liquid core (see Appendix A). The injection causes the chamber to inflate, which leads to increased displacement  $\vec{u}_{rock}$  and elastic stress  $\sigma_{rock}$  in the surrounding crustal rocks, following the constitutive relation for linear elastic material

$$\boldsymbol{\sigma_{rock}} = (K_r - \frac{2}{3}\mu_r)\nabla \cdot \vec{u}_{rock}\boldsymbol{I} + \mu_r \left(\nabla \vec{u}_{rock} + \nabla \vec{u}_{rock}^T\right)$$
(4)

where  $K_r$  and  $\mu_r$  are the bulk and shear modulus of the host rock, respectively. It is worth 79 noting that both the stress component in the tensile direction  $\sigma^{\theta\theta}$  on the chamber-rock 80 boundary (Figure 1a) and overpressure increase during the inflation of the chamber, which 81 may cause the chamber's wall to rupture (Pinel & Jaupart, 2003; Grosfils, 2007; Cur-82 renti & Williams, 2014; Albino et al., 2010; Karlstrom et al., 2010; Gudmundsson, 2012; 83 Zhan & Gregg, 2019, e.g.,). In our current model, the rupture of magma chamber is omit-84 ted. We describe the deformation and stress in the crystal mush using a poroviscoelas-85 tic rheology, combining linear poroelasticity with a Maxwell viscoelastic model. The strain 86  $\boldsymbol{\epsilon}_m$ , stress  $\boldsymbol{\sigma}_m$ , variation in fluid content m and pore pressure  $P_f$  obey the constitutive 87 relations 88

$$\left(\frac{\partial \boldsymbol{\sigma}_m}{\partial t} + \frac{\mu_m}{\eta_m}\boldsymbol{\sigma}_m\right) - \frac{1}{3}\frac{\mu_m}{\eta_m}Tr(\boldsymbol{\sigma}_m)\mathbf{I} = 2\mu_m\frac{\partial \boldsymbol{\epsilon}_m}{\partial t} + \left(K_m - \frac{2}{3}\mu_m\right)\frac{\partial Tr(\boldsymbol{\epsilon}_m)}{\partial t}\mathbf{I} - \alpha\frac{\partial P_f}{\partial t}\mathbf{I}$$
(5a)

$$m = \rho_f \alpha \left( Tr(\boldsymbol{\epsilon}_m) + \frac{\alpha}{K_u - K_m} P_f \right)$$
(5b)

where  $K_m$  is the bulk modulus of the crystalline framework (i.e., drained modulus), and 89  $K_u$  is the bulk modulus of the crystal-fluid ensemble (i.e., undrained modulus).  $\alpha$  is the 90 poroelastic constant (also known as Biot constant) with a value from 0 to 1, determined 91 by the strength of the crystalline framework relative to that of the single crystal (represented by its bulk modulus  $K_s$ ) as  $\alpha = 1 - \frac{K_m}{K_s}$ . We assume that the crystalline net-92 93 work itself is weak compared to the single crystals, thus  $K_m \ll K_s$ , leading to a large 94  $\alpha$ . We use  $\alpha = 0.9$  for the rest of the study. The viscoelastic relaxation of the crystalline 95 matrix is determined by its rigidity  $\mu_m$  and viscosity  $\eta_m$ . We can verify that the poroe-96 lastic and viscoelastic rheologies are two end members of the poroviscoelastic rheology: 97 when matrix viscosity  $\eta_m \to \infty$ , (5) reduces to linear poroelasticity (Cheng, 2016); when 98 pore pressure is decoupled from the stress (i.e.,  $\alpha = 0$ ), (5) becomes the classical Maxwell 99 formulation (Segall, 2016; Jellinek & DePaolo, 2003). In the model, we assume that the 100 viscous relaxation of the mush network primarily occurs in the shear component, hence 101 omitting the compaction effect. The deformation in the host rocks and the mush shell 102 obey quasi-equilibrium condition 103

$$\nabla \cdot \boldsymbol{\sigma}_{m,rock} = 0 \tag{6}$$

and boundary conditions,

$$P_l + \sigma_m^{rr}(r_o) = 0 \tag{7a}$$

$$P_l - P_f(r_o) = 0 \tag{7b}$$

$$\sigma_m^{rr}(R_o) - \sigma_{rock}^{rr}(R_o) = 0 \tag{7c}$$

$$\vec{u}_m(R_o) - \vec{u}_{rock}(R_o) = 0 \tag{7d}$$

$$\frac{\partial P_f}{\partial r}(R_o) = 0 \tag{7e}$$

$$u_{rock}(r \to \infty) = 0 \tag{7f}$$

which prescribes force balance, continuity (in displacement and fluid pressure) at both the magma-mush and mush-rock boundaries, and a chamber wall impermeable to the pore magma. The above constraints determine the unique time-dependent solutions, which are calculated using Laplace transform (see Appendix A). We follow earlier studies to approximate the surface deformation resulting from the deformation of a spherical chamber (McTigue, 1987; Segall, 2016, 2019)

$$u_{z}(\rho,t) = -\frac{\sigma_{m}^{rr}(R_{0},t)}{\mu_{r}} \frac{R_{0}^{3}}{d^{2}} \frac{1-\nu}{\left(\frac{\rho^{2}}{d^{2}}+1\right)^{\frac{3}{2}}} u_{\rho}(\rho,t) = -\frac{\sigma_{m}^{rr}(R_{0},t)}{\mu_{r}} \frac{R_{0}^{3}}{d^{2}} \frac{1-\nu}{\left(\frac{\rho^{2}}{d^{2}}+1\right)^{\frac{3}{2}}} \frac{\rho}{d}$$

$$\tag{8}$$

where  $u_z$  and  $u_\rho$  are the vertical and horizontal displacement on the surface z = 0, measured at a radial distance  $\rho$ ;  $\nu$  is the Poisson's ratio of the elastic crust,  $\sigma_m^{rr}$  is the radial component of stress at the chamber-crust interface. Earlier works demonstrated that when the depth of the magma chamber d is modestly larger than the chamber's radius  $d/R_0 \geq$ 2, (8) provides good estimations for the deformation on the surface (Segall, 2016). In our study, we assume  $d/R_0$  between 3 to 10 for precise approximation of the ground deformation. Because the poroviscoelastic mush is subjected to two different mechanisms (poroelastic diffusion and viscoelastic relaxation), we identify two timescales that represent the two mechanisms respectively (see Appendix A)

$$\tau_{diffusion} = \frac{R_o^2 \eta_f}{\kappa} \frac{\alpha^2 \left(K_u + \frac{4}{3}\mu_m\right)}{\left(K_u - K_m\right) \left(K_m + \frac{4}{3}\mu_m\right)} \tag{9a}$$

$$\tau_{relaxation} = \frac{\eta_m}{\mu_m} \tag{9b}$$

where  $\tau_{diffusion}$  is the poroelastic diffusion time and  $\tau_{relaxation}$  is the viscoelastic re-104 laxation time. We verify that the crystal much is poroelastic when  $\tau_{relaxation} = \infty$ , and 105 viscoelastic if  $\tau_{diffusion} = \infty$ . Given the uncertainties in parameters such as much per-106 meability, crystalline rigidity and viscosity, magma viscosity and compressibility,  $\tau_{relaxation}$ 107 and  $\tau_{diffusion}$  can have a wide range of values. For example, the poroelastic diffusion 108 time  $\tau_{diffusion}$  ranges from 6 days to 160 years assuming a magma chamber with 1km 109 radius and parameters similar to those used in Liao et al. (2018) and others ( $\alpha = 0.9$ , 110  $\mu_m^o = 1$  GPa,  $K_f = 1$  GPa,  $\kappa \in [10^{-10}, 10^{-8}]m^2$ , and  $\eta_f \in [10^1, 10^3]$  Pa.s). Further, 111 assuming a crystalline viscosity similar or smaller than heated rock  $(\eta_m \in [10^{16}, 10^{18}])$ 112 Pa.s), the resulting viscoelastic relaxation time  $\tau_{relaxation}$  ranges from 4 months to 30 113 years (Segall, 2016; Cheadle et al., 2004; McKenzie, 2011). Below, we choose the case 114 of a poroviscoelastic mush subjected to both mechanisms with comparable time scales 115  $\tau_{diffusion} = \tau_{relaxation}$  to illustrate the basic features of a poroviscoelastic mushy cham-116 ber. 117

It is worth noting that, although the current model fills the gap in rheology assumed in Liao et al. (2018), many assumptions are still made to simplify the problem. These assumptions, including the spherical geometry, radial symmetry in magma chamber deformation, homogeneity in crystal mush distribution, and neglected thermal effects could
all affect how a more realistic mushy magma chamber reacts to magma injection, and,
while beyond the scope of this study, should be examined and evaluated in future studies.

#### 3 Model results

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Similar to poroelastic or viscoelastic mush, the poroviscoelastic mush causes the magma chamber and its surrounding crust to continue evolving after the injection has stopped, as opposed to a fluid chamber that reaches steady state as soon as the injection ends (Figure 4). We find that the time-dependent evolution of the poroviscoelastic mushy chamber is, at different times, dominated by either poroelastic diffusion or viscoelastic relaxation. Below, we examine the features of deformation, pressure, stress, and magma transport in both stages.

#### 3.1 Syn- and post- injection evolution of magma chamber with poroviscoelastic mush shell

We examine time-dependent magma chamber deformation during three stages: syn-135 injection, shortly after the injection, and long the after the injection. During the syn-136 injection period, magma is added into the liquid core at a constant rate (shaded area in 137 Figure 1b), increasing the pressure in the core magma (Figure 4a), and pushing both the 138 magma-mush boundary at  $r = r_o$  and the mush-rock boundary at  $r = R_o$  outward 139 (Figure 3a). The expansion of the whole chamber causes the tensile stress in the rock 140 surrounding the chamber and ground deformation to increase with time (Figure 4b, c). 141 During the syn-injection period, pressure in the liquid core always exceeds the pore pres-142 sure in the mush shell. As a result, some magma in the liquid core flows into the mush 143 (Figure 5a), increasing the pore pressure in the mush (See Figure B2 in Appendix B). 144 The syn-injection period ends at  $t = t_{inj}$ , when the injection rate drops to 0. At the 145 end of the injection, a fluid pressure gradient remains that sustains magma flow from 146 the core fluid into the mush. 147

The short post-injection period begins when the injection stops, at  $t = t_{inj}$ . Dur-148 ing this period, the evolution of the deformation is similar to that of a chamber with porce-149 lastic mush (see Figure 3b in Liao et al. (2018)). Without more magma injection, the 150 fluid core loses magma due to porous flow into the mush, causing the pressure in the liq-151 uid core to decrease. The liquid-mush boundary retracts inward and the liquid core shrinks 152 in response to the decreasing core pressure and mush expansion (Figure 5b, Figure 4a, 153 Figure 3b). Although viscous relaxation also occurs during this period, it is not strong 154 enough to noticeably deviate the evolution of the system from that of a poroelastic cham-155 ber. Because of these qualitative similarities, we consider the short time period post-injection 156 evolution to be dominated by the poroelastic diffusion mechanism (middle panel in Fig-157 ure 2). 158

With time, the effect of viscoelastic relaxation becomes more apparent – as the poroe-159 lastic effects diminish – and the system begins to show features similar to those displayed 160 by a purely viscoelastic mushy chamber. During this period, the viscoelastic relaxation 161 causes outward creeping and compression of the whole mush shell (Figure 3c), revers-162 ing the motion of the previously retracting liquid-mush boundary and pushing it out-163 ward again (Figure 2b). The outward movement of the liquid-mush boundary causes the 164 volume of the liquid core to expand, and the pressure in it to further decrease (Figure 4a). 165 The outward creeping of the mush-rock boundary causes the tensile stress in the host 166 rock and ground deformation to continue increasing (Figure 4b, Figure 8a). Eventually, 167 the liquid core pressure becomes less than the pore pressure in the adjacent mush due 168 to the loss of core magma and the expansion of the core. This reverses the pressure gra-169



**Figure 2.** Cartoon illustration of the three stages in the dynamic evolution of a mushy magma chamber: syn-injection stage, poroelastic diffusion-dominated stage, and viscoelastic relaxation-dominated stage. Grey arrows indicate the direction of the radial displacement of the magma-mush and mush-rock boundaries, and red arrows show the direction of magma transport. Illustration of pore magma transport and their possible chemical signatures are shown in the zoom-in panels. The deformation dominated by poroelastic diffusion is consistent with the evolution shown in Figure 3(b), and the viscous relaxation-dominated regime is consistent with Figure 3(c).



Figure 3. Displacement in the poroviscoelastic mush shell during and after injection. The thickness of the mush shell is half of the total chamber radius ( $r_o$ =  $R_o/2$ ) with equal relax- $= \tau_{diffusion}$ . A total amount of magma  $\delta M = 0.02 M_o$ ation and diffusion times  $\tau_{relaxation}$ is injected for the duration of  $t_{injection}$ =  $\tau_{diffusion}/10$ . Left panel shows the displacement  $u(r)/R_o$  (normalized by the chamber radius) as a function of radial position r during the injection  $0 \leq t \leq t_{injection}$ , where the black dash line indicates the displacement profile at the end of the injection  $t = t_{injection}$ ; middle panel shows the displacement during a short time period after the injection  $t_{injection} \leq t \leq 4t_{injection}$ , where the black dash line and black solid line show the profile at  $t = t_{injection}$  and  $t = 4t_{injection}$ , respectively; right panel shows the displacement for longer period after the injection  $t > 4t_{injection}$ , where the black solid line indicates the profile at  $t = 4t_{injection}$ . The left and middle panels are qualitatively similar to the evolution of a poroelastic shell (see Figure 3 in Liao et al. (2018)). The poroelastic dominated and viscoelastic dominated deformations are also shown in cartoon illustration in Figure 2. Other parameters include  $\alpha = 0.9, r_o/R_o = 1/2, K_f/\mu_r = 0.5, K_l/\mu_r = 0.1, K_s/\mu_r = 5/3, \mu_m/\mu_r = 1/2, \phi_o = 0.2.$ 

dient direction at the magma-mush boundary resulting in porous flow from the mush into 170 the core (Figure 5c), returning most of the previously leaked magma back into the core 171 at a slower speed (Figure 6). This stage, where the magma chamber is dominated by vis-172 coelastic relaxation, lasts until the system reaches a new steady state. Although the de-173 crease in chamber pressure and increase in tensile stress of the crust during this period 174 are similar in sign to the poroelastic diffusion dominated stage, the rate of change in these 175 quantities is much lower, as is reflected by a nearly indiscernible strain rate at the wall 176 of the chamber (Figure B1 in Appendix Appendix B) and slow increase in ground ele-177 vation (Figure 8). 178

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#### 3.2 Timescales in post-injection evolution

Compared to the poroelastic case where one timescale can be identified to describe 180 its post-injection evolution (Liao et al., 2018), a chamber with poroviscoealstic mush re-181 quires two timescales to characterize the non-monotonic changes in pressure, stress, and 182 magma transport (Figure 4 and 6). To determine the short-period evolution time  $t_{post}^{short}$ 183 we numerically calculate the time it takes for the pressure gradient at the magma-mush 184 interface to reverse, and for magma to begin to leak back into the liquid core (Figure 6b) 185 after a sudden injection. To determine the long-period evolution time  $t_{post}^{long}$ , we calcu-186 late the time it takes for the system to approach a final steady state after injection, us-187 ing the same analytical approach in Liao et al. (2018) for a poroelastic/viscoelastic cham-188 ber. Following a sudden injection at t = 0, the evolution of the system during time pe-189 riod  $0 < t \leq t_{post}^{short}$  is consistent with a poroelastic diffusion dominated stage, repre-190 sented by a relatively rapid decrease in chamber's pressure  $P_l$ , a rapid increase in ten-191 sile stress  $\sigma^{\theta\theta}$ , and core-to-mush magma transport. Over the time period  $t_{post}^{short} < t \leq$ 192



Figure 4. Syn- and post-injection evolution of liquid core fluid pressure  $P_l$  (panel a), and tensile stress  $\sigma^{\theta\theta}$  (panel b) as functions of time, with initial short period evolutions zoomed in insert panels. Purple broken line corresponds to a mushless liquid chamber with the mushy chamber's liquid core radius  $r_0 = 0.5R_0$ ; blue solid lines, black dotted lines, and black solid lines correspond to a mushy chamber with poroviscoelastic, poroelastic, or viscoelastic mush shell respectively. Other parameters are the same as in Figure 3.

 $t_{post}^{long}$ , the system behaves consistently with a viscoelastic relaxation dominated stage, characterized by a slower decrease in chamber's pressure, slow increase in tensile stress, and mush-to-core magma transport. Over the time period  $t > t_{post}^{long}$ , the system remains dominated by viscoelastic relaxation, although its evolution is slow enough to be regarded as approaching a new steady state.

We found that both  $t_{post}^{short}$  and  $t_{post}^{long}$  depend on the material properties (e.g.,  $\tau_{diffusion}$ and  $\tau_{relaxation}$ ) and geometry of the system (e.g.,  $r_o/R_o$ ). Although  $\tau_{diffusion}$  and  $\tau_{relaxation}$ 198 199 both affect  $t_{post}^{short}$  and  $t_{post}^{long}$ , it is clear that the short-period evolution time  $t_{post}^{short}$  is more 200 sensitive to  $\tau_{diffusion}$ ; whereas the long-period evolution time  $t_{post}^{long}$  changes more sen-201 sitively with  $\tau_{relaxation}$  (Figure 7). Considering that the early post-injection evolution of 202 the system corresponds to faster change and higher strain-rate, we consider it to be po-203 tentially more relevant to geophysical observations (e.g., deformation, seismicity), hence 204 constraining the value of  $\tau_{diffusion}$  is important for comparing the model to field data. 205 According to (9a),  $\tau_{diffusion}$  is determined by parameters with potentially large degrees 206 of uncertainty, such as the poorly constrained much permeability  $\kappa$ , and the magma vis-207 cosity  $\eta_f$ , which has a wide range of values depending on temperature, degree of crys-208 tallization, and chemical compositions. Reasonable variations in these parameters can 209 cause  $\tau_{diffusion}$  to vary across orders of magnitudes from days to hundreds of years. For 210 these reasons, better constraints on these parameters via petrological observations and 211 thermodynamic models are crucial for evaluating rheological models such as the one pro-212 posed here. It is also worth noting that the two post-injection timescales are defined based 213 on the evolution of magma chamber following a sudden injection, and can qualitatively 214 describe the behavior of a mushy chamber when the injection is much shorter than both 215  $\tau_{diffusion}$  or  $\tau_{relaxation}$ . For very long injection times (i.e., low injection rates), however, 216 the diffusion-dominated stage becomes very short, and the chamber would qualitatively 217 display characteristics of the relaxation-dominated stage soon after the injection (see Fig-218 ure B3 in Appendix Appendix B). 219



Figure 5. Darcy velocity of pore magma  $\vec{q}$  (radial component) in the poroviscoelastic mush shell, as a function of radial position r, during and after injection. The thickness of the mush shell is half of the total chamber radius  $(r_o = R_o/2)$  with equal relaxation and diffusion time  $\tau_{relaxation} = \tau_{diffusion}$ . A total amount of magma  $\delta M = 0.02M_o$  is injected for the duration of  $t_{injection} = \tau_{diffusion}/10$ . The velocity is normalized by velocity scale  $\kappa \mu_r / \eta_f R_o$ , where  $\kappa$  is the mush permeability,  $\mu_r$  is the crustal rock rigidity,  $\eta_f$  is the viscosity of pore magma, and  $R_o$ the radius of the chamber. Positive values of q indicate the magma flowing from the core to the mush, and negative values indicate flow from the mush into the core. Left panel corresponds to syn-injection evolution  $0 \le t \le t_{injection}$ , where the black dash line indicates the velocity profile at the end of the injection  $t = t_{injection}$ ; middle panel shows the pore magma velocity during a short time period after the injection  $t_{injection} \leq t \leq 5.4 t_{injection}$ , where the black dash line and black solid line show the profile at  $t = t_{injection}$  and  $t = 5.4 t_{injection}$ , respectively; right panel shows the velocity for longer period after the injection  $t > 5.4t_{injection}$ , where the black solid line indicates the profile at  $t = 5.4 t_{injection}$ . The poroelastic dominated and viscoelastic dominated pore magma flow direction are also shown in cartoon illustration in Figure 2. The region where q < 0 in the right panel indicates the change in flow direction of the pore magma, which corresponds to the onset of decrease in the amount of cumulated leaked magma (see Figure B2 in Appendix B for the amount of transported magma). Other parameters are the same as in Figure 3.



Figure 6. Post-injection short-term (insert panels) and long-term evolution of tensile stress (left) and leaked magma  $M_{leak}$  (right) from the liquid core to the shell following a sudden injection. Grey dashed lines indicate the two post-injection timescales  $t_{post}^{long}$  and  $t_{post}^{short}$  identified for the post-injection evolution.



Figure 7. Post-injection short-term evolution timescale  $t_{post}^{short}$  (right) and long-term evolution timescale  $t_{post}^{long}$  (left) shown as functions of viscoelastic relaxation time  $\tau_{relaxation}$  and poroelastic diffusion time  $\tau_{diffusion}$ . The long-term evolution time  $t_{post}^{long}$  is more sensitive to the change in viscoelastic relaxation time; the short-term evolution time is more sensitive to the change in poroelastic diffusion time.

#### 4 Implications and future studies

Our model allows to explore the consequences of magma injection in a chamber with a poroviscoelastic mush layer on some common observations made in magmatic systems. In this section we discuss two examples of implications of our model for geodesy and petrology. Although these predictions are highly generalized at this stage, they indicate the potential for future model development that incorporates more realistic and complex features of natural magmatic systems to provide novel ways to interpret volcano geophysical and petrological data.

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#### 4.1 Implication on the interpretation of ground deformation

One consequence of the existence of mush in a magma chamber is prolonged ground 229 deformation after the injection has ceased due to redistribution of pore magma and/or 230 relaxation of the crystalline framework. For example, a 1.5 km magma chamber at 4.5 231 km depth undergoing a one-year injection with a moderate rate of  $1.12m^3/s$  would ex-232 perience an additional 30mm of ground uplift (1/3 of total uplift), in the period of three 233 years after the injection has stopped (Figure 8a). For an injection at a constant rate, a 234 mushy chamber results in time-dependent changes in the rate of ground deformation dis-235 tinct from a liquid chamber hosted in elastic rock. Specifically, our mushy chamber model 236 predicts an increasing syn-injection ground uplift rate, and decreasing post-injection up-237 lift rate, such that the strain rate and uplift rate reach their maximum at the end of the 238 injection (Figure 8b). These characteristics (i.e., increasing then decreasing uplift rates 239 of ground deformation) have been observed at various volcanic systems, for example, at 240 Long Valley Caldera, Campi Flegrei, and Laguna del Maule (Le Mével et al., 2015). At 241 Laguna del Maule volcanic field in Chile, they are explained as consequences of time-varying 242 injection rates (Le Mével et al., 2016). While time-dependent injection rates driven by 243 magma supply dynamics from deeper reservoirs or mantle plumes are possible (Poland 244 et al., 2012; Bato et al., 2018, e.g.), the combination of injection, pore magma transport, 245 and relaxation in a mushy chamber provides an alternative explanation that corresponds 246 to many physical models which still typically consider injection rates to be constant or 247



Figure 8. Vertical surface uplift (panel a) and rate of surface uplift (panel b) as functions of time during and after injection, for a liquid chamber (purple broken lines) and a mushy chamber with either poroviscoelastic (blue solid lines) or viscoelastic (black solid lines) mush (diffusion and/or relaxation time  $\sim 10$  years). The center of the magma chamber is located at a depth of 4.5km, with a radius of 1.5km. The injection assumes a volumetric injection rate of  $1.12m^3/s$  for the duration of 1 year, indicated by black dash line in panel a. The rate of ground deformation has been smoothed using a piece-wise, low-pass Butterworth filter to eliminate numerical artifacts caused by the Laplace inversion algorithm.

decrease exponentially (Segall, 2016; Huppert & Woods, 2002; Biggs & Pritchard, 2017).
 The mushy chamber model provides an alternative explanation for such features, where
 the combination of injection, pore magma transport and relaxation modulate deforma tion rates.

Although the time-dependent features in ground deformation may suggest the ex-252 istence of a mushy chamber, the magnitude of ground deformation caused by a deform-253 ing mushy chamber is limited in its ability to constrain key parameters of the chamber 254 such as its volume, pressure, and likelihood to rupture. Similar to classical models, the 255 depth of the magma chamber d can be straightforwardly obtained from (8) by compar-256 ing the vertical and horizontal components of the displacement  $d = u_z \rho / u_\rho$  (Segall, 2019). 257 With d and the elastic properties of crustal rock constrained, the ground deformation 258 further constraints  $\sigma_m^{rr} V_0 \propto \Delta V$  (or  $P_l V_0$  if there is no mush,  $\Delta V$  is injected volume), 259 but can not constrain pressure/stress and chamber volume individually. We find that 260 when the depth d is fixed, the amplitude of ground deformation  $u_{\rho,z} \propto \Delta V \frac{R_o^3}{r^3}$ . There-261 fore the ground deformation increases with the volume ratio of mush and is independent 262 of the size of the chamber (Figure 9): for the same injection event, a large chamber with 263 50% mush and a small chamber with 50% mush cause the same ground deformation, and that a liquid chamber always causes smaller ground deformation than a mushy cham-265 ber, regardless of its size. On the other hand, the pressure and tensile stress depend on 266 both the volume ratio of mush and the total volume of the chamber. Therefore, a small 267 liquid chamber may cause smaller ground elevation compared to a large mushy cham-268 ber, but is more likely to erupt due to higher pressure and tensile stress. This non-uniqueness 269 poses a challenge to applying our forward models to interpret ground deformation data. 270 Combining ground deformation data with other geophysical measurements, such as seis-271 mic, electromagnetic, and gravimetry measurements, is necessary to provide constraints 272 on the volumes of liquid and mush, and to increase the applicability of models as pro-273 posed here (Magee et al., 2018; Ward et al., 2014). 274



Figure 9. (a) and (b) show vertical and horizontal displacement at the surface for different combination of burial depth d (km), mush volume fraction, and injected volume  $\Delta V$  ( $km^3$ ). The ground deformation increases with mush volume fraction, injected volume  $\Delta V$ , and decreases with burial depth d, but does not vary with the size of the chamber. (c)-(e) are cartoons illustrating three different magma chambers under the same magma injection. Tensile stress, chamber pressure, and ground deformation in the new steady state ( $t \rightarrow \infty$ ) are shown in all three cases (not to scale). Case (c) represents a liquid chamber with radius  $r_0$ ; case (d) represents a mushy chamber with total chamber radius  $r_0$ ; case (e) represents a mushy chamber with liquid core radius  $r_0$ . All three chambers are buried at the same depth d and subjected to the same amount of injected magma  $\Delta V$ . Cases (d) and (e) cause the same ground deformation as they have the same mush volume fraction, but cause different tensile stress and pressure.

#### 4.2 Implication on the interpretation of crystal zoning

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One implication of the poroviscoelastic magma chamber model for petrologic in-276 terpretations is the potential reversal of melt transport directions to produce chemical 277 zonation in phenocrysts via exposing crystals to pore magma with evolving chemical fin-278 gerprints (Figure 2, Figure 6b and Figure B2). Chemically zoned phenocrysts are seen 279 as sensitive recorders of magmatic conditions. A variety of processes are linked to zona-280 tion including changes in the temperature, composition, pressure, water content, and oxy-281 gen fugacity of the host magma (Ruprecht & Wörner, 2007, e.g.,) or by transport of crys-282 tals through gradients in physico-chemical properties in a zoned magma chamber (Ginibre 283 et al., 2002, e.g.,). Whereas simple zonation of a mafic core and more evolved rim (or 284 vice versa) are commonly explained by magma mixing events; more complex zonation, 285 including oscillatory zoning, require similarly complex physical mechanisms ((Perugini 286 et al., 2005; Ginibre & Wörner, 2007, e.g.,)). An example from the 2001 eruption of Shiv-287 eluch Volcano finds multiple phases with distinct zoning features ((Humphreys et al., 2006)). 288 Sieve textured Ab-rich plagioclase feldspars with overgrowths of An-rich rims are inter-289 preted to reflect the mixing of a hotter, more primitive melt with the existing evolved 290 melt. In the same eruption, oscillatory zoned plagioclase are observed that are interpreted 291 to reflect oscillations in pressure and pH2O resulting from unstable conduit flow during 292 ascent. A subset of oscillatory zoned plagioclase have patchy cores that are typically more 293 anorthitic and are thought to form from a more primitive melt than simple oscillatory zoned phenocrysts. 295

These interpretations of distinct mechanisms for zoning are well-supported and an-296 other explanation is not necessarily required; however, we postulate that similar zona-297 298 tion features could develop in phenocrysts due to transport of melt in and out of the mush zone. Oscillatory zoning, for example, could form near the melt-mush interface as crys-299 tals are washed by outward (e.g., more primitive, hotter) and inward (e.g., less primi-300 tive, cooler) melt. Sieve textured phenocrysts might be located further into the mush 301 zone, where only a larger injection event would allow a more primitive melt to encounter 302 the crystals, and which would be less subjected to significant changes in flow direction. 303 In addition to injection-induced pressure gradients, other processes such as vesiculation 304 and or gas loss may also allow melt transport through the mush producing 'in-place'zonation. 305 The potential to produce chemical zonation within magmatic mush merits further ex-306 amination including the physical processes of disaggregating the mush and the proba-307 bility of incorporating those crystals into the melt (Parmigiani et al., 2014, e.g.,), and 308 the examination of asymmetric zonation patterns (e.g., non-concentric) that might re-309 sult in a partially interconnected network of crystals. 310

#### 4.3 Future studies

Our current viscoelastic model serves as a foundation for understanding of how mush 312 rheology impacts the first-order mechanical responses of a magmatic reservoir, with as-313 sumed simplifications such as isothermal condition, radial symmetry, uniform material 314 properties, and simplified injection time series. As natural volcanic system are more com-315 plex, there is room for future refinement of the current model. Theses future studies will 316 yield a more thorough understandings of the role of crystal mush in magmatic reservoirs 317 with more complex features or under more realistic conditions, such as non-uniform (e.g., 318 radially varying) material properties (Degruyter & Huber, 2014), evolving magma-mush 319 boundary undergoing phase- and rheological transitions, as suggested by Karlstrom et 320 al. (2012), and more complex injection processes informed by field observations (Poland 321 et al., 2012; Bato et al., 2018, e.g.). Better constraints on the properties of crustal mag-322 matic system from improved geophysical observations (Kiser et al., 2018, e.g.,), and in-323 corporation of more complex features described above, will allow for a more realistic de-324 scription of the mechanical behaviors of mushy magmatic reservoirs and better interpre-325 tations on the observed geodetic and petrologic observations. 326

Recent studies focusing on the multiphase nature of crustal magmatic systems also 327 shed light on some potentially important physical processes that may be incorporated 328 or combined to our current model. In a recent study by Mittal and Richards (2019), the 329 two-phase nature of the hosting crust of the magma chamber was modeled using sim-330 ilar quantitative methods, with the additional incorporation of a thermal effect (i.e., a 331 thermal-poroviscoelastic description). In this study, gas percolation out of the magma 332 chamber was studied in detail, while the dynamics and deformation of the magma cham-333 ber itself was modeled in a simplified fashion (Mittal & Richards, 2019). Future imple-334 mentation of our current model with a thermal-poroviscoelastic rheology, combined with 335 a crustal-percolation model similar to Mittal and Richards (2019), could extend the one-336 phase description of the crustal system to a fully two-phase description extending from 337 within the magma chamber to the surface. 338

In geodynamic models, two-phase systems consisting of melt and rock, such as in 339 mid-ocean-ridges, upper mantle, and subduction zones, have been typically studies us-340 ing a two-phase fluid models, where compaction of the rock matrix plays an important 341 role in localizing the transport of the lighter, melt phase (McKenzie, 1984; Turcotte & 342 Morgan, 1992; Dymkova & Gerya, 2013; Montési & Zuber, 2002). In the current study, 343 the effect of compaction of the mush matrix is omitted while the mush is considered pri-344 marily as a solid phase in resting state with an infinitely large bulk viscosity. It is pos-345 sible that for a mush layer accumulating in chamber's floor and compacting under crys-346 tal settling, a scenario described by McKenzie (2011), could lead to a more prominent 347 effect from compaction and melt segregation. Future studies that relax the radial sym-348 metry condition and incorporate this compaction effect, in combination with chamber 349 deformation, will further extend our understanding on complex much rheology on the 350 responses of magmatic reservoirs and provide a potential link between magma segrega-351 tion and ground deformation processes. 352

#### 353 5 Summary

In this study, we extend a previous mechanical model by Liao et al. (2018) on mushy 354 magma chambers with poroelastic or viscoelastic mush, by incorporating a more gen-355 eral mush rheology of poroviscoelasticity. We subject the new mushy magma chamber 356 model to an external perturbation of a magma injection with constant injection rate for 357 a duration of time, and observe the similarities and differences caused by different mush 358 rheology on evolution of pressure, stress, magma transport, and surface elevation. We 359 found that the poroviscoelastic mush display both mechanisms of poroviscoelastic dif-360 fusion, and viscoelastic relaxation, and that the magma chamber displays features sim-361 ilar to both end members at different stages during its evolution in time. Based on these 362 features, we identify two characteristic timescales that describe the post-injection evo-363 lution of the poroviscoelastic mushy chamber: a short-term post-injection time  $t_{post}^{short}$  and a long-term post-injection time  $t_{post}^{long}$ . Over  $t_{post}^{short}$ , the chamber is dominated by poroe-lastic diffusion characterized by relatively rapid chamber pressure decrease, crustal ten-364 365 366 sile increase, and transport (i.e., leaking) of magma from the fluid region to the mush.  $t_{post}^{long}$  indicates the period dominated by viscoelastic relaxation, which is characterized 368 by relatively slow decrease in chamber pressure, increase in tensile stress, and inverse trans-369 port (i.e., leaking-back) of magma from the mush region to the fluid region. The two char-370 acteristic timescales are determined by material properties and geometry of the cham-371 ber, but the short-term timescale is more sensitive to the poroelastic diffusion time  $\tau_{diffusion}$ , 372 and the long-term timescale to the viscoelastic relaxation time  $\tau_{relaxation}$ . The features 373 of the post-injection evolution of a poroviscoelastic chamber indicate that the poroelas-374 tic diffusion mechanism, which causes higher rates of chamber deformation and strain, 375 is more likely to be relevant for potential interpretation of surface observations, while 376 the viscoelastic relaxation, which causes drastic change in the magma transport direc-377

- tion, is potentially relevant for interpreting petrological and geochemical evidence of crys-
- tal growth.

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#### <sup>541</sup> Appendix A Governing equations and solution method

The quantitative treatment of the equations of motions and boundary conditions follows closely (Liao et al., 2018). Specifically, we could obtain the poroviscoelastic solutions by transforming the poroelastic solutions in (Liao et al., 2018) under correspondence principle. The poroviscoelastic rheology can be alternatively expressed using Laplace transform

$$\widetilde{\boldsymbol{\sigma}_m} = (K_m - \frac{2}{3}\overline{\mu_m})\nabla \cdot \widetilde{\vec{u}_m}\boldsymbol{I} + \overline{\mu_m} \left(\nabla \widetilde{\vec{u}_m} + \nabla \widetilde{\vec{u}_m}^T\right) - \alpha \widetilde{P_f}\boldsymbol{I}$$
(A1a)

$$\widetilde{m} = \rho_f \alpha (\nabla \cdot \widetilde{\vec{u}_m} + \frac{\alpha}{K_u - K_m} \widetilde{P_f})$$
(A1b)

where the Laplace transform is defined as  $f(r,s) \equiv \int_0^\infty f(r,t)e^{-st} dt$ . The effect of viscous relaxation is reflected by a rigidity that varies with time (i.e., function of s under Laplace transform)

$$\widetilde{\mu_m} = \mu_m \frac{\eta_m s}{\eta_m s + \mu_m}$$

From the equilibrium condition  $\nabla \cdot \tilde{\boldsymbol{\sigma}} = 0 \rightarrow \nabla \left( (K_m + \frac{4}{3}\overline{\mu_m})\nabla \cdot \tilde{\vec{u}} - \alpha \widetilde{P_f} \right) = 0$ , we can define time-dependent function  $\zeta(t)$  such that its Laplace transform

$$\widetilde{\zeta}(s) = (K_m + \frac{4}{3}\overline{\mu_m})\nabla \cdot \widetilde{\vec{u}} - \alpha \widetilde{P_f}$$

Following steps in (Liao et al., 2018) and non-dimensionelize the system by length scale  $R_o$  (chamber radius), time scale  $\eta_m/\mu_m$  (relaxation time) and stress/pressure scale  $\mu_r$  (rock rigidity), the boundary values have the relation

$$\widetilde{P_f}\left(\frac{r_o}{R_o}\right) = \overline{a_1}\widetilde{m}\left(\frac{r_o}{R_o}\right) + \overline{a_2}\widetilde{\zeta} \tag{A2a}$$

$$\widetilde{u_m}\left(\frac{r_o}{R_o}\right) = \overline{b_1} \int_{\frac{r_o}{R_o}}^{1} r'^2 \widetilde{m}(r') \mathrm{d}r' + \overline{b_2} \widetilde{\zeta} + \widetilde{u_m}(1) \frac{R_o^2}{r_o^2} \tag{A2b}$$

$$\widetilde{\sigma_m^{rr}}\left(\frac{r_o}{R_o}\right) = \overline{c_1} \int_{\frac{r_o}{R_o}}^1 r'^2 \widetilde{m}(r') \mathrm{d}r' + \overline{c_2} \widetilde{\zeta} + \overline{c_3} \widetilde{u_m}(1) \tag{A2c}$$

$$\widetilde{\sigma_m^{rr}}(1) = \widetilde{\zeta} - 4 \frac{\overline{\mu_m}}{\mu_r} \widetilde{u_m}(1) \tag{A2d}$$

$$\widetilde{P}_{l} = \overline{d_{1}} \int_{\frac{r_{o}}{R_{o}}}^{1} r^{2} \widetilde{m}(r) \mathrm{d}r + \overline{d_{2}} \widetilde{\zeta} - \frac{3K_{l}R_{o}^{3}}{\mu_{r}r_{o}^{3}} \widetilde{u_{m}}(1) + \overline{f_{4}}$$
(A2e)

where  $\overline{f_4} = \frac{K_L}{\mu_r} \frac{\Delta M}{M_o} \frac{1}{s}$  (for instantaneous injection) or  $\overline{f_4} = \frac{K_L}{\mu_r} \frac{\Delta M}{M_o} \frac{1-e^{st_{inj}}}{s^2 t_{inj}}$  (for gradual injection), and the s-dependent coefficients  $\overline{a_1}, \overline{a_2}, \overline{b_1}, \overline{b_2}, \overline{c_1}, \overline{c_2}, \overline{d_1}, \overline{d_2}$  have the same forms as those defined in Appendix A.2.4 in (Liao et al., 2018) while substituting  $\overline{\mu}(s)$ for mush rigidity. Substituting (A2) into the boundary conditions and into Darcy's law, mass conservation, and equilibrium condition, we obtain (dimensionless) constraint on the fluid content  $\widetilde{m}$ 

$$\nabla^2 \widetilde{m} - \frac{\tau_{diffusion}}{\tau_{relaxation}} \frac{s\left(s + \frac{K_u}{K_u + \frac{4}{3}\mu_m^o}\right)}{\left(s + \frac{K_m}{K_m + \frac{4}{3}\mu_m^o}\right)} \widetilde{m} = 0$$
(A3)

and the boundary conditions

$$\frac{\partial \widetilde{m}}{\partial r}(r=1) = 0, \qquad \widetilde{a_1} \widetilde{m}(\frac{r_o}{R_o}) + \overline{h_o} \int \widetilde{m} r^2 dr = \overline{h1}$$

where  $\overline{h_0}$  and  $\overline{h_1}$  have the same form of  $h_0$  and  $h_1$  in §A.2.4 in (Liao et al., 2018) with  $\mu_m \to \overline{\mu_m}$ . Solving (A3) with the boundary conditions and using the relations between  $m, \vec{u}$  and  $P_f$  similar to those in (Liao et al., 2018), we can find the solutions for  $\tilde{m}$ 

$$\widetilde{m} = \frac{Ae^{r\sqrt{S_o}}}{\sqrt{S_o}r} + \frac{Be^{-r\sqrt{S_o}}}{\sqrt{S_o}r}$$
(A4)

with

$$S_o = \frac{\tau_{diffusion}}{\tau_{relaxation}} \frac{s\left(s + \frac{K_u}{K_u + \frac{4}{3}\mu_m^o}\right)}{\left(s + \frac{K_m}{K_m + \frac{4}{3}\mu_m^o}\right)}, \qquad A = \frac{\widetilde{h_1}S_o^{\frac{3}{2}}(\sqrt{S_o} + 1)e^{-\sqrt{S_o}}}{2\overline{g}}, \qquad B = \frac{\widetilde{h_1}S_o^{\frac{3}{2}}(\sqrt{S_o} - 1)e^{\sqrt{S_o}}}{2\overline{g}}$$

$$\overline{g} = \sqrt{S_o} \left( \frac{\overline{a_1} R_o}{r_o} S_o + \overline{h_0} \left( 1 - \frac{r_o}{R_o} \right) \right) \cosh\left( \sqrt{S_o} \left( 1 - \frac{r_o}{R_o} \right) \right) + \left( \left( \overline{h_0} \frac{r_o}{R_o} - \frac{\overline{a_1} R_o}{r_o} \right) S_o - \overline{h_0} \right) \sinh\left( \sqrt{S_o} \left( 1 - \frac{r_o}{R_o} \right) \right)$$

The Laplace transform of other quantities can all be obtained via (A4), such as core pressure, rock tensile stress and radial stress at the chamber's wall

$$\begin{split} \widetilde{\sigma_{rock}^{\theta\theta}}(1) &= -2\frac{\overline{f_4}}{\overline{g_2}} - 2\frac{\overline{g_1}}{\overline{g_2}} \int_{\frac{r_o}{R_o}}^1 \widetilde{m}r^2 dr \\ \widetilde{\sigma_m^{rr}}(1) &= \widetilde{\sigma_{rock}^{rr}}(1) = -2\widetilde{\sigma_{rock}^{\theta\theta}}(1) \\ \widetilde{\zeta} &= 2\left(4\frac{\overline{\mu_m}}{\mu_r} - 1\right)\widetilde{\sigma^{\theta\theta}} \\ \widetilde{P}_l &= \overline{a_1}\widetilde{m}\left(\frac{r_o}{R_o}\right) + \overline{a_2}\widetilde{\zeta} \end{split}$$
(A5)

Following (McTigue, 1987), we apply a first order correction to obtain surface deformation. The pressure-stress coupling in (McTigue, 1987) is here replaced by a stress-stress coupling at the chamber-crust interface, and the radial component of poroviscoelastic stress plays the role of a virtual pressure in the chamber, leading to the surface deformation (McTigue, 1987; Segall, 2016)

$$\widetilde{u_z}(\rho,0) = -\widetilde{\sigma_m^{rr}}(1)\frac{d}{R_0} \left(\frac{R_0}{d}\right)^3 \frac{1-\nu}{\left(\frac{\rho^2}{d^2}+1\right)^{\frac{3}{2}}}$$

$$\widetilde{u_\rho}(\rho,0) = -\widetilde{\sigma_m^{rr}}(1)\frac{\rho}{R_0} \left(\frac{R_0}{d}\right)^3 \frac{1-\nu}{\left(\frac{\rho^2}{d^2}+1\right)^{\frac{3}{2}}}$$
(A6)

where  $u_z$  and  $u_\rho$  are vertical and horizontal displacement on the surface (normalized by chamber radius  $R_0$ ) measured at distance  $\rho$  from the center of the chamber's projection,  $\nu$  is Poisson's ratio of the elastic crust. We numerically invert the Laplace solutions to obtain solutions using a matlab code shared on Mathworks File Exchange, which is based on the scheme proposed in (Abate & Whitt, 2006). The Laplace solution allows us to define the longest timescale in the system. Similar to (Liao et al., 2018), the Laplace solutions can be inverted using the Mellin inversion formula, which yields the solutions in real space as a superposition of exponentially decaying terms in the form of

$$A(r,t) = A_0(r) + A_1(r)e^{-t/\tau_1} + A_2(r)e^{-t/\tau_2} + \dots$$

where  $\tau_1$  is the largest decay period, and can be solved graphically given the parameters of the system. We use this timescale to determine the longest timescale in the system's post-injection evolution  $t_{post}^{long}$  (Liao et al., 2018).

#### 545 Appendix B Additional model results



Figure B1. Panel (a) and (b): post-injection short-term and long-term evolution for core pressure and mushy deformation for three cases (poroviscoelastic, poroelastic, and viscoelastic). Inset panels are zoom-in of the beginning period of the evolution, and grey broken lines indicate the two post-injection timescales  $t_{post}^{long}$  and  $t_{post}^{short}$ . Panel (c): tensile strain rate  $\dot{\epsilon}^{\theta\theta} = \dot{u}(R_o)/R_o$ at the wall of the chamber during and after the injection, for four different cases. For mushy chamber, the strain rate is highest at the end of the injection, and remains positive during shortterm post-injection evolution. During long-term post-injection evolution, the strain rate becomes indiscernible.



Figure B2. Panel (a) cumulative amount of leaked magma  $M_{leak}$  as a function of time during and after the injection. Panel (b) shows the the relative pore pressure  $\frac{P_f - min(P_f)}{max(P_f) - min(P_f)}$  as function of radial position in the mush shell. Colored lines in (b) correspond to colored data points in (a). The decrease in  $M_{leak}$  with time corresponds to the shift of maximum pore pressure from the inner boundary of the much outwards.



**Figure B3.** Evolution of core pressure and tensile stress with time for varying injection time length  $t_{inj}$ . The system has  $\tau_{diffusion} = \tau_{relaxation}$ . Insets show the values at the end of the injection. As  $t_{inj}$  increases, the short-term evolution period shortens and become less apparent.